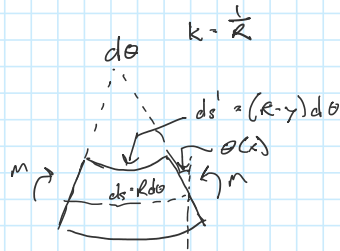
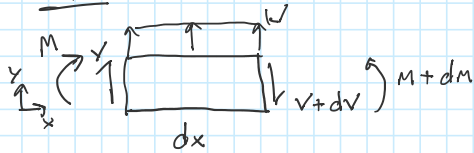


Timoshenko Point Load

Thursday, August 31, 2023 1:00 PM

Basis



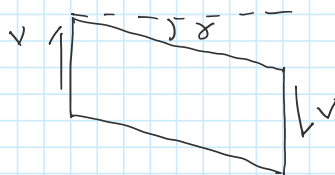
• POSITIVE LOADS POINT IN POSITIVE Y

→ • POSITIVE MOMENT = COUNTER CLOCKWISE

• POSITIVE INTERNAL SHEAR IN NEGATIVE Y

THIS MEANS POSITIVE NORMAL ROTATION OF CROSS SECTION, θ , IS ALSO COUNTER CLOCKWISE

PURE SHEAR DEFORMATION



$$V = G k A \gamma, \text{ WHERE } kA = \text{SHEAR AREA}$$

$$\gamma = \frac{V}{G k A}$$

• ASSUME NO LONG STRAIN FROM SHEAR DEFORMATION

$$\therefore \frac{dv}{dx} = \theta - \gamma$$

↑
NOTE "-" SIGN.

PUTTING IT TOGETHER:

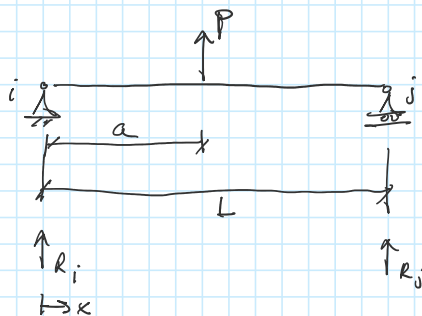
WHERE u = DISPLACEMENT IN Y, POSITIVE UPWARD.

$$\frac{dv}{dx} = \theta(x) - \frac{V(x)}{G k A} \Rightarrow V(x) = G k A \left(\theta(x) - \frac{dv}{dx} \right)$$

$$\frac{d\theta}{dx} = \frac{M(x)}{EI}$$

$$M(x) = EI \frac{d\theta}{dx}$$

POINT LOAD



STATICS

$$\uparrow \sum F_y = 0 \Rightarrow R_i + P + R_j = 0$$

$$R_i = -R_j - P = \frac{P(a-L)}{L} \quad \text{or} \quad \frac{-P(L-a)}{L}$$

$$\curvearrowright \sum M_i = 0 \Rightarrow Pa + R_j L = 0$$

$$R_j = \frac{-Pa}{L}$$

$$R_i + P = -R_j$$

PRECISE FUNCTIONS!

$$0 \leq x \leq a$$

← x

→

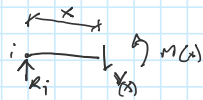
|

$$a \leq x \leq L$$

→

1. ELEMENT FUNCTIONS:

$$0 \leq x \leq a$$



$$\uparrow \sum F_y = 0 = R_i - V(a) \Rightarrow$$

$$V(a) = R_i$$

$$\curvearrowright \sum M_i = 0 = -V(a)x + M(a) = 0$$

$$M(a) = V(a)x = R_i x$$

$$V(x) = R_i$$

$$M(x) = R_i x$$

APPLICATION OF TIMOSHENKO RELATIONSHIPS

$$\textcircled{1} R_i = kAG \left(\theta(a) - \frac{du}{dx} \right)$$

$$\textcircled{2} R_i x = EI \frac{d\theta}{dx}$$

From $\textcircled{2}$

$$\int \frac{R_i x}{EI} dx = \int d\theta$$

$$\frac{R_i x^2}{2EI} + C_1 = \theta \quad \textcircled{5}$$

From $\textcircled{1}$ & $\textcircled{5}$

$$R_i = kAG \left(\frac{R_i x^2}{2EI} + C_1 - \frac{du}{dx} \right)$$

$$\frac{R_i}{kAG} = \frac{R_i x^2}{2EI} + C_1 - \frac{du}{dx}$$

$$\frac{R_i}{kAG} - \frac{R_i x^2}{2EI} - C_1 = - \frac{du}{dx}$$

$$\int \left(-\frac{R_i}{kAG} + \frac{R_i x^2}{2EI} + C_1 \right) dx = \int du$$

$$-\frac{R_i x}{kAG} + \frac{R_i x^3}{6EI} + C_1 x + C_2 = u \quad \textcircled{6}$$

BOUNDARY & COMPATIBILITY CONDITIONS

$$u = 0 \quad x = 0 \quad \text{BC1}$$

$$u = 0 \quad x = L \quad \text{BC2}$$

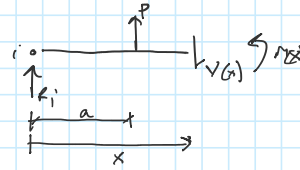
$$\theta = \text{CONSTANT} \quad x = a \quad \text{BC3}$$

$$u = \text{CONSTANT} \quad x = a \quad \text{BC4}$$

BC1

$$C_2 = 0$$

$$a \leq x \leq L$$



$$\uparrow \sum F_y = 0 \Rightarrow \overbrace{R_j + P}^{-R_j} - V(L) = 0$$

$$V(L) = -R_j$$

$$\curvearrowright \sum M_i = 0 \Rightarrow Pa - V(L)x + M(L) = 0$$

$$M(L) = V(L)x - Pa = -R_j x - Pa$$

APPLICATION OF TIMOSHENKO RELATIONSHIPS

$$\textcircled{3} -R_j = kAG \left(\theta(L) - \frac{du}{dx} \right)$$

$$\textcircled{4} -R_j x - Pa = EI \frac{d\theta}{dx}$$

From $\textcircled{4}$

$$\int \left(-\frac{R_j x}{EI} - \frac{Pa}{EI} \right) dx = \int d\theta$$

$$-\frac{R_j x^2}{2EI} - \frac{Pax}{EI} + C_3 = \theta \quad \textcircled{7}$$

From $\textcircled{3}$ & $\textcircled{7}$

$$-R_j = kAG \left(-\frac{R_j x^2}{2EI} - \frac{Pax}{EI} + C_3 - \frac{du}{dx} \right)$$

$$-\frac{R_j}{kAG} = -\frac{R_j x^2}{2EI} - \frac{Pax}{EI} + C_3 - \frac{du}{dx}$$

$$\int \left(\frac{R_j}{kAG} - \frac{R_j x^2}{2EI} - \frac{Pax}{EI} + C_3 \right) dx = \int du$$

$$\frac{R_j x}{kAG} - \frac{R_j x^3}{6EI} - \frac{Pax^2}{2EI} + C_3 x + C_4 = u \quad \textcircled{8}$$

BC2

$$\frac{R_j L}{kAG} - \frac{R_j L^3}{6EI} - \frac{PaL^2}{2EI} + C_3 L + C_4 = 0$$

$$L C_3 + C_4 = -\frac{R_j L}{kAG} + \frac{R_j L^3}{6EI} + \frac{PaL^2}{2EI}$$

BC3

$$\frac{R_i a^2}{2EI} + C_1 = \frac{-R_j a^2}{2EI} - \frac{Pa^2}{EI} + C_3$$

$$C_1 - C_3 = \frac{-R_j a^2}{2EI} - \frac{R_i a^2}{2EI} - \frac{Pa^2}{EI}$$

BC4

$$-\frac{R_i a}{kAG} + \frac{R_i a^3}{6EI} + C_1 a + C_2 = \frac{R_j a}{kAG} - \frac{R_j a^3}{6EI} - \frac{Pa^3}{2EI} + C_3 a + C_4$$

$$a C_1 + C_2 - a C_3 - C_4 = \frac{R_i a}{kAG} - \frac{R_i a^3}{6EI} + \frac{R_j a}{kAG} - \frac{R_j a^3}{6EI} - \frac{Pa^3}{2EI}$$

$$\left[\begin{array}{c} \frac{Pa^3}{6EIL} - \frac{Pa^2}{2EI} + \frac{LPa}{3EI} \\ 0 \\ \frac{Pa^3}{6EIL} + \frac{LPa}{3EI} \\ \frac{Pa}{A_s G} - \frac{Pa^3}{6EI} \end{array} \right] = \left[\begin{array}{c} C_1 \\ C_2 \\ C_3 \\ C_4 \end{array} \right]$$

$$A_s = kA$$

FIXED END MOMENTS

$$\left[\begin{array}{c} -C_1 \\ \frac{R_j L^2}{2EI} + \frac{PaL}{EI} - C_3 \end{array} \right] = \left[\begin{array}{cc} k_{s11} & k_{s1j} \\ k_{sji} & k_{sjj} \end{array} \right] \left[\begin{array}{c} M_i \\ M_j \end{array} \right]$$