

REFERRED RCO223 CLASSICAL CONTROL  
LABORATORY REPORTS FOR COURSEWORK 2018  
STUDENT NUMBER: 10557913

GITHUB LINK TO MATLAB FILES: <https://github.com/bwickenden/RCO223.git>

## 1. Linearize the non-linear differential equation

1. Linearise a non linear equation.

$$\frac{d^2\theta}{dt^2} = -\frac{\mu}{(I+ml^2)} \frac{d\theta}{dt} + \frac{mgl}{(I+ml^2)} \sin(\theta) + \frac{ml}{(I+ml^2)} \cos(\theta) u$$

$u$  = Control variable

State Space Variables:

$$x_1 = \theta$$
$$x_2 = \frac{d\theta}{dt}$$
$$\dot{x}_1 = \frac{d\theta}{dt} \quad \dot{x}_2 = \frac{d^2\theta}{dt^2}$$
$$\dot{x}_2 = \frac{-\mu}{(I+ml^2)} x_2 + \frac{mgl}{(I+ml^2)} \sin(x_1) + \frac{ml}{(I+ml^2)} \cos(x_1) u$$
$$f_1 = \dot{x}_1 = x_2$$
$$f_2 = \dot{x}_2 = \frac{-\mu}{(I+ml^2)} x_2 + \frac{mgl}{I+ml^2} \sin x_1 + \frac{ml}{(I+ml^2)} \cos x_1 u$$

Equilibrium

$$\rightarrow \dot{x}_1 = 0 \rightarrow x_2 = 0$$
$$\dot{x}_2 = 0 \rightarrow \frac{mgl}{(I+ml^2)} \sin(x_1) + \frac{ml}{(I+ml^2)} \cos x_1 u = 0$$

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When it is at equilibrium the input is equal to zero  
 $\rightarrow u = 0$

$$\Rightarrow \frac{mgl}{(I \sin^2)} \sin(x_1) = 0$$

$$\Rightarrow \sin(x_1) = 0$$

This means that it is at equilibrium when

$$x_2 = 0$$

and

$$x_1 = (0, \pi)$$

$$x_1, x_2 = (0, 0)$$

$$\text{Or } x_1, x_2 = (\pi, 0)$$

Now we have the points of equilibrium we need to complete the Jacobian matrix

$$J = \begin{bmatrix} \frac{\partial f_1}{\partial x_1} & \frac{\partial f_1}{\partial x_2} \\ \frac{\partial f_2}{\partial x_1} & \frac{\partial f_2}{\partial x_2} \end{bmatrix}$$

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$$\begin{aligned} \text{So } \frac{\partial \mathcal{L}}{\partial x_1} &= \\ f_1 &= x_2 \\ f_1 &= 0 \cdot x_1 + 1 \cdot x_2 \\ \Rightarrow \frac{\partial \mathcal{L}}{\partial x_1} &= 0 \\ \frac{\partial \mathcal{L}}{\partial x_2} &= 1 \end{aligned}$$

$$f_2 = \frac{-\mu}{(I+ml^2)} x_2 + \frac{mgl}{(I+ml^2)} \sin(x_1) + \frac{ml}{(I+ml^2)} \cos(x_1) u$$

$$\frac{\partial \mathcal{L}}{\partial x_1} = \frac{mgl}{(I+ml^2)} \cos(x_1) + \frac{ml}{(I+ml^2)} - \sin(x_1) u$$

$$\frac{\partial \mathcal{L}}{\partial x_2} = \frac{-\mu}{(I+ml^2)}$$

$$\begin{bmatrix} 0 & 1 \\ \frac{mgl}{(I+ml^2)} \cos(x_1) + \frac{ml}{(I+ml^2)} - \sin(x_1) u & \frac{-\mu}{(I+ml^2)} \end{bmatrix}$$

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$\frac{\partial f_1}{\partial u} = \begin{bmatrix} 0 \\ \frac{ml}{I+ml^2} \sin(x_1) \end{bmatrix}$

$\frac{\partial f_2}{\partial u} = \frac{x_2}{u} \rightarrow u = \frac{d^2 x}{dt^2} = 0$

$\begin{bmatrix} 0 & 1 \\ \frac{mgl}{I+ml^2} & \frac{-\mu}{I+ml^2} \end{bmatrix} x_1 + \begin{bmatrix} 0 & 1 \\ \frac{-mgl}{I+ml^2} & \frac{-\mu}{I+ml^2} \end{bmatrix} x_2 + \begin{bmatrix} 0 \\ \frac{ml}{I+ml^2} \sin x_1 \end{bmatrix}$

$\text{Expand.}$

$(I+ml^2) \frac{d^2 \theta}{dt^2} + \mu \frac{d\theta}{dt} = mgl\theta + ml \frac{d^2 x}{dt^2}$

## 2. Write down the state space model of the system

For this task I worked through the statespace model both by hand and by using MatLab.

By hand:

Firstly I assigned my state variables

X1 and X2, along with X1 dot and X2 dot

I then rearranged the equation so the it was equal to X2 dot.

Next I let  $b_0 = \frac{ml}{(I+ml^2)}$  and then continued to simplify

Then I substituted X1 and X2 into each equation and then followd up by putting the equation in statespace form

MatLab code :

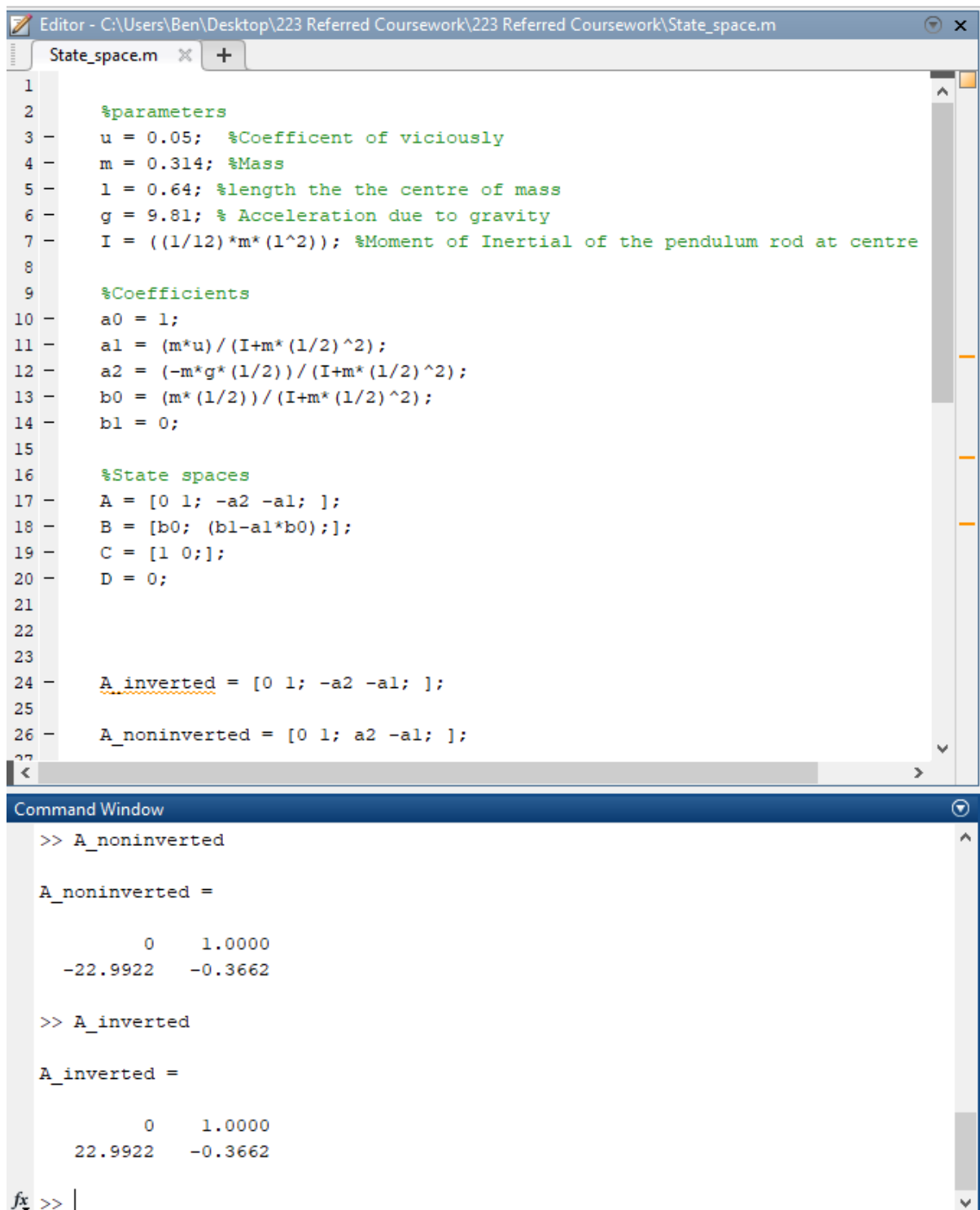
I started off by declaring the parameters for all of the components necessary

for the statespace model, including the calculation of  $I = \frac{1}{12} * m * l^2$

Next I added a list of coefficents, followed by the state spaces.

I then found the eigen vales for both A and A inverted.

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The image shows a MATLAB Editor window with a script named 'State\_space.m' and a Command Window below it. The script defines parameters, coefficients, and state-space matrices for a pendulum system.

```
1
2 %parameters
3 u = 0.05; %Coefficient of viciously
4 m = 0.314; %Mass
5 l = 0.64; %length the the centre of mass
6 g = 9.81; % Acceleration due to gravity
7 I = ((1/12)*m*(l^2)); %Moment of Inertial of the pendulum rod at centre
8
9 %Coefficients
10 a0 = 1;
11 a1 = (m*u)/(I+m*(l/2)^2);
12 a2 = (-m*g*(l/2))/(I+m*(l/2)^2);
13 b0 = (m*(l/2))/(I+m*(l/2)^2);
14 b1 = 0;
15
16 %State spaces
17 A = [0 1; -a2 -a1];
18 B = [b0; (b1-a1*b0)];
19 C = [1 0];
20 D = 0;
21
22
23
24 A_inverted = [0 1; -a2 -a1];
25
26 A_noninverted = [0 1; a2 -a1];
27
```

The Command Window shows the results of the calculations for the state-space matrices:

```
>> A_noninverted

A_noninverted =

    0    1.0000
-22.9922  -0.3662

>> A_inverted

A_inverted =

    0    1.0000
 22.9922  -0.3662
```

fx >> |



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Roco 223 - State Space Model 4/5/18

$$(I + ml^2) \frac{d^2\theta}{dt^2} + \mu \frac{d\theta}{dt} = mgl\theta + ml \frac{d^2z}{dt^2}$$
$$\dot{x} = Ax + Bu$$
$$y = Cx + Du$$
$$\frac{d^2\theta}{dt^2} = \frac{-\mu}{(I + ml^2)} \frac{d\theta}{dt} + \frac{mgl\theta}{(I + ml^2)} + \frac{ml}{(I + ml^2)} \left( \frac{d^2z}{dt^2} \right)$$
$$x_1 = \theta \quad \dot{x}_1 = \frac{d\theta}{dt}$$
$$x_2 = \left( \frac{d\theta}{dt} - b_0 v_c \right)$$
$$\frac{d\theta}{dt} = (x_2 + b_0 v_c)$$
$$\dot{x}_2 = \frac{d^2\theta}{dt^2} - b_0 \frac{dv_c}{dt}$$
$$\Rightarrow \frac{d^2\theta}{dt^2} - b_0 \frac{dv_c}{dt} = \frac{-\mu}{(I + ml^2)} \frac{d\theta}{dt} + \frac{mgl\theta}{(I + ml^2)} + \frac{ml}{(I + ml^2)} \frac{dv}{dt} - b_0 \frac{dv_c}{dt}$$
$$b_0 = \frac{ml}{(I + ml^2)}$$

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$$\Rightarrow \left( \frac{d^2\theta}{dt^2} - \frac{ml}{(I+ml^2)} \frac{dv}{dt} \right)$$

$$\ddot{x}_2 = \frac{-\mu}{(I+ml^2)} \frac{d\theta}{dt} + \frac{mgl}{(I+ml^2)} \theta$$

$$\ddot{x}_2 = \frac{-\mu}{I+ml^2} \frac{d\theta}{dt} + \frac{mgl}{(I+ml^2)} x_1$$

$$\ddot{x}_2 = \frac{-\mu}{(I+ml^2)} \left[ x_2 + \left[ \frac{ml}{(I+ml^2)} \right] V_c \right] + \frac{mgl}{I+ml^2} x_1$$

$$\ddot{x}_2 = \frac{-\mu}{(I+ml^2)} x_2 + \frac{mgl}{I+ml^2} x_1 - \frac{\mu}{(I+ml^2)} \frac{ml}{(I+ml^2)} V_c$$

$$\ddot{x}_2 = \frac{mgl}{I+ml^2} x_1 - \frac{\mu}{(I+ml^2)} x_2 - \frac{\mu ml}{(I+ml^2)} V_c$$

$$\dot{x}_1 = \frac{d\theta}{dt} = x_2 + \frac{ml}{(I+ml^2)} V_c$$

$$\begin{bmatrix} \dot{x}_1 \\ \ddot{x}_2 \end{bmatrix} = \begin{bmatrix} 0 & 1 \\ \frac{mgl}{(I+ml^2)} & \frac{-\mu}{I+ml^2} \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} + \begin{bmatrix} \frac{ml}{(I+ml^2)} \\ \frac{-\mu ml}{(I+ml^2)} \end{bmatrix} V_c$$



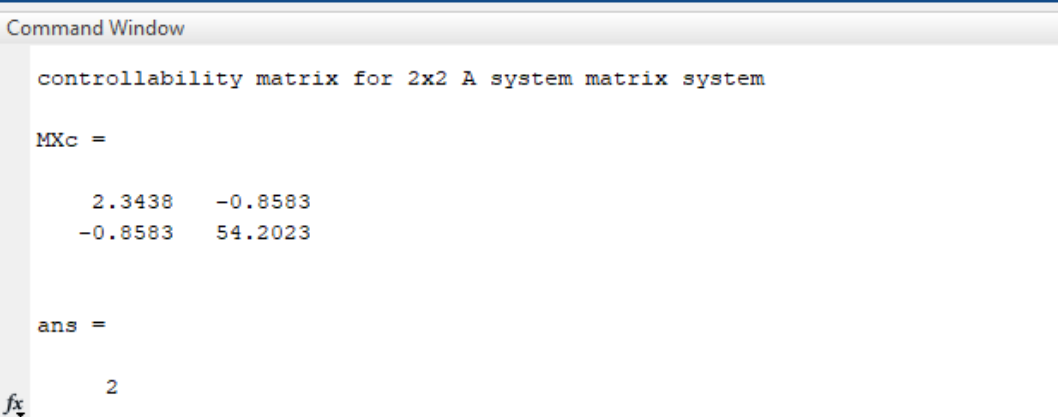
### 3. Observability, controllability and stability

Once again we did completed this task both by hand and by using MatLab

#### Controllability

From here we can see that controllability matrix is rank 2 which is full rank which means that it is indeed controllable.

```
35
36 %Controllability
37 - disp('controllability matrix for 2x2 A system matrix system');
38 - AB = A * B;
39 - MXc=[B AB ]
40 - rank(MXc)
41
```



```
Command Window

controllability matrix for 2x2 A system matrix system

MXc =

    2.3438   -0.8583
   -0.8583   54.2023

ans =

     2
```

Below is us calculating this by hand and coming to the same conclusion.

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Task 3 - Controllability ①

$$A = \begin{bmatrix} 0 & 1 \\ 23.544 & -0.027 \end{bmatrix}$$
$$B = \begin{bmatrix} 2.4 \\ -0.0648 \end{bmatrix}$$

Controllability

$$M_c = \begin{bmatrix} B & AB \end{bmatrix} = \begin{bmatrix} 2.4 \\ -0.0648 \end{bmatrix} \times \begin{bmatrix} 0 & 1 \\ 23.544 & -0.027 \end{bmatrix} \begin{bmatrix} 2.4 \\ -0.027 \end{bmatrix}$$
$$AB = \begin{bmatrix} (2.4 \times 0) + (1 \times -0.0648) \\ (23.544 \times 2.4) + (-0.027 \times -0.0648) \end{bmatrix}$$
$$AB = \begin{bmatrix} -0.0648 \\ 56.5073 \end{bmatrix}$$

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~~B~~

$$M_c = \begin{bmatrix} B & AB \end{bmatrix}$$

$$M_c = \begin{bmatrix} 2.4 & -0.0648 \\ -0.0648 & 56.5073 \end{bmatrix}$$

This shows that it is rank 2 which is full rank. Therefore it is controllable

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## Observability

Once again we can see that the observability matrix is rank two which is full rank, which indicates that it is observable. This is also see in our hand notes.

```
28
29     %Observability, controllability and stability |
30
31 -   disp('observability matrix for 2x2 A system matrix system');
32 -   CA = C*A;
33 -   MXo=[C; CA;]
34 -   rank(MXo)
35
```

### Command Window

```
>> State_space
observability matrix for 2x2 A system matrix system

MXo =

     1     0
     0     1

ans =

     2
```

*fx* 2

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Task 3 Observability

$$A = \begin{bmatrix} 0 & 1 \\ 23.544 & -0.027 \end{bmatrix}$$

$$C = \begin{bmatrix} 1 \\ 0 \end{bmatrix}$$

$$M_o = \begin{bmatrix} C & CA \end{bmatrix}$$

$$CA = \begin{bmatrix} (0 \times 1) + (1 \times 0) \\ (23.544 \times 1) + (0 \times -0.027) \end{bmatrix} = \begin{bmatrix} 0 \\ 23.544 \end{bmatrix}$$

$$M_o = \begin{bmatrix} 1 & 0 \\ 0 & 23.544 \end{bmatrix}$$

Due to this being rank 2 this means that this is observable as its full rank

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Inverted A

$$A = \begin{bmatrix} 0 & 1 \\ -23.544 & -0.027 \end{bmatrix} \quad I = \begin{bmatrix} 1 & 0 \\ 0 & 1 \end{bmatrix}$$
$$|A - \lambda I| = \begin{vmatrix} \begin{bmatrix} 0 & 1 \\ -23.544 & -0.027 \end{bmatrix} - \lambda \begin{bmatrix} 1 & 0 \\ 0 & 1 \end{bmatrix} \end{vmatrix}$$
$$= \begin{vmatrix} -\lambda & 1 \\ -23.544 & -0.027 - \lambda \end{vmatrix}$$

so  $(-\lambda) \times (-0.027 - \lambda) - (-23.544) = 0$

$$= (-\lambda^2 - 0.027\lambda) + 23.544 = 0$$
$$\Rightarrow \lambda^2 + 0.027\lambda - 23.544 = 0$$

$\Rightarrow$  quadratic formula  $\Rightarrow$  shows  $\lambda = 4.8387$   
 $\lambda = -4.8657$

one positive & one negative eigenvalue  
therefor not stable



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## Stability

From looking at  $A_{\text{inverted}}$  Eigen values we can see that it is not stable due to positive values.

```
41
42 %Inverted config
43 - A_inverted = [0 1; -a2 -a1; ];
44
45 % eigen values of non-inverted config
46 - eig(A_inverted)
47
```

Command Window

```
ans =

    4.6154
   -4.9816
```

From looking at  $A_{\text{nonInverted}}$  Eigen values we can see that they aren't far off from the Imaginary axis and thus would be stable.

```
47
48 %Get non-inverted config
49 - A_nonInverted = [0 1; a2 -a1; ];
50
51 %Eigen values of non-inverted config
52 - eig(A_nonInverted)
53
```

```
ans =

   -0.1831 + 4.7915i
   -0.1831 - 4.7915i
```

$f_x$  >>

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Task 3 - Stability

$$A = \begin{bmatrix} 0 & 1 \\ 23.544 & -0.027 \end{bmatrix}$$

$$I A - A$$

$$I = \begin{bmatrix} 1 & 0 \\ 0 & 1 \end{bmatrix} \quad \det A = \begin{bmatrix} -23.544 \end{bmatrix}$$

$$\Rightarrow \begin{bmatrix} 0 & 1 \\ 23.544 & -0.027 \end{bmatrix} - \lambda \begin{bmatrix} 1 & 0 \\ 0 & 1 \end{bmatrix} = 0$$

$$= \begin{bmatrix} -\lambda & 1 \\ 23.544 & -0.027 - \lambda \end{bmatrix} = 0$$

$$= (-\lambda) \times (-0.027 - \lambda) - 23.544 = 0$$

$$\Rightarrow 0.027\lambda - \lambda^2 - 23.544 = 0$$

$$-\lambda^2 - 23.571 = 0$$

$$\lambda^2 = -23.571$$

$\lambda = \text{imaginary}$

so the system would be stable & oscillate

$$= -\lambda^2 - 0.027\lambda - 23.544 = 0$$

quadratic formula  $\Rightarrow$  shows 2 negative imaginary numbers

$\therefore$  stable and is damped

$$\lambda = -0.0135 + 4.85219i$$

$$\lambda = -0.01354 - 4.85219i$$

## 4. Simulate your state space module using the Matlab ode45 function

Youtube videos Animation 1: <https://www.youtube.com/watch?v=5aATlaNZaQI>

Animation 2: <https://www.youtube.com/watch?v=tIKLcAGnLvE>

$$\dot{X} = AX + BU$$

$$Y = CX + DU$$

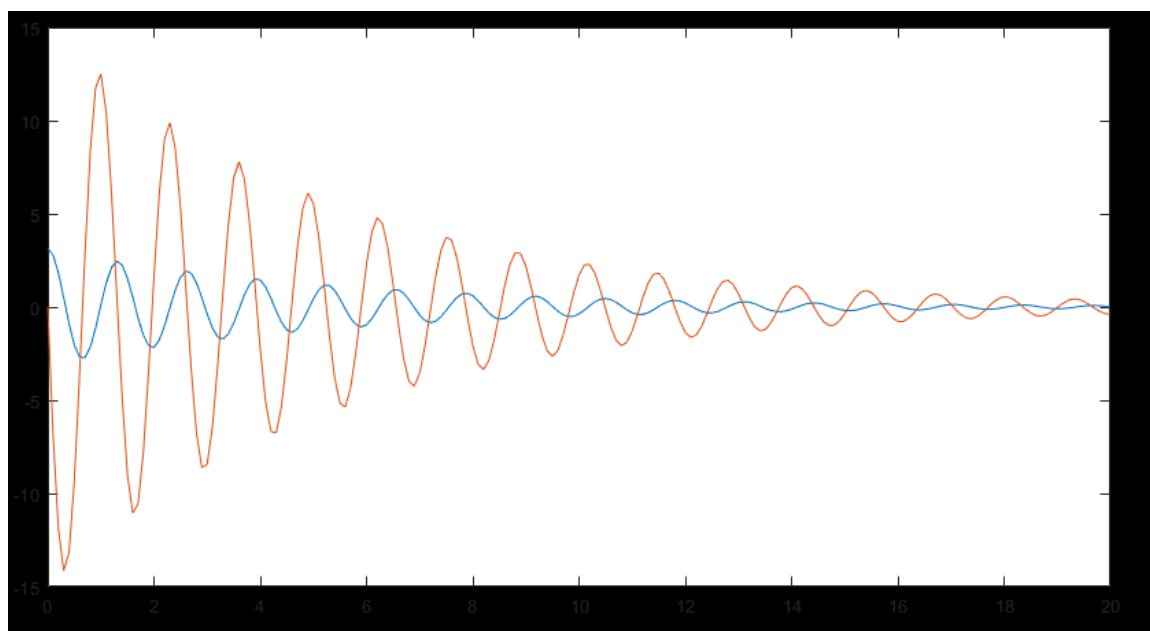
For this task I created a function to be used with the ode 45 function as shown below.

```
Simulate.m  X Main_simFCOde45.m  X FCPendOnCart.m  X AnimatePendulumCart.m  X +
1  function xDot = Simulate(A, x, B, u)
2
3      xDot = A*x + B*u;
4
5  end
6
```

This is the function that I used in my animation

```
50  % representing a force controlled pendulum on a cart
51  % model introduces slight amount of noise to wont stay balanced
52  [t,y] = ode45(@(t,y) Simulate(A, y, B, 0), tspan, y0);
53
```

Below is the graph from the 2<sup>nd</sup> animation, I decided to run another animation due to the first one didn't run long enough



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## 5. Design a state feedback controller

YouTube video Ode with Feedback:

<https://www.youtube.com/watch?v= GHqLaz QUA>

$$\dot{X} = AX + BU$$

$$Y = CX + DU$$

To use feedback in my system I have used state feedback where  $U = -KX$

Where the matrix  $K$  is the feedback gain of the system. So the system can now be written as  $\dot{X} = (A - BK)X$

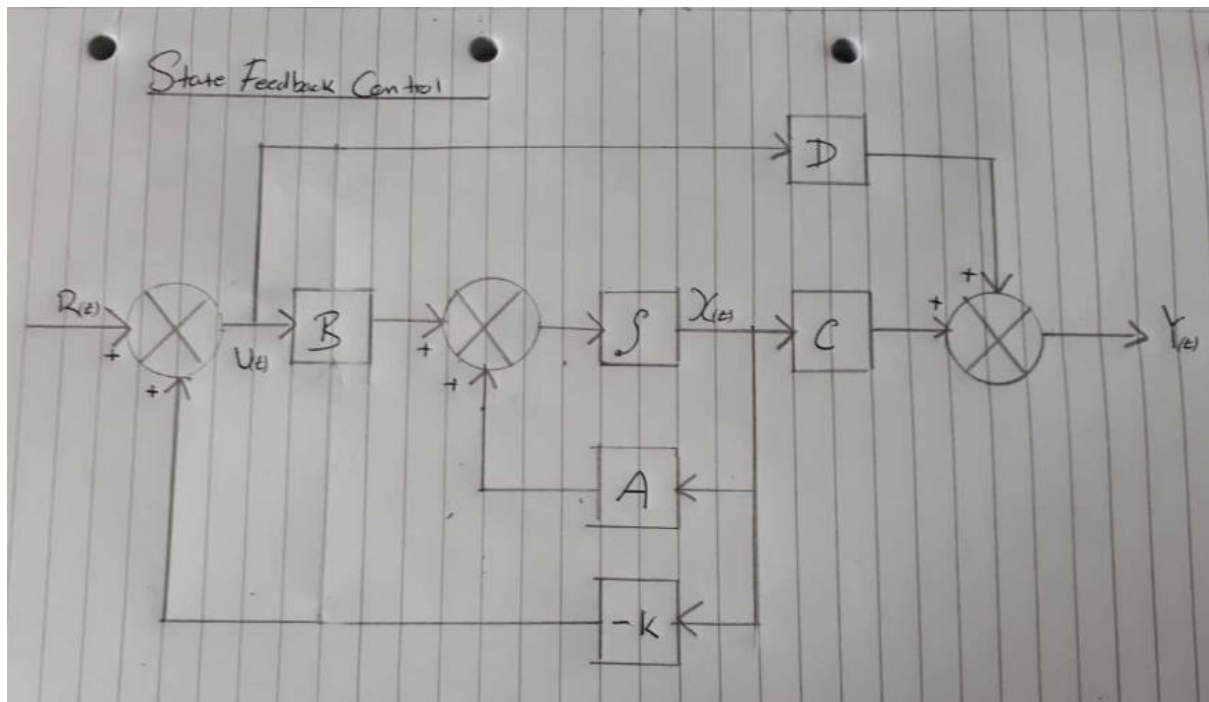
We can now implement this to find the eigen values  $|\lambda I - (A - BK)| = 0$

This shows us that we can influence the location of the eigen values by changing  $K$

Command Window

Feedback =

6.6896    -0.8797



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For this task I wrote a separate function from task 4

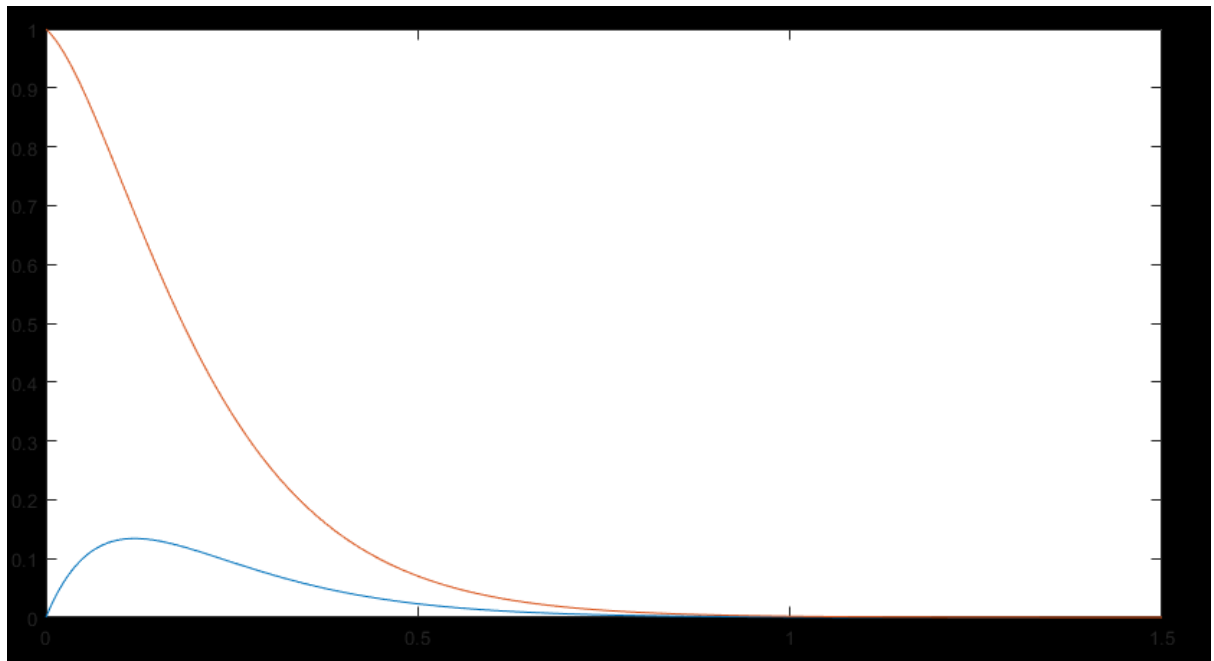
```
Feedback_function.m  Main_simFCOde45.m  AnimatePendulumCart.m  +
1  function Feedback = Feedback_function(A, x, B, u)
2
3
4  -   Feedback = A*x + B*u;
5  -   end
```

I then wrote a feedback controller and added it to the Main\_simFCOde45.m along with my statespace model

```
7  -   u = 0.05; %Coefficient of viciously
8  -   m = 0.314;% pendulum point mass
9  -   M = 2;% cart mass
10 -   L = 1; % pendulum length
11 -   l=0.64;
12 -   g = -9.81;% acceleration due to gravity
13 -   d = 1;% damping
14 -   I = ((1/12)*m*(l^2)); %Moment of Inertial of the pendulum rod at centre of mass
15
16   %Coefficients
17 -   a0 = 1;
18 -   a1 = (m*u)/(I+m*(l/2)^2);
19 -   a2 = (-m*g*(l/2))/(I+m*(l/2)^2);
20 -   b0 = (m*(l/2))/(I+m*(l/2)^2);
21 -   b1 = 0;
22
23   %State spaces
24 -   A = [0 1; -a2 -a1; ];
25 -   B = [b0; (b1-a1*b0);];
26 -   C = [1 0;];
27 -   D = 0;
28
29   % Inverted config
30 -   A_inverted = [0 1; -a2 -a1; ];
31
32   %Feedback
33 -   PX = 8 *[-1 -1.1];
34 -   Feedback = place(A,B,PX);
35
```

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Task 5 - State feedback control

$$|\lambda I - (A - BK)| = 0$$

$$A = \begin{bmatrix} 0 & 1 \\ 25.544 & -0.027 \end{bmatrix}$$

$$B = \begin{bmatrix} 2.4 \\ -0.0648 \\ -0.648 \end{bmatrix}$$

$$\lambda = \begin{bmatrix} 0.0135 + 4.8522i \\ -0.0135 - 4.8522i \end{bmatrix}$$

$$\dot{x} = (A - BK)x \quad \text{and} \quad Y = (C - DK)x$$

$$\lambda I_2 \begin{bmatrix} 0.0135 + 4.8522i & 1 \\ -0.0135 - 4.8522i & 0 \end{bmatrix} \begin{bmatrix} 1 \\ 0 \end{bmatrix} = \begin{bmatrix} 0.0135 + 4.8522i \\ 0 \end{bmatrix}$$

$$0.0135 + 4.8522i - (A - BK) = 0$$

$$0.0135 + 4.8522i = A - BK$$

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$$Bk = \begin{bmatrix} 2.4k \\ -0.0648k \end{bmatrix}$$

$$\det |\lambda I - (A - Bk)| = 0$$

$$\begin{bmatrix} 0.0135 + 4.8522i \\ 0 \end{bmatrix} - \begin{bmatrix} 0 & 1 \\ 23.544 & -0.027 \end{bmatrix} - \begin{bmatrix} 2.4k \\ -0.0648k \end{bmatrix} = 0$$

$$\begin{bmatrix} 0.0135 + 4.8522i \\ 0 \end{bmatrix} = \begin{bmatrix} -2.4k & -1.4k \\ 23.544 + 0.0648k & -0.027 + 0.0648k \end{bmatrix} = 0$$

$$\Rightarrow \begin{bmatrix} 0.0135 + 4.8522i + 2.4k & 0.0135 + 4.8522i + 1.4k \\ -23.544 + 0.0648k & +0.027 - 0.0648k \end{bmatrix} = 0$$

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$$B_k = \begin{bmatrix} 2.4k \\ -0.0648k \end{bmatrix}$$

$$\det |\lambda I - (A - B_k)| = 0$$

$$\begin{bmatrix} 0.0135 + 4.8522i \\ 0 \end{bmatrix} - \begin{bmatrix} 0 & 1 \\ 23.544 & -0.027 \end{bmatrix} - \begin{bmatrix} 2.4k \\ -0.0648k \end{bmatrix} = 0$$

$$\begin{bmatrix} 0.0135 + 4.8522i \\ 0 \end{bmatrix} = \begin{bmatrix} -2.4k & -1.4k \\ 23.544 + 0.0648k & -0.027 + 0.0648k \end{bmatrix} = 0$$

$$\Rightarrow \begin{bmatrix} 0.0135 + 4.8522i + 2.4k & 0.0135 + 4.8522i + 1.4k \\ -23.544 + 0.0648k & +0.027 - 0.0648k \end{bmatrix} = 0$$

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## 6. Implement the controller/observer system using Euler integration

For this task I created a new function to be used instead of the Ode45 called "SimulateSFC"

```
1  function [y, t, xout] = SimulateSFC(A, B, C, D, K, t, x0)
2
3
4  %get signal length
5  len = length(t);
6
7  %init output
8  y = zeros(1,len);
9  xout = zeros(2,len);
10
11 %record the initial state
12 xout(:, 1) = x0;
13 x = x0;
14
15 %calculate the command
16 u(1) = C(1) * x(1) + C(2) * x(2);
17
18 %calculate output from theta and thetaDot states
19 y(1) = C(1) * x(1) + C(2) * x(2) + D(1) * u(1);
20
21 %for all remaining data points, simulate state space model using C
22
23 for idx = 2:len
24
25     %state feedback rule
26     u(idx) = -K(1) * x(1) - K(2) * x(2);
27
28     %get the duration between updates
29     h = t(idx) - t(idx-1);
30
31     %calculate state derivative
32     xdot(1) = A(1,1) * x(1) + A(1,2) * x(2) + B(1) * u(idx);
33     xdot(2) = A(2,1) * x(1) + A(2,2) * x(2) + B(2) * u(idx);
34
35     %update the state
36     x(1) = x(1) + h * xdot(1);
37     x(2) = x(2) + h * xdot(2);
38
39     %record the state
40     xout(:, idx) = x;
41
42     %calculate output from theta and thetaDot staets only
43     y(idx) = C(1) * x(1) + C(2) * x(2) + D(1) * u(idx);
44 end
```

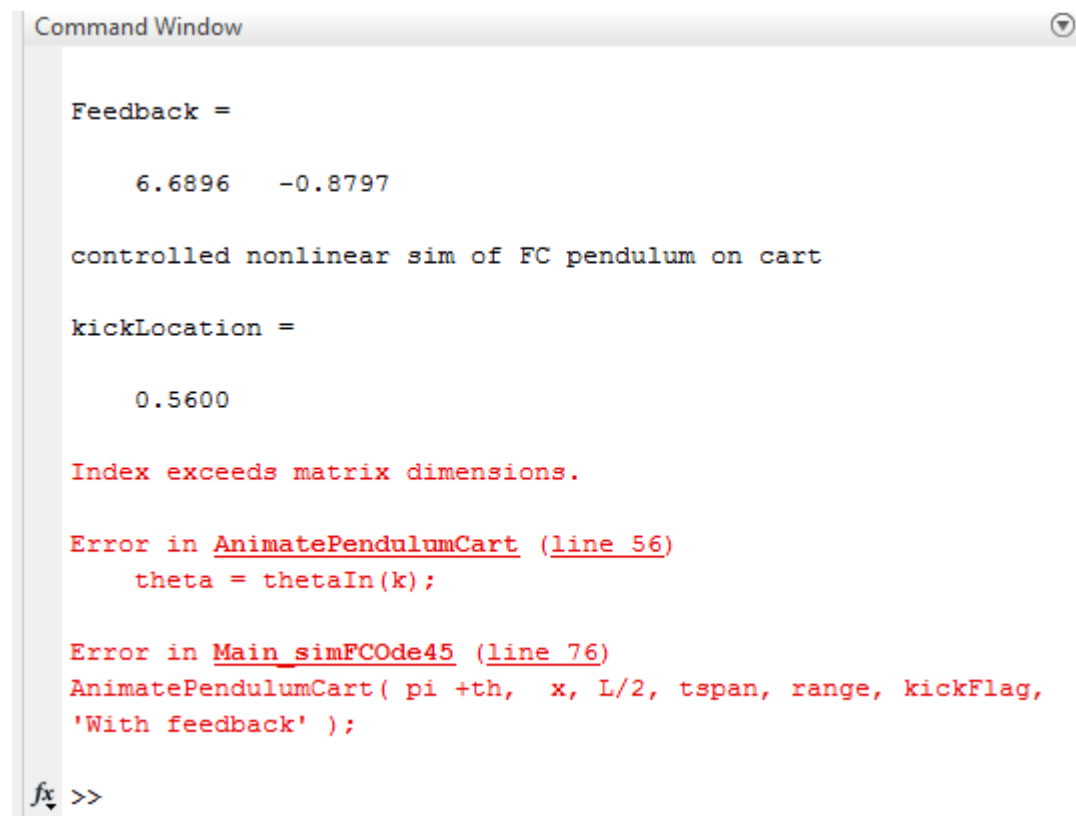
---

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I then implemented the function onto my code, which replaced the Ode45 function.

```
58
59 % use ode to solve with FCPendOnCart with no control force input u
60 % representing a force controlled pendulum on a cart
61 % model introduces slight amount of noise to wont stay balanced
62 - [y,t, xout] = SimulateSFC(A, B, C, D, Feedback, tspan, y0);
63
```

Unfortunately when I ran the code it came up with an error, which I was unable to solve.



The screenshot shows the MATLAB Command Window with the following content:

```
Command Window
```

```
Feedback =  
  
    6.6896    -0.8797  
  
controlled nonlinear sim of FC pendulum on cart  
  
kickLocation =  
  
    0.5600  
  
Index exceeds matrix dimensions.  
  
Error in AnimatePendulumCart (line 56)  
    theta = thetaIn(k);  
  
Error in Main_simFCODE45 (line 76)  
AnimatePendulumCart( pi +th,  x, L/2, tspan, range, kickFlag,  
    'With feedback' );  
  
fx >>
```

---

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6. Implement the Controller System using Euler Integration.

$$\dot{x} = Ax + Bu$$

$$y = Cx + Du$$

$$\Rightarrow U = -Kx$$

Recurrence relationship

$$\dot{x} = Ax + B(-Kx)$$

$$y = Cx + D(-Kx)$$



## 7. Add a Luenberger observer to your state feedback controller

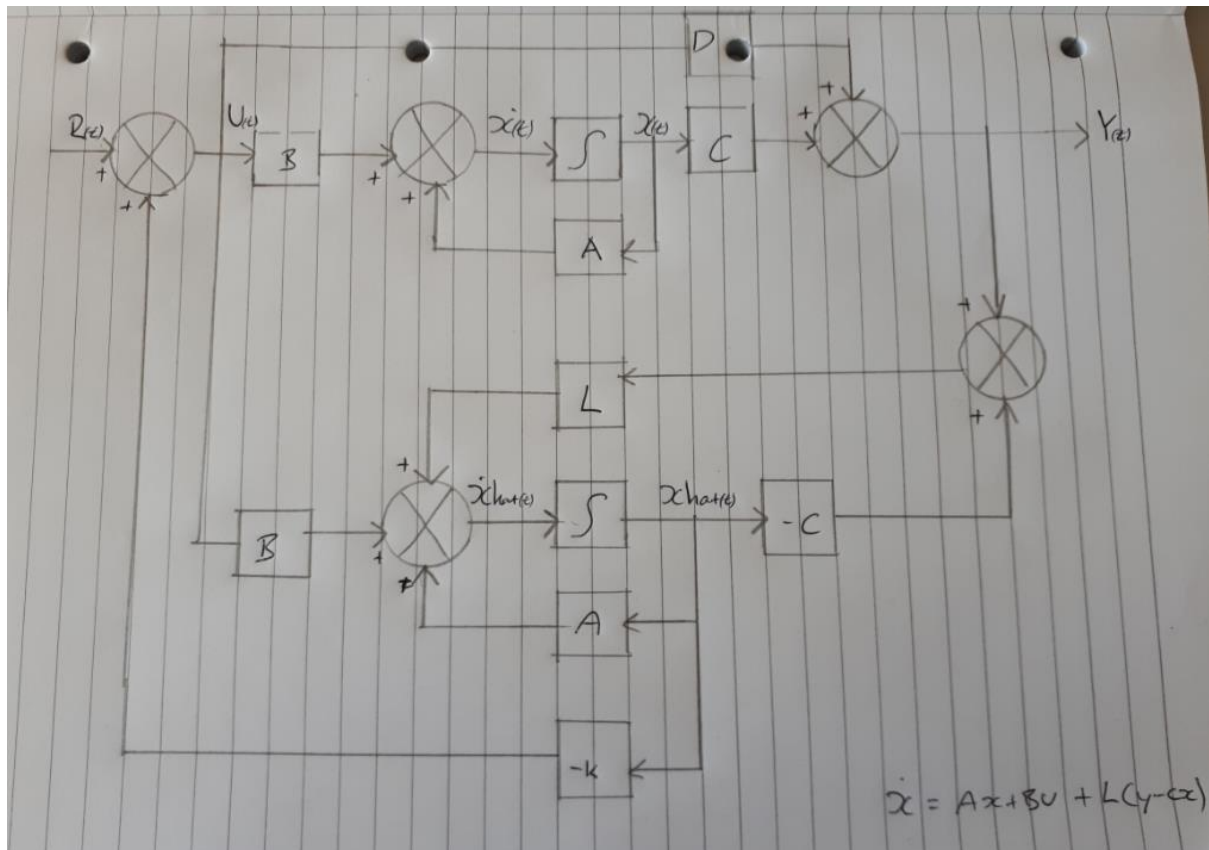
### Luenberger gain

$$\dot{X} = AX + BU + L(y - CX)$$

### Set up params with Observer gain

```
1
2   % clean up matlab before launching script
3 - clear all
4 - close all
5 - clc
6
7 - u = 0.05; %Coefficient of viciously
8 - m = 0.314;% pendulum point mass
9 - M = 2;% cart mass
10 - L = 1; % pendulum length
11 - l = 0.64;
12 - g = -9.81;% acceleration due to gravity
13 - d = 1;% damping
14 - I = ((1/12)*m*(l^2)); %Moment of Inertial of the pendulum rod at centre of mass
15
16 %Coefficients
17 - a0 = 1;
18 - a1 = (m*u)/(I+m*(l/2)^2);
19 - a2 = (-m*g*(l/2))/(I+m*(l/2)^2);
20 - b0 = (m*(l/2))/(I+m*(l/2)^2);
21 - b1 = 0;
22
23 %State spaces
24 - A = [0 1; -a2 -a1; ];
25 - B = [b0; (b1-a1*b0);];
26 - C = [1 0;];
27 - D = 0;
28 |
29 % Inverted config
30 - A_inverted = [0 1; -a2 -a1; ];
31
32 %Feedback
33 - PX = 8 *[-1 -1.1];
34 - Feedback = place(A,B,PX);
35 - Feedback
36
37 %observer gain
38 - PX = 20 * [-1 -1.2]
39 - L = place(A, C, PX);
40 - LT=L;
```

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## 8. Augment positional state into your state space model

8. Augment Positional state into your State Space Model

$x_3 = \text{Input Velocity Signal}$

$\dot{x}_3 = \frac{d\theta}{dt}$

$a_1 = \mu$        $a_2 = \frac{-mgL}{(I+ml^2)}$        $b_0 = \frac{ml}{(I+ml^2)}$

Velocity Controlled State Space predictions

$$\frac{d}{dt} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} = \begin{bmatrix} 0 & 1 \\ -a_2 & -a_1 \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} + \begin{bmatrix} b_0 \\ -a_1 b_0 \end{bmatrix} v_c$$

$y = \begin{bmatrix} 1 & 0 \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix}$       //  $y = \text{pendulum angle } (\theta)$

With the derivative of  $x_3$  being zero  $x_3$  is just the Velocity as input

$$\frac{d}{dt} \begin{bmatrix} x_1 \\ x_2 \\ x_3 \end{bmatrix} = \begin{bmatrix} 0 & 1 & 0 \\ -a_2 & -a_1 & 0 \\ 0 & 0 & 0 \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \\ x_3 \end{bmatrix} + \begin{bmatrix} b_0 \\ -a_1 b_0 \\ 1 \end{bmatrix} v_c$$

With  $y$  being

$$y = \begin{bmatrix} 1 & 0 & 0 \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \\ x_3 \end{bmatrix}$$

**9. Implement the augmented state feedback controller**

**10. Implement the augmented state feedback controller on the Arduino Mega**