1 - n, = 1/47 Dm = 30 ps /(n m. 1cm) D = 5. tx 103

U'=/11 =) (1-Y)U'=UJ => UJ = 1'1167

 $\Delta T$  model =  $\frac{L}{C_0} \frac{\Lambda^2}{\Lambda_0} \Delta = \frac{L}{C_0} \frac{\Lambda^2}{\Lambda_0} \frac{\Lambda_0 - \Lambda_0}{\Lambda_0} = \frac{L}{C_0} \frac{(\Lambda_0 - \Lambda_0) \Lambda_0}{\Lambda_0}$ 

DTy = DLDA

 $T_{g} = D L \Delta \lambda$   $D = D_{W} + D_{M} = D_{M}$   $= 30 \times 10^{-9} \times 10^{9} \times 10^{3} \text{ S/m}^{2}$   $= 30 \times 10^{-6}$   $= 30 \times 10^{-6}$ 

AX = 8,988 ×10 7 m > 898.8 nm

2-0) N=1,49 , 2 = 1310 rm V= 2,405 @ single-rode V= 2 d [n=12] => n2 = n.(1-1) = 1,47704 2> d= V20 (10,2-03) = 10,219 mm

D=0.02 N2=1,4509 d= (2,405) (1316 Am) (1,442-1,452)= 3,4 µm

At a larger diameter the D is smaller which means it has a higher crotical engle. Therefore, with a higher crotical engle. The dia veter is they greater to so that the TIR on he achieved in propogation.

b) 
$$V = \frac{d^{3}}{2}$$
 [  $n \ge -n^{3}$ ]  $d = 5 \mu m$ 
 $\lambda_{enhfl} > \frac{d^{3}}{2}$  [  $n \ge -n^{3}$ ]

 $\lambda_{enhfl} > \frac{d^{$ 

9 = 38, Flem

b) Vy = 9 201 h 26,626 ×10-34 J.S Eg LV L Efc - Efv 3,143×1014 Ha L U 3,2639×1014 Hz V = 9 · 3·10 × 3,143010 42 6 4.39 ×1013 6 3, 2634 × 104 AE 3666,926 g 6 3807,9 3807-3667 + 1 = 141 modes  $4-a) \quad n_{z}=3.3 \quad \Delta = 950 \text{ nm} \quad (int zo, F) \quad V_{o}=1V$  1 = (ext (int av)) 1 = (ext (int av)) $\alpha_{mir}^{2} = \frac{1}{2(200\mu m)} \ln \left( \frac{1}{(0,7)(0,7)} \right) = 1783,37m^{-1}$ Part = n(n+1) = 3,3(3,3+1) = 0,01638 164 = 1 col 1:11 AV = (0,01638)(0,5) (3×108×15) (6,626×10-345) Ctot 2 0,01196 2 1,196%.

Hilloy

b) 
$$g = d_{11} + \frac{1}{3L} \ln \left( \frac{1}{2(20)} \right)^{2}$$

$$= 200 \text{ m}^{2} + \frac{1}{2(200)} \ln \left( \frac{1}{(0,7)(0,7)} \right)^{2}$$

$$= 200 \text{ m}^{2} + 1773,33 \text{ m}^{2}$$

$$= 200 \text{ m}^{2} + 1773,33 \text{ m}^{2}$$

$$g = \Gamma g = 2$$
  $g = \frac{9}{\Gamma} = \frac{1983,37 n^{-1}}{0.11}$