

## 1 Mechanical Design

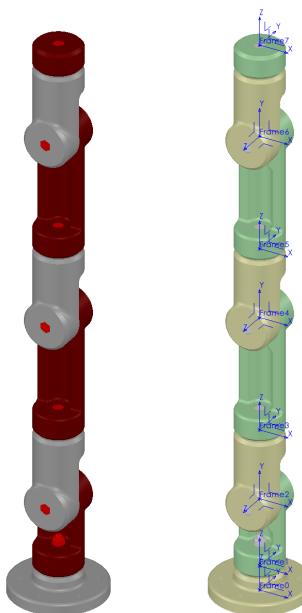
- Design commentary
  - ★ 7R spatial
- Selfies



Physical manipulator

## 2 Kinematics

- Frame definitions
- D-H parameters
- Forward kinematics



Frame definitions

Joint $i$	$\alpha_{i-1}$	$a_{i-1}$	$d_i$	$\theta_i$
1	$0^\circ$	0	$l_1 + b$	$q_1$
2	$90^\circ$	$l_2$	0	$q_2$
3	$-90^\circ$	0	$l_2 + b$	$q_3$
4	$90^\circ$	$l_3$	0	$q_4$
5	$-90^\circ$	0	$l_2 + b$	$q_5$
6	$90^\circ$	$l_3$	0	$q_6$
7	$-90^\circ$	0	$l_1 + l_2 + b$	$q_7$

where  $b = \frac{1}{16}$ " is the plain bearing flange thickness,  $l_1 = 1"$ ,  $l_2 = 3"$ , and  $l_3 = 5"$ .

$$\begin{aligned}
{}^0_1 T &= \begin{bmatrix} cq_1 & -sq_1 & 0 & 0 \\ sq_1 & cq_1 & 0 & 0 \\ 0 & 0 & 1 & l_1 + b \\ 0 & 0 & 0 & 1 \end{bmatrix} = \begin{bmatrix} cq_1 & -sq_1 & 0 & 0 \\ sq_1 & cq_1 & 0 & 0 \\ 0 & 0 & 1 & 1.0625 \\ 0 & 0 & 0 & 1 \end{bmatrix} \\
{}^1_2 T &= \begin{bmatrix} cq_2 & -sq_2 & 0 & l_2 \\ 0 & 0 & -1 & 0 \\ sq_2 & cq_2 & 0 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix} = \begin{bmatrix} cq_2 & -sq_2 & 0 & 3 \\ 0 & 0 & -1 & 0 \\ sq_2 & cq_2 & 0 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix} \\
{}^2_3 T = {}^4_5 T &= \begin{bmatrix} cq & -sq & 0 & 0 \\ 0 & 0 & 1 & l_2 + b \\ -sq & -cq & 0 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix} = \begin{bmatrix} cq & -sq & 0 & 0 \\ 0 & 0 & 1 & 3.0625 \\ -sq & -cq & 0 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix} \\
{}^3_4 T = {}^5_6 T &= \begin{bmatrix} cq & -sq & 0 & l_3 \\ 0 & 0 & -1 & 0 \\ sq & cq & 0 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix} = \begin{bmatrix} cq & -sq & 0 & 5 \\ 0 & 0 & -1 & 0 \\ sq & cq & 0 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix} \\
{}^6_7 T &= \begin{bmatrix} cq_7 & -sq_7 & 0 & 0 \\ 0 & 0 & 1 & l_1 + l_2 + b \\ -sq_7 & -cq_7 & 0 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix} = \begin{bmatrix} cq_7 & -sq_7 & 0 & 0 \\ 0 & 0 & 1 & 4.0625 \\ -sq_7 & -cq_7 & 0 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}
\end{aligned}$$

where  $q = q_i$  for  ${}^{i-1}_i T$ .

### 3 Control

- Description
- Lyapunov stability proof
- Impulse response plots

downflop\_bullet.mp4

upflop\_bullet.mp4