

Question 5

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(c) Yes it is possible to determine the peak modal base shear and base overturning moments without determining time histories of  $A_n(t)$ . We can use the response spectrum for this purpose. We only need the peak pseudo acceleration response values.

equivalent static force =  $f_n(t) = S_n A_n$

$$\Rightarrow f_{n1} = S_{n1} A_n$$

we can do any analysis for this force now.  
instead of  $S_n$  in RHA.

Question 5 :-

Roof slab dimensions = 7m x 5m.

$$\begin{aligned} \text{Weight} &= 5 \text{ kN/m}^2 \\ \text{Total weight} &= (5 \times 7 \times 5) \text{ kN} \\ &= 175 \text{ kN} = \frac{175 \times 10^3}{10} \end{aligned}$$

$$K_A = K_B = 500 \text{ kN/m.} \quad = (17500 \text{ kg})$$

$$K_C = 250 \text{ kN/m}$$

$$K_D = 400 \text{ kN/m.}$$

$$P_{GT} = 0.3g.$$

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$$\tilde{m} = \begin{bmatrix} 17500 & 0 & 0 \\ 0 & 17500 & 0 \\ 0 & 0 & \frac{17500(7^2+5^2)}{12} \end{bmatrix} \text{ kg.}$$

$$\tilde{k} = \begin{bmatrix} (K_A + K_B) & 0 & 2(K_B - K_A) \\ 0 & (K_C + K_D) & 3(K_C - K_D) \\ 2(K_B - K_A) & 3(K_C - K_D) & 3^2(K_C + K_D) + 2^2(K_A + K_B) \end{bmatrix}$$

$$\Rightarrow K_n = \begin{bmatrix} 1000 & 0 & 0 \\ 0 & 650 & -450 \\ 0 & -450 & 9850 \end{bmatrix} \times 10^3 \text{ N/m.}$$

Now for modal frequencies, eigen  
values  $\rightarrow$

$$|K_n - \omega_n^2 I| = 0.$$

$$\begin{vmatrix} 1000 - \omega_n^2 (17500) & 0 & 0 \\ 0 & 650 - \omega_n^2 (17500) & -450 \\ 0 & -450 & 9850 - \omega_n^2 (107916.67) \end{vmatrix} = 0$$

$\Rightarrow$  Solving, we get  $\omega_n^2 = 35.23, 57.143,$   
(in the order) rad/s  $93.1874$   
 $\omega_n^2 = 5.935, 7.56$  rad/s.  
and 9.65 rad/s.

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for Mode 1 :-

$$\Phi_1 = \begin{Bmatrix} 0 \\ -0.0074 \\ -0.006 \end{Bmatrix}.$$

$$\Phi_2 = \begin{Bmatrix} 0.0076 \\ 0 \\ 0 \end{Bmatrix}.$$

$$\Phi_3 = \begin{Bmatrix} 0 \\ -0.0014 \\ 0.0030 \end{Bmatrix}.$$

We see that the x-DOF is completely independent, so we can separate it

$$m_{xx} \ddot{u}_x + (k_x + k_B) u_x = 0. \quad (1)$$

and

$$\begin{bmatrix} m & 0 \\ 0 & I \end{bmatrix} \begin{Bmatrix} \ddot{u}_y \\ \ddot{u}_0 \end{Bmatrix} + \begin{bmatrix} k_c + k_D & 3(k_c - k_D) \\ 3(k_c - k_D) & 9(k_c + k_D) + 4(k_B + k_D) \end{bmatrix} \begin{Bmatrix} u_y \\ u_0 \end{Bmatrix} = -m \ddot{u}_y$$

$$\text{Now, } \Phi = \begin{bmatrix} -0.0074 & -0.0014 \\ -0.006 & 0.0030 \end{bmatrix}$$

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$$\text{Now, } S_n = \Gamma_n m \Phi_n.$$

$$\begin{aligned} M_n &= \Phi^T m \Phi \\ &= \begin{pmatrix} -0.0074 & -0.006 \\ -0.0014 & 0.003 \end{pmatrix} \begin{pmatrix} 17500 & 0 \\ 0 & 107916.62 \end{pmatrix} \times \Phi \end{aligned}$$

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which gives  $M_n = \begin{pmatrix} 1 & 0 \\ 0 & 1 \end{pmatrix}.$

Next,  $L_n^2 = \sum_{j=1}^N m_j \Phi_j \Gamma_n.$

$$\begin{aligned} &= \Phi^T m \Gamma_n \\ &\Gamma_n = \begin{pmatrix} 1 \\ 0 \end{pmatrix}. \\ &\therefore L_n^2 = \begin{pmatrix} -0.0074 & -0.006 \\ -0.0014 & 0.003 \end{pmatrix} \times m \times \begin{pmatrix} 1 \\ 0 \end{pmatrix}. \\ &= \begin{pmatrix} -130.086 \\ -24.035 \end{pmatrix} \rightarrow \begin{matrix} L_1^2 \\ L_2^2 \end{matrix}. \end{aligned}$$

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$$\Gamma_n = \frac{L_n^2}{M_n} = L_n^2 \text{ as } M_n = 1.0.$$

$$\therefore \Gamma_n = \left\{ \begin{array}{l} -130.086 \\ -24.035 \end{array} \right\}.$$

$$\therefore S = \sum_{n=1}^{2N} S_n = \sum_{n=1}^{2N} \Gamma_n \left\{ \begin{array}{l} m^4 y_n \\ r_m \Phi_n \end{array} \right\}.$$

$$\text{But } S_1 = \Gamma_1 m \Phi_1.$$

$$= -130.086 \begin{pmatrix} 17500 & 0 \\ 0 & 107916.62 \end{pmatrix} \left\{ \begin{array}{l} -0.001 \\ -0.006 \end{array} \right\}$$

$$= 10^4 \left\{ \begin{array}{l} 1.685 \\ 8.4231 \end{array} \right\}.$$

you don't need  $S_n$ 

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$$\begin{aligned} S_2 &= T_2 m \phi_2 \\ &= -24.035 \begin{pmatrix} 17500 & 0 \\ 0 & 107916.67 \end{pmatrix} \begin{Bmatrix} -0.004 \\ +0.003 \end{Bmatrix} \\ &= \begin{pmatrix} 10^4 \\ -8.4231 \end{pmatrix}. \end{aligned}$$

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