

Momentum-Aware Planning Synthesis for Dynamic Legged Locomotion

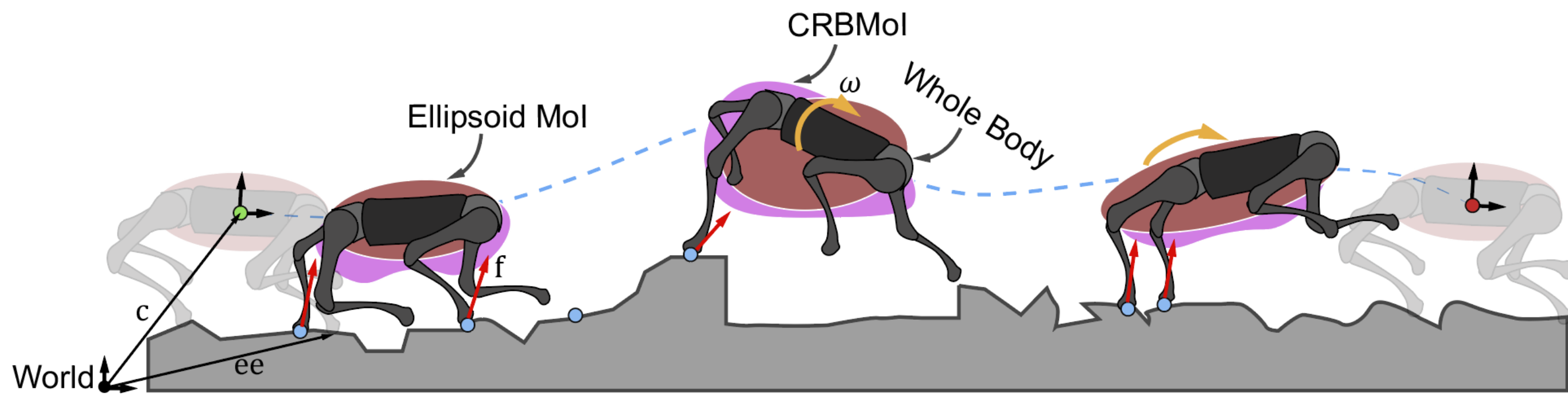
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Introduction and Objective

- Hierarchical gait-->centroidal-->whole-body pipelines reduce planning complexity, additional constraints on momentum and full-body kinematics enable more dynamically feasible solutions.
- **Design a centroidal optimization capable of discovering both contact sequences and angular momentum trajectories.**
- **Achieve a dynamic consensus between centroidal and whole-body models** using constrained ADMM.

Centroidal and Whole-Body Optimization

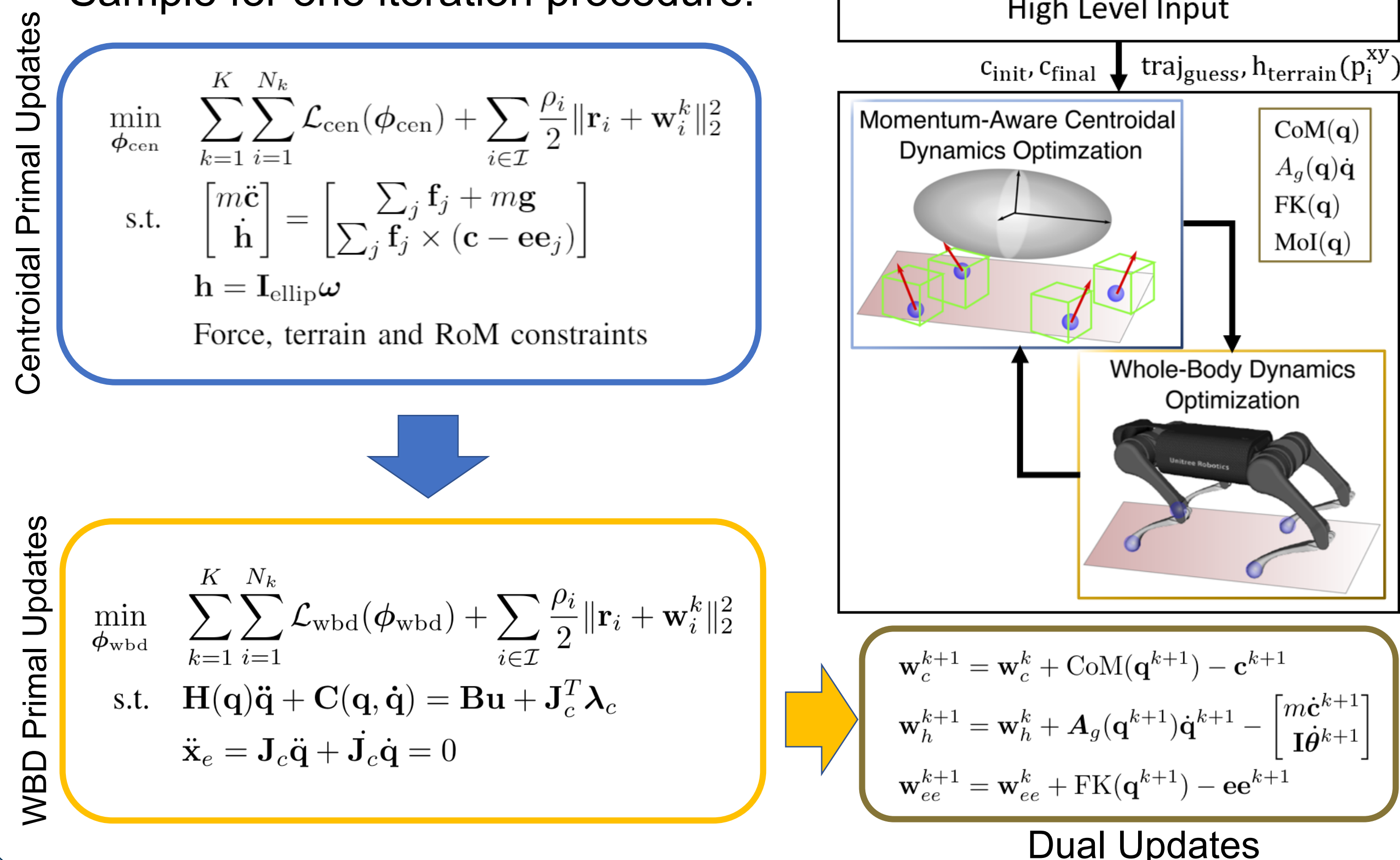
- Centroidal optimization utilizes a single rigid body model with equimomental-ellipsoid-based Moment of Inertia (MoI) [2, 3].
- Simultaneously solve for footholds, contact forces, centroidal and momentum trajectories.
- **Ellipsoid MoI tracks joint motion effects on Composite Rigid Body MoI** from whole-body model for accurate momentum generation.
- WBD tracks the consensus quantities from centroidal optimization, and then solved via Differential Dynamic Programming (DDP).



ADMM Constrained Trajectory Optimization

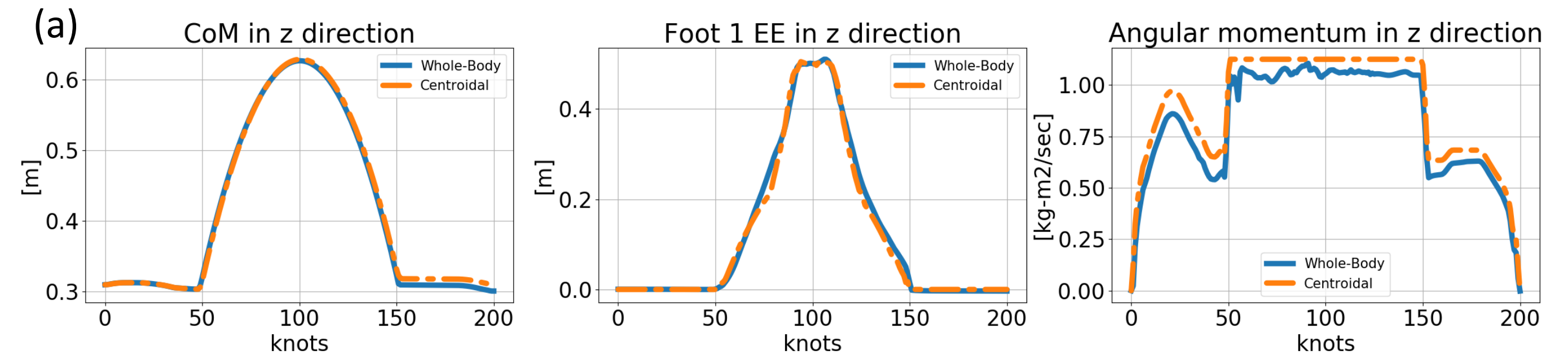
- The consensus [1] is enforced by adding equality **consistency constraints for Center of Mass (CoM) positions, momentum, footholds**. The MoI is directly computed from whole-body CRBMol.

Sample for one iteration procedure:

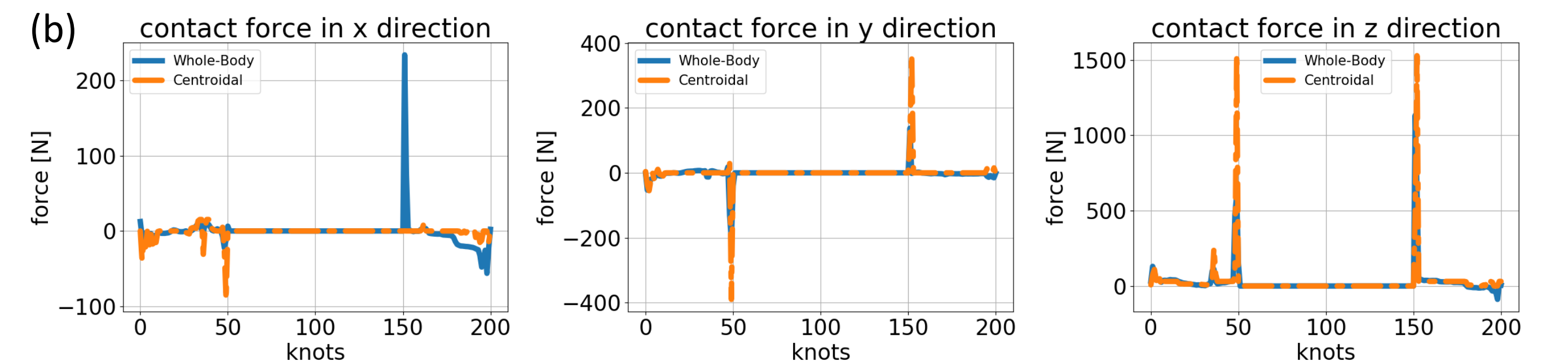


Results

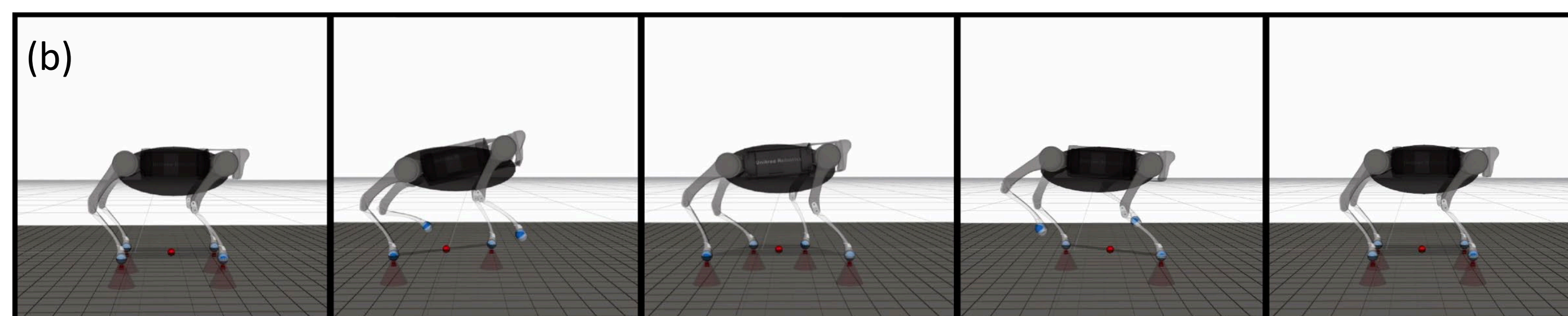
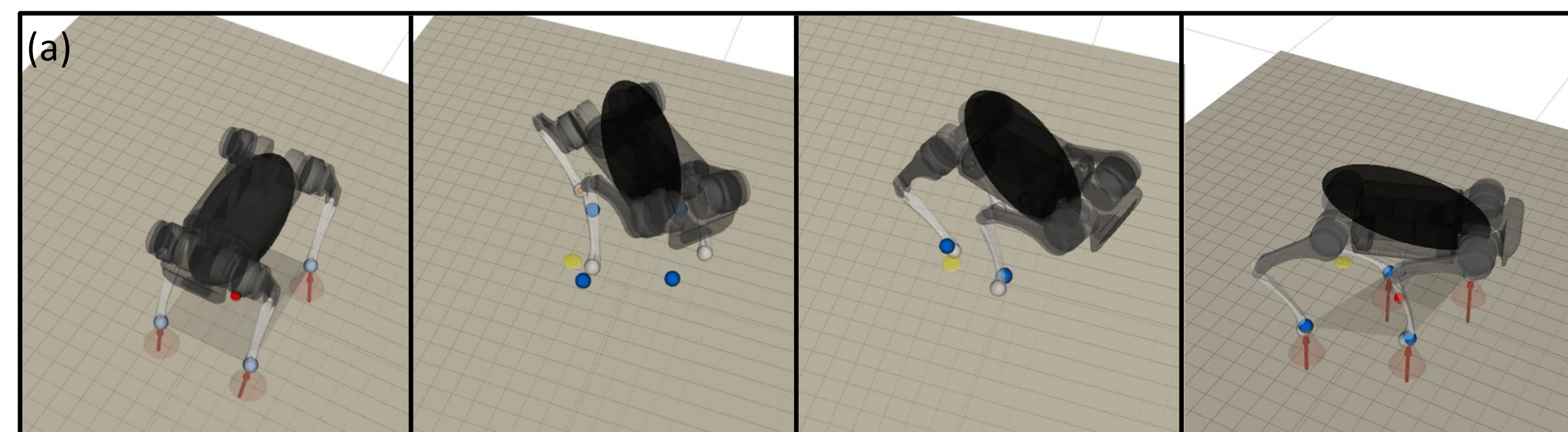
Quadruped Robot jump-twist and trotting examples.



Dynamic consensus of the desired variables for a jump-twist maneuver between centroidal and whole-body models.



Dynamic consensus for a trotting gait motion between centroidal and whole-body models.



Snapshots of an athletic jump-twist maneuver (a) and quadruped trotting gait (b) solved by SNOPT [4] and Crocoddyl [5] for centroidal and whole-body updates respectively.

Discussion and On-going Work

- Designed a centroidal optimization scheme for generating contact sequences and momentum.
- Dynamic **consensus between centroidal and full body** dynamic models.
- On-going work includes improving the angular momentum and inertia tracking. We are also exploring **real-time constrained MPC implementations**. This would require more improvements on the algorithm efficiency and scope for real applications.

References

[1] Z. Zhou and Y. Zhao (2020), [2] A. W. Winkler, C. D. Bellicoso, M. Hutter, and J. Buchli (2018), [3] V. Zordan, D. Brown, A. Macchietto, and K. Yin (2014), [4] P. Gill, W. Murray, and M. Saunders (2005), [5] C. Mastalli, R. Budhiraja, W. Merkt, G. Saurel, B. Hammoud, M. Naveau, J. Carpentier, L. Righetti, S. Vijayakumar and N. Mansard (2020)

Introduction and Objective

- Hierarchical gait-->centroidal-->whole-body pipelines reduce complexity, but additional constraints are required to ensure feasible solutions.
- Create a centroidal optimization capable of discovering both contact sequences and angular momentum trajectories.**
- Achieve a dynamic consensus between centroidal and whole-body models**

Centroidal and Whole-Body Optimization

- Centroidal optimization utilizes phase-based gait [2] and equimomental-ellipsoid-based Moment of Inertia (Mol) [3].

$$\begin{aligned} \min_{\phi_{cen}, \phi_{wbd}} & \sum_{k=1}^K \int_{t_k}^{t_k+\Delta t_k} \mathcal{L}_{wbd}(\phi_{wbd}) dt + \int_{t_k}^{t_k+\Delta t_k} \mathcal{L}_{cen}(\phi_{cen}) dt \\ \text{subject to} & \mathbf{H}(\mathbf{q})\ddot{\mathbf{q}} + \mathbf{C}(\mathbf{q}, \dot{\mathbf{q}}) = \mathbf{B}\mathbf{u} + \mathbf{J}_c^T \lambda_c \quad (2a) \\ & m\ddot{\mathbf{r}} = \sum_j \mathbf{f}_j - m\mathbf{g} \quad (2b) \\ & \dot{\mathbf{L}} = \sum_j (\mathbf{p}_j - \mathbf{r}_j) \times \mathbf{f}_j \quad (2c) \\ & \dot{\phi} = W(\mathbf{I}^{-1}\mathbf{L}) \quad (2d) \\ & \dot{\mathbf{e}} = C_e(t, u_e) \quad (2e) \\ & \dot{\mathbf{v}} = C_v(t, u_v) \quad (2f) \\ & [\mathbf{r}, \theta](t=0) = [\mathbf{r}_0, \theta_0] \quad (2g) \\ & \mathbf{r}(t=T) = \mathbf{r}_g \quad (2h) \end{aligned}$$

for every foot i :

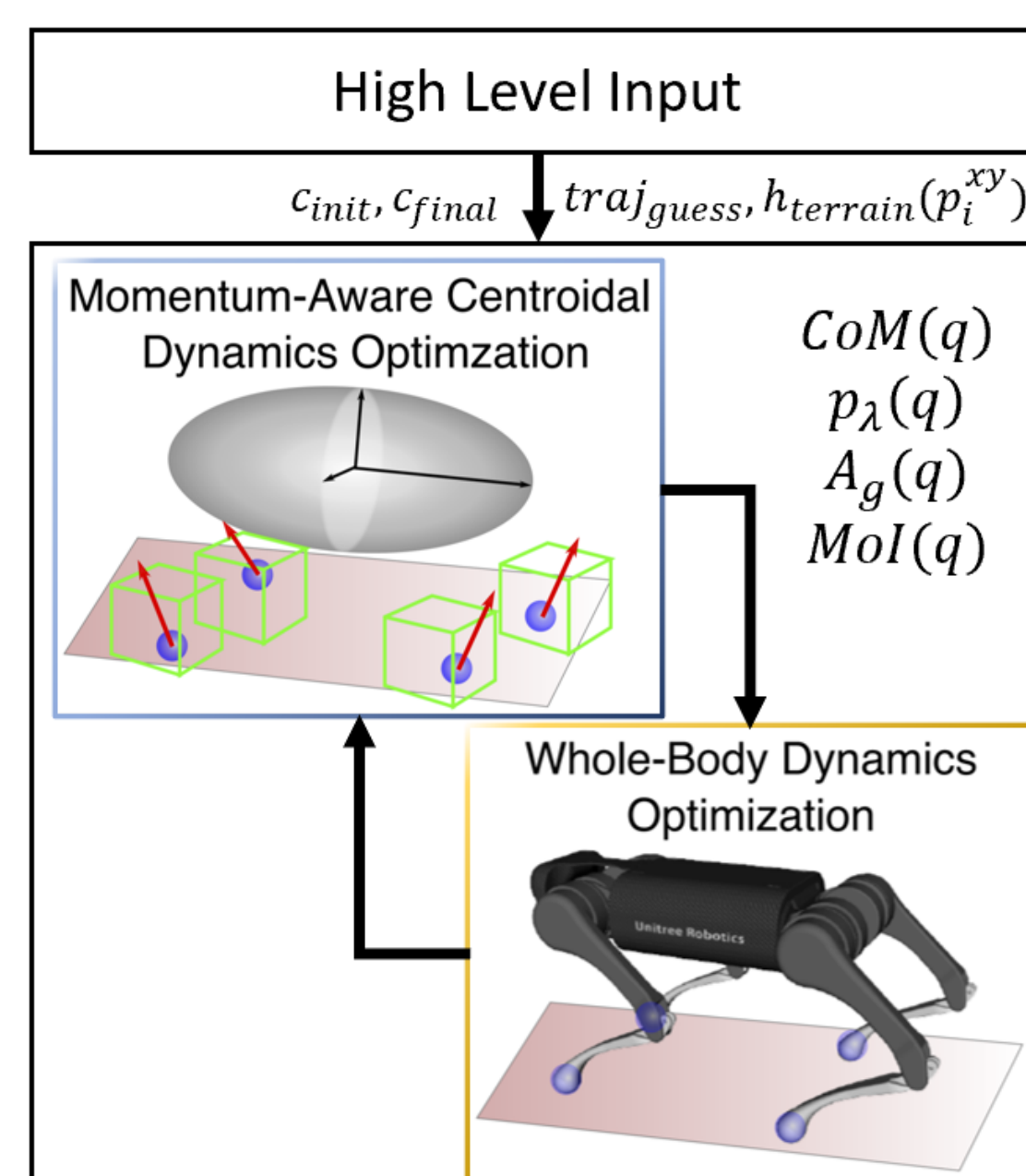
$$\begin{aligned} \mathbf{p}_i(t) & \in \mathcal{F}_i(\mathbf{r}, \theta) \quad (2i) \\ \text{if foot } i \text{ is in contact:} & \quad (2j) \\ \dot{\mathbf{p}}_i(t \in \mathcal{C}_i) & = 0 \quad (2k) \\ \mathbf{p}_i^z(t \in \mathcal{C}_i) & = h_{terrain}(\mathbf{p}_i^{xy}) \quad (2l) \\ \mathbf{f}_i(t \in \mathcal{C}_i) \cdot \mathbf{n}(\mathbf{p}_i^{xy}) & \geq 0 \quad (2m) \\ \mathbf{f}_i(t \in \mathcal{C}_i) & \in \mathcal{F}(\mu, \mathbf{n}, \mathbf{p}_i^{xy}) \quad (2n) \\ \text{if foot } i \text{ is in air:} & \quad (2o) \\ \mathbf{f}_i(t \notin \mathcal{C}_i) & = 0 \quad (2p) \\ \sum_{j=1}^{2n_{s,i}} \Delta T_{i,j} & = T \quad (2q) \\ \text{CoM}(\mathbf{q}) & = \mathbf{r} \quad (2r) \\ FK(\mathbf{q}) & = \mathbf{p} \quad (2s) \\ A_g(\mathbf{q})\dot{\mathbf{q}} & = \begin{bmatrix} m\dot{\mathbf{r}} \\ \mathbf{L}_g \end{bmatrix} \quad (2t) \\ \mathbf{I}_{cen}(\mathbf{q}) & = \mathbf{I} \quad (2u) \\ \mathbf{s} \in \mathcal{S}, \mathbf{u} \in \mathcal{U} & \quad (2v) \\ \lambda_j \in \mathcal{F}_j, \forall j \in \mathcal{I}_{\text{contact}} & \quad (2w) \end{aligned}$$

- Ellipsoid Mol tracks joint motion effects on Composite Rigid Body Mol from whole-body model for accurate momentum generation
- Track the consensus quantities from centroidal optimization, and then solved via Differential Dynamic Programming (DDP).

ADMM Constrained Trajectory Optimization

- Stage-wise Accelerated Alternating Direction Method of Multiplier (SWA-ADMM) framework [1] alternately updates optimization

$$\begin{aligned} \text{Primal updates:} \\ \phi_{cen}^{k+1} & := \arg \min_{\phi_{cen}} \sum_{i=1}^N \mathcal{L}_{cen}(\phi_{cen}) \quad (32a) \\ & + \frac{\rho_c}{2} \|\text{CoM}(\mathbf{q}^k) - \mathbf{c} + \mathbf{w}_i^k\|_2^2 \quad (32b) \\ & + \frac{\rho_h}{2} \|A_g(\mathbf{q}^k)\dot{\mathbf{q}}^k - \begin{bmatrix} m\dot{\mathbf{c}} \\ \mathbf{I}\dot{\theta} \end{bmatrix} + \mathbf{w}_i^k\|_2^2 \quad (32c) \\ & + \frac{\rho_\lambda}{2} \|g_\lambda(\mathbf{q}^k, \dot{\mathbf{q}}^k, \mathbf{u}^k) - \lambda + \mathbf{w}_i^k\|_2^2 \quad (32d) \\ & + \frac{\rho_{cc}}{2} \|FK(\mathbf{q}^k) - \mathbf{p} + \mathbf{w}_i^k\|_2^2 \quad (32e) \\ \phi_{wbd}^{k+1} & := \arg \min_{\phi_{wbd}} \sum_{i=1}^N \mathcal{L}_{wbd}(\phi_{wbd}) \quad (32f) \\ & + \frac{\rho_c}{2} \|\text{CoM}(\mathbf{q}) - \mathbf{c}^{k+1} + \mathbf{w}_i^k\|_2^2 \quad (32g) \\ & + \frac{\rho_h}{2} \|A_g(\mathbf{q})\dot{\mathbf{q}} - \begin{bmatrix} m\dot{\mathbf{c}}^{k+1} \\ \mathbf{I}\dot{\theta}^{k+1} \end{bmatrix} + \mathbf{w}_i^k\|_2^2 \quad (32h) \\ & + \frac{\rho_\lambda}{2} \|g_\lambda(\mathbf{q}, \dot{\mathbf{q}}, \mathbf{u}) - \lambda^{k+1} + \mathbf{w}_i^k\|_2^2 \quad (32i) \\ & + \frac{\rho_{cc}}{2} \|FK(\mathbf{q}) - \mathbf{p}^{k+1} + \mathbf{w}_i^k\|_2^2 \quad (32j) \\ \text{Dual updates:} \\ \mathbf{w}_c^{k+1} & = \mathbf{w}_c^k + \text{CoM}(\mathbf{q}^{k+1}) - \mathbf{c}^{k+1} \quad (32k) \\ \mathbf{w}_h^{k+1} & = \mathbf{w}_h^k + A_g(\mathbf{q}^{k+1})\dot{\mathbf{q}}^{k+1} - \begin{bmatrix} m\dot{\mathbf{c}}^{k+1} \\ \mathbf{I}\dot{\theta}^{k+1} \end{bmatrix} \quad (32l) \\ \mathbf{w}_\lambda^{k+1} & = \mathbf{w}_\lambda^k + g_\lambda(\mathbf{q}^{k+1}, \dot{\mathbf{q}}^{k+1}, \mathbf{u}^{k+1}) - \lambda^{k+1} \quad (32m) \end{aligned}$$



Results

- Quadruped Robot two block ADMM optimization problem

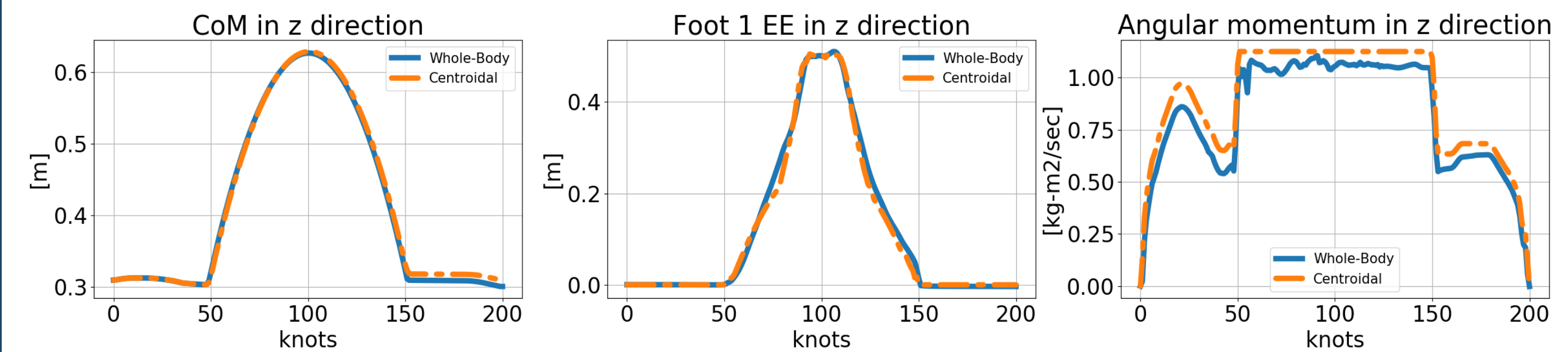
Dynamic Consensus

Center of Mass

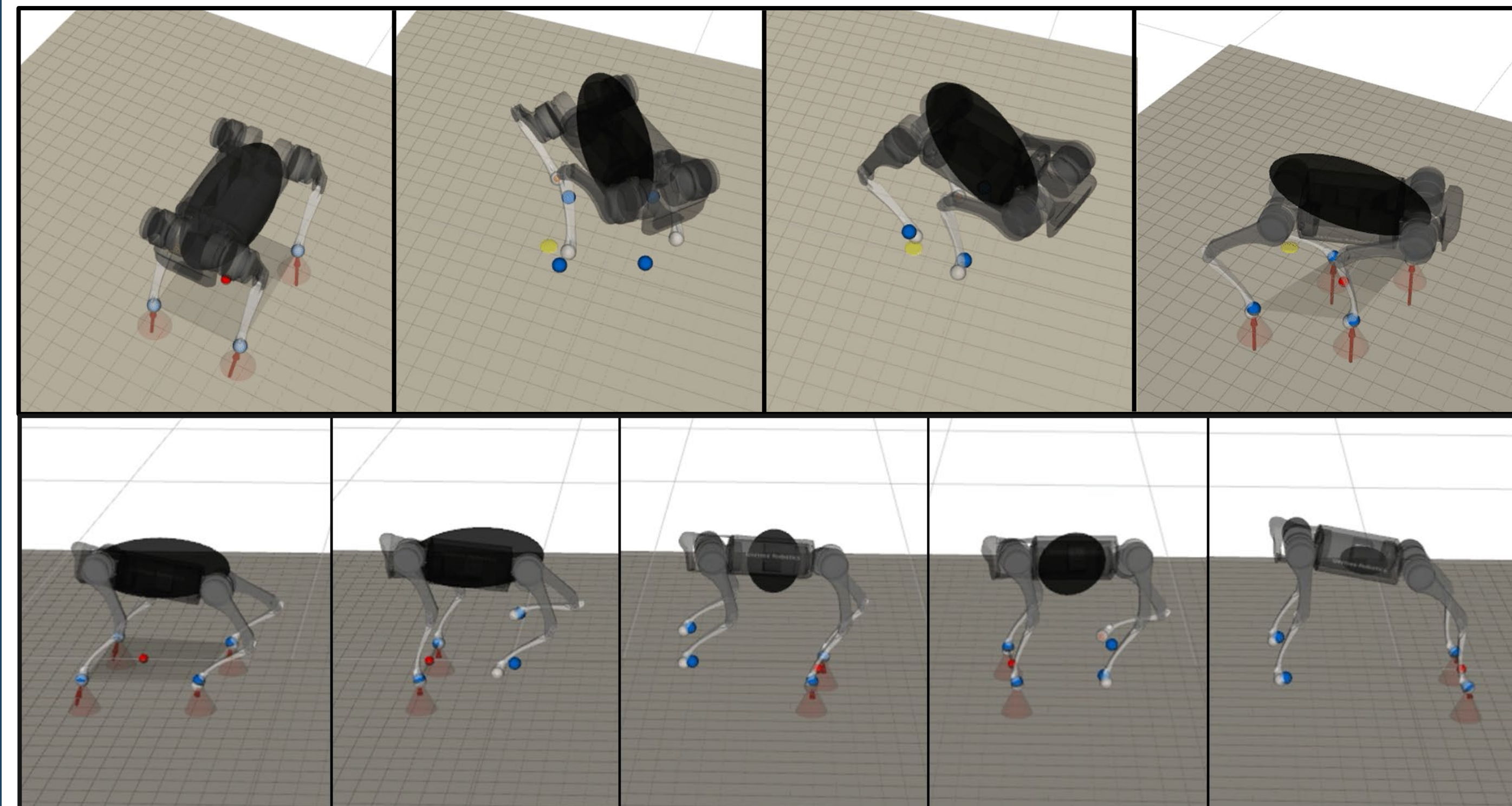
Momentum

Foothold Position

Moment of Inertia



Dynamic consensus of a jump-twist maneuver between centroidal and whole-body model.



Snapshots of an athletic jump-twist maneuver (a) and quadruped bound gait (b) computed by the proposed approach.

Discussion and Future Work

- Designed a centroidal optimization scheme for generating contact sequences and momentum
- Dynamic consensus between template and full body dynamic models

Future work includes improving the angular momentum and inertia tracking. We are also considering exploring real-time constrained MPC implementations. This would require more multiple improvements on the algorithm efficiency and scope for real applications.

References

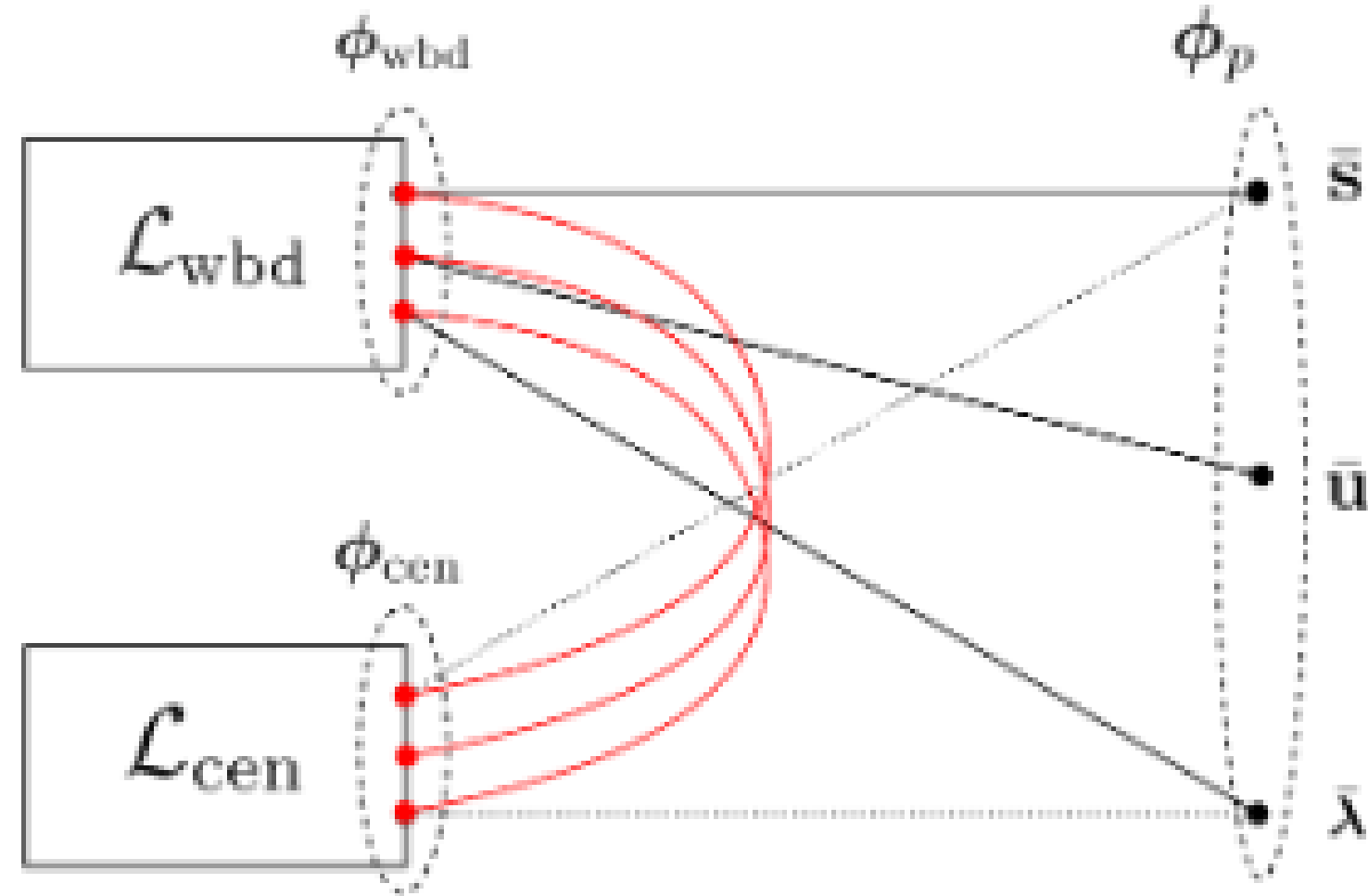
Momentum-Aware Planning Synthesis for Dynamic Legged Locomotion

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Introduction

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Algorithm 1

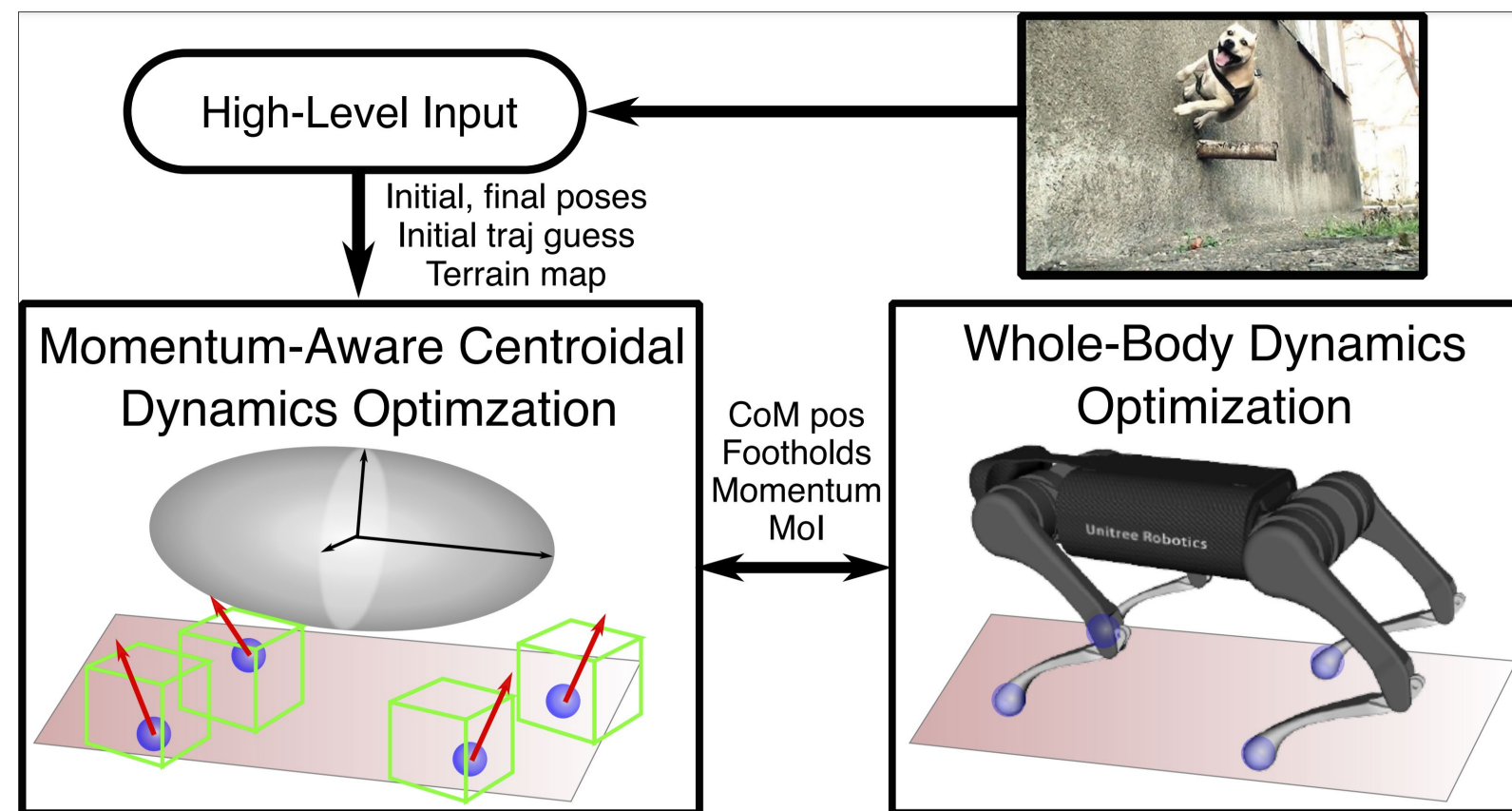
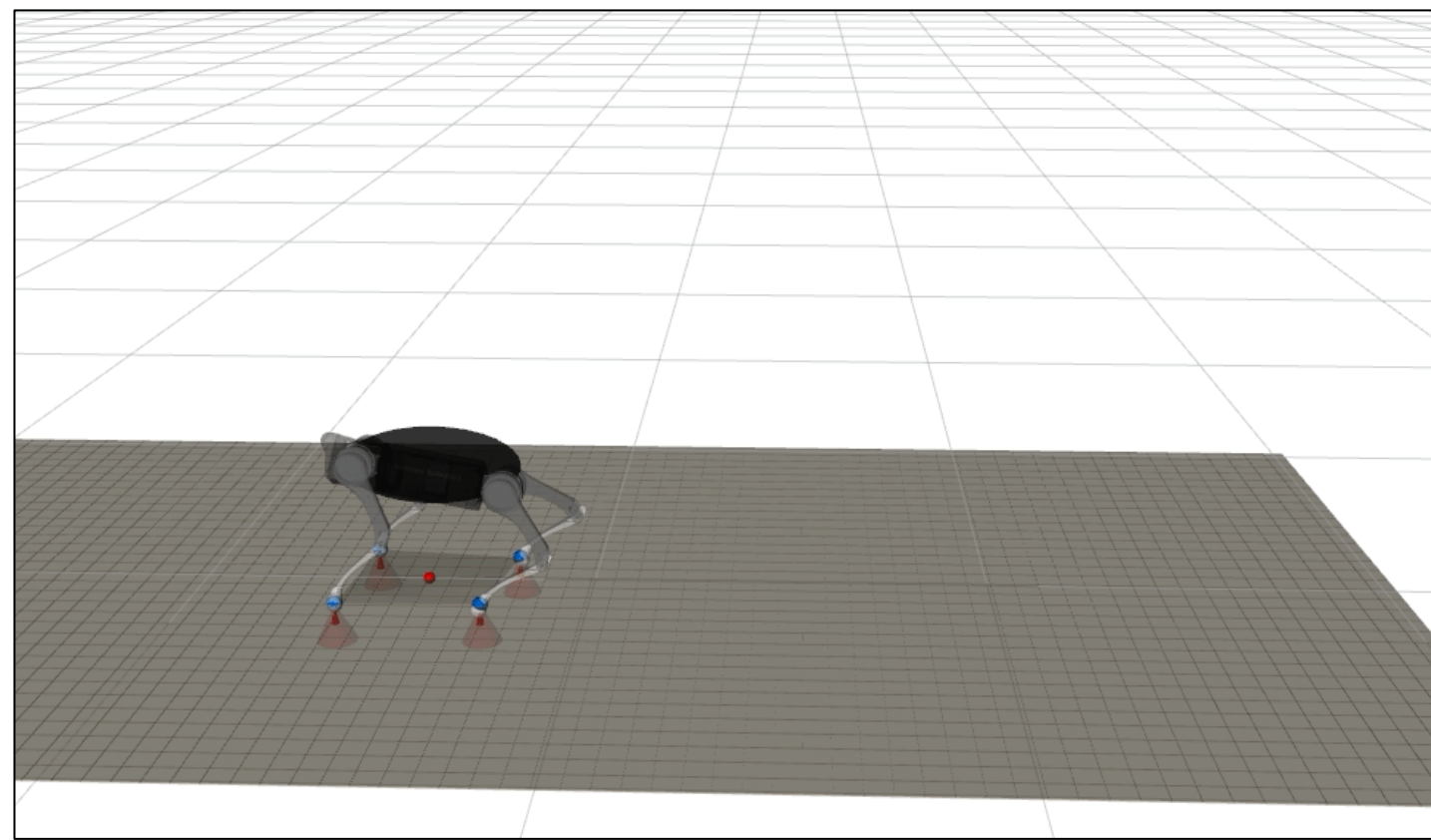
```

1:  $\phi_{cen} \leftarrow \phi_{cen}^0, \phi_{wbd} \leftarrow \phi_{wbd}^0, \phi_p \leftarrow \phi_p^0$ 
2:  $\mathbf{w}_i \leftarrow \mathbf{w}_i^0, \rho_i \leftarrow \rho_i^0, i = \mathcal{I}$ 
3: repeat
4:    $\phi_{cen} \leftarrow \text{DDP-centroidal}(\phi_{cen}, \phi_{wbd}, \phi_p, \mathbf{w}_i, \rho_i)$ 
      $i = \{c, h, \lambda\}$ 
5:    $\phi_{wbd} \leftarrow \text{DDP-wholebody}(\phi_{wbd}, \phi_{cen}, \phi_p, \mathbf{w}_i, \rho_i)$ 
      $i = \mathcal{I}$ 
6:    $\phi_p \leftarrow \text{Projection}(\phi_{wbd}, \phi_{cen}, \mathbf{w}_i, \rho_i) \quad i = \{j, t, f\}$ 
7:    $\mathbf{w}_i \leftarrow \mathbf{w}_i + \mathbf{r}_i \quad i = \mathcal{I}$ 
8: until stopping criterion is satisfied
    
```

Algorithm 3 Stage-wise Accelerated ADMM solver

```

1:  $\phi_{cen} \leftarrow \phi_{cen}^0, \phi_{wbd} \leftarrow \phi_{wbd}^0, \phi_p \leftarrow \phi_p^0$ 
2:  $\mathbf{w}_i \leftarrow \mathbf{w}_i^0, \rho_i \leftarrow \rho_i^0, i = \mathcal{I}$ 
3: repeat
4:    $\phi_{cen} \leftarrow \text{DDP-centroidal}(\phi_{cen}, \phi_{wbd}, \phi_p, \mathbf{w}_i, \rho_i)$ 
      $i = \{c, h, \lambda\}$ 
5:    $\phi_{wbd} \leftarrow \text{DDP-wholebody}(\phi_{wbd}, \phi_{cen}, \phi_p, \mathbf{w}_i, \rho_i)$ 
      $i = \mathcal{I}$ 
6:    $\phi_p' \leftarrow \alpha(\mathbf{s}, \mathbf{u}, \lambda) + (1 - \alpha)(\bar{\mathbf{s}}, \bar{\mathbf{u}}, \bar{\lambda})$ 
7:    $\phi_p \leftarrow \text{Projection}(\phi_p', \mathbf{w}_i, \rho_i) \quad i = \{j, t, f\}$ 
8:    $\mathbf{w}_i \leftarrow \mathbf{w}_i + \mathbf{r}_i \quad i = \mathcal{I}$ 
9:   if current iteration  $> h_{cw}$  then
10:    if  $\|\mathbf{r}_i\|_2^2 > \mu \|\mathbf{d}_i\|_2^2$  then
11:       $\rho_i = \gamma^{incr} \rho_i$ 
12:    else if  $\|\mathbf{d}_i\|_2^2 > \mu \|\mathbf{r}_i\|_2^2$  then
13:       $\rho_i = \rho_i / \gamma^{decr}$ 
14:    end if
15:  end if
16: until stopping criterion is satisfied
    
```



Results

- Dfa;hdjljadf

$$\begin{aligned}
 & \min_{\phi_{cen}, \phi_{wbd}} \sum_{k=1}^K \int_{t_k}^{t_k + \Delta t_k} \mathcal{L}_{wbd}(\phi_{wbd}) dt + \int_{t_k}^{t_k + \Delta t_k} \mathcal{L}_{cen}(\phi_{cen}) dt \\
 & \text{subject to} \quad \mathbf{H}(\mathbf{q})\ddot{\mathbf{q}} + \mathbf{C}(\mathbf{q}, \dot{\mathbf{q}}) = \mathbf{B}\mathbf{u} + \mathbf{J}_c^T \lambda_c \quad (2a) \\
 & \quad m\ddot{\mathbf{r}} = \sum_j \mathbf{f}_j - m\mathbf{g} \quad (2b) \\
 & \quad \dot{\mathbf{L}} = \sum_j (\mathbf{p}_j - \mathbf{r}_j) \times \mathbf{f}_j \quad (2c) \\
 & \quad \dot{\phi} = \mathbf{W}(\mathbf{I}^{-1}\mathbf{L}) \quad (2d) \\
 & \quad \dot{\mathbf{e}} = \mathbf{C}_e(t, u_e) \quad (2e) \\
 & \quad \dot{\mathbf{v}} = \mathbf{C}_v(t, u_v) \quad (2f) \\
 & \quad [\mathbf{r}, \boldsymbol{\theta}](t=0) = [\mathbf{r}_0, \boldsymbol{\theta}_0] \quad (2g) \\
 & \quad \mathbf{r}(t=T) = \mathbf{r}_g \quad (2h)
 \end{aligned}$$

for every foot i :

$$\mathbf{p}_i(t) \in \mathcal{R}_i(\mathbf{r}, \boldsymbol{\theta}) \quad (2i)$$

$$\text{if foot } i \text{ in contact:} \quad (2j)$$

$$\dot{\mathbf{p}}_i(t \in \mathcal{C}_i) = 0 \quad (2k)$$

$$\mathbf{p}_i^z(t \in \mathcal{C}_i) = h_{terrain}(\mathbf{p}_i^{xy}) \quad (2l)$$

$$\mathbf{f}_i(t \in \mathcal{C}_i) \cdot \mathbf{n}(\mathbf{p}_i^{xy}) \geq 0 \quad (2m)$$

$$\mathbf{f}_i(t \in \mathcal{C}_i) \in \mathcal{F}(\mu, \mathbf{n}, \mathbf{p}_i^{xy}) \quad (2n)$$

$$\text{if foot } i \text{ in air:} \quad (2o)$$

$$\mathbf{f}_i(t \notin \mathcal{C}_i) = 0 \quad (2p)$$

$$\sum_{j=1}^{2n_{s,i}} \Delta T_{i,j} = T \quad (2q)$$

$$\text{CoM}(\mathbf{q}) = \mathbf{r} \quad (2r)$$

$$\mathbf{FK}(\mathbf{q}) = \mathbf{p} \quad (2s)$$

$$\mathbf{A}_g(\mathbf{q})\dot{\mathbf{q}} = \begin{bmatrix} m\dot{\mathbf{r}} \\ \mathbf{L}_g \end{bmatrix} \quad (2t)$$

$$\mathbf{I}_{cen}(\mathbf{q}) = \mathbf{I} \quad (2u)$$

$$\mathbf{s} \in \mathcal{S}, \mathbf{u} \in \mathcal{U} \quad (2v)$$

$$\lambda_j \in \mathcal{F}_j, \quad \forall j \in \mathcal{I}_{\text{contact}} \quad (2w)$$

Future Work

- dfasfdadf

References

dafdafadf

updates:

$$\phi_{cen}^k := \arg \min_{\phi_{cen}} \sum_{i=1}^N \mathcal{L}_{cen}(\phi_{cen}) \quad (32a)$$

$$\| \text{CoM}(\mathbf{q}^k) - \mathbf{c} + \mathbf{w}_i^k \|^2_2 \quad (32b)$$

$$\| \mathbf{A}_g(\mathbf{q}^k) \dot{\mathbf{q}}^k - \begin{bmatrix} m \dot{\mathbf{c}} \\ \mathbf{I} \dot{\boldsymbol{\theta}} \end{bmatrix} + \mathbf{w}_i^k \|^2_2 \quad (32c)$$

$$\| g_{\lambda}(\mathbf{q}^k, \dot{\mathbf{q}}^k, \mathbf{u}^k) - \boldsymbol{\lambda} + \mathbf{w}_i^k \|^2_2 \quad (32d)$$

$$\| FK(\mathbf{q}^k) - \mathbf{p} + \mathbf{w}_i^k \|^2_2 \quad (32e)$$

$$\phi_{wbd}^k := \arg \min_{\phi_{wbd}} \sum_{i=1}^N \mathcal{L}_{wbd}(\phi_{wbd}) \quad (32f)$$

$$\| \text{CoM}(\mathbf{q}) - \mathbf{c}^{k+1} + \mathbf{w}_i^k \|^2_2 \quad (32g)$$

$$\| \mathbf{A}_g(\mathbf{q}) \dot{\mathbf{q}} - \begin{bmatrix} m \dot{\mathbf{c}}^{k+1} \\ \mathbf{I} \dot{\boldsymbol{\theta}}^{k+1} \end{bmatrix} + \mathbf{w}_i^k \|^2_2 \quad (32h)$$

$$\| g_{\lambda}(\mathbf{q}, \dot{\mathbf{q}}, \mathbf{u}) - \boldsymbol{\lambda}^{k+1} + \mathbf{w}_i^k \|^2_2 \quad (32i)$$

$$\| FK(\mathbf{q}) - \mathbf{p}^{k+1} + \mathbf{w}_i^k \|^2_2 \quad (32j)$$

$$\mathbf{c}^{k+1} = \mathbf{w}_c^k + \text{CoM}(\mathbf{q}^{k+1}) - \mathbf{c}^{k+1} \quad (32k)$$

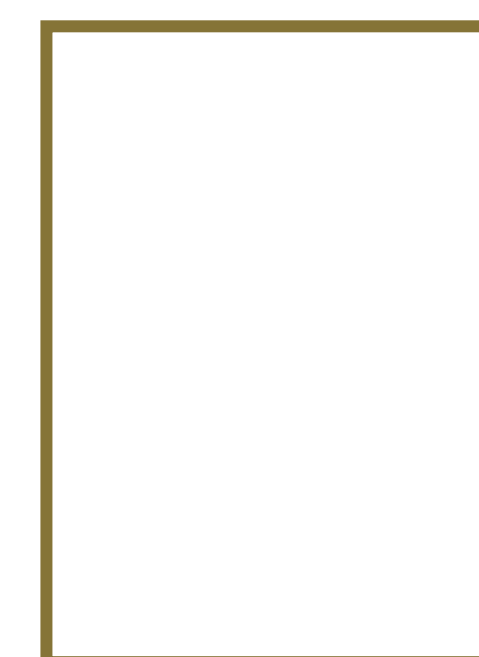
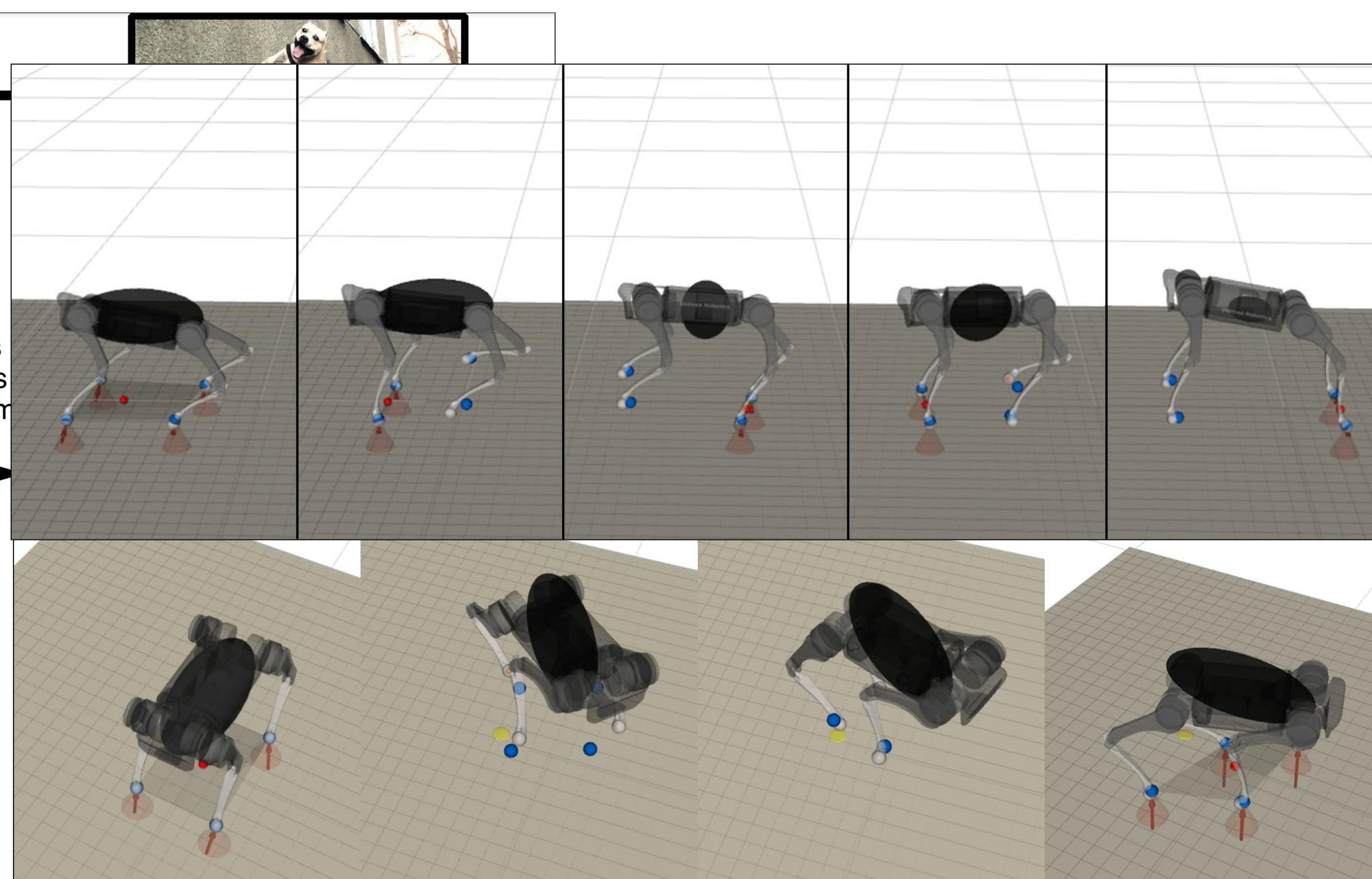
$$\mathbf{w}_h^k = \mathbf{w}_h^k + \mathbf{A}_g(\mathbf{q}^{k+1}) \dot{\mathbf{q}}^{k+1} - \begin{bmatrix} m \dot{\mathbf{c}}^{k+1} \\ \mathbf{I} \dot{\boldsymbol{\theta}}^{k+1} \end{bmatrix} \quad (32l)$$

$$\mathbf{w}_{\lambda}^k = \mathbf{w}_{\lambda}^k + g_{\lambda}(\mathbf{q}^{k+1}, \dot{\mathbf{q}}^{k+1}, \mathbf{u}^{k+1}) - \boldsymbol{\lambda}^{k+1} \quad (32m)$$

Centroidal Dynamics

Whole Body Dynamics

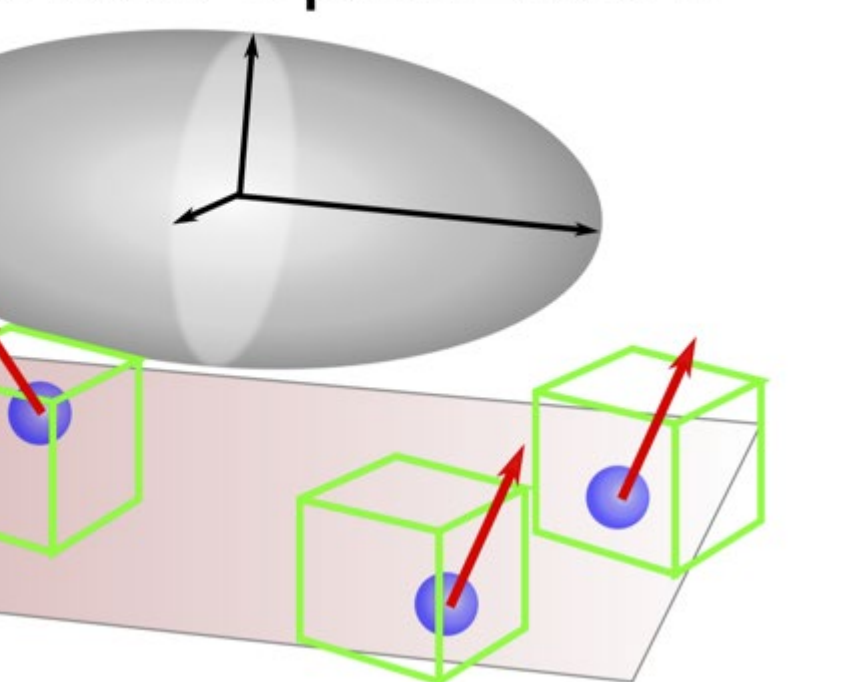
CoM pos
Footholds
Momentum
Mol



High Level Input

$\mathbf{c}_{init}, \mathbf{c}_{final}$ \downarrow $\text{traj}_{guess}, h_{terrain}(\mathbf{p}_i^{xy})$

Centroidal Dynamics Optimization



$$\min_{\phi_{wbd}} \sum_{k=1}^K \sum_{i=1}^{N_k} \mathcal{L}_{wbd}(\phi_{wbd}) + \sum_{i \in \mathcal{I}} \frac{\rho_i}{2} \|\mathbf{r}_i + \mathbf{w}_i^k\|_2^2$$

$$\text{s.t. } \mathbf{H}(\mathbf{q}) \ddot{\mathbf{q}} + \mathbf{C}(\mathbf{q}, \dot{\mathbf{q}}) = \mathbf{B}\mathbf{u} + \mathbf{J}_c^T \boldsymbol{\lambda}_c$$

$$\ddot{\mathbf{x}}_e = \mathbf{J}_c \ddot{\mathbf{q}} + \dot{\mathbf{J}}_c \dot{\mathbf{q}} = 0$$

$$\min_{\phi_{cen}} \sum_{k=1}^K \sum_{i=1}^{N_k} \mathcal{L}_{cen}(\phi_{cen}) + \sum_{i \in \mathcal{I}} \frac{\rho_i}{2} \|\mathbf{r}_i + \mathbf{w}_i^k\|_2^2$$

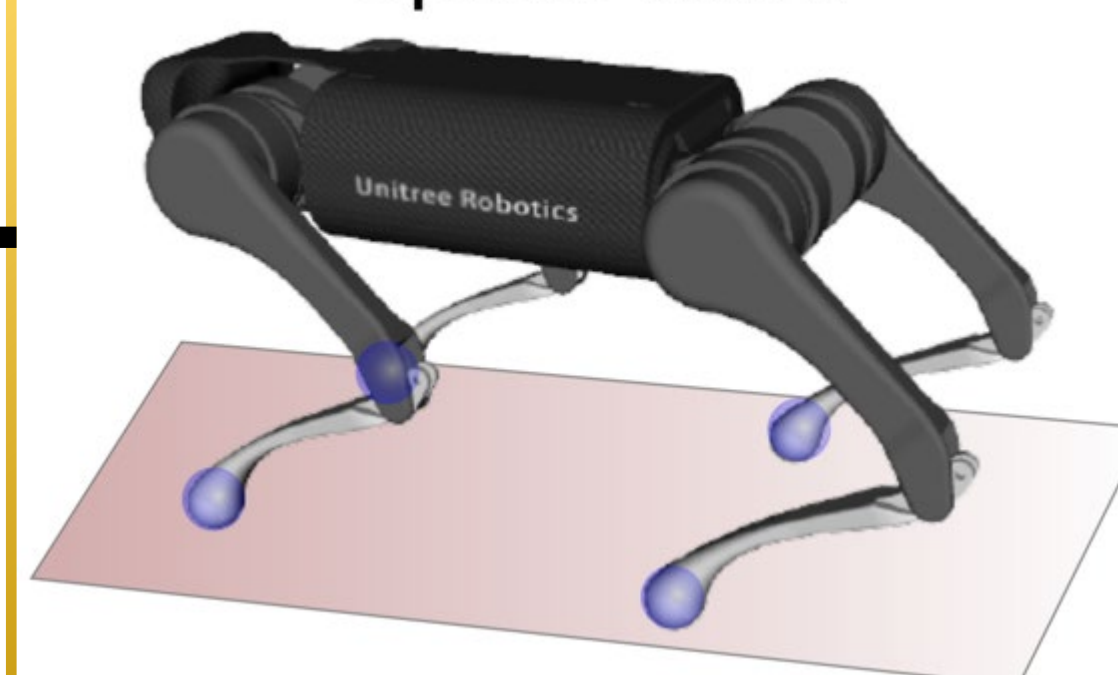
$$\text{s.t. } \begin{bmatrix} m \ddot{\mathbf{c}} \\ \dot{\mathbf{h}} \end{bmatrix} = \begin{bmatrix} \sum_j \mathbf{f}_j + m\mathbf{g} \\ \sum_j \mathbf{f}_j \times (\mathbf{c} - \mathbf{ee}_j) \end{bmatrix}$$

$$\mathbf{h} = \mathbf{I}_{ellip} \boldsymbol{\omega}$$

Force, terrain and RoM constraints

Centroidal Dynamics

Whole-Body Dynamics Optimization



Iteration k+1:

$$\min_{\phi_{cen}} \sum_{k=1}^K \sum_{i=1}^{N_k} \mathcal{L}_{cen}(\phi_{cen}) + \sum_{i \in \mathcal{I}} \frac{\rho_i}{2} \|\mathbf{r}_i + \mathbf{w}_i^k\|_2^2$$

$$\text{s.t. } \begin{bmatrix} m \ddot{\mathbf{c}} \\ \dot{\mathbf{h}} \end{bmatrix} = \begin{bmatrix} \sum_j \mathbf{f}_j + m\mathbf{g} \\ \sum_j \mathbf{f}_j \times (\mathbf{c} - \mathbf{ee}_j) \end{bmatrix}$$

$$\mathbf{h} = \mathbf{I}_{ellip} \boldsymbol{\omega}$$

Force, terrain and RoM constraints

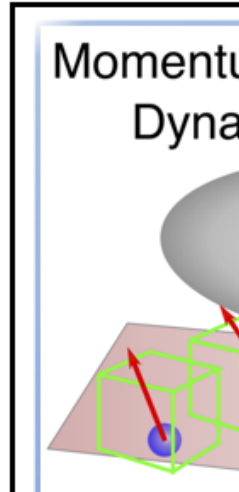
Centroidal Dynamics

Whole Body Dynamics

$$\min_{\phi_{wbd}} \sum_{k=1}^K \sum_{i=1}^{N_k} \mathcal{L}_{wbd}(\phi_{wbd}) + \sum_{i \in \mathcal{I}} \frac{\rho_i}{2} \|\mathbf{r}_i + \mathbf{w}_i^k\|_2^2$$

$$\text{s.t. } \mathbf{H}(\mathbf{q}) \ddot{\mathbf{q}} + \mathbf{C}(\mathbf{q}, \dot{\mathbf{q}}) = \mathbf{B}\mathbf{u} + \mathbf{J}_c^T \boldsymbol{\lambda}_c$$

$$\ddot{\mathbf{x}}_e = \mathbf{J}_c \ddot{\mathbf{q}} + \dot{\mathbf{J}}_c \dot{\mathbf{q}} = 0$$



Momentum Dynamics

