

# Structural Analysis Report

# Self-Supporting Tubular Crank-Up Tower

Mast Model: MA-40

# **Prepared for Gary Loving**

Design Code: 2012 IBC & 2009 ANSI/TIA-222-G (2)

Basic Wind Velocity: 90 mph 3 second gust

Exposure C

Ice Thkn's (in): 0

Topographic Category: 1
Structure Classification: 1

**Tower Fully Retracted** 

Max. Allowable Antenna Wind Load - Unfactored (lbs) 85

Max. Allowable Antenna Weight (lbs): 75

Max. Allowable Antenna Effective Wind Area (sq. ft.): 4.8

Note: The maximum antenna values shown above include the antenna, rotator, and any other items placed at the top of the tower. For purposes of these calculations the antenna was placed above the top of the tower a distance of (ft):

Per the Operation Instructions, the tower shall be fully retracted if winds over 50 mph are expected



**Date Prepared:** 

6/9/2017

Sheet 1 of 12

Prepared By:

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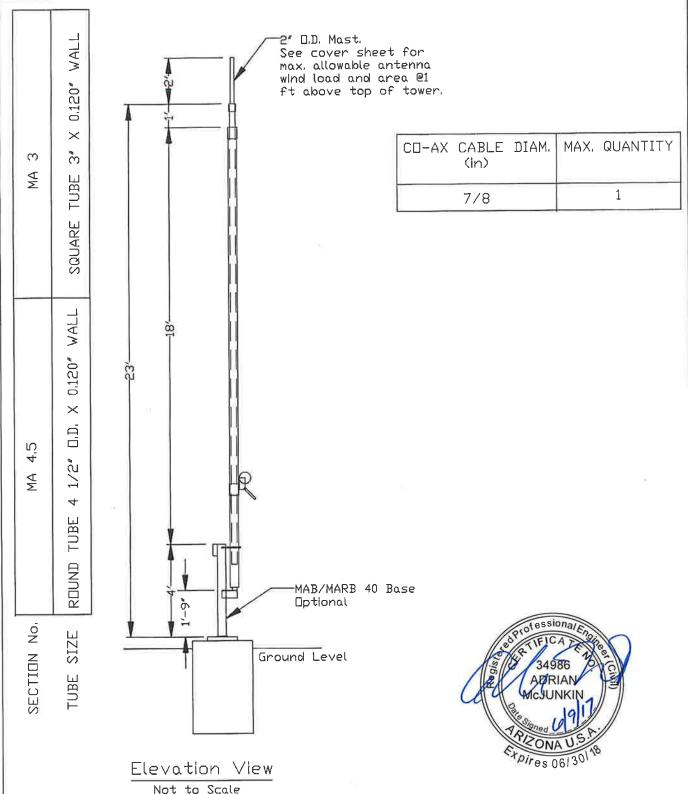
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# ELEVATION

MA-40

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OR REPRODUCED OR ITS CONTENT
DISCLOSED, IN WHOLE OR IN PART,
WITHOUT THE PRIOR WRITTEN CONSENT
OF US TOWER CORPORATION





### **General Notes**

### Tower Model: MA-40

- All work shall be in conformance with the requirements of the 2012 IBC / 2013 CBC and "Structural Standards for Steel Antenna Towers and Antenna Supporting Structures ANSI/TIA-222-G", by the Telecommunications Industry Association.
- 2. The 2012 IBC / 2013 CBC requires the use ANSI/TIA-222-G for tower design.
- **3.** All concrete shall have a minimum compressive strength of 2500 psi at 28 days unless noted otherwise. All concrete shall conform to the requirements of the International/California Building Code and referenced edition of ACI 318. Slump shall not exceed 4-1/2 inches.
- **4.** Reinforcing steel shall be intermediate grade deformed bars conforming to ASTM A-615. No. 4 bars and smaller shall be Grade 40, No. 5 bars and larger shall be Grade 60. All reinforcing details, placement etc. shall conform to the requirements of the International Building Code and ACI 318. No welding allowed.
- **5.** All reinforcing steel, anchor bolts, dowels and other inserts etc. shall be securely anchored in place, in the required positions, prior to pouring concrete.
- **6.** Steel fabrication and erection shall conform to the requirements of the AISC Manual of Steel Construction and the Electronic Industries Association (as referenced in note 1 & 2 above).
- **7.** All welding shall be performed by AWS certified welders for each type of weld used. (Using the GMAW (spray arc) welding process with ER70S-6 welding wire).
- **8.** All tower section lift cables & guy cables shall be 7 x 19 Aircraft cable with the following minimum strengths:

<u>Cable diameter (in)</u>	<u> Minimum Strength (lbs)</u>
3/16	4200
1/4	7000
5/16	9800

- **9.** This tower analysis is based the antenna being installed at a height of one foot above the top of the tower. The wind load of the antenna(s) shall not exceed the load shown in these calculations. The Owner of the tower shall assume full liability for verification of the antenna loading.
- **10.** This tower is designed to be used in its fully extended position.
- **11.** The design of the hoist system is not with in the scope of these calculations and shall be designed by others.
- **12.**This tower has not been designed to meet any twist or sway criteria.
- **13.** The Owner shall verify that the quantity and size of waveguide / Coax cables match the values used in these calculations.
- **14.** The engineering and design of the antennas are not with-in the scope of these calculations.
- **15.** Installations on hills, escarpments and other special wind areas is not with-in the scope of these calcuations.
- **16.** US Tower Corp. recommends that the installation of this tower and its foundation be performed by a Professional, licensed Contractor with experience installing these types of structures.
- 17. The Contractor is responsible for conducting all construction in accordance with all Federal, State, OSHA, and Local laws and ordinances. The Contractor is also responsible for checking the site for underground facilities prior to the start of work.
- **18.** US Tower Corp. and it's Engineers shall not be responsible for errors and omissions in the project not in conformance with these calculations and the Codes and Standards referenced here-in.
- **19.** US Tower Corp. and it's Engineers accept no responsibility for field inspection during construction nor for the method of construction.
- **20.** The Owner shall assume full responsibility & liability for the periodic inspection of all tower section lift cables & guy cables. Any cable with any sign of distress or excessive stretch shall be replaced immediately.
- **21.** The information contained in these calculations is the property of US Tower Corp. and shall only be used to obtain an installation permit. Any other use shall be authorized by US Tower in writing prior to utilizing the information contained herein.
- 22. Per ASI/TIA-222-G, Ice and Seismic loads do not apply for Class I structures. (Table 2-3)



### Code & Material Specifications

### Mast Model: MA-40

# Governing Codes, Stresses, and Materials (Min.)

International Building Code 2012 Edition

**TIA-222-G** 

AISC Specification for Steel Bldgs 360-05
ACI 318 2008 Edition

Wind Loading

Governed by the TIA/EIA standard

Basic Wind Speed

90 mph, 3 second gust

(Exposure C Terrain)

Structural Steel ASTM A36

(All plates, bars, angles) (Fy = 36 ksi)

(Min. Fy for plates - 42 ksi)

Structural Pipe ASTM A53 Gr. B, A500 Gr. B

(Fy = 50 ksi for tower legs)

Structural Tubing (HSS) ASTM A500 Gr. B (Sq. Tube)

(Fy = 46 ksi)

ASTM A513 Type 1A (Rnd Tube)

(Fy = 36 ksi)

Welding AWS D1.1-04

GMAW w/ ER70S-6 wire

Hot-Dip Galvanizing ASTM A123
Hardware ASTM A153

Bolts: Tower & Accessories ASTM A325

Reinforced Concrete 2500 psi strength @ 28 days

Reinforcing Steel ASTM A615

Gr. 40 for #4 & smaller dia. Gr. 60 for \$5 & larger dia.

Anchor Rods ASTM F1554 Gr. 36

or ASTM A36

Foundation & Soils 1500 psf Bearing (TL = DL+LL)

Lateral Bearing Pressure 100 psf/ft of depth

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### Mast Section Properties

Mast Model: MA-40

Design per ANSI/TIA-222-G(2) Structure Classification: Wind velocity (mph): Exposure: Z-g: alpha:	1 90 C 900 9.5	Importance Tower Hei Topo Cate	ght (ft): gory: K-t: f:	0.87 <b>23 1</b> 1	Ice Thickno Ice Weight Design Ice Material De	t (lb/in3): t (in): ensity:	0 56 0.00 0.284	(lb/in^3)
K-z min:	0.85		H (ft):	0		t above surr	ounding ter	rain
K-e: K-d:	1 0.95		K-h: K-zt:	N.A. 1.00	Reduction	tactor speed up fa	actor	
Gust Factor:	1.1		K-zt. K-z:	0.929		essure coef		
				0.020	, a.a.a., p.			
Section Name	MA3	MA4.5	NA	NA	NA	NA	NA	NA
Section length (ft):	20	20	0	0	0	0	0	0
Top lap length (ft):	0	4	0	0	0	0	0	0
Bot lap length (ft):	4	0	0	0	0	0	0	0
Tube shape:								
1=round, 2=sq., 3=16 side	2	1	1	1	1	1	1	1
Tube O.D.:	3	4.5	6.625	8	10	12	14	16
(Note: OD = face width of square								
Wall thk'ness:	0.12	0.135	0.135	0.135	0.135	0.135	0.135	0.135
Tube I.D.:	2.76 <b>36000</b>	4.23 <b>36000</b>	6.36	7.73 <b>36000</b>	9.73	11.73 <b>36000</b>	13.73	15.73 <b>36000</b>
Tube F-y: (Steel only) C: (For sq. tubes is aspect ratio)		29.0	<b>36000</b> 42.7	51.6	<b>36000</b> 64.5	77.4	<b>36000</b> 90.3	103.2
C-f, force coefficient:	2.00	1.20	0.90	0.74	0.60	0.60	0.60	0.60
O-1, Torce docincient.	2.00	1.20	0.50	0.74	0.00	0.00	0.00	0.00
Linear Appurtenances:		ble dia. (in):	0.875		Lift Cable o	` '	0.188	
	Cable wt		0.3		Cable wt. (		0.07	
	No. of Ca	bles:	1		No. of Cab	les:	1	
Projected Area:			No ICE					
Tube (s.f. / ft.):	0.500	0.450	0.496	0.496	0.500	0.600	0.700	0.800
Co-ax cable (s.f./ft.):	0.088	0.088	0.088	0.088	0.088	0.088	0.088	0.088
Lift cable(sq. ft. /ft.):	0.019	0.019	0.019	0.019	0.019	0.019	0.019	0.019
Tot. Unif. EPA (sq.ft./ft.):	0.606	0.556	0.000	0.000	0.000	0.000	0.000	0.000
Appurtenance @ top of Section:	(Includos	ton conc 9	other items	oogy arma	not included	Lainea Bla	< 0.1\	
Width (in):	(IIICIUUES 6	7.5	9.625	, coax anns	13	1511106 13-a 1	~ 0.1) 17	19
Height (in):	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000
C-f, force coefficient (Tbl. 2-8)	1.2	1.2	1.2	1.2	1.2	1.2	1.2	1.2
Conc. EPA @ top (sq. ft.):	0.050	0.063	0.000	0.000	0.000	0.000	0.000	0.000
Weight:								
Top cap:	5	6	10	12	15	20	25	30
Tube:	94	126	0	0	0	0	0	0
Bot. anchor:	5	5	8	10	12	15	20	25
Lift cable & standoff:	5	5	5	5	5	5	5	5
Misc.:	11	14	2	3	3	4	5	6
Total weight:	120	156	0	0	0	0	0	0
Top Mounted Equipment: (Ant	enna etc.)							
Antenna / Camera Area (sq.ft.):	4			Mast Diame	ter (in.):	2.000		
Shape (1= round, 2 = flat):	1		Mast Len	gth (ft):		1.0		
C-f:	1.2		C-f:	rated DA /a	a ft \	1.2 0.200		
Concentrated PA (sq. ft.) Weight (lbs):	4.8 <b>75</b>		Weight (	rated PA (s	q. it.)	0.200 10		
Troigitt (183).	73		Troigin (			10		Dana 5



#### Mast Loading

Mast Model: MA-40

#### Tower Loading, Shear & Moments:

Design per EIA-222-G Wind velocity (mph): G-h: 1.1 Gust factor Exposure: С 0.87 Importance factor l: Topo Category: 1 Kd: 0.95 Wind direction probablility factor Tower Height (ft): 23 f: 1 Topographic coefficient Structure Class: 1 Zg: 900 Exposure category coefficient H (ft): 0 Ht. of crest above surrounding terrain alpha: 9.5 Exposure category coefficient K-h: N.A. Height reduction factor Kz-min: 0.85 Exposure category coefficient K-zt: 1.00 Topo wind speed up factor Load Factor - Wind: 1.6 K-e: 1 Terrain constant Load Factor - Dead: 1.2 Kt: Topographic constant Are lift cables used? (Y/N) Υ Ant. Height Above Top

Wind Velocicity Coeficient

Kz = 2.01\*(z/Zg)^(2/a) z > 15' q-z = 0.00256 \* Kz \* Kzt \* Kd \* I \* G-h \* V^2

of Mast (ft): Approx. Width of

1 Payload Spread (ft): (For determining min. torsion value to apply at top of mast.)

q-2 - 0.00230	NZ NZL I	tu i G-ii	V Z							to apply at top t	oi mast.)					
							Factored Loads - No ICE							Controlling Loading & Condition		
Tower Section	Projected Area	Analysis height (ft)	z height (ft)	<u>Kz</u>	q-z (basic)	w (plf) or P (lb)	Shear (lbs)	Moment (ft-lbs)	P-Delta Mom. (ft-lbs)	Total Moment	Deflection (in)	Sway (deg)	<u>Shear</u> (lbs)	Moment (ft-lbs)	<u>Load</u> Condition	
Antenna	4.8	24	24	0.937	16.06	135.7	136	0	0	0	8.8	3.4	136	0	No Ice	
Mast	0.200	23	23.5	0.933	15.99	5.6	141	141	0	141	8.8	3.4	141	141	No Ice	
Top of Section MA3	0.050 0.606	23 <b>22</b>	23 22.5	0.929 0.925	15.92 15.84	1.4 16.9	143 160	141 292	3	141 296	8.8 8.4	3.4 3.4	160	296	No Ice	
Top of Section	0.063	22	22	0.920	15.77	1.7	161	292	3	296	8.4	3.4				
MA4.5	0.556	4.5	13.25	0.850	14.57	14.3	411	5300	200	5500	0.2	0.4	411	5500	No Ice	
Top of Section	0.000	4.5	4.5	0.850	14.57	0.0	411	5300	200	5500	0.2	0.4				
NA	0.000	0	0	0.850	14.57	0.0	0	0	0	0	0.0	0.0	0	0	No Ice	
Top of Section	0.000	0	0	0.850	14.57	0.0	0	0	0	0	0.0	0.0				
NA	0.000	0	0	0.850	14.57	0.0	0	0	0	0	0.0	0.0	0	0	No Ice	
Top of Section	0.000	0	0	0.850	14.57	0.0	0	0	0	0	0.0	0.0				
NA	0.000	0	0	0.850	14.57	0.0	0	0	0	0	0.0	0.0	0	0	No Ice	
Top of Section	0.000	0	0	0.850	14.57	0.0	0	0	0	0	0.0	0.0				
NA	0.000	0	0	0.850	14.57	0.0	0	0	0	0	0.0	0.0	0	0	No Ice	
Top of Section	0.000	0	0	0.850	14.57	0.0	0	0	0	0	0.0	0.0				
NA	0.000	0	0	0.850	14.57	0.0	0	0	0	0	0.0	0.0	0	0	No Ice	
Top of Section	0.000	0	0	0.850	14.57	0.0	0	0	0	0	0.0	0.0				
NA	0.000	0	0	0.850	14.57	0.0	0	0	0	0	0.0	0.0	0	0	No Ice	

Note: Top of \_\_\_\_ = concentrated load applied at the top of the tower section.

Tower Section F	Factored W	<u>eights: (No Ice)</u>		Lift cable	Vert. Component of
Section	Weight		Section	force (lbs)	Guy Cables (lbs)
	(lbs)		MA3	254	0
Ant. + Mt.	102		MA4.5	509	0
Co-ax Wt:	8	(at top of tower)	NA	0	0
MA3	144		NA	0	0
MA4.5	188		NA	0	0
NA	0		NA	0	0
NA	0		NA	0	0
NA	0		NA	0	0
NA	0				Note: Enter vert.comp. of guys
NA	0				only if a lift cable system is
NA	0				not utilized.
Total:	442	lbs			

Vertical Load per Section (Factored) P (lbs) MA3 254 MA4.5 509 NA 0 NA 0 NA 0 NA NA 0 NA 0

Torsion at Base (Factored) Tm (lb.ft) =

(Based on 15% eccentricity of payload)



Sum F-vp:

### Lift Cable Analysis

### No Ice

Mast Model: MA-40

#### **Factored Loads Used**

0 (=Lift cable force for section analysis)

Note: All units are in po	unds.	Tower Section:	Section Wt. (lb):	Vert. Component of Guy Cables (lb):	Lift Cables	factors:			
Tower Data:		MA3	144	0	End Efficien		1.00		
No. of twr. sections:	2	MA4.5	188	0	Resistance I	,	0.60	(phi)	
Ant. + Mt. wght (lb):	102	NA	0	0				(F)	
Accessories wt. (lb):	0	NA	0	0					
Coax cable wt. (lb):	8	NA	0	0					
	-	NA	0	0					
Weight at Top (lbs):	110	NA	0	0					
11 o.g. 11 at 1 op (120).		NA	0	0					
Anchor Frame-Tower					Anchor Frame-Tower		Α		
Cable dia (in):	0.25				Cable dia (in):	0.25			
Cable MBS:	7000	Cable force	per face:	254	Cable MBS:	7000		Cable force per face:	0
No. of faces w/cable:	1				No. of faces w/cable:	1			
F-v = CFtot:	254	Cable CSI:		0.06	F-v = CFtot:	0		Cable CSI:	N/A
Pulley Frame-Tower S	ection: MA4.5				Pulley Frame-Tower S	ection: N	Δ		
Sum F-vp:		ble force for se	ction analy	sis)	Sum F-vp:			le force for section analys	is)
Anchor Frame-Tower	Section: MA4.5				Anchor Frame-Tower	Section: N	Α		
Cable dia (in):	0.25				Cable dia (in):	0.25			
Cable MBS:	7000	Cable force	per face:	0	Cable MBS:	7000		Cable force per face:	0
No. of faces w/cable:	1				No. of faces w/cable:	1			
F-v = CFtot:	0	Cable CSI:		N/A	F-v = CFtot:	0		Cable CSI:	N/A
Pulley Frame-Tower S	ection: NA				Pulley Frame-Tower S	ection: N	Δ		
Sum F-vp:		ble force for se	ction analy	eie)	Sum F-vp:			le force for section analys	ie)
oum r -vp.	o (-Ent oc	10100 101 30	otion analy	313)	Guill 1 -vp.	-) 0	Liit oab	ne force for section analys	13)
Anchor Frame-Tower	Section: NA				Anchor Frame-Tower	Section: N	Α		
Cable dia (in):	0.25				Cable dia (in):	0.25			
Cable MBS:	7000	Cable force	per face:	0	Cable MBS:	7000		Cable force per face:	0
No. of faces w/cable:	2		•		No. of faces w/cable:	1		•	
F-v = CFtot:	0	Cable CSI:		NA	F-v = CFtot:	0		Cable CSI:	N/A
Pulley Frame-Tower S	ection: NA				Pulley Frame - Tower	Continu N	۸		
Sum F-vp:		ble force for se	ction analy	cic)	Sum F-vp:			le force for section analys	ic)
Sum r -vp.	U (-Liit Ca	ible lorce lor se	Clion analy	515)	Sum i -vp.	-) 0	·LIII Cab	ne lorce for section analys	15)
Anchor Frame-Tower					Note:				
Cable dia (in):	0.25				At the bottom tower :				
Cable MBS:	7000	Cable force	per face:	0				ower made up of 6 section	S
No. of faces w/cable:	4				you would input 5 as	the no. of fa	ces w/ o	cable.)	
F-v = CFtot:	0	Cable CSI:		NA					
Pulley Frame-Tower S	ection: NA								
·									

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# Mast Section Analysis

# Round & Square Sections (Steel)

Note: All units are in inches and lbs unless noted otherwise.

Modulus of Elasticity:	29000000		Design Thi	ckness Mod	ifier:	0.93		
				Section				
	MA3	MA4.5	NA	NA	NA	NA	NA	NA
Tube Shape:	Square	Round	Round	Round	Round	Round	Round	Round
Tube OD:	, 3	4.5	6.625	8	10	12	14	16
Tube Design. Thkn's:	0.112	0.126	0.126	0.126	0.126	0.126	0.126	0.126
Tube Spec. Thkn's:	0.120	0.135	0.135	0.135	0.135	0.135	0.135	0.135
Tube ID:	2.777	4.249	6.374	7.749	9.749	11.749	13.749	15.749
Tube Area:	1.29	1.73	2.56	3.11	3.89	4.68	5.47	6.26
Tube I (in^4):	1.80	4.13	13.54	24.08	47.48	82.56	131.69	197.24
Tube S (in^3):	1.20	1.84	4.09	6.02	9.50	13.76	18.81	24.66
Tube r: `	1.18	1.55	2.30	2.78	3.49	4.20	4.91	5.61
Tube Z (in^3):	1.40	2.40	5.30	7.79	12.24	17.70	24.17	31.64
Tube J (in^4):	2.69	8.26	27.08	48.16	94.95	165.12	263.38	394.48
Tube F-y (psi):	36000	36000	36000	36000	36000	36000	36000	36000
Design Length(ft):	16	20	0	0	0	0	0	0
Factored Forces: (Includes	P-delta mon	nents)						
Dead Ld. (P-u):	254	509	0	0	0	0	0	0
Shear (V-u):	234	411	0	0	0	0	0	0
Torsion Mom (T-u) ft-lb:	42	42	42	42	42	42	42	42
Moment (M-u) ft-lb:	296	5500	0	0	0	0	0	0
Tube D/t:	23.9	35.8	52.8	63.7	79.6	95.6	111.5	127.4
	Note: D/t sh	all not exce	eed 400					
Axial Strength	phi:	0.9	K:	2.1				
F-y' (round), F-e (sq):	2452	36000	36000	36000	36000	35499	33857	32625
Lamda-c (round), L-p (sq):	31.79	3.65	0.00	0.00	0.00	0.00	0.00	0.00
F-cr:	2150	2366	0	0	0	0	0	0
phi*P-n (lbs):	2495	3673	0	0	0	0	0	0
Flexural Strength	phi:	0.9						
phi*M-n (in-lbs):	45272	77862	171858	246086	372062	523600	700699	903357
Shear Strength	phi:	0.9						
phi*V-n:	12849	27952	41530	50316	63095	74819	83376	91923
phi*T-n: (in-lbs)	64714	118958	264901	390085	615300	879232	1146499	1447847
			•					
Tube CSI:	<b>0.13</b> MA3	<b>0.99</b> MA4.5	<b>0.00</b> NA	<b>0.00</b> NA	<b>0.00</b> NA	<b>0.00</b> NA	<b>0.00</b> NA	<b>0.00</b> NA



#### Anchor Bolt Anchorage

Tower Model: MA-40

#### ACI 318-05 App. D Tension Anchorage Calculations - Cast in Place Straight Anchors

All units are pounds and inches unless noted otherwise. 6/9/2017

#### Anchorage Description: 4 - 3/4" dia, A36 anchor rods

Concrete f-c' (psi):	2500	Is this in a moderate or High Seismic area	1.00	Factored Req'd Tens. Load (lb):	12625	(LRFD value)
Embedment:	21	AND do the loads include seismic loads? (Yes	= 0.75. No = 1.	0) ACI D.3.3 doesn't require this if loads do	n't include	seismic.

h-ef: 10.17 If embedment x 1.5 is > 3 of the edge distances then use h-ef = the largest of the 3 edge distances / 1.5 App. D Section D5.2.3.

Anchor Input:		Edge Distance	<u>S:</u>	Concrete E	<u> Breakout Inp</u>	out: (Tension)
No. of Anchors n:	1	c-a1:	15.25	A-Nco:	930.3	Projected breakout area of single anchor
Anchor dia:	0.750	c-a2:	15.25	A-Nc:	930.3	Proj'd breakout area of anchor group (For a single anchor use A-Nco value)
No. of threads / in:	10	c-a3:	15.25			(If have more than two anchors need to hand input A-Nc)
Anchor f-y (psi):	36000	c-a4:	15.25	ecc:	0	Eccentricity of tension load - anchor groups only
Anchor f-u (psi):	58000			AdjF-ec,N:	1.000	(ACI D5.2.4) for anchor groups loaded eccentrically
phi:	0.75			AdjF-ed,N:	: 1.150	(ACI D5.2.5) for edge effects
phi = 0.65 if material used	is not ductile			AdfF-c,N:	1.25	(ACI D5.2.6) Assumed cracked at service load levels

#### Steel Strength of Anchor in Tension (ACI D5.1)

	J .			•	. ,
A-se:	0.334	Effective	anch	or area	(in^2)

N-sa:

#### Concrete Breakout Strength of Anchor in Tension (ACI D5.2)

N-b:	38173	ACI D5.2.2

N-cb: 54873

#### Anchor Pullout Strength (ACI D5.3)

N-p: 18220 N-pn: 25508

#### Concrete Side-Face Blowout, Tension

N-sb: 58222 Note: If Ca1 is >0.4\*h-ef then blowout does

not occur

#### Anchor Design Strength - LRFD

14549 Steel: Breakout: 38411 Pullout: 17856 Blowout: 40756

(Note: If supplemental reinforcement is provided then the concrete

strength limit does not apply, App. D D.4.2.1.)

#### Notes:

- 1. For normal weight concrete only.
- 2. Anchors shall be either a headed bolt or have nuts and a bearing plate at the embed end as indicated above.
- 3. ACI Section D.5.2.3 is not included in this spreadsheet. (i.e. End of wall applications are not covered.)
- 4. If the design is controlled by concrete failure (i.e. non-ductile failure) then the Design Strengths controlled by concrete must be at least 2.5 times the factored forces transmitted by the attachment. (2006 IBC 1908.1.16) Alternatively, the steel anchor "or the attachment that the anchor is connecting to the structure shall be designed so that the attachment will undergo ductile yielding at a load level corresponding to anchor forces no greater than the design strength of the anchors" determined above. If "Steel Tension" controlled above then the connection is considered ductile and no further adjustments etc. are required. (Also see note 6.)
- Any supplemental reinforcing shall have f-y = 60,000 psi min.
- 6. Per ACI D.3.3 if anchor design does not include seismic loads then the design does not have to be controlled by steel ductility.

Can use 1.25 if is uncracked 0.7 Use 0.75 if supplemental reinforcement is provided Use 0.70 is supplemental reinforcement is not provided Concrete Pullout Input: A-head: 0.911 Area of anchor bolt head (Input 0 if plate washer is used) 0.00 Width of plate washer at embed end of anchor Plate w: 0.00 Length of plate washer at embed end of anchor Plate L: A-pl: 0.911 Area of plate washer minus rod area (Plate thkn's must be >= 0.5 \* bolt dia.)

AdfF-c,P: 1.4 Assumed cracked at service load levels Can used 1.4 if is uncracked

phi: Use 0.75 if supplemental reinforcement is provided

Use 0.70 is supplemental reinforcement is not provided

#### Side Face Blowout Input

LRFD Design Strength:

ASD Design Strength:

Min. center to center of anchor spacing (in): 3

Min. edge distance is same as min. cover per ACI 7.7.

Design Controlled By:

Min. distance between multiple anchors (input 0 for one anchor) Spacing: 5.50 c2: 15.25 Edge distance perp. to c-min. c-min: 15.25 Min. edge distance considering all fasteners AdjF1: 0.500 Factor for single anchor if c2 < 3(c-min) Factor for multiple anchors if c-min < .4(h-ef) AdjF2: 1.000 and anchor spacing is < 6(c-min) phi:

Use 0.75 if supplemental reinforcement is provided

14549 Lbs

10392 Lbs

Steel Tension

Use 0.70 is supplemental reinforcement is not provided

Loads at Bolts Vu = 103 Pu = 12625

ACI D.8.1 Stress check Phi = 0.75 14549 lbs Pn =

n = 0.55 Det.C F4.4  $(Pu+Vu/n)/(Phi.Pn) \le 1.0$ 

CSI =

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# Foundation Design MA-40

<u>Tower Reactions:</u> <u>Foundation Design Reactions:</u>

 Moment (ft-lbs):
 5194
 Moment (ft-lbs):
 8586

 Shear (lbs):
 257
 Shear (lbs):
 411

 Mast Weight (lbs):
 424
 Mast Weight (lbs):
 509

Concrete f-c' (psi): 2500

Base Plate (in):

Distance from ground Soil Design Parameters:

to top of concrete (ft):

Square ft'g width (ft):

4llow. Lateral bearing (psf/ft):

Allow. Soil bearing (psf):

100

Footing depth (ft): 4.5 Design is for non-constained condition per IBC reqmt's.

H (ft): 20.89 **Allow. bearing (psf): 1500** Increased 20% for ea.

S-1: 300 **Act. bearing (psf): 722** ft. of depth

(Increased S1 by 2x per IBC 1804.3.1 for isolated footing not adversely affected by 1/2" motion at

ground surface.)

A: 0.472

Depth req'd (ft): 3.5 Max. Moment in Footing (ft-lbs): 9839

Check concrete tensile stress: (neglect outer 2" of footing)

S-x (in<sup>3</sup>): 5461

f-t (psi): 22 CSI is < 1.0 therefore reinforcing is not req'd. Use

F-t (psi): 138 minimal reinforcing.

CSI: 0.16 rho: 0.0018

A-s reg'd (sq. in.): 2

A-s req'd (sq. in.): 2.33
Rebar dia (in): 0.625
No. of bars provided: 8

A-s provided (sq. in.): 2.45 OK

Anchor Bolt Anchorage Design Load:

Anchorage Tension Design Force (lbs): 12625 (LRFD level force)

(See Anchor Bolt Anchorage page for anchorage design)

### **Summary:**

Use foundation 3 ft. square by 5 ft. deep (below undisturbed soil).

Reinforce foundation with 8 #5 vertical bars (total) with #3 ties at 12" on center, and 3 ties in the top 5".

Use 2 vertical bar at each corner of the foundation.

Use 3/4" dia. ASTM A-36 or F1554 Gr.36 anchor bolts, 27" long.

Total of 4 anchor rods, one at each corner of the base plate with a minimum embedment of 21". Use hex nuts.



# MA 40 FOUNDATION

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8 - #5Vertical Bars(1 bar @ corners & center)

② #3 Ties ③ 12" O.C. (max) 3 in Top 5" Foundation has been designed to accommodate the following loads:

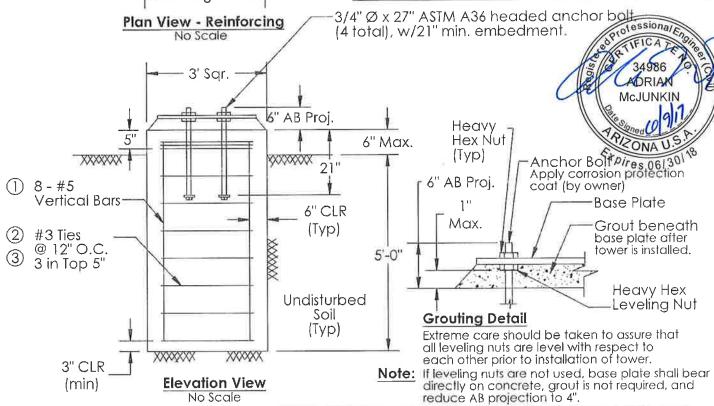
Overturning Moment = 7.2 ft - kips Base Shear = 0.54 kips Structure Weight = 0.50 kips

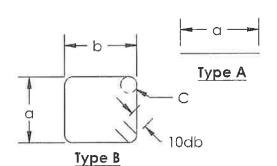
Soil and Concrete Design Parameters.

Allowable Foundation Pressure 1500 psf (Increases based on depth)

Lateral Bearing Pressure 100 psf/ft (Increases based on depth)

Concrete fc'= 2500 psi min. @ 28 days.





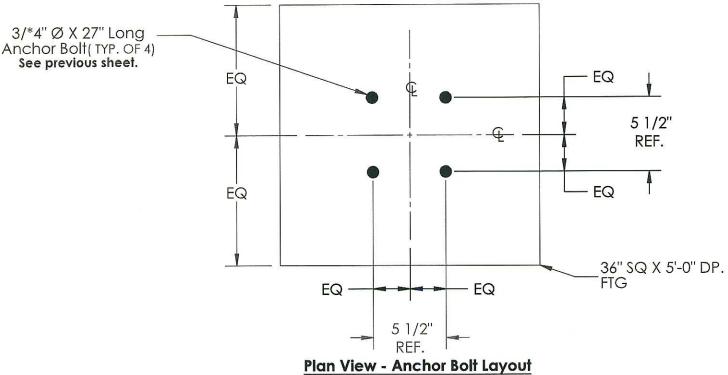
Reir	Reinforcement Material List										
Sym	Туре	Bar	Dimensions a				Qtv				
Sylli	Type	Size	а	р	C	10db	Giry				
	Α	#5	5' - 0" *	100		-	8				
2	В	#3	2' - 0" *	2' - 0" *	2"	3.75"	9				
3	В	#3	1'-5" *	1'-5" *	2"	3.75"	9				

\* = Nominal dimension



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No Scale

"REF" dimensions are provided for reference only. Use the tower base plate assembly to locate anchor bolts.

### **Foundation Notes:**

- 1. All concrete shall have a minimum compressive strength of 2500 psi at 28 days unless noted otherwise. All concrete shall conform to the requirements of the International Building Code and the referenced edition of ACI 318. Slump shall not exceed 4-1/2 inches.
- 2. Reinforcing steel shall be intermediate grade deformed bars conforming to ASTM A-615. No. 4 bars and smaller shall be Grade 40, No. 5 bars and larger shall be Grade 60. All reinforcing details, placement etc. shall conform to the requirements of the International Building Code and ACI 318. No welding allowed.
- 3. All reinforcing steel, anchor bolts, dowels and other inserts etc. shall be securely anchored in place, in the required positions, prior to pouring concrete.
- 4. The owner is responsible for verifying the soil at the site provides a minimum safety factor of 2.0 for the soil parameters used for this design.
- 5. The allowable lateral soil bearing value was doubled as allowed per 2012 IBC section 1806.3.4 for isolated foundations not adversely affected by a 0.5" motion at the ground surface que to short term lateral loads.
- 6. The foundation design does not consider the effects of ground water.
- The contractor is responsible for safe excavations in accordance with all Federal & Local laws and ordinances and OSHA requirements.
- 8. The contractor is responsible for the correct placement of all anchor bolts. US Tower recommends that the anchor bolts be placed using the tower base plate assembly provided with the tower. (The base plate assembly can be provided before the tower if desired.)
- 9. The foundation shall be one continuous pour such that cold joints do not develop. The contractor is responsible for verifying adequate concrete coverage is provided for all reinforcement to avoid the potential for rebar corrosion. Concrete shall be consolidated using vibratory methods.
- 10. The top of the footing shall be troweled level and smooth (or have a broom finish if preferred) in the area of the tower. Water shall be directed away from the tower base and anchor bolts outside of the tower area.
- 11. See General Notes sheet (earlier in calcs) for additional information & requirements.