

ML2025

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# Chapter 1

## Introduction

### 1.1 Data types

**Goal:** Define notation of data.

#### 1.1.1 Basic

Typically, the data types of interest are:

##### Numerical

**Binary** Used for binary information represented by  $\{0, 1\}$  or  $\{\text{True}, \text{False}\}$ . Typically used for binary classification problems.

**Integer** Typically used to describe the data with limited number of possible numerical descriptors. The most popular representations used signed or unsigned numbers with 8, 16, 32 or 64 bit representation.

**Real** The basic numerical representation. Standard representations are 32 or 64 bit for CPU and 8(new!), 16, 32 bit for GPU.

##### Categorical

**Nominal** Variables with values selected from a group of categories, while not having any kind of natural order. Example: car type

**Ordinal** A categorical variable whose categories can be meaningfully ordered. Example: age, grade of exam.

#### 1.1.2 Signals and time-series

Two main categories:

- Discrete-time signals that are representation of physical continuous-time prototype signal. Signals typically have constant sampling frequency, and typically handled by signal processing techniques. Example: Voltage measurement is a signal and once-an-hour power-meter measurements.
- Time-series are typically derived from a time-stamped discrete-time origin in social sciences. Sometimes have an arbitrary sample times. Example: economical parameters.

#### 1.1.3 Dataset

The basic dataset includes matrix  $\mathbf{X} \in \mathcal{R}^{M \times N}$  ( $M$  rows and  $N$  columns) and vector  $\mathbf{y} \in \mathcal{R}^M$ .

A single dataset entry is a vector

$$\mathbf{x}_i^T = [x_{i1} \quad x_{i2} \quad \cdots \quad x_{iN}], \quad (1.1)$$

where  $i$  is the number of *features* (row) and  $N$  if the dimension (number of columns),  $\mathbf{x}_i \in \mathcal{R}^N$  and  $x_{ij} \in \mathcal{R}$ . All the values of  $M$  entries are organized in a matrix form,

$$\mathbf{X} = \begin{bmatrix} - & \mathbf{x}_1^T & - \\ - & \mathbf{x}_2^T & - \\ - & \vdots & - \\ - & \mathbf{x}_M^T & - \end{bmatrix} = \begin{bmatrix} x_{11} & x_{12} & \cdots & x_{1N} \\ x_{21} & x_{22} & \cdots & x_{2N} \\ \vdots & \vdots & \ddots & \vdots \\ x_{M1} & x_{M2} & \cdots & x_{MN} \end{bmatrix} \quad (1.2)$$

### 1.2 Tasks

Typical related task:

- Prediction or regression,  $\mathbf{y}$  is quantitative (Fig. 1.1).
- Classification,  $\mathbf{y}$  is categorical.
- Segmentation
- Anomaly detection
- Simulation
- Clustering, no  $\mathbf{y}$  is provided - it is learned from dataset.
- Signal processing tasks: noise removal, smoothing (filling missing values), event/condition detection.

**Regression and classification problem formulation** We assume that there is an underlying problem is of the form

$$y = f(\mathbf{x}) + \epsilon \quad (1.3)$$

where the values of  $\mathbf{x}$  (scalar or vector) and  $y$  are known (it is the dataset) and  $\epsilon$  is some irreducible noise.

The goal is to find the function  $f(\cdot)$ . The way to define the  $f(\cdot; \mathbf{w})$  is termed *model* that depends on some model parameters vector  $\mathbf{w}$ . The process of finding regression solution by a set of parameters  $\mathbf{w}$  is called learning, such as the resulting model can provide output

$$\hat{y}_0 = f(\mathbf{x}_0; \mathbf{w}) \quad (1.4)$$

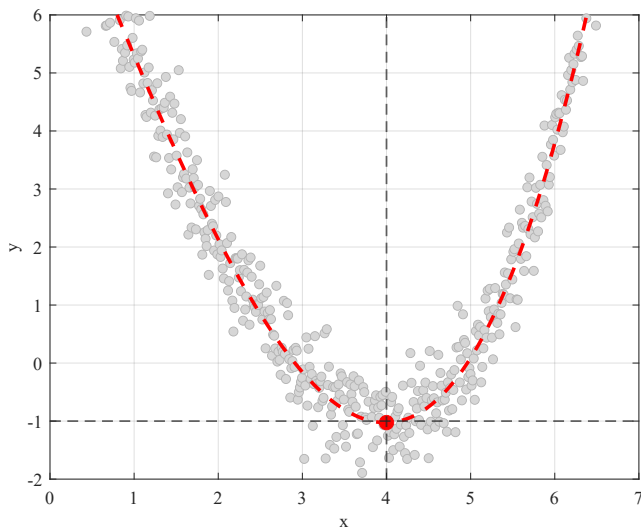


Figure 1.1: Regression example: what is the value of  $y$  for given  $x$ ?

for some new data  $\mathbf{x}_0$ .

### Parameters vs hyper-parameters

**Model parameters:** Model parameters are learned directly from a dataset.

**Hyper-parameters:** Model parameters that are not learned directly from a dataset are called **hyper-parameters**. They are learned in in-direct way during cross-validation process in the follow.

### Parametric vs non-parametric models

There are two main classes of models: parametric and non-parametric, summarized in Table 1.1.

## 1.3 Basic workflow

The basic ML/DL workflow is presented in Fig. 1.2. The workflow parts are:

- Data: available data
- Model: basic assumptions about the hidden pattern within the data
- Model training: minimization of the loss functions to derive the most appropriate parameters.
- Performance assessment according predefined metrics.

**Baseline** The basic end-to-end workflow implementation is called baseline.

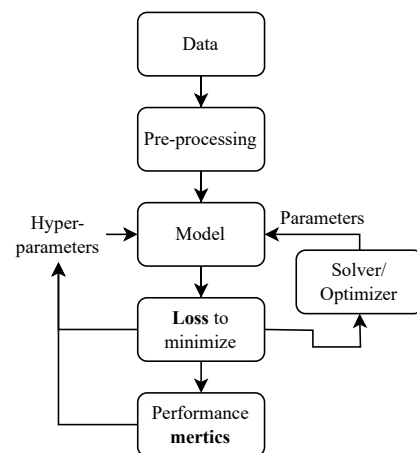


Figure 1.2: Workflow

Table 1.1: Comparison of parametric and non-parametric models.

Aspect	Parametric	Non-parametric
Dependence on number of parameters on dataset size	Fixed	Flexible
Interpretability	Yes	No
Underlying data assumptions	Yes	No
Risk	Underfitting due to rigid structure	Overfitting due to high flexibility
Dataset size	Smaller	Best for larger
Complexity	Often fast	Often complex
Examples	Linear regression	k-NN, trees

# Chapter 2

## Basic Signal Analysis

**Goal:** This chapter introduces the fundamental concepts and methods for analyzing and estimating (learning) parameters of a discrete-time sinusoidal signal observed in additive noise.

### Preface

In recent years, the convergence of machine learning (ML) and signal processing (SP) has gathered growing attention in engineering education. Students are often introduced to ML principles at an early stage, yet many advanced SP topics, ranging from linear systems and time-frequency analysis to probabilistic modeling, traditionally require multiple specialized courses [?]. Although these SP methods yield comprehensive performance insights and rigorous conclusions, teaching them can be both timely and demanding. A key bridge between basic ML concepts and advanced SP techniques is the *least squares* (LS) method. LS is grounded in a simple and intuitive idea: minimizing the sum of squared errors. While direct LS computations may be  $\mathcal{O}(N^3)$  and thus less efficient than typical SP methods ( $\mathcal{O}(N \log N)$  to  $\mathcal{O}(N^2)$ ), the LS perspective fosters a simpler, data-driven understanding of fundamental SP tasks. For example, estimating sinusoidal signal parameters in noise can be introduced by viewing it purely as a regression problem, bypassing the need for more involved probabilistic analyses. Likewise, the discrete Fourier transform (DFT) can be reframed as an extension of sinusoidal parameter estimation, illustrating SP principles with only real arithmetic. This LS-centric viewpoint aligns well with the foundational prerequisites of many ML courses and can be integrated at relatively early stages of engineering or data science programs. It offers an accessible path for teaching core SP ideas to engineering students who might lack extensive mathematical or probabilistic training. Although the underlying techniques are not new, this data-driven, regression-based interpretation may prove more intuitive for those already familiar with basic ML concepts, enabling them to explore SP topics with minimal additional theoretical overhead.

### 2.1 Sinusoidal signal

A general continuous-time cosine signal can be written as

$$\begin{aligned} y(t) &= A \cos(2\pi F_0 t + \theta) + \epsilon(t), \\ &= A \cos(\Omega_0 t + \theta) + \epsilon(t), \end{aligned} \quad (2.1)$$

where

- $A > 0$  is the amplitude,
- $-\pi < \theta \leq \pi$  is the phase,
- $F_0$  is the frequency in Hz,
- $\Omega_0 = 2\pi F_0$  is the radial frequency in rad/sec,
- $\epsilon(t)$  is zero-mean additive noise.

The only assumption for the additive noise is that it is zero-mean,

$$\sum_n \epsilon[n] = 0. \quad (2.2)$$

No additional assumptions, such as Gaussianity, are applied; however, the special case of additive white Gaussian noise (AWGN) is further refined as tips for selected topics. For the further analysis, we use the sampled version  $x[n]$  of the continuous-time signal  $x(t)$ , sampled with frequency  $F_s = 1/T$ ,

$$\begin{aligned} y[n] &= y(nT) \\ &= A \cos(\omega_0 n + \theta) + \epsilon[n] \quad n = 0, \dots, L-1, \end{aligned} \quad (2.3)$$

where

$$\omega_0 = 2\pi F_0 T = 2\pi \frac{F_0}{F_s} \quad (2.4)$$

is the angular frequency (measured in rad) derived from the analog frequency  $F_0$  and  $L$  is the resulting number of samples. In order to accurately reproduce a cosine signal, Nyquist criterion demands  $F_0 < F_s/2$ , which implies  $\omega_0 < \pi$ . This requirement can be easily illustrated by the following example. Consider two signals:

$$x_1(t) = \cos(0.6\pi t), \quad x_2(t) = \cos(2.6\pi t)$$

Sampling with  $F_s = 1$  Hz results in two identical signals,

$$\begin{aligned} x_1[n] &= \cos(0.6\pi n), \\ x_2[n] &= \cos(2.6\pi n) = \cos(0.6\pi n + 2\pi n) = x_1[n]. \end{aligned}$$

This phenomenon is called aliasing. Note, when  $\omega_0 = 0$  the signal is DC level,  $y(t) = y[n] = A \cos(\theta)$ . Therefore,

the sampling frequency requirement is  $0 \leq \omega < \pi$ . This relation holds for all the following discussions and derivations. The energy of the signal  $x[n]$  is defined as

$$E_{\mathbf{x}} = \|\mathbf{x}\|^2 = \sum_n x^2[n], \quad (2.5)$$

where  $\mathbf{x}$  is the vector of samples of the signal  $x[n]$ . The corresponding power is

$$P_{\mathbf{x}} = \frac{1}{N} E_{\mathbf{x}} = \frac{1}{N} \|\mathbf{x}\|^2. \quad (2.6)$$

## 2.2 Amplitude estimation

**Goal:** Find the amplitude of a sinusoidal signal in noise that best fits the model in a least squares (LS) sense.

Given a signal model with a known frequency  $\omega_0$ ,

$$y[n] = A \cos(\omega_0 n) + \epsilon[n] \quad n = 0, \dots, L-1 \quad (2.7)$$

the goal is to estimate the amplitude  $A$  that best fits a provided model. Technically, we are looking for the value of  $A$  that minimizes the squared error,

$$\mathcal{L}(A) = \sum_n (y[n] - A \cos(\omega_0 n))^2. \quad (2.8)$$

In the linear LS regression formulation, we define the corresponding parameters  $\mathbf{y}$ ,  $\mathbf{X}$  and  $\mathbf{w}$ . First, the required weight is  $\mathbf{w} = A$ . The matrix  $\mathbf{X}$  is formed by samples of the signal  $\{\cos(\omega_0 n)\}_{n=0}^{L-1}$ ,

$$\mathbf{X} = \begin{bmatrix} 1 & \cos(\omega_0) & \cos(2\omega_0) & \dots & \cos((L-1)\omega_0) \end{bmatrix}^T \quad (2.9)$$

Finally,  $\mathbf{y}$  is the vector of samples of  $\{y[n]\}_{n=0}^{L-1}$ . The resulting solution is straightforward,

$$\begin{aligned} \hat{A} &= (\mathbf{X}^T \mathbf{X})^{-1} \mathbf{X}^T \mathbf{y} \\ &= \frac{\sum_n x[n] y[n]}{\sum_n x^2[n]} \\ &= \frac{\sum_n y[n] \cos(\omega_0 n)}{\sum_n \cos^2(\omega_0 n)} \end{aligned} \quad (2.10)$$

If we substitute the model into the resulting solution,

$$\begin{aligned} \hat{A} &= \frac{\sum_n x[n] (Ax[n] + \epsilon[n])}{\sum_n x^2[n]} \\ &= A + \frac{\sum_n x[n] \epsilon[n]}{\sum_n x^2[n]}, \end{aligned} \quad (2.11)$$

it produces a true value of  $A$  with some additive noise. The resulting residual error is given by

$$\mathbf{e} = \mathbf{y} - \hat{\mathbf{y}}. \quad (2.12)$$

Since  $\mathbf{e} \perp \hat{\mathbf{y}}$  the power/energy terms can be decomposed as follows,

$$\|\mathbf{y}\|^2 = \|\hat{\mathbf{y}}\|^2 + \|\mathbf{e}\|^2, \quad P_{\mathbf{y}} = P_{\hat{\mathbf{y}}} + P_{\mathbf{e}}. \quad (2.13)$$

The interesting interpretation is estimated signal to noise ratio (SNR),

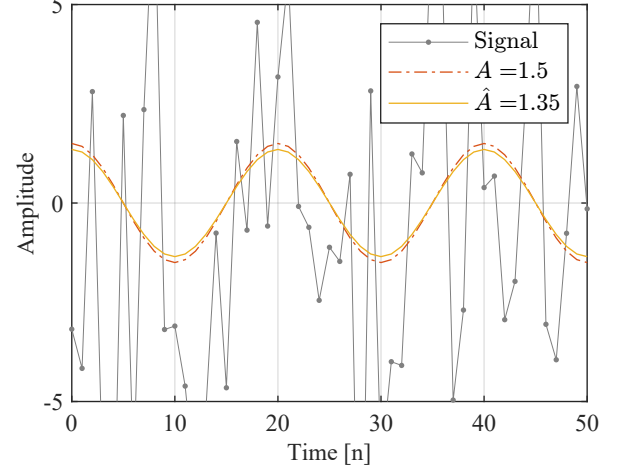
$$\widehat{SNR} = \frac{\|\hat{\mathbf{y}}\|^2}{\|\mathbf{e}\|^2} \quad (2.14)$$

Moreover, due to zero-mean property of the noise, the estimated variance of the noise is

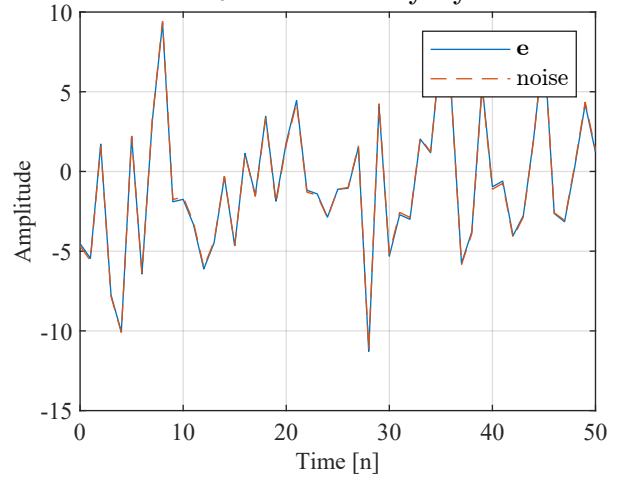
$$\hat{\sigma}_{\epsilon}^2 = \frac{1}{L} \|\hat{\mathbf{e}}\|^2. \quad (2.15)$$

The following example (Fig. 2.1) uses a synthetic cosine signal of length  $L = 51$  samples, angular frequency  $\omega_0 = 0.1\pi$  and amplitude  $A = 1.5$ . Gaussian noise with standard deviation  $\sigma = 5$  is then added to create a noisy observation. A least-squares regression is applied to estimate the amplitude, yielding  $\hat{\sigma}_{\epsilon} = 4.43$ .

$SNR_{theory} : 0.0584$  ( $-12.3dB$ ),  $SNR_{est} : 0.0474$  ( $-13.2dB$ )



(a) Reconstructed signal,  $\hat{\mathbf{y}}$ .  
Residual error  $\mathbf{e} = \mathbf{y} - \hat{\mathbf{y}}$



(b) Residual error. Ideally, if the model was perfect, the residual would equal the added noise.

Figure 2.1: Example of the cosine signal amplitude estimation.

## 2.3 Amplitude and phase estimation

**Goal:** Find amplitude and phase of a sinusoidal signal in noise.

The analysis is for the more general model,

$$y[n] = A \cos(\omega_0 n + \theta) + \epsilon[n] \quad n = 0, \dots, L-1, \quad (2.16)$$

with two unknown parameters, the amplitude  $A$  and the phase  $\theta$ . The linear LS reformulation of the signal model

$$\hat{y}[n] = A \cos(\omega_0 n + \theta) \quad (2.17)$$

involves the use trigonometric identities to express the cosine with a phase shift as a linear combination of cosine and sine,

$$A \cos(\omega_0 n + \theta) = w_c \cos(\omega_0 n) + w_s \sin(\omega_0 n), \quad (2.18)$$

where

$$\begin{aligned} w_c &= A \cos(\theta) \\ w_s &= -A \sin(\theta). \end{aligned} \quad (2.19)$$

This transforms a problem into a two-parameter linear LS in terms of  $w_c$  and  $w_s$  [?]. The resulting LS formulation involves a two-valued vector of linear coefficients,  $\mathbf{w} = [w_c \ w_s]^T$ , the vector  $\mathbf{y}$  of samples of  $y[n]$  and the matrix  $\mathbf{X}$  of dimensions  $L \times 2$  that is given by

$$\mathbf{X} = \begin{bmatrix} 1 & 0 \\ \cos(\omega_0) & \sin(\omega_0) \\ \cos(2\omega_0) & \sin(2\omega_0) \\ \vdots & \vdots \\ \cos((L-1)\omega_0) & \sin((L-1)\omega_0) \end{bmatrix}. \quad (2.20)$$

Once  $\hat{\mathbf{w}}$  is found, amplitude and phase can be recovered by

$$\begin{aligned} A &= \sqrt{w_c^2 + w_s^2} \\ \theta &= -\arctan\left(\frac{w_c}{w_s}\right) \end{aligned} \quad (2.21)$$

SNR and noise variance interpretations are similar to the previous model in Eqs. (2.14) and (2.15). The numerical example is presented in Fig. 2.2. The configuration is similar to the previous figure, except the lower noise variance,  $\sigma = 1.5$ . Nevertheless, there is a decrease in performance, since two parameters are estimated simultaneously.

### Implementation Tip

- This estimation procedure is optimal in the maximum likelihood (ML) sense under additive white Gaussian noise (AWGN) and achieves the Cramér-Rao lower bound (CRLB) [?, ?].

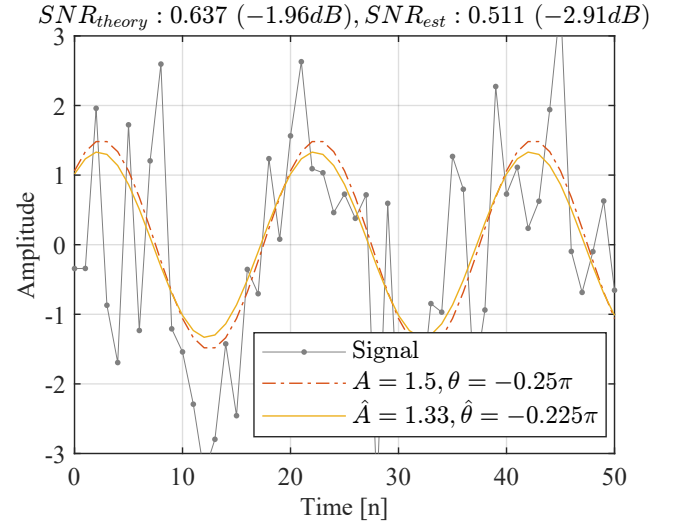


Figure 2.2: Example of the cosine signal parameters estimation.

- The theoretical lower bound (also termed Cramér-Rao lower bound (CRLB)) on the average estimation accuracy of  $w_c, w_s$  is given by [?, Eqs. (5.47-48)]

$$\text{Var}[\hat{w}_{c,s}] \gtrsim \frac{2\sigma^2}{L} \quad (2.22)$$

This bound is the tightest for the AWGN case and is less accurate for other noise distributions.

- The approximated estimation variance can be easily evaluated by Monte-Carlo simulations for any set of parameters and any distribution of interest.

## 2.4 Frequency estimation

**Goal:** If the frequency  $\omega_0$  is unknown, it can be estimated by searching for the  $\hat{\omega}_0$  that best fits a sinusoidal model to the observed data, i.e., that minimizes the residual error norm or maximizes the reconstructed signal energy.

Since  $\omega_0$  is unknown, the matrix  $\mathbf{X}$  may be parameterized as frequency-dependent one,  $\mathbf{X}(\omega)$ . This time, the estimated signal is frequency-dependent,

$$\hat{\mathbf{y}}(\omega) = \mathbf{X}(\omega)\mathbf{w}(\omega), \quad (2.23)$$

where  $\mathbf{w}(\omega)$  are the estimated parameters  $w_c$  and  $w_s$  at that frequency. The correspondent frequency-dependent residual error is given by

$$\mathbf{e}(\omega) = \mathbf{y} - \hat{\mathbf{y}}(\omega). \quad (2.24)$$

Since the error  $\mathbf{e}(\omega)$  is orthogonal to  $\hat{\mathbf{y}}$ ,

$$\|\mathbf{y}\|^2 = \|\hat{\mathbf{y}}(\omega)\|^2 + \|\mathbf{e}(\omega)\|^2. \quad (2.25)$$

To find the frequency that best represents the data, we seek the one that maximizes the energy of the reconstructed signal or equivalently minimizes the residual



error,

$$\hat{\omega}_0 = \arg \min_{\omega} \|\mathbf{e}(\omega)\|^2 = \arg \max_{\omega} \|\hat{\mathbf{y}}(\omega)\|^2. \quad (2.26)$$

Note, this optimization problem can be challenging because the objective function may exhibit multiple local maxima/minima. Therefore, an appropriate numerical global optimization method is required. Once  $\hat{\omega}_0$  is found, the amplitude and phase are estimated using the corresponding linear LS solution  $\mathbf{w}(\omega_0)$ . This solution also results in SNR and noise variance estimation, as in Eqs. (2.14) and (2.15).

**Tip: Interpretation in Terms of the Periodogram**  
The function

$$P(\omega) = \frac{1}{L} \|\mathbf{y}(\omega)\|^2 \quad (2.27)$$

as a function of  $\omega$  is termed a periodogram that is a frequency-dependent measure of signal power that approximates the power spectral density (PSD) of the signal. By scanning over frequencies, the  $\omega$  that yields the maximum periodogram value is taken as the frequency estimate,  $\omega_0$ . The example of the signal is presented in Fig. 2.3. The configuration is similar to the previous example with even lower noise variance,  $\sigma = 1$ . First, periodogram peak is found (Fig. 2.3a). Then, the subsequent amplitude/phase estimation result is presented in Fig. 2.3b.

**Tip: Theoretical performance bounds** Under AWGN assumption, theoretical SNR is given by

$$SNR = \frac{A^2}{2\sigma^2} \quad (2.28)$$

and the corresponding CRLB on the estimation variances are [?]

$$\text{Var}[\hat{A}] \geq \frac{2\sigma^2}{L} [V^2] \quad (2.29)$$

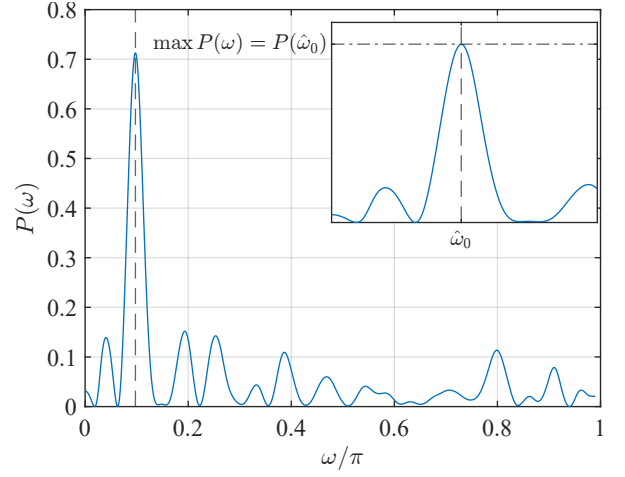
$$\text{Var}[\hat{\omega}_0] \geq \frac{12}{SNR \times L(L^2 - 1)} \approx \frac{12}{SNR \times L^3} \left[ \left( \frac{\text{rad}}{\text{sample}} \right)^2 \right] \quad (2.30)$$

$$\text{Var}[\hat{\theta}] \geq \frac{2(2L - 1)}{SNR \times L(L + 1)} \approx \frac{4}{SNR \times L} [\text{rad}^2] \quad (2.31)$$

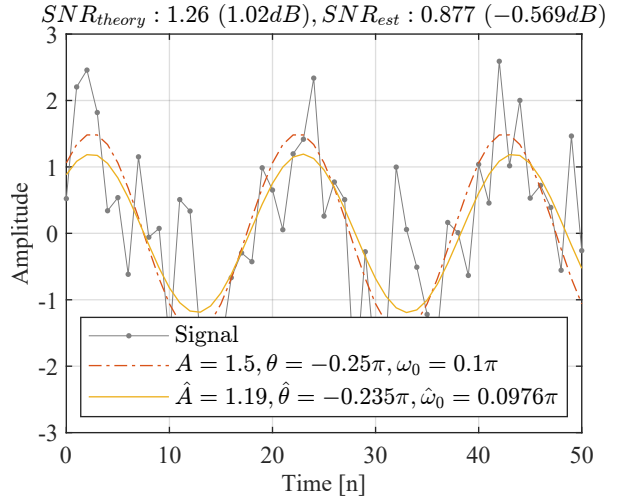
For analog frequency  $F_0 = \frac{\omega_0}{2\pi} F_s$ ,

$$\text{Var}[F_0] = \text{Var}[\omega_0] \left( \frac{F_s}{2\pi} \right)^2 [Hz^2] \quad (2.32)$$

In practice, for short data lengths or non-Gaussian noise, these bounds provide only approximate guides to achievable performance.



(a) The periodogram  $P(\omega)$  with a prominent peak at  $\omega_0 \approx 0.1\pi$ .



(b) Reconstructed signal.

Figure 2.3: The reconstruction in (b) uses the estimated amplitude, phase, and angular frequency ( $\hat{A}, \hat{\theta}, \hat{\omega}_0$ ) found by maximizing the periodogram in (a).

## 2.5 Harmonic Signal Analysis

A particularly important class of signals encountered in many practical applications is the *harmonic* or *periodic* signal. Such a signal can be expressed as a sum of cosine terms whose frequencies are integer multiples (harmonics) of a fundamental frequency  $\omega_0$ .

$$y[n] = A_0 + \sum_{m=1}^M A_m \cos(m\omega_0 n + \theta_m), \quad (2.33)$$

where:

- $A_0$  is the constant (DC) component,
- $A_m$  and  $\theta_m$  represent the amplitude and phase of the  $m$ -th harmonic,
- $\omega_0$  is the fundamental angular frequency,
- $m\omega_0$  corresponds to the frequency of the  $m$ -th harmonic,
- and  $M$  is the number of harmonics in the model.

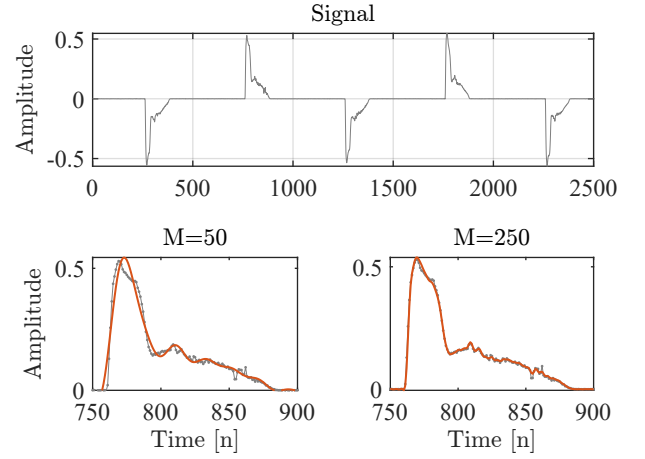
Given  $\omega_0$ , the model is linear in terms of the unknown parameters  $\{A_m, \theta_m\}$  for each harmonic  $m = 1, \dots, M$ . Similar to the single-frequency case, the LS matrix  $\mathbf{X}$  is constructed with columns corresponding to  $\cos(m\omega_0 n)$  and  $\sin(m\omega_0 n)$  for  $m = 1, \dots, M$ , plus a column of ones for the DC component. Each pair  $(A_m, \theta_m)$  can be recovered from the LS estimated cosine and sine coefficients in the manner described for single-frequency amplitude-phase estimation. The resulting SNR and noise variance estimates are similar to the previous sections. The model order  $M$  (number of harmonics) is a hyper-parameter that should be chosen carefully. Too few harmonics can fail to capture essential signal structure, while too many may overfit noise. The maximum value of  $M$  is bounded by the Nyquist criterion,  $M < \pi/\omega_0$ . If  $\omega_0$  is not known, the approach that is described in the frequency estimation section can be also applied here. Once  $\hat{\omega}_0$  is determined by a maximum of the harmonic periodogram,

$$P_h(\omega) = \frac{1}{L} \sum_{m=1}^M \|\mathbf{y}(m\omega)\|^2, \quad (2.34)$$

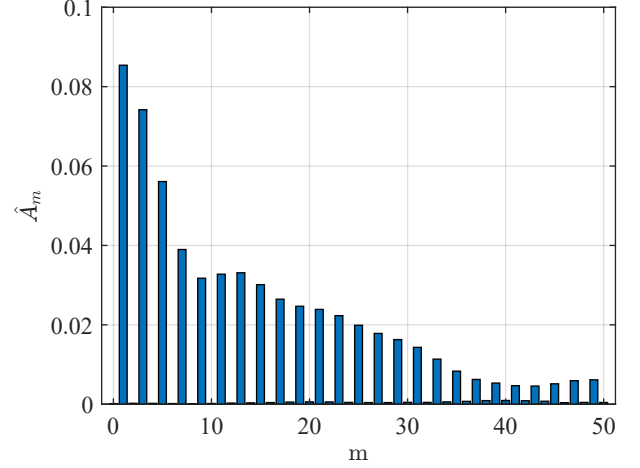
the harmonic amplitudes and phases can be estimated via LS at this frequency [?]. Total harmonic distortion (THD) is a measure commonly used in electrical engineering, audio processing, and other fields to quantify how much the harmonic components of a signal differ from a pure sinusoid at the fundamental frequency. It is defined as the ratio of the root-sum-square of the harmonic amplitudes to the amplitude of the fundamental,

$$THD = \frac{\sqrt{\sum_{m=2}^M A_m^2}}{A_1}. \quad (2.35)$$

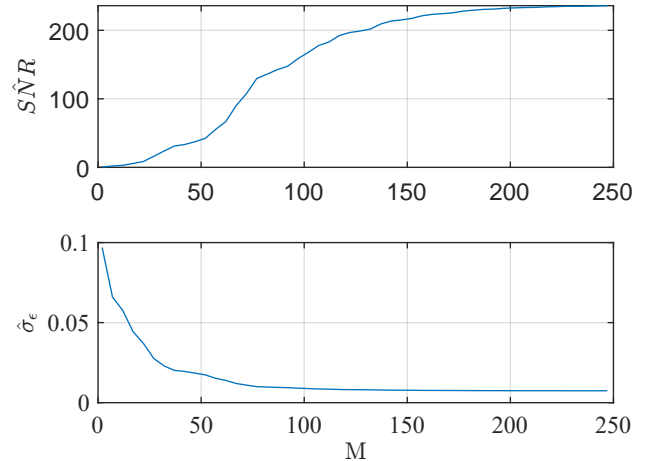
A lower THD value indicates that the signal is closer to a pure sinusoidal shape, whereas a higher THD signifies a stronger presence of higher-order harmonics. The example is sampled current of a switch-mode power supply in 50Hz network sampled with 50kHz frequency [?]. Figure 2.4a shows a reconstruction of the signal with  $M = 250$  harmonics. The estimated amplitudes  $\hat{A}_m$  are shown (Fig. 2.4b) as a function of the harmonic index  $m$ , including the DC term at  $m = 0$ . A larger magnitude indicates a more prominent harmonic component. The first non-DC harmonic amplitude  $m = 1$  corresponds to the fundamental frequency,  $\omega_0$ , while higher indices capture additional harmonics in the signal. The estimated fundamental frequency is 50.104Hz with the corresponding THD of about 1.6. Figure 2.4c shows estimated SNR (top) and the noise standard deviation (bottom) vary as the number of harmonics  $M$  in the model increases. **Tip:** The frequency estimator is an effective ML estimator with known analytical CRLB [?].



(a) This plot shows the signal with the harmonic reconstruction using the estimated frequency, amplitude, and phase parameters. The inset zooms in on a smaller portion of the time axis for different values of  $M$ , demonstrating challenging shape of the signal.



(b) Harmonic amplitudes,  $A_m$ .



(c) Estimated SNR and noise std,  $\hat{\sigma}_\epsilon$ .

## 2.6 Discrete Fourier Transform (DFT)

The discrete Fourier transform (DFT) can be viewed as a systematic way of decomposing a finite-length signal

into a sum of harmonically related sinusoids. In fact, it is a special case of the harmonic signal representation discussed earlier. Specifically, setting the fundamental angular frequency to  $\omega_0 = \frac{2\pi}{N}$  and using  $N \geq L - 1$  harmonics, the harmonic model reduces exactly to a DFT decomposition that provides a natural harmonic decomposition of the signal into  $N$  harmonics that are evenly spaced in frequency. DFT representation assumes that any arbitrary, finite-time signal  $y[n]$  may be represented as a sum of sinusoidal signals,

$$y[n] = \sum_{k=0}^{N-1} A_k \cos\left(k \frac{2\pi}{N} n + \theta_k\right), \quad n = 0, \dots, L-1 \quad (2.36)$$

When  $N \geq L$ , the DFT allows for perfect reconstruction of the signal using its harmonic representation:

$$\mathbf{y} = \mathbf{X}\hat{\mathbf{w}}.$$

It is also worth noting the symmetry in the DFT,

$$\begin{aligned} \cos((N-k)\Delta\omega) &= \cos(k\Delta\omega) \\ \sin((N-k)\Delta\omega) &= -\sin(k\Delta\omega), \end{aligned} \quad (2.37)$$

resulting redundant information for frequencies  $k\omega_0$  above and below  $\pi$ ,

$$\begin{aligned} A_k &= A_{N-k} \\ \theta_k &= -\theta_{N-k} \end{aligned} \quad (2.38)$$

As a result, only frequencies  $k\omega_0 \leq \pi$  need be considered uniquely.

### 2.6.1 Single frequency analysis

Consider a signal  $y[n]$  assume a discrete frequency  $\omega_0 = \frac{2\pi}{N}k$  is given. To estimate amplitude and phase at this predefined frequency, we can form a matrix  $\mathbf{X}$ ,

$$\mathbf{X}_1 = \begin{bmatrix} \mathbf{x}_c & \mathbf{x}_s \end{bmatrix},$$

where

$$\mathbf{x}_c = \begin{bmatrix} \cos\left(2\pi \frac{k}{N} \cdot 0\right) \\ \cos\left(2\pi \frac{k}{N} \cdot 1\right) \\ \vdots \\ \cos\left(2\pi \frac{k}{N} (L-1)\right) \end{bmatrix} \text{ and } \mathbf{x}_s = \begin{bmatrix} \sin\left(2\pi \frac{k}{N} \cdot 0\right) \\ \sin\left(2\pi \frac{k}{N} \cdot 1\right) \\ \vdots \\ \sin\left(2\pi \frac{k}{N} (L-1)\right) \end{bmatrix}.$$

By evaluating  $\mathbf{X}_1^T \mathbf{X}_1$ , we find that the sine and cosine columns form an orthogonal basis for this single frequency, with

$$\mathbf{x}_c^T \mathbf{x}_c = \frac{N}{2}, \quad (2.39a)$$

$$\mathbf{x}_s^T \mathbf{x}_s = \frac{N}{2}, \quad (2.39b)$$

$$\mathbf{x}_c^T \mathbf{x}_s = 0. \quad (2.39c)$$

Stacking these results for all  $k = 0, \dots, N-1$  yields the complete DFT matrix forms a complete orthogonal basis for the  $L$ -sample signal space. The further discussion of  $(\mathbf{X}^T \mathbf{X})^{-1}$  matrix properties may be found in

Examples 4.2 and 8.5 in [?]. Moreover, since  $(\mathbf{X}^T \mathbf{X})^{-1}$  takes a particularly simple diagonal form, and the least squares solution  $\hat{\mathbf{w}}$  for the parameters  $w_{c,k}$  and  $w_{s,k}$  (corresponding to amplitude and phase components at  $\omega_k$ ) is

$$w_{c,k} = \frac{2}{N} \sum_{n=0}^{L-1} y[n] \cos\left(2\pi \frac{k}{N} n\right), \quad (2.40a)$$

$$w_{s,k} = \frac{2}{N} \sum_{n=0}^{L-1} y[n] \sin\left(2\pi \frac{k}{N} n\right). \quad (2.40b)$$

**Tip** The fast Fourier transform (FFT) algorithm efficiently computes  $Y[k]$ , providing  $A_k = |Y[k]|/N$  and  $\theta_k = \angle(Y[k])$  with significantly lower memory requirements and complexity than Eq. (2.40). When only a single frequency value is of interest, Goertzel algorithm is more efficient method for the task. Moreover, it can be used for computationally effective peaking of the maximum in Eq. (2.26).

### 2.6.2 Power Spectral Density

The power of the signal of the form

$$x_k[n] = A_k \cos\left(k \frac{2\pi}{N} n + \theta_k\right) \quad (2.41)$$

is

$$P_{y_k} = \frac{1}{L} \|\mathbf{y}_k\|^2 = \frac{A_k^2}{2}. \quad (2.42)$$

This value is known as a power spectral density (PSD) at the frequency  $\omega = k \frac{2\pi}{N}$ . The corresponding squared magnitude values  $A_k^2/2$  are known as the discrete-frequency periodogram (Eq. (2.27)) and is the basic method for the PSD estimation of a signal. Plotting such a periodogram gives a frequency-domain representation of the signal's power distribution, highlighting which frequencies carry the most power. DFT is energy conservation transform (Parseval's Theorem) that states the relation

$$\sum_{k=0}^{N-1} A_k^2 = \frac{1}{L} \|\mathbf{y}\|^2. \quad (2.43)$$

### 2.6.3 Spectral Spreading and Leakage

In an idealized setting, a pure cosine signal has a perfectly defined frequency representation. For instance, consider the discrete-time signal,

$$x[n] = A \cos\left(k_0 \frac{2\pi}{L} n\right), \quad k_0 \in \{1, \dots, L-1\} \quad (2.44)$$

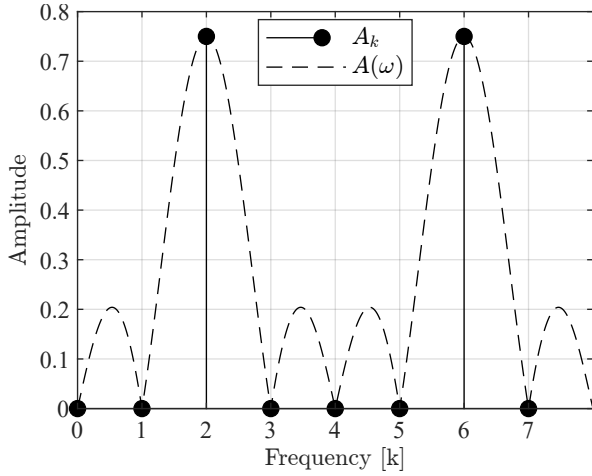


Figure 2.5: Illustration of a single-frequency cosine signal’s spectrum under ideal assumptions (discrete, integer-multiple frequencies) versus practical conditions (denser frequency grid or non-integer frequencies). Note how the ideal single peak broadens and additional low-level components appear, highlighting the effects of spectral spreading and leakage.

where  $k_0$  is the frequency index. The Fourier transform of this signal yields a single spectral component at frequency  $\omega_0 = k_0 \frac{2\pi}{L}$ , such that the spectral amplitude  $A_k$  at each value of  $k$  is given by

$$A_k = \begin{cases} \frac{A}{2} & k = k_0, N - k_0 \\ 0 & \text{otherwise} \end{cases}. \quad (2.45)$$

Under these conditions, the signal’s spectral representation seems to be strictly localized at the specific frequency  $\omega_k$ , with no energy distributed elsewhere in the spectrum. However, practical scenarios deviate from this ideal case. In particular, if a denser frequency grid is employed (i.e.  $N > L$ ) or the frequency varies continuously (as in Eq. (2.23)), the resulting spectral distribution can differ substantially from the discrete, single-peak ideal (Fig. 2.5). This difference arises because, in general,  $\mathbf{X}(\omega)^T \mathbf{X}(\omega)$  is not orthogonal as in Eq. (2.39). As a result, two effects are introduced:

- The main frequency peak broadens, resulting in “spectral spreading”.
- Additional frequency components emerge beyond the broadened main peak, termed “spectral leakage.”

## 2.7 Summary

The summary of the presented approach is shown in Table 2.1. The presented approach involves a design of matrix  $\mathbf{X}$  and using LS to estimate unknown parameters. The key addressed tasks are as follows.

**Amplitude Estimation** With a known frequency  $\omega_0$ , the amplitude  $A$  is found via LS. The resulting residuals

provide noise variance and SNR estimates. **Amplitude and Phase Estimation:** For known  $\omega_0$ , rewriting

$$A \cos(\omega_0 n + \theta) = w_c \cos(\omega_0 n) + w_s \sin(\omega_0 n)$$

transforms the problem into a two-parameter LS regression.

**Frequency Estimation:** If  $\omega_0$  is unknown, it is found by searching for the frequency that maximizes the fitted signal energy.

**Harmonic Signal Analysis:** Signals can be expressed as sums of multiple harmonics. Extending the LS approach to multiple harmonics allows estimation of each amplitude and phase. THD quantifies deviations from a pure tone.

**Discrete Fourier Transform (DFT):** The DFT is a special case of harmonic modeling, decomposing a signal into equally spaced frequency components. Efficiently computed by the FFT, the DFT is central to signal spectral analysis. Although the estimators presented above have been extensively analyzed for the specific case of additive white Gaussian noise (AWGN) in the statistical signal processing literature [?, ?], conducting such an analysis requires a significantly more extensive mathematical framework. Furthermore, it is worth noting that any bias and variance in these estimators can be readily approximated via Monte Carlo simulations under various parameter settings and noise distributions.

## Appendices

### 2.A Single frequency analysis

#### 2.A.1 Theory

- $\mathbf{X}^T \mathbf{X}$  analysis:

$$\mathbf{X}^T \mathbf{X} = \begin{bmatrix} \mathbf{x}_c^T \mathbf{x}_c & \mathbf{x}_s^T \mathbf{x}_c \\ \mathbf{x}_s^T \mathbf{x}_c & \mathbf{x}_s^T \mathbf{x}_s \end{bmatrix} \quad (2.46)$$

with the following values

$$\begin{aligned} \mathbf{x}_c^T \mathbf{x}_c &= \sum_{n=0}^{N-1} \cos^2 \left( 2\pi \frac{k}{N} n \right) = \frac{N}{2} \\ \mathbf{x}_c^T \mathbf{x}_s &= \sum_{n=0}^{N-1} \cos \left( 2\pi \frac{k}{N} n \right) \sin \left( 2\pi \frac{k}{N} n \right) = 0 \\ &= \mathbf{x}_s^T \mathbf{x}_c \\ \mathbf{x}_s^T \mathbf{x}_s &= \sum_{n=0}^{N-1} \sin^2 \left( 2\pi \frac{k}{N} n \right) = \frac{N}{2} \end{aligned} \quad (2.47)$$

Table 2.1: Comparison and summary of different signal estimation methods.

Task	Parameters	Matrix $\mathbf{X}$	SNR
Amplitude only	$A$ given $\omega_0$	A single column of $\cos(\omega_0 n)$	$\frac{\ \hat{\mathbf{y}}\ ^2}{\ \mathbf{e}\ ^2}$
Amplitude & phase	$A, \theta$ given $\omega_0$	Two columns of $\cos(\omega_0 n)$ and $\sin(\omega_0 n)$	$\frac{\ \hat{\mathbf{y}}\ ^2}{\ \mathbf{e}\ ^2}$
Frequency estimation	$\omega_0, A, \theta$	Frequency-dependent $\cos(\omega n)$ and $\sin(\omega n)$ columns	Maximum of $\frac{\ \hat{\mathbf{y}}(\omega)\ ^2}{\ \mathbf{e}(\omega)\ ^2}$
Fourier series (harmonic decomposition)	$A_0, \{A_m, \theta_m\}_{m=1}^M$ , possibly $\omega_0$	Harmonic $\cos/\sin$ columns at multiples of $\omega_0$ , $\cos(m\omega_0 n)$ , $\sin(m\omega_0 n)$	$\frac{\ \hat{\mathbf{y}}\ ^2}{\ \mathbf{e}\ ^2}$ , can include frequency dependence if $\omega_0$ unknown
DFT	$\{A_k, \theta_k\}_{k=0}^{N-1}$	Multiple pairs of columns $\cos\left(\frac{2\pi k}{N}n\right)$ , $\sin\left(\frac{2\pi k}{N}n\right)$ for $k = 0, \dots, N-1$	Not used directly. Perfect reconstruction for $N \geq L$

- $(\mathbf{X}^T \mathbf{X})^{-1}$  analysis: The resulting matrix

$$(\mathbf{X}^T \mathbf{X})^{-1} = \begin{bmatrix} \frac{2}{N} & 0 \\ 0 & \frac{2}{N} \end{bmatrix} \quad (2.48)$$

that results from the time-limited origin of the signal  $y[n]$ . For the infinite number of samples, the resulting power converges to a continuous-time power expression,

$$\lim_{L \rightarrow \infty} P_{\mathbf{y}} \rightarrow \frac{A^2}{2} \quad (2.55)$$

- Finally,  $(\mathbf{X}^T \mathbf{X})^{-1} \mathbf{X}^T \mathbf{y}$  is

$$w_{c,k} = \frac{2}{N} \sum_{n=0}^{L-1} y[n] \cos\left(2\pi \frac{k}{N} n\right) \quad (2.49a)$$

$$w_{s,k} = \frac{2}{N} \sum_{n=0}^{L-1} y[n] \sin\left(2\pi \frac{k}{N} n\right) \quad (2.49b)$$

The orthogonality in more general form is given by

$$\sum_{n=0}^{N-1} \cos\left(2\pi \frac{j}{N} n\right) \cos\left(2\pi \frac{k}{N} n\right) = \frac{N}{2} \delta[j - k] \quad (2.50)$$

$$\sum_{n=0}^{N-1} \cos\left(2\pi \frac{k}{N} n\right) \sin\left(2\pi \frac{k}{N} n\right) = 0 \quad \forall j, k \quad (2.51)$$

$$\sum_{n=0}^{N-1} \sin\left(2\pi \frac{j}{N} n\right) \sin\left(2\pi \frac{k}{N} n\right) = \frac{N}{2} \delta[j - k], \quad (2.52)$$

### 2.1.2 Power

For a more general case of an arbitrary  $\omega$  values, the signal of the form

$$y[n] = A \cos(\omega_0 n) \quad (2.53)$$

has the  $\omega_0$ -dependent power,

$$P_{\mathbf{y}} = \frac{A^2}{4L} \left( 1 + 2L - \frac{\sin(\omega_0 - 2L\omega_0)}{\sin(\omega_0)} \right), \quad (2.54)$$

# Chapter 3

## Notation

### Numbers and indexing

$a$	Scalar
$\mathbf{a}$	Vector
$a_i$	Element $i$ of a vector $a$ , indexing starting at 1
$\mathbf{A}$	Matrix
$a_{ij}$	Element $i, j$ of a matrix $\mathbf{A}$ , indexing starting at 1
$\mathcal{R}$	Real numbers domain
$\mathcal{R}^D$	$D$ -dimensional vector
$\mathcal{R}^{D_1 \times D_2}$	matrix of a dimension $D_1 \times D_2$

### Datasets

$N$	Number of features
$M$	Number of entries in the dataset
$K$	Number of classes
$\mathbf{w}$	Model parameters
$f(\cdot; \mathbf{w})$	Model
$x_{ij}$	Singe data value
$\mathbf{x}_i$	Singe data vector, $i$ column number in $\mathbf{X}$
$\mathbf{X}$	Data matrix
$\mathbf{y}$	Target vector for the data in $\mathbf{X}$
$\hat{\mathbf{y}}$	Prediction vector of $\mathbf{y}$
$y_i$	Target value
$\hat{y}_i$	Predicted target value
$\mathcal{L}(\mathbf{y}, \hat{\mathbf{y}})$	Loss function (vector domain)
$\mathcal{L}(y_i, \hat{y}_i)$	Loss function (scalar domain)
$\mathbf{a}^{[k]}$	Activation of layer $k$
$\mathbf{z}^{[k]}$	Output of layer $k$
$g_k(\cdot)$	Activation function of layer $k$