

Computational Approaches to  
Understanding Surface Heat Flow, the  
Metamorphic Rock Record, and Subduction  
Geodynamics

by

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# DEDICATION

To my mentors, colleagues, friends, and loved ones who take special interests in my life.

This work is yours as much as it is mine.

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# ABSTRACT

Pressure-temperature-time (PTt) estimates from high-pressure (HP) metamorphic rocks and global surface heat flow (SHF) rates evidently encode information about pressure-temperature-strain (PTS) fields deep in subduction zones (SZs). Previous work demonstrates the possibility of decoding such geodynamic information by comparing physics-based numerical models with empirical observations of SHF and the metamorphic rock record. However, antithetical interpretations of (non)uniformity with respect to PTS fields are emerging from this line of inquiry. For example, while mechanical coupling depths (CDs) inverted from SHF are narrowly distributed among SZs, maximum pressure-temperature (PT) conditions inverted from exhumed metamorphic rocks are relatively wide-ranging, and yet also uniformly distributed across pressures up to 2.4 GPa. This dissertation scrutinizes (dis)similarities among SZs inferred from large numerical and empirical datasets by applying a variety of computational techniques. First, CDs for 13 modern SZs are predicted after observing coupling in 64 numerical geodynamic simulations. Second, spatial patterns of SHF are assessed in two-dimensions by interpolating thousands of SHF observations near several SZ segments. Third, PTt distributions of over one million markers traced from the previous set of 64 SZ simulations are compared with hundreds of empirical PTt estimates

from the rock record to assess the effects of thermo-kinematic boundary conditions (TKBCs) on deep mechanical processing of rock in SZs. These studies conclude the following. Mechanical coupling between plates is primarily controlled by the upper plate lithospheric thickness, with marginal responses to other TKBCs. SHF interpolations show high variance within and among SZ segments, suggesting local, rather than widespread, continuity of PTS fields deep within SZs. Computed marker recovery rates correlate with TKBCs, and are therefore expected to vary among SZs. Finally, computed PTt distributions of markers show patterns consistent with transient, localized recovery from a cooling, serpentinizing plate interface. Together, this work encourages more antireductionist and diversified views of subduction geodynamics until SHF and PTt datasets can more precisely distinguish (dis)similarities in PTS fields within and among SZs. Strategically scaling PTt and SHF datasets in the future will improve computational precision and confidence, and thus will advance subduction zone research.



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# LIST OF ABBREVIATIONS

**CD** coupling depth

**HP** high-pressure

**PT** pressure-temperature

**PTS** pressure-temperature-strain

**PTt** pressure-temperature-time

**SHF** surface heat flow

**SZ** subduction zone

**TKBCs** thermo-kinematic boundary conditions

**UPT** upper plate thickness

# LIST OF SYMBOLS

$GPa$  Gigapascal

$K$  Kelvin

$Ma$  *Mega annum* or million-years

$Z_{UP}$  Upper plate thickness

$Z_{cpl}$  Mechanical coupling depth

$\Phi$  Thermal parameter

$\eta$  viscosity

$\vec{q}$  surface heat flow

$\vec{v}_{conv}$  convergence velocity

$^{\circ}C$  Celcius

$km$  kilometer

$t_{OP}$  oceanic plate age

*wt. %* weight percent





# CHAPTER 1:

## INTRODUCTION

**Keypoints:**

- Proxy datasets are key for inference about geodynamics deep in **SZs**
- Computation leverages large data to infer, build, and test geodynamic models



# CHAPTER 2:

## EFFECTS OF THERMO-KINETIC BOUNDARY CONDITIONS ON MECHANICAL PLATE COUPLING IN SUBDUCTION ZONES

### Keypoints:

- Mechanical coupling responds strongly to **upper plate thickness (UPT)**
- Inverting **surface heat flow (SHF)** allows **coupling depth (CD)** estimation
- Globally consistent **SHF** implies consistent **UPT**, and thus uniform **CDs**

## 2.1 Abstract

Deep mechanical coupling between converging plates is implicated in plate motions, crustal deformation, seismic cycles, arc magmatism, detachment of subducting material, and is considered a key feature of **subduction zone (SZ)** geodynamics. This study uses two-

dimensional numerical models of oceanic-continental convergent margins to investigate effects of **thermo-kinematic boundary conditions (TKBCs)** on coupling—specifically focusing on thermal parameter ( $\Phi$ ) and **upper plate thickness (UPT)**. Numerical experiments implement coupling by including the metamorphic (de)hydration reaction *antigorite*  $\Leftrightarrow$  *olivine* + *orthopyroxene* +  $H_2O$  in the upper-plate mantle. Visualizing **pressure-temperature-strain (PTS)** fields show thermal feedbacks regulating **coupling depth (CD)** dynamically with strong responses to **UPT** and weak responses to  $\Phi$ . The results imply estimation of **CD** is possible by inverting **UPT** from **surface heat flow (SHF)**. Moreover, **SHF** sampled from the backarc region near 13 modern **SZs** imply consistent **UPT**, and thus uniform **CDs** among **SZs**.

## 2.2 Introduction

Subduction geodynamics are largely defined by plate motions and mechanical behaviour along the plate interface. For example, a transition from mechanically decoupled (moving differentially with respect to each other) to coupled plates (moving with the same local velocity) dramatically increases temperature by inducing mantle circulation in the upper plate (Peacock *et al.*, 1994; Peacock, 1996). Observations from numerical experiments and forearc **SHF** imply coupling transitions occurring globally within a narrow range of depths in modern **SZs** (70-80 km). Further, coupling appears essentially unresponsive to important **TKBCs**, including oceanic-plate age, convergence velocity, and subduction geometry (Furukawa, 1993; Wada *et al.*, 2008; Wada & Wang, 2009). While uniform **CDs**

among **SZs** are inferred from different datasets, this phenomenon remains curious and unconfirmed to a large extent. To understand **SZ** geodynamics, it is essential to understand why modern subduction zones appear to achieve similar **CDs** despite differences in their physical characteristics.

Notwithstanding, many numerical geodynamic models use **CDs** of 70-80 *km* as a boundary condition (Abers *et al.*, 2017; Currie *et al.*, 2004; Syracuse *et al.*, 2010; van Keken *et al.*, 2011, 2018; Wada *et al.*, 2012; Gao & Wang, 2014; Wilson *et al.*, 2014), although not exclusively (e.g. 40-56 *km*, England & Katz, 2010; Peacock, 1996). Similar **CDs** among **SZs** is an attractive hypothesis for at least two reasons. First, it helps explain a relatively narrow range of depths to subducting oceanic-plates beneath volcanic arcs (England *et al.*, 2004; Syracuse & Abers, 2006) as mechanical coupling is expected to be closely associated with the onset of flux melting. Second, mechanical coupling is required to detach crustal fragments from the subducting plate (Agard *et al.*, 2016), so uniform **CDs** may also help explain why maximum pressures recorded by subducted oceanic material worldwide is  $\leq$  2.3-2.5 *GPa* (roughly 80 *km*, Agard *et al.*, 2009, 2018).

The location and extent of mechanical coupling along the plate interface is implicated in myriad geodynamic phenomena, including seismicity, metamorphism, volatile flux, volcanism, plate motions, and crustal deformation (Čížková & Bina, 2013; Gonzalez *et al.*, 2016; Hirauchi *et al.*, 2010; Peacock, 1990, 1991, 1993, 1996; Peacock & Hyndman, 1999; Hacker *et al.*, 2003; van Keken *et al.*, 2011; Grove *et al.*, 2012; Gao & Wang, 2017).

Consequently, the mechanics of coupling have been extensively studied and discussed. Coupling fundamentally depends on the strength (viscosity) of materials above, within, and below the plate interface. Water flux from compaction and dehydration of hydrous minerals with increasing **pressure-temperature (PT)** forms layers of low viscosity sheet silicates near the plate interface. Transmission of shear stress between plates is inhibited by formation of talc and serpentine in the shallow upper-plate mantle (Peacock & Hyndman, 1999). Lack of traction along the interface, combined with cooling from the subducting plate surface, ensures a positive feedback between hydrous mineral formation and mechanical decoupling. Experimentally determined flow laws, petrologic observations, and geophysical observations all support the plausibility of this conceptual model of subduction interface behaviour (e.g., Agard *et al.*, 2016, 2018; Gao & Wang, 2014; Peacock & Hyndman, 1999).

Experimental control over important **TKBCs** makes numerical modelling essential for investigating such complex geodynamic environments. Wada & Wang (2009) previously investigated the effects of  $\Phi$  on **CDs** by numerically simulating 17 active subduction zones. Among other **TKBCs**, their models specify convergence rate, subduction geometry, thermal structure of oceanic- and overriding-plates, and degree of coupling along the subduction interface. Notably, their experiments control for interface rheology and discriminate best-fit **CDs** based on observed forearc **SHF**.

This study similarly specifies **TKBCs** to numerically simulate the range of modern **SZ** systems, but regulates interface rheology dynamically by implementing metamorphic

reactions that respond to evolving PTS fields. Subduction geometry and CD are not fully determined features, in other words, but rather spontaneous model outcomes within the range of specified boundary conditions discussed in section 2.3. As in previous studies (e.g., [Ruh et al., 2015](#)), rheological effects of the dehydration reaction *antigorite*  $\Leftrightarrow$  *olivine* + *orthopyroxene* +  $H_2O$  are implemented to drive mechanical coupling. An abrupt viscosity increase accompanies antigorite destabilization, thereby inducing mechanical coupling, as defined by empirically-determined flow laws used in the experiments (Table 2.1).

This chapter focuses on two fundamental questions. How does CD respond to  $\Phi$  and UPT? And how stable is CD through time? First, 64 convergent margins with variable UPT and  $\Phi$  are numerically simulated and mechanical plate coupling is observed. Thermal feedbacks within the system are visualized in terms of mantle temperature, viscosity, and velocity fields and CD responses to a range of  $\Phi$  and UPT are quantified using multi-variate linear regression. Three different regression models are then used to predict CDs for 13 modern SZs, which all predict similarly narrow ranges of CDs. Implications and questions about UPT and CD uniformity among SZs are finally discussed before further investigation into SHF in Chapter 3.

## 2.3 Numerical modelling methods

This study simulates converging oceanic-continental plates, where an ocean basin is being consumed by subduction at a continental margin (Figure 2.1). Initial conditions are modified from previous numerical experiments of active margins ([Sizova et al., 2010](#); [Gorczyk et al.,](#)

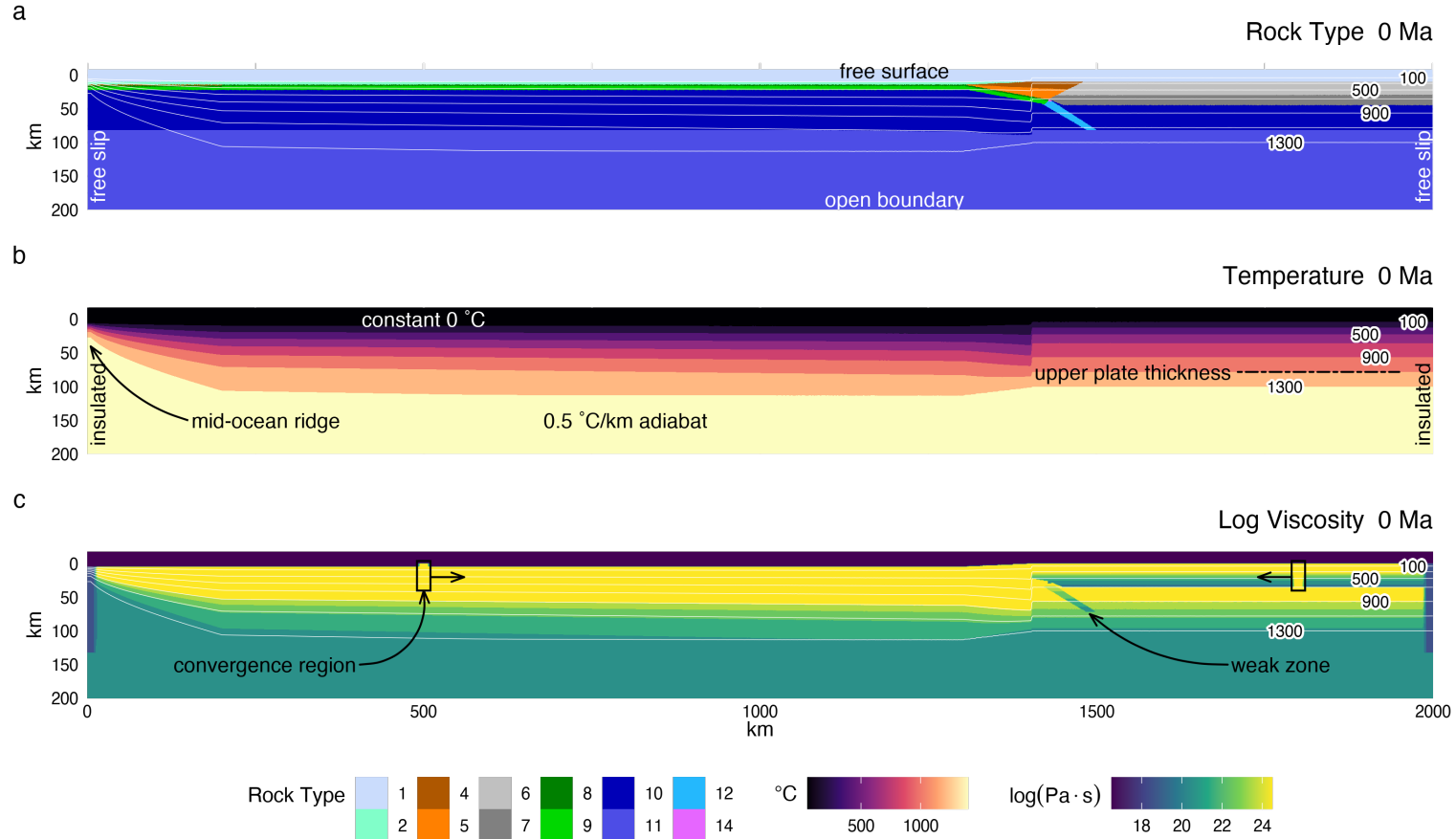
2007) using the code I2VIS (Gerya & Yuen, 2003), although plate coupling was not the focus of their studies. Identical material properties (Tables 2.1 & 2.2), rheologic model, and hydration/melt model (see Appendix) as Sizova *et al.* (2010) are used. However, the version of I2VIS in this study differs from Sizova *et al.* (2010) in its initial setup, overall dimension, resolution, continental geotherm, dehydration model, and left boundary condition (origin of new oceanic lithosphere). Differences are outlined in this section and in Appendix @ref(!!!). Sixty-four I2VIS models constructed with varying convergence rates ( $\vec{v}_{conv}$ ), oceanic-plate ages ( $t_{OP}$ ), and UPTs (Figure 2.2) were ran on the Euler cluster at ETH, Zürich until achieving at least 10 *Ma* of subduction.

### 2.3.1 Initial setup and boundary conditions

Simulations are 2000 *km* wide and 300 *km* deep (Figure 2.1). In the model domain, three governing equations of heat transport, momentum, and continuity are discretized and solved with a conservative finite-difference marker-in-cell approach on a fully staggered grid as outlined in Gerya & Yuen (2003). Numerical resolution is non-uniform with higher resolution (1 *km* x 1 *km*) in a 600 *km* wide area surrounding the contact between the oceanic-plate and continental margin, then gradually changing to lower resolution towards the model boundaries (5 *km* x 1 *km*, x- and z-directions, respectively). The left and right boundaries are free-slip and thermally insulating (Figure 2.1a, b). Implementation of “sticky” air and water allows for a free topographical surface with a simple linear sedimentation and erosion model. The lower boundary is open to allow for oceanic-plate descent with a spontaneous



subduction angle ([Burg & Gerya, 2005](#)).



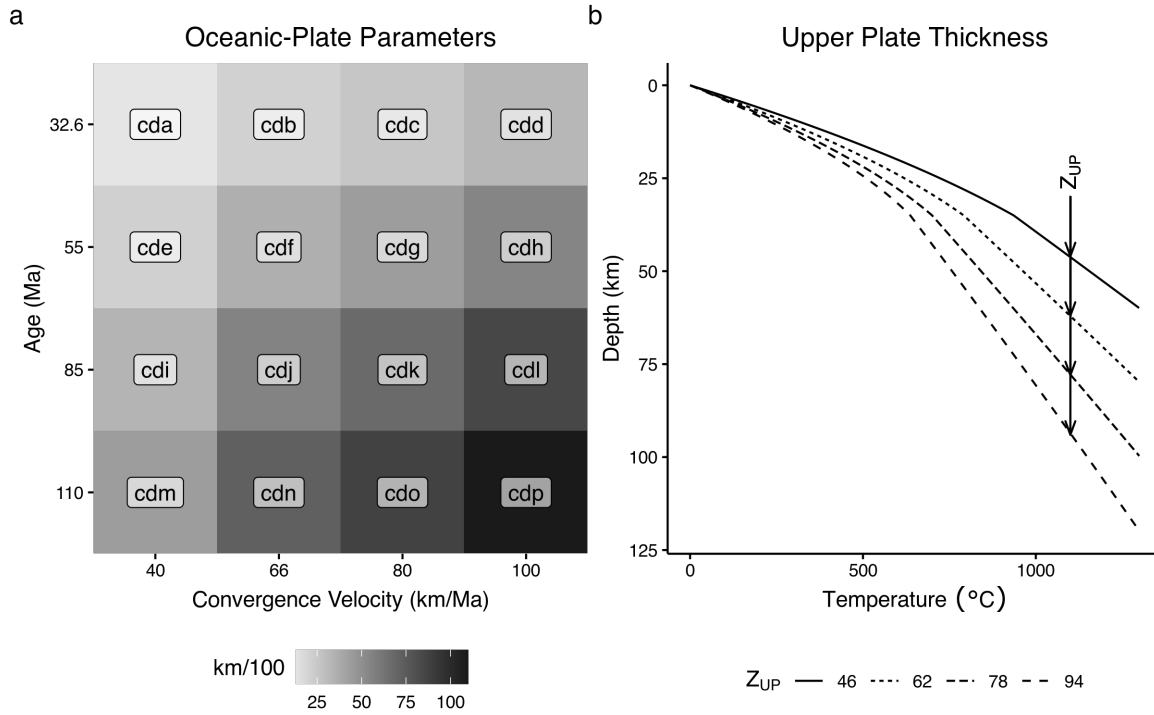
**Figure 2.1: Initial model configuration and boundary conditions.** (a) A free sedimentation/erosion boundary at the surface is maintained by implementing a layer of "sticky" air and water, and an infinite-like open boundary at the bottom allows for spontaneous oceanic-plate descent and subduction angle. Left and right boundaries are free slip and thermally insulating. Initial material distribution includes 7 km of oceanic crust (2 km basalt, 5 km gabbro), 1 km of oceanic sediments, and 35 km of continental crust, thinning ocean-ward. (b) Oceanic lithosphere is continually created at the left boundary. The oceanic geotherm is calculated using a half-space cooling model and the continental geotherm is calculated using a one-dimensional steady-state conductive cooling model to 1300 °C. The base of the upper plate lithosphere ( $Z_{UP}$ ) is defined by visualizing viscosity and generally coincides with the 1100 °C isotherm. (c) Oceanic crust is bent under loading from passive margin sediments, and a weak zone extends through the lithosphere to help induce subduction. Convergence velocities are imposed at stationary, high-viscosity regions far from the trench. Rock type colors are: [1] air, [2] water, [4,5] sediments, [6,7] felsic crust, [8] basalt, [9] gabbro, [10,11] dry mantle, [12] hydrated mantle, [14] serpentinized mantle.

A horizontal convergence force is applied to both plates in a rectangular region far from the continental margin (Figure 2.1c). An initial weak layer cutting the lithosphere permits subduction to initiate. The high-viscosity ( $\eta = 10^{25} \text{ Pa} \cdot \text{s}$ ) rectangular convergence regions apply constant horizontal velocities without deforming the lithosphere. Subduction angle is governed by free-motion of the subducting plate. Similarly, subduction velocity varies with time in response to extension or shortening of the overriding plate.  $\Phi$  is thus calculated as the product of the horizontal convergence velocity and the oceanic-plate age (c.f. McKenzie, 1969). For convenience and consistency with the literature, this study presents  $\Phi$  in units of  $\text{km}/100$  (Figure 2.2a).

### 2.3.2 Calculating geotherms and defining lithospheric thickness

Oceanic crust is modeled as 1  $\text{km}$  of sediment cover overlying 2  $\text{km}$  of basalt and 5  $\text{km}$  of gabbro (Figure 2.1a). Oceanic lithosphere is continually made at a pseudo-mid-ocean ridge at the left boundary of the model (Figure 2.1b). An enhanced vertical cooling condition applied at 200  $\text{km}$  from left boundary adjusts for the proper oceanic-plate age, and therefore its lithospheric thickness as it enters the trench (Agrusta *et al.*, 2013). Oceanic-plate ages range from 32.6 to 110  $\text{Ma}$  and convergence velocities from 40 to 100  $\text{km}/\text{Ma}$  (Figure 2.2a). This range of parameters broadly reflects the middle-range of modern global subduction systems (Syracuse & Abers, 2006).

Initial continental geotherms are determined by solving the heat flow equation in one-dimension to 1300  $^{\circ}\text{C}$  (Figure 2.2b). This study assumes a fixed temperature of 0  $^{\circ}\text{C}$  at



**Figure 2.2: Range of thermo-kinematic boundary conditions used in numerical experiments. (a) Thermal parameters (grayscale) range from 13 to 110  $km/100$  and broadly reflect the distribution of oceanic-plate ages and convergence velocities in modern subduction zones. Model names include the prefix "cd" for "coupling depth" with increasing alphabetic suffixes. Note that neither axes are continuous. (b) Upper plate thickness ( $Z_{UP}$ ) is defined by a range of continental geotherms. Geotherms were constructed using a one-dimensional steady-state conductive cooling model with  $T(z=0) = 0^\circ C$ ,  $\vec{q}(z=0) = 59, 63, 69, 79 mW/m^2$ , and constant radiogenic heating of  $1.0 \mu W/m^3$  for a 35 km-thick crust and  $0.022 \mu W/m^3$  for the mantle. Continental geotherms are calculated up to  $1300^\circ C$  with a constant  $0.5^\circ C/km$  gradient (the mantle adiabat) extending to the base of the model domain.**

the surface, constant radiogenic heating of  $1 \mu\text{W}/\text{m}^3$  in the 35 km-thick continental crust,  $0.022 \mu\text{W}/\text{m}^3$  in the mantle, with thermal conductivities of  $2.3 \text{ W}/\text{mK}$  and  $3.0 \text{ W}/\text{mK}$  for the continental crust and mantle, respectively. Above,  $1300^\circ\text{C}$ , temperature is assumed to constantly increase by  $0.5^\circ\text{C}/\text{km}$  (the mantle adiabat) to the base of the model domain.

Many studies define the base of the continental lithosphere at the  $1300^\circ\text{C}$  isotherm, but it can be determined directly by visualizing viscosity and strain rate as the model progresses. The mechanical base of the lithosphere ( $Z_{UP}$ ) in the models generally occurs near the  $1100^\circ\text{C}$  isotherm—characterized by a rapid decrease in viscosity and increase in strain rate (Figures ??, ??, ??). As such, this study considers oceanic and continental lithospheres as mechanical layers defined by viscosity, rather than defined merely by temperature.  $Z_{UP}$  corresponding to backarc surface heat flow of 59, 63, 69, and  $79 \text{ mW}/\text{m}^2$  are used in this study (Figure 2.2b).

### 2.3.3 Metamorphic (de)hydration reactions

Using Lagrangian markers (Harlow, 1962, 1964) to store and update material properties and PTS fields allows for straight-forward numerical implementation of metamorphic reactions. This approach is key to regulating mechanical coupling dynamically in SZ simulations. For example, dehydration (eclogitization) of the oceanic-plate and (de)stabilization of antigorite in the upper-plate mantle may be effectively modelled by tracing marker PTt paths while changing marker properties according to thermodynamically-stable mineral assemblages (e.g., Connolly, 2005). For computational efficiency, however, water contents in this study

are not computed by iteratively solving thermodynamic systems of equations. Instead, gradual eclogitization of oceanic crust is computed as a linear function of lithostatic pressure to a maximum depth of 150 *km*, or temperature of 1427 °C, while including garnet-in and plagioclase-out reactions defined by [Ito & Kennedy \(1971\)](#). Mantle (de)hydration is computed according reactions boundaries defined by [Schmidt & Poli \(1998\)](#) with a maximum water content of 2 *wt. %* (explained below). This approach effectively simulates continuous influx of water to the upper-plate mantle with relatively low computational cost, beginning with compaction and release of connate water at shallow depths, followed by a sequence of reactions consuming major hydrous phases (chlorite, lawsonite, zoisite, chloritoid, talc, amphibole, and phengite) in different parts of the hydrated basaltic crust ([Schmidt & Poli, 1998](#); [van Keken \*et al.\*, 2011](#)).

The extent of metamorphic reaction effects on mechanical coupling, and the exact (de)hydration reaction(s) likely responsible, are unknown. However, formation of brucite and serpentine from dry olivine near the plate interface are inferred to strongly regulate mechanical behaviour ([Hyndman & Peacock, 2003](#); [Peacock & Hyndman, 1999](#); [Agard \*et al.\*, 2016](#)). Brucite notably breaks down at much lower temperatures than serpentine ([Schmidt & Poli, 1998](#)), so serpentine (de)stabilization arguably represents the key transition from a weak-to-strong upper-plate mantle deep in *SZs*. This study elects an implement of antigorite (de)hydration for this reason. The reaction is assumed to be abrupt and discontinuous, which is a fine approximation for near-endmember compositions like (Mg-rich) peridotites. The *PT*

conditions of the reaction  $\text{antigorite} \rightleftharpoons \text{olivine} + \text{orthopyroxene} + H_2O$  were numerically implemented by the following equation (after [Schmidt & Poli, 1998](#)):

$$T_{atg-out}(z) = \begin{cases} 751.50 + 6.008 \times 10^{-3}z - 3.469 \times 10^{-8}z^2, & \text{for } z < 63000m \\ 1013.2 - 6.039 \times 10^{-5}z - 4.289 \times 10^{-9}z^2, & \text{for } z > 63000m \end{cases} \quad (2.1)$$

where  $z$  is the depth of a marker from the surface in meters and  $T$  is temperature in Kelvins. This reaction boundary is consistent to within  $25^\circ C$  of more recent experiments by [Shen et al. \(2015\)](#). Markers with internal temperature exceeding  $T_{atg-out}(z)$  spontaneously form  $\text{olivine} + \text{orthopyroxene} + H_2O$  and release their crystal-bound water. This implementation tacitly assumes thermodynamic equilibrium and is common to many versions of I2VIS.

Oceanic-plates of different ages are also tacitly assumed to dehydrate similarly with the above implementation. However, older (colder) oceanic-plates are expected to carry water to greater depths than younger (warmer) plates because of relatively delayed water-releasing reactions ([Peacock, 1996](#)). Abrupt water release at the antigorite dehydration reaction boundary defined by Equation (2.1) was tested to model deep water retention in cold oceanic-plates. Mechanical coupling behaviour was indistinguishable from gradual water release models. This implies rates of water release are less important than the depth of antigorite dehydration. Explicitly modelling other major dehydration reactions are

thus unlikely to significantly affect mechanical coupling behaviour, yet likely to introduce numerical artifacts at great computational cost. A simplified gradual water release model for all oceanic-plates is therefore preferred.

Water released by rock forms discrete fluid particles that migrate with relative velocities defined by local deviatoric (non-lithostatic) pressure gradients (see Appendix @ref(!!!), [Faccenda \*et al.\*, 2009](#)). Fluid velocities are scaled by a 10 *cm/yr* vertical percolation velocity to account for purely lithostatic pressure gradients in the mantle ([Gorczyk \*et al.\*, 2007](#)). Fluid particles migrate until encountering rock that can consume additional water by equilibrium hydration or melting reactions, (Table 2.2).

The shallow upper-plate mantle can theoretically store large amounts of water as antigorite may contain up to 13 *wt.%* water ([Reynard, 2013](#)) and is generally stable at shallow mantle conditions. Thermodynamic models predict 8 *wt.%* water in the shallow upper-plate mantle ([Connolly, 2005](#)). However, seismic studies suggest most shallow upper-plate mantles are only partially serpentized (< 20-40%), equating to water contents of ca. 3-6 *wt.%* ([Abers \*et al.\*, 2017](#); [Carlson & Miller, 2003](#)). Many modes of mantle hydration are documented or inferred, including evidence for channelized fluid flow within ophiolites exhumed from SZs ([Angiboust \*et al.\*, 2012, 2014](#); [Zack & John, 2007](#); [Plümper \*et al.\*, 2017](#)). This study limits mantle wedge hydration to  $\leq 2$  *wt.%*  $H_2O$  and assumes any excess  $H_2O$  exits the system through channelized fluid flow during plastic or brittle deformation ([Davies, 1999](#)).



### 2.3.4 Rheologic model

Contributions from dislocation and diffusion creep are accounted for by computing a composite rheology for ductile rocks,  $\eta_{effective}$ :

$$\frac{1}{\eta_{effective}} = \frac{1}{\eta_{diff}} + \frac{1}{\eta_{disl}} \quad (2.2)$$

where  $\eta_{diff}$  and  $\eta_{disl}$  are effective viscosities for diffusion and dislocation creep.

For the crust and serpentinized mantle,  $\eta_{diff}$  and  $\eta_{disl}$  are computed as:

$$\begin{aligned} \eta_{diff} &= \frac{1}{2} A \sigma_{crit}^{1-n} \exp \left[ \frac{E + PV}{RT} \right] \\ \eta_{disl} &= \frac{1}{2} A^{1/n} \dot{\epsilon}_{II}^{(1-n)/n} \exp \left[ \frac{E + PV}{nRT} \right] \end{aligned} \quad (2.3)$$

where  $R$  is the gas constant,  $P$  is pressure,  $T$  is temperature in  $K$ ,  $\dot{\epsilon}_{II} = \sqrt{\frac{1}{2} \dot{\epsilon}_{ij}^2}$  is the square root of the second invariant of the strain rate tensor,  $\sigma_{crit}$  is an assumed diffusion-dislocation transition stress, and  $A$ ,  $E$ ,  $V$  and  $n$  are the material constant, activation energy, activation volume, and stress exponent, respectively (Table 2.1, [Hilaliret et al., 2007](#); [Ranalli, 1995](#)).

For the mantle,  $\eta_{diff}$  and  $\eta_{disl}$  are computed as ([Karato & Wu, 1993](#)):

$$\begin{aligned} \eta_{diff} &= \frac{1}{2} A^{-1} G \left[ \frac{h}{b} \right]^{m/n} \exp \left[ \frac{E + PV}{RT} \right] \\ \eta_{disl} &= \frac{1}{2} A^{-1/n} G \dot{\epsilon}_{II}^{(1-n)/n} \exp \left[ \frac{E + PV}{nRT} \right] \end{aligned} \quad (2.4)$$

**Table 2.1: Material properties used in numerical experiments**

Material	$\rho$	$H_2O$	Flow Law	$\log_{10}A$	$E$	$V$	$n$	$\phi$	$\sigma_{crit}$	$k_1$	$k_2$	$k_3$	$H$
sediments	2600	5.0	wet quartzite	-3.5	154.0	3.0	2.3	0.15	0.03	0.64	807	4e-06	2.000
felsic crust	2700		wet quartzite	-3.5	154.0	3.0	2.3	0.45	0.03	0.64	807	4e-06	1.000
basalt	3000	5.0	plag an75	-3.5	238.0	8.0	3.2	0.45	0.03	1.18	474	4e-06	0.250
gabbro	3000		plag an75	-3.5	238.0	8.0	3.2	0.45	0.03	1.18	474	4e-06	0.250
mantle dry	3300		dry olivine	4.4	540.0	20.0	3.5	0.45	0.30	0.73	1293	4e-06	0.022
mantle hydrated	3300	0.5	wet olivine	3.3	430.0	10.0	3.0	0.45	0.24	0.73	1293	4e-06	0.022
serpentine	3200	2.0	serpentine	3.3	8.9	3.2	3.8	0.15	3.00	0.73	1293	4e-06	0.022

*key:*  $\rho$ : density [ $kg/m^3$ ],  $H_2O$ : water content [wt.%],  $A$ : material constant,  $E$ : activation energy [ $kJ/mol$ ],  $V$ : activation volume [ $J/MPa \cdot mol$ ],  $n$ : power law exponent,  $\phi$ : internal friction angle,  $\sigma_{crit}$ : critical stress [ $MPa$ ],  $H$ : heat production [ $\mu W/m^3$ ]

*constants:*  $C_p$ : heat capacity = 1 [ $kJ/kg$ ],  $\alpha$ : expansivity =  $2 \times 10^{-5}$  [ $1/K$ ],  $\beta$ : compressibility = 0.045 [ $1/MPa$ ]

*thermal conductivity:*  $k$  [ $W/m \cdot K$ ] =  $(k_1 + \frac{k_2}{T+77}) \times \exp(k_3 \cdot P)$  with  $P$  in [ $MPa$ ] and  $T$  in [ $K$ ]

*references:* Turcotte & Schubert (2002), Ranalli (1995), Hilairt et al. (2007), Karato & Wu (1993)

**Table 2.2: Melting curves used in numerical experiments**

Material	a	b	c	d	e	f	g	h	i	j
sediments	1200	889	1.79e+04	54	2.02e+04	831	6.00e-02		1262	0.009
felsic crust	1200	889	1.79e+04	54	2.02e+04	831	6.00e-02		1262	0.009
basalt	1600	973	7.04e+05	354	7.78e+07	935	3.50e-03	6.2e-05	1423	0.105
gabbro	1600	973	7.04e+05	354	7.78e+07	935	3.50e-03	6.2e-05	1423	0.105
mantle dry						1394	1.33e-01	-5.1e-05	2073	0.114
mantle hydrated	2400	1240	4.98e+04	323			1.27e+05	3.5e-05	2073	0.114
serpentine	2400	1240	4.98e+04	323			1.27e+05	3.5e-05	2073	0.114

*solidus curve:*  $T(P) = [b + \frac{c}{(P+d)} + \frac{e}{(P+d)^2}]$  at  $P < a$  and  $[f + gP + hP^2]$  at  $P \geq a$

*liquidus curve:*  $T(P) = i + jP$  with  $T$  in [ $K$ ] and  $P$  in [ $MPa$ ]

*reference:* Schmidt & Poli (1998)

where  $b=5 \times 10^{-10}$  m is Burgers vector,  $G=8 \times 10^{10}$  Pa is shear modulus,  $h=1 \times 10^{-3}$  m is the assumed grain size,  $m = 2.5$  is the grain size exponent, and the other flow law parameters are given in Table 2.1. Our models limited viscosity for all rocks at  $\eta_{min} = 10^{17}$  Pa·s and  $\eta_{max} = 10^{25}$  Pa·s.

An effective visco-plastic rheology is achieved by limiting  $\eta_{effective}$  with a brittle (plastic) yield criterion:

$$\eta_{effective} \leq \frac{C + \phi P}{2 \dot{\epsilon}_{II}} \quad (2.5)$$



# CHAPTER 3:

## A COMPARISON OF HEAT FLOW INTERPOLATIONS NEAR SUBDUCTION ZONES

### Keypoints:

- Inconsistent spatial patterns characterize heat flow near subduction zones
- Heat flow investigations favour 2D interpolations over 1D transects
- Scaling datasets and new interpolation schema will advance **SZ** research

### 3.1 Abstract

Heat fluxing through the Earth's surface provides indirect observations of **pressure-temperature-strain (PTS)** fields deep in **SZs**. Global heat flow databases, therefore, are invaluable for generating and testing belief about **SZ** geodynamics. Investigating **surface heat flow (SHF)** in two-dimensions by interpolation, rather than in one-dimension by

projection, arguably forms better interpretations about spatial continuity of deep processes. Direct comparisons of interpolations based on the First (spatial continuity) and Third (similarity) Laws of Geography applied to the most updated global heat flow database. Inconsistent spatial patterns of SHF near SZs are observed in magnitude and variance, regardless of interpolation method. The implications include discontinuous PTS fields at depth, countering hypotheses of commonly thin upper plate lithospheres and mechanical CDs among subduction zones. Strategic scaling of SHF datasets will improve interpolation precision and confidence—leading to better tools for distinguishing differences within and among SZs. New data acquisition and composite interpolation schema are proposed as avenues for future SZ research.

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