

ME518 - Final project

Due by 12/15/2017

Problem 1 (3 points)

Write a code to calculate numerically $u^+(y^+)$ using Van Driest formula:

$$u^+(y^+) = \int_0^{y^+} \frac{2}{1 + \sqrt{1 + 4l_m^+(y')^2}} dy' \quad (1)$$

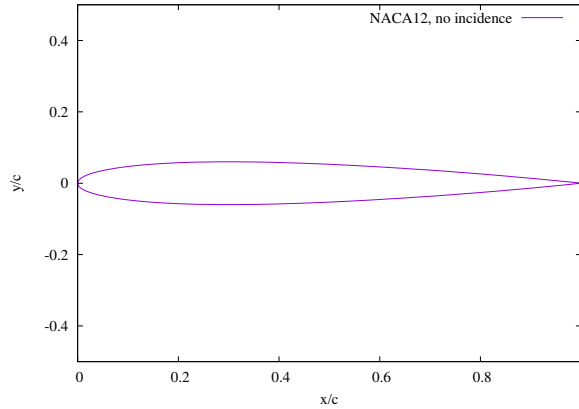
where the mixing length l_m^+ varies as

$$l_m^+(y^+) = ky^+[1 - \exp(-y^+/A^+)] \quad \text{with } k = 0.41, A^+ = 26. \quad (2)$$

Output of problem 1: Plot the graph $u^+(y^+)$ and compare the numerical solution with the approximate solutions valid in the viscous sublayer and in the log-law layer.

Problem 2 (7 points)

The external velocity distribution $U_e(x)/U_\infty$ for a symmetric NACA0012 airfoil is given in the file naca12_airfoil_0000.dat.



Compute the complete boundary-layer development (laminar and turbulent) on this airfoil for a chord Reynolds number $Re_c = cU_\infty/\nu = 6.67 \times 10^6$. Assume $c = 1$ m and $\nu = 1.5 \times 10^{-5} \text{ m}^2/\text{s}$.

- For the laminar portion use the semi-empirical Thawites's method to calculate the boundary layer integral proprieties: the momentum thickness distribution is modeled as

$$\frac{1}{\nu} \frac{d}{dx} (\theta^2 U_e^6) = 0.45 U_e^5 \quad (3)$$

and for a boundary layer starting at a stagnation point on the airfoil ($x_0 \equiv 0$ in this case with no incidence), it can be shown from potential theory and perturbation analysis that

$$\theta_0^2 = \frac{0.075\nu}{(dU_e/dx)_0} \quad \text{for } x = 0 \quad (4)$$

$$\theta^2(x) = \frac{0.45\nu}{U_e^6(x)} \int_0^x U_e^5(x') dx' \quad \text{for } x > 0 \quad (5)$$

The flatness factor $H \equiv \delta^*/\theta$ is calculated using the empirical correlations

$$H(x) = 2.61 - 3.75\lambda(x) + 5.24\lambda^2(x) \quad 0 < \lambda < 0.1 \quad (6)$$

$$H(x) = 2.088 + \frac{0.0731}{\lambda(x) + 0.14} \quad -0.1 < \lambda < 0 \quad (7)$$

where the Thwaites' parameter is $\lambda(x) = \frac{\theta^2}{\nu} \frac{dU_e}{dx}$.

• For the turbulent portion use the semi-empirical Head's method to calculate the boundary layer integral proprieties. Define

$$H \equiv \frac{\delta^*}{\theta} \quad (8)$$

$$H_1 \equiv \frac{\delta - \delta^*}{\theta} \quad (9)$$

and assume the following dependence

$$\frac{1}{U_e} \frac{d}{dx} (U_e(\delta - \delta^*)) \equiv \frac{1}{U_e} \frac{d}{dx} (U_e H_1 \theta) = F(H_1) \quad (10)$$

with

$$F(H_1) = \frac{0.0306}{(H_1 - 3.0)^{0.6169}} \quad (11)$$

$$H_1 = G(H) = 3.0445 + \frac{0.8702}{(H - 1.1)^{1.2721}} \quad (12)$$

Expand Eq. 10 and combine with the Von Karman integral momentum equation,

$$\frac{d\theta}{dx} + (2 + H) \frac{\theta}{U_e} \frac{dU_e}{dx} = \frac{C_f}{2} \quad (13)$$

to get

$$\frac{dH}{dx} = \left(\frac{(1 + H) \frac{G(H)}{U_e} \frac{dU_e}{dx} - \frac{G(H)}{\theta} \frac{C_f}{2} + \frac{0.0299}{\theta (G(H) - 3.0)^{0.6169}}}{\frac{dG}{dH}} \right) \quad (14)$$

The drag coefficient is given by

$$C_f = \frac{0.246}{10^{0.678 H} \left(\frac{U_e}{U_\infty} R_\theta \right)^{0.268}}, \quad R_\theta = \frac{U_\infty \theta}{\nu} \quad (15)$$

Equations 13, 14 supplemented with Eq. 15 constitute two equations in θ and H that completely solve the boundary layer: the displacement thickness δ^* and the boundary layer thicknesses δ are readily deduced from Eqs. 8-9.

Output of problem 2: Integrate numerically Eqs. 13, 14 and plot δ , δ^* and θ as a function of the chord abscissa along the profile.

NOTE 1: Assume that transition to turbulence occurs at $x/c = 0.2$, hence switch the integration of θ from Thwaites' to Head's method for $x/c > 0.2$. To initialize integration of Eqs. 13, 14 in the turbulent portion of the BL, use the value obtained in the laminar portion: $\theta_{\text{init}} = \theta_{\text{lam}}(x/c = 0.2)$ where θ_{lam} is obtained from Eq. 5. Also assume that $H_{\text{init}} = 1.4$.

NOTE 2: Use any integration scheme (but at least second order) for the integration (ideally Runge-Kutta 4 is excellent). Also use any language or numerical package of your preference, e.g. Fortran, C++, or Matlab, etc.