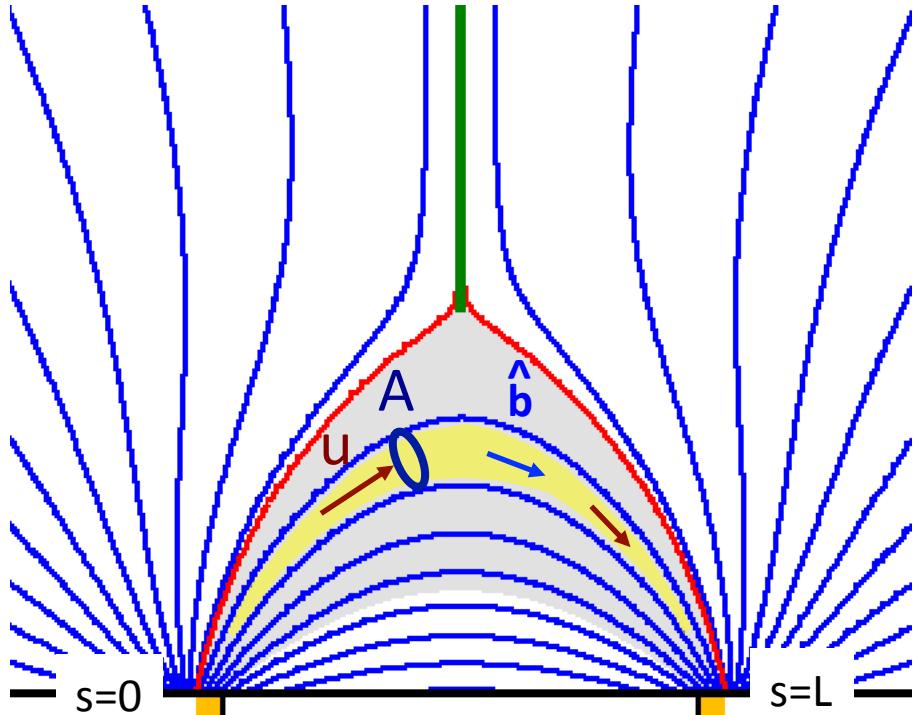


# Flare Loops

1d Gas dynamics & 0-d models

Lecture 9

Feb. 15, 2017



$$\mathbf{E} = -\mathbf{u} \times \mathbf{B} = 0$$

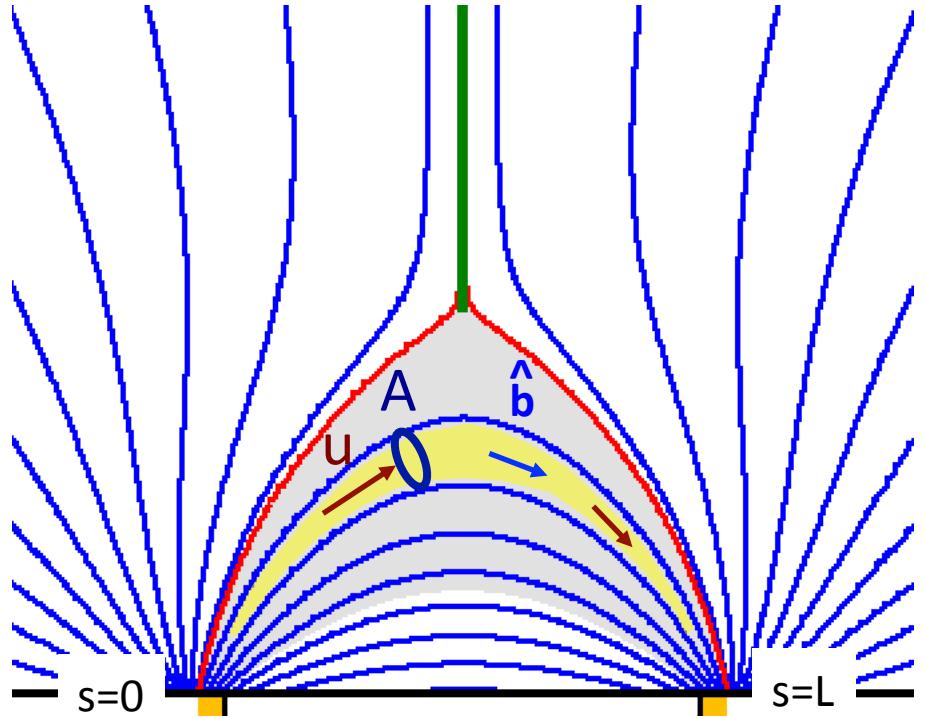
$$\mathbf{B} \parallel \mathbf{u} = u \hat{\mathbf{b}}$$

Flow inside a static tube:  
length coord  $s$   
X-section  $A(s)$

$$\frac{\partial \rho}{\partial t} = -\nabla \cdot (\rho \mathbf{u}) \quad \rightarrow \quad \boxed{\frac{\partial \rho}{\partial t} = -\frac{1}{A} \frac{\partial}{\partial s} (A \rho u)}$$

$$\rho \left( \frac{\partial}{\partial t} + \mathbf{u} \cdot \nabla \right) \mathbf{u} = -\nabla p + \frac{1}{c} \mathbf{J} \times \mathbf{B} + \rho \mathbf{g} + \nabla \cdot (\mu \nabla \mathbf{u})$$

$\hat{\mathbf{b}}$  component  $\rightarrow$  
$$\boxed{\rho \left( \frac{\partial u}{\partial t} + u \frac{\partial u}{\partial s} \right) = -\frac{\partial p}{\partial s} + \rho g_{||} + \frac{\partial}{\partial s} \left( \frac{4}{3} \mu \frac{\partial u}{\partial s} \right)}$$



## Energy equation

Thermal energy density

$$\frac{3}{2} p = \rho c_v T$$

$$\rho c_v \left( \frac{\partial T}{\partial t} + \mathbf{u} \cdot \nabla T \right) = -p(\nabla \cdot \mathbf{u}) + \mu \|\nabla \mathbf{u}\|^2 - \nabla \cdot \mathbf{F}_c - L_{rad}$$

conductive flux

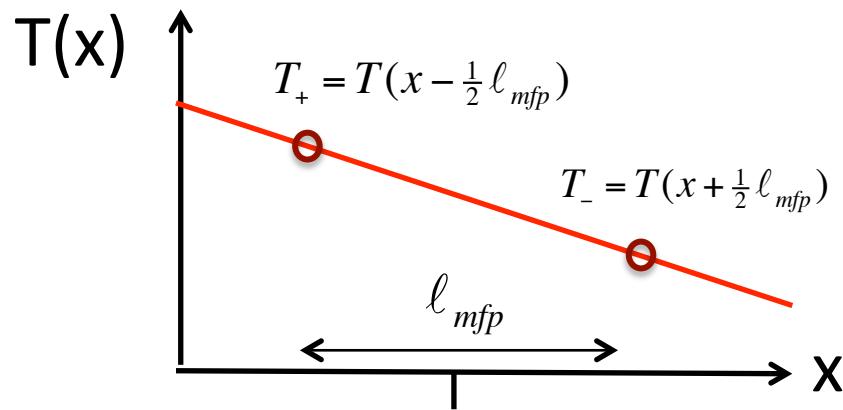
p dV work

viscous heat

radiative loss

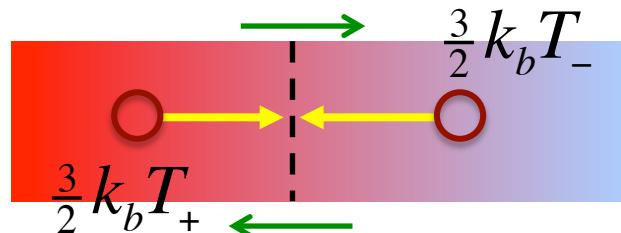
$$\rightarrow \rho c_v \left( \frac{\partial T}{\partial t} + u \frac{\partial T}{\partial s} \right) = -\frac{p}{A} \frac{\partial}{\partial s} (Au) + \frac{4}{3} \mu \left| \frac{\partial \mathbf{u}}{\partial s} \right|^2 - \frac{1}{A} \frac{\partial}{\partial s} (A \mathbf{F}_c) - L_{rad}$$

# Conductive flux



energy flux:  $\rightarrow F_c$

greater from left  $\xrightarrow{(3/2) nv k_b T_+}$



particle flux:  $nv$

same both directions  $(3/2) nv k_b T_-$

$$F_c = \frac{3}{2} nv k_b (T_+ - T_-)$$

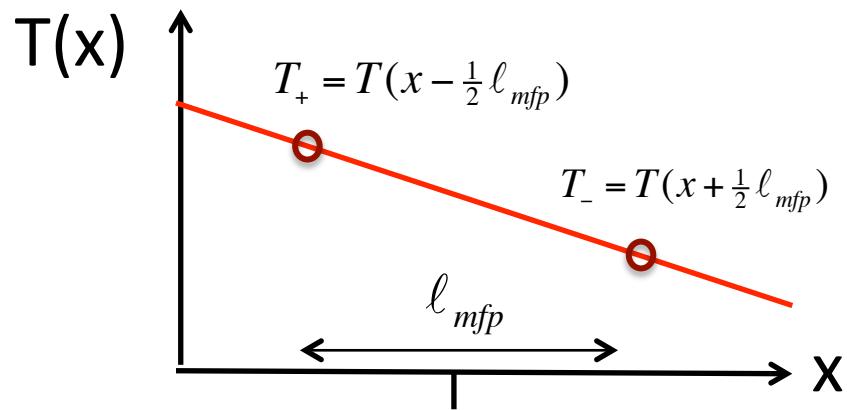
**IF** gradient is shallow  
or m.f.p. is small

$$F_c \approx - \boxed{\frac{3}{2} nv k_b \ell_{mfp}} \frac{\partial T}{\partial x} = \kappa$$

$$\vec{F}_c = -\kappa \nabla T$$

Fourier's law –  
classical heat flux

# Conductive flux



$$\kappa = \frac{3}{2} k_b v_{th} n \ell_{mfp} = \frac{3}{2} \frac{k_b v_{th}}{\sigma_{sc}}$$

$$\sigma_{sc} \sim \frac{q^4}{m^2 v_{th}^4}$$

Rutherford scattering

$$\kappa \sim \frac{k_b m^2 v_{th}^5}{q^4} \sim \boxed{\frac{k_b^{7/2}}{m^{1/2} q^4}} T^{5/2}$$

$$F_c = \frac{3}{2} n v k_b (T_+ - T_-)$$

**IF** gradient is shallow  
or m.f.p. is small

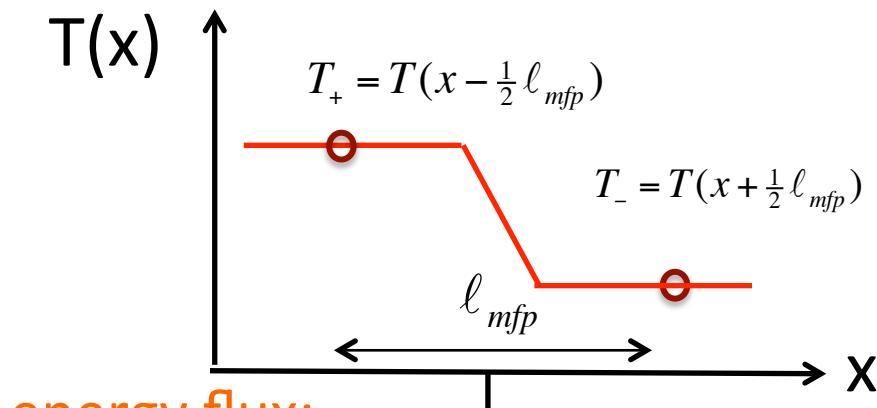
$$F_c \approx - \boxed{\frac{3}{2} n v k_b \ell_{mfp}} \frac{\partial T}{\partial x} = \kappa$$

e<sup>-</sup>s : smallest m →  
most heat flux

$$\kappa = \kappa_0 T^{5/2} \quad [\text{erg cm}^{-2} \text{s}^{-1} \text{K}^{-1}]$$

$$\kappa_0 \approx 10^{-6} \text{ erg cm}^{-2} \text{s}^{-1} \text{K}^{-7/2}$$

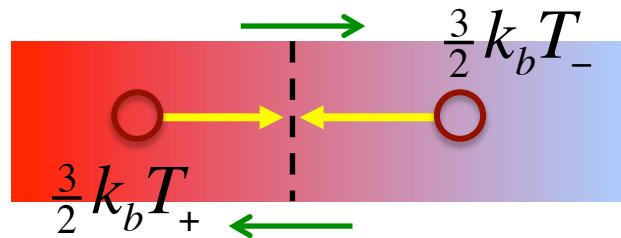
# Conductive flux



energy flux:  
greater from  
left

$$(3/2) n v k_b T_+ \xrightarrow{nv} F_c$$

$$|F_c| < \frac{3}{2} n v_{th} k_b T_+$$



particle flux:  $n v$   
same both  
directions  $(3/2) n v k_b T_- \xleftarrow{v}$

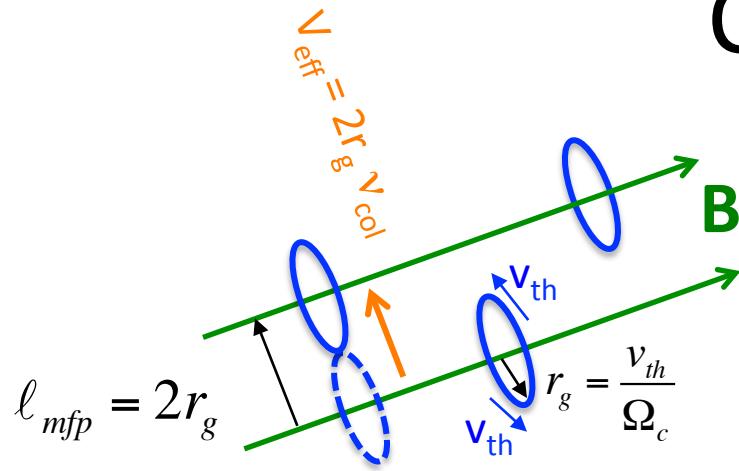
$$F_c = \frac{3}{2} n v k_b (T_+ - T_-)$$

**IF NOT**

$$\frac{k_b^{3/2}}{\frac{3}{2} n_e \frac{m_e^{1/2}}{k_b} T_e^{3/2}} = F_{fs}$$

**Free-streaming**  
heat flux:  
upper bound

# Conductive flux $\perp$ to $\mathbf{B}$



$$F_c \approx -\left[ \frac{3}{2} n v k_b \ell_{mfp} \right] \frac{\partial T}{\partial x} = \kappa$$

$$\kappa_{\perp} = \frac{3}{2} k_b n v_{eff} \ell_{mfp} = 6 k_b n r_g^2 v_{col} = 6 k_b n \frac{v_{th}^2}{\Omega_c^2} v_{col}$$

$$= 6 k_b v_{th} \left( \frac{n v_{th}}{v_{col}} \right) \left( \frac{v_{col}}{\Omega_c} \right)^2 \\ 1/\sigma_{sc}$$

$$\kappa_{\perp} = 6 \frac{k_b v_{th}}{\sigma_{sc}} \left( \frac{v_{col}}{\Omega_c} \right)^2 = 4 \kappa_{||} \left( \frac{v_{col}}{\Omega_c} \right)^2$$

$\sim 10^{-14}$

Heat flows **ONLY** || to  $\mathbf{B}$

## Constraints on heat flux:

Volumetric heating  $\dot{Q} = -\nabla \cdot \vec{F}_c$

heat exchange  
across bndry

Entropy change  $\frac{dS}{dt} = \int_V \frac{\dot{Q}}{T} d^3x = - \int_V \frac{\nabla \cdot \vec{F}_c}{T} d^3x = - \oint_{\partial V} \frac{\vec{F}_c}{T} \cdot d\vec{a} - \int_V \frac{\vec{F}_c \cdot \nabla T}{T^2} d^3x$

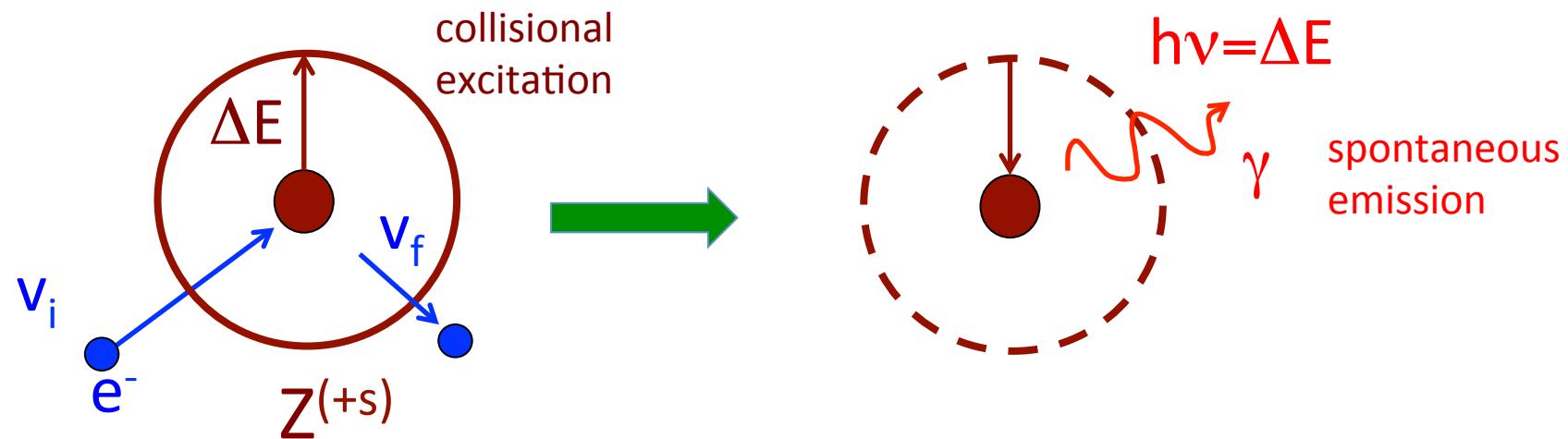
2<sup>nd</sup> law of thermo:

$$\vec{F}_c \cdot \nabla T \leq 0$$

Classical flux:  $\nabla T \cdot \vec{F}_c = -(\nabla T) \cdot \vec{\kappa} \cdot (\nabla T)$

$\kappa$  must have **no negative e-values**

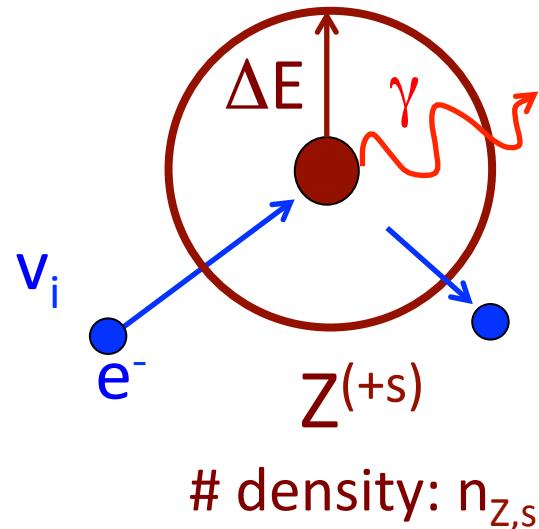
# Energy loss by optically thin radiation



- $e^-$  collides with element  $Z$  ionized  $+s$
- $e^-$  **loses**  $\Delta E = m_e(v_i^2 - v_f^2)/2$
- excites ion to state @  $\Delta E$
- ion de-excites, emitting  $\gamma$  w/  $h\nu = \Delta E$
- $\gamma$  escapes to  $\infty$  carrying away  $\Delta E$

optically thin radiation

# Energy loss by optically thin radiation



- excitation cross section:  $\sigma_{Z,s}(v_e)$
  - average  $\gamma$  energy  $\varepsilon_{Z,s}(v_e)$
  - rate of energy loss **per e<sup>-</sup>**
- $$\dot{E}_e = \underbrace{n_{Z,s} v_e \sigma_{Z,s}(v_e)}_{\text{collision frequency}} \varepsilon_{Z,s}(v_e)$$
- sum over all transition!

**Assumption I:** e<sup>-</sup>s have **Maxwellian** dist'n w/ temp  $T_e$

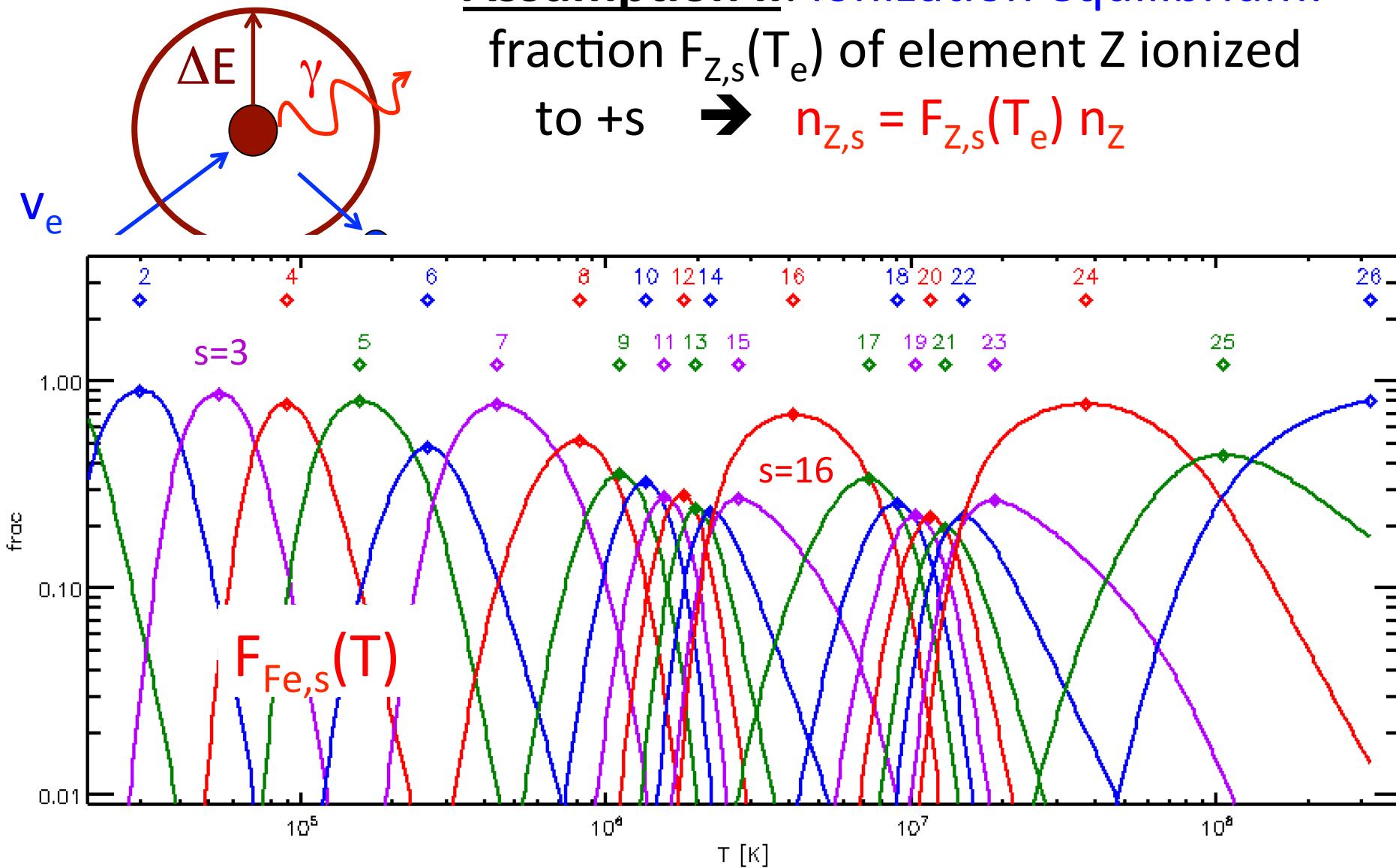
$$L_{Z,s} = n_{Z,s} n_e \int \frac{e^{-m_e v_e^2 / 2k_b T_e}}{(2\pi k_b T_e / m_e)^{3/2}} v_e \sigma_{Z,s}(v_e) \varepsilon_{Z,s}(v_e) d^3 v_e$$

volumetric energy loss rate [ erg cm<sup>-3</sup> s<sup>-1</sup>]  $R_{Z,s}(T_e)$  [erg cm<sup>3</sup> s<sup>-1</sup>]

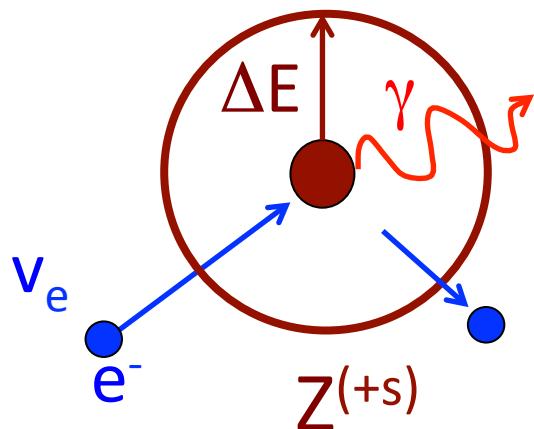
to  $Z^{(+)s}$

# Energy loss by optically thin radiation

Assumption II: ionization equilibrium:  
fraction  $F_{Z,s}(T_e)$  of element Z ionized  
to +s  $\rightarrow n_{Z,s} = F_{Z,s}(T_e) n_Z$



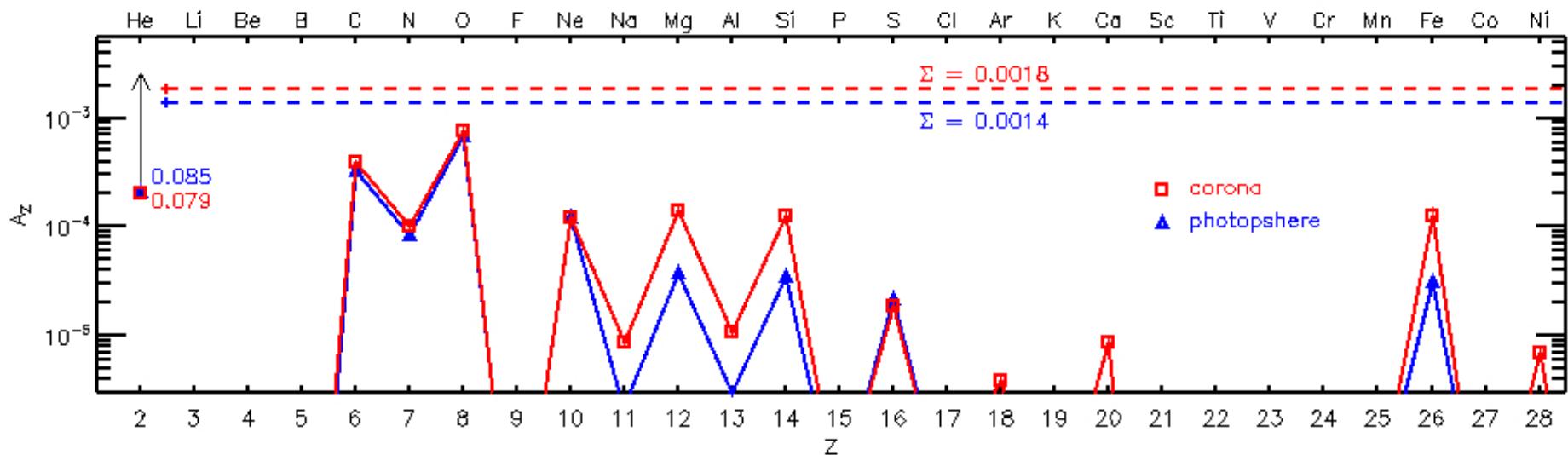
# Energy loss by optically thin radiation



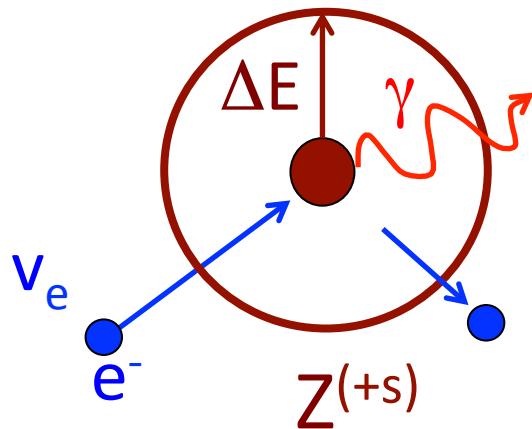
**Assumption II:** ionization equilibrium:  
fraction  $F_{Z,s}(T_e)$  of element Z ionized  
to  $+s \rightarrow n_{Z,s} = F_{Z,s}(T_e) n_z$

**Assumption III:** known abundances  
 $n_z = A_z n_H$

$$\text{H \& He fully ionized: } n_e = \sum_Z n_H A_z \sum_s s F_{Z,s} \approx n_H (1 + 2A_{He}) \approx 1.17 n_H$$



# Energy loss by optically thin radiation



**Assumption II:** ionization equilibrium:  
fraction  $F_{Z,s}(T_e)$  of element Z ionized  
to  $+s \rightarrow n_{Z,s} = F_{Z,s}(T_e) n_z$

**Assumption III:** known abundances  
 $n_z = A_z n_H$

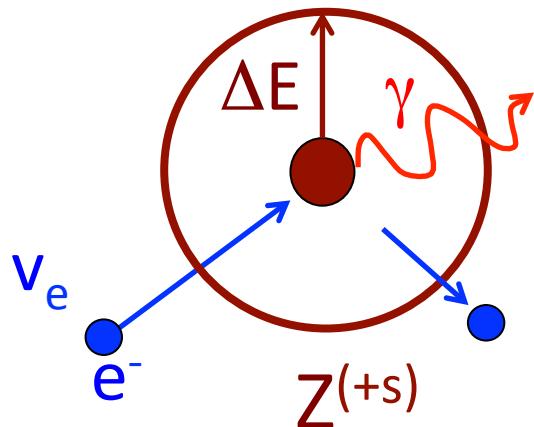
$$\text{H \& He fully ionized: } n_e = \sum_Z n_H A_Z \sum_s s F_{Z,s} \approx n_H (1 + 2A_{He}) \approx 1.17 n_H$$

**Assumption I:**  $e^-$ s have **Maxwellian** dist'n w/ temp  $T_e$

$$L_{Z,s} = n_{Z,s} n_e \int \frac{e^{-m_e v_e^2 / 2k_b T_e}}{(2\pi k_b T_e / m_e)^{3/2}} v_e \sigma_{Z,s}(v_e) \epsilon_{Z,s}(v_e) d^3 v_e$$

volumetric  
energy loss rate [ erg cm<sup>-3</sup> s<sup>-1</sup>]  $R_{Z,s}(T_e)$  [erg cm<sup>3</sup> s<sup>-1</sup>]  
to  $Z^{(+)s}$

# Energy loss by optically thin radiation



**Assumption II:** ionization equilibrium:  
fraction  $F_{Z,s}(T_e)$  of element Z ionized  
to  $+s \rightarrow n_{Z,s} = F_{Z,s}(T_e) n_z$

**Assumption III:** known abundances  
 $n_z = A_z n_H$

$$\text{H \& He fully ionized: } n_e = \sum_Z n_H A_Z \sum_s s F_{Z,s} \approx n_H (1 + 2A_{He}) \approx 1.17 n_H$$

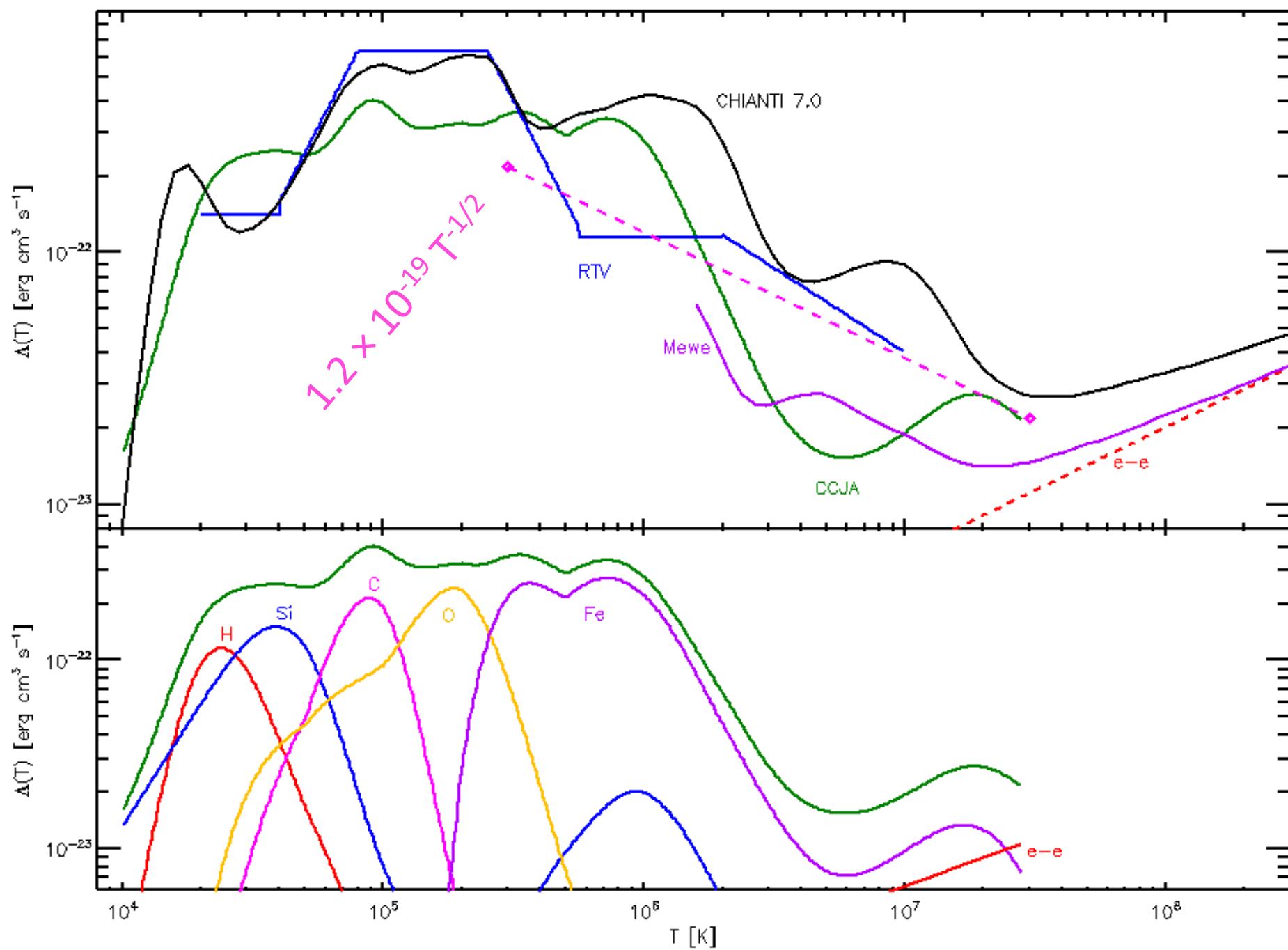
volumetric energy  
loss rate to  $Z^{(s)}$

$$L_{Z,s} = n_e n_{Z,s} R_{Z,s}(T_e) = \frac{n_e^2}{1.17} A_Z F_{Z,s}(T_e) R_{Z,s}(T_e)$$

volumetric  
energy loss  
rate  
[ erg cm<sup>-3</sup> s<sup>-1</sup> ]

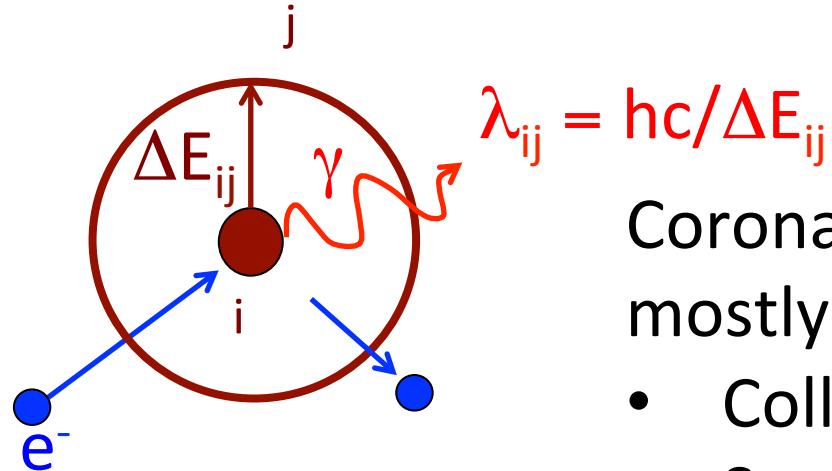
$$L = n_e^2 \boxed{\sum_Z \frac{A_Z}{1.17} \sum_s F_{Z,s}(T_e) R_{Z,s}(T_e)} = n_e^2 \boxed{\Lambda(T_e)}$$

Radiative loss function  $\Lambda(T_e)$



# Emission measure

a sidebar



$$\lambda_{ij} = hc/\Delta E_{ij}$$

Corona & TR:

mostly optically thin

- Collisional excitation
- Spontaneous emission

$$I_\lambda = \int n_e^2(\mathbf{x}) G_\lambda[T_e(\mathbf{x})] d^3x \approx G_\lambda(\bar{T}_e) \boxed{\int n_e^2(\mathbf{x}) d^3x}$$

Emission measure: EM [cm<sup>-3</sup>]

Regions of highest density emit most –

$$n_e \uparrow \times 10 \quad \rightarrow \quad I \sim EM \uparrow \times 100$$

# The 1d flare loop

$\rho(s,t)$ ,  $u(s,t)$  &  $T(s,t)$

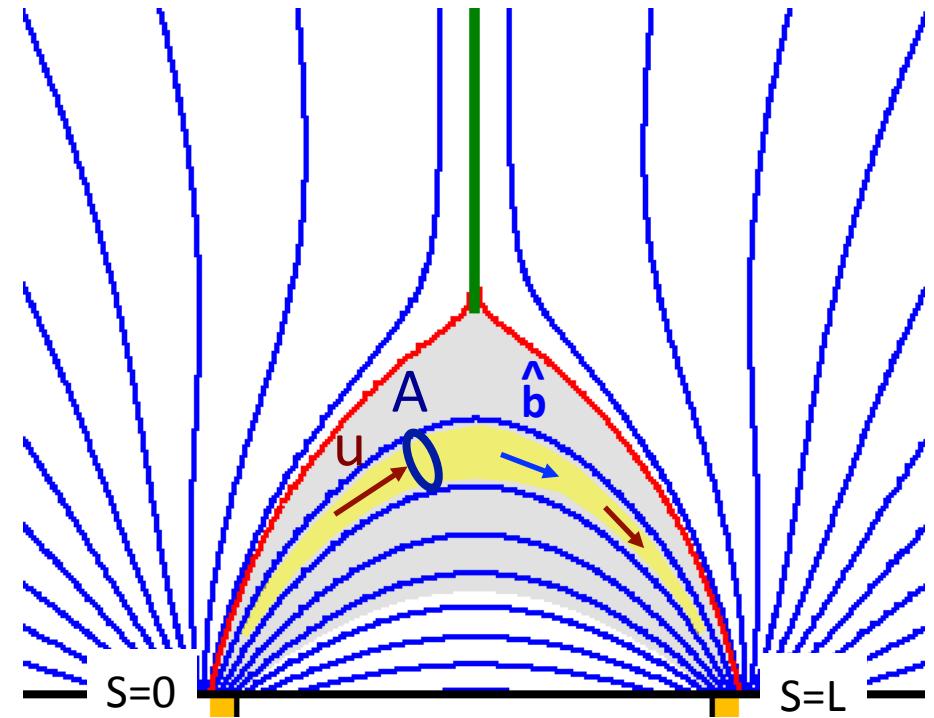
Fixed  $A(s)$  &  $g_{||}(s)$

$$\frac{\partial \rho}{\partial t} = -\frac{1}{A} \frac{\partial}{\partial s} (A \rho u)$$

$$\rho \left( \frac{\partial u}{\partial t} + u \frac{\partial u}{\partial s} \right) = -\frac{\partial p}{\partial s} + \rho g_{||} + \frac{\partial}{\partial s} \left( \frac{4}{3} \mu \frac{\partial u}{\partial s} \right)$$

$$\rho c_v \left( \frac{\partial T}{\partial t} + u \frac{\partial T}{\partial s} \right) = -\frac{p}{A} \frac{\partial}{\partial s} (Au) + \frac{4}{3} \mu \left| \frac{\partial u}{\partial s} \right|^2 + \frac{1}{A} \frac{\partial}{\partial s} \left[ A \kappa \frac{\partial T}{\partial s} \right] - n_e^2 \Lambda(T) + h$$

$$p = \frac{k_b}{\bar{m}} \rho T \quad c_v = \frac{3}{2} \frac{k_b}{\bar{m}}$$



Source of flare energy



# Integral quantities

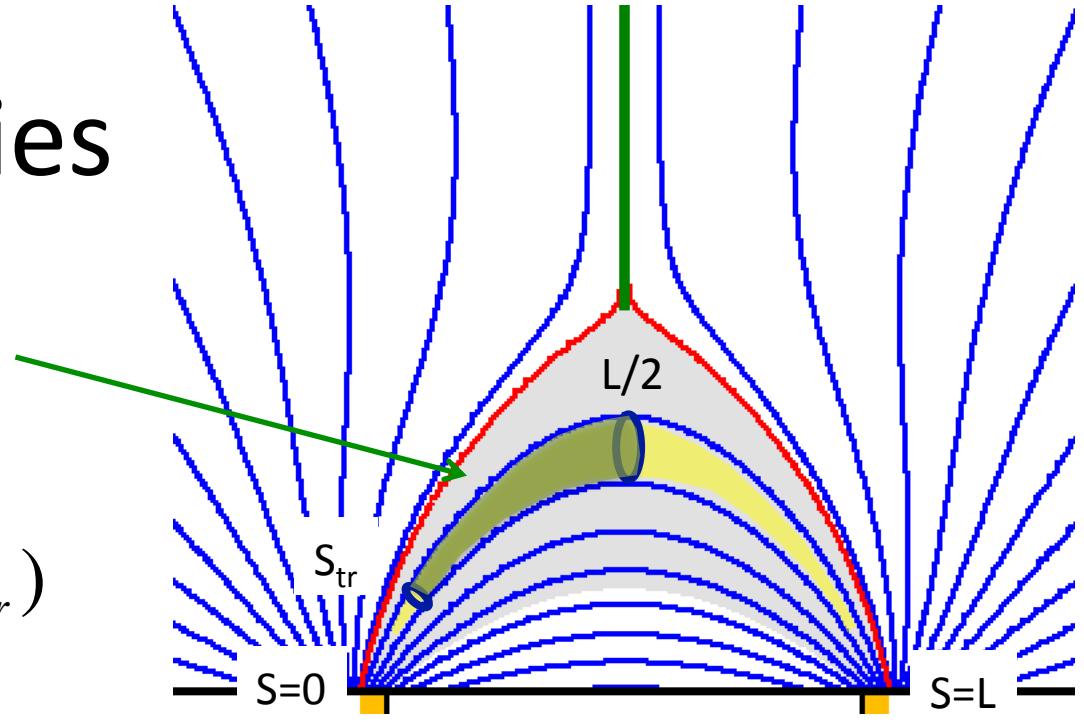
$$M = \int_{s_{tr}}^{L/2} \rho(s, t) A(s) ds$$

$$\frac{dM}{dt} = \rho(s_{tr}) u(s_{tr}) A(s_{tr})$$

$$E_{tot} = \int_{s_{tr}}^{L/2} \left[ \frac{1}{2} \rho u^2 + \frac{3}{2} p + \rho \Psi \right] A ds$$

$$\frac{dE_{tot}}{dt} \approx - \int_{s_{tr}}^{L/2} n_e^2 \Lambda(T) A ds + \frac{1}{2} u^3 A \Big|_{tr} + \underbrace{\frac{5}{2} p u A \Big|_{tr}}_{\text{enthalpy flux}} - \kappa \frac{\partial T}{\partial s} A \Big|_{tr} + \underbrace{\int_{s_{tr}}^{L/2} h A ds}_{\text{conductive flux}}$$

flare heat



# Their evolution: 0d models

$$M = \int_{s_{tr}}^{L/2} \rho(s, t) A(s) ds \equiv \frac{L}{2} A m_p \bar{n}_e$$

$$\frac{d\bar{n}_e}{dt} = \frac{2}{L} n_{e,tr} u_{tr}$$

$$E_{tot} = \int_{s_{tr}}^{L/2} \left[ \frac{1}{2} \rho \overline{u}^2 + \frac{3}{2} p \right] A ds \equiv \frac{3L}{4} A \bar{p}$$

$$\frac{d}{dt} \left( \frac{3}{2} \bar{p} \right) \approx - \frac{2}{L} \int_{s_{tr}}^{L/2} n_e^2 \Lambda(T) ds + \underbrace{\frac{5}{L} p_{tr} u_{tr}}_{\text{radiative loss}} - \frac{2}{L} K \frac{\partial T}{\partial s} \Big|_{tr}$$

$$\approx -\bar{n}_e^2 \Lambda(\bar{T})$$

enthalpy flux

$$+ \frac{2}{L} \int_{s_{tr}}^{L/2} h ds$$

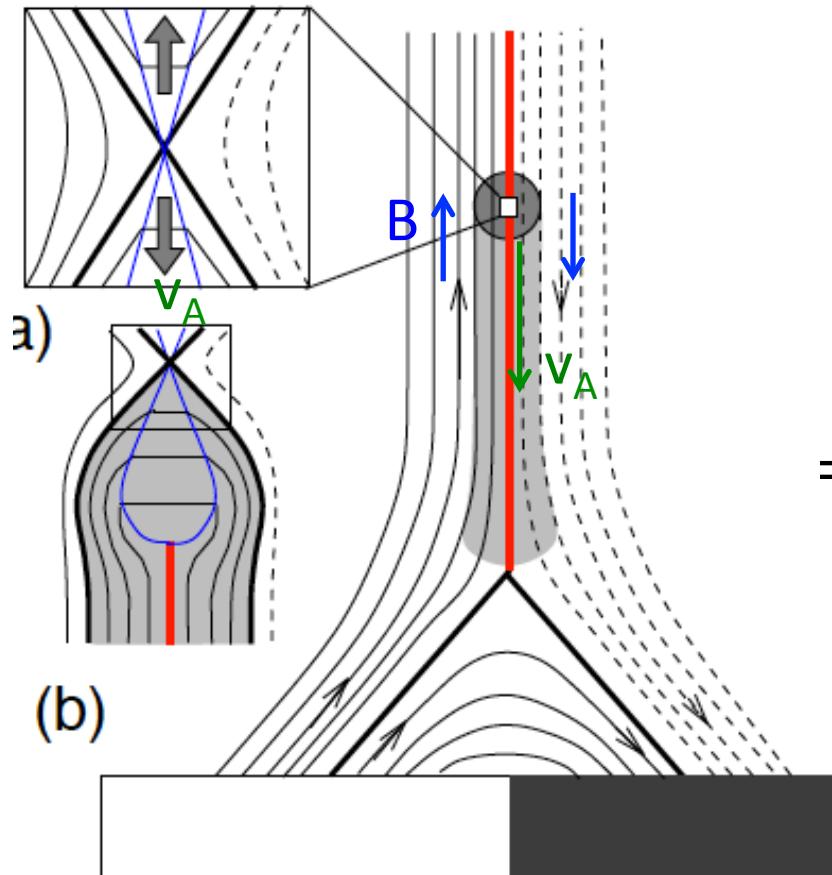
conductive flux

$$\approx \frac{8K_0}{7L^2} \bar{T}^{7/2}$$

$$F_{fl}$$

$$\frac{d}{dt} \left( \frac{3}{2} \bar{p} \right) \approx -\bar{n}_e^2 \Lambda(\bar{T}) + \frac{5}{L} p_{tr} u_{tr} - \frac{8K_0}{7L^2} \bar{T}^{7/2} + \frac{2}{L} F_{fl}$$

# What will be the value of $F_{\text{fl}}$ ?



$$F_{\text{fl}} = \zeta \frac{B^2}{8\pi} v_A = \frac{\zeta}{2\sqrt{\rho}} \left( \frac{B^2}{4\pi} \right)^{3/2}$$

$$B = 100 \text{ G}$$

$$\rho = 10^{-15} \text{ g cm}^{-3}$$

$$\Rightarrow F_{\text{fl}} = \zeta 3 \times 10^{11} \text{ erg s}^{-1} \text{ cm}^{-2}$$

Compare to upward fluxes:

- Steady AR:

$$F \sim 10^7 \text{ erg cm}^{-2} \text{ s}^{-1}$$

- Luminosity (white light)

$$L_\odot / 4\pi R_\odot^2 = 6 \times 10^{10}$$

$$\frac{d}{dt} \left( \frac{3}{2} \bar{p} \right) \approx - \underbrace{\bar{n}_e^2 \Lambda(\bar{T})}_{\text{green bracket}} + \frac{5}{L} p_{tr} u_{tr} - \underbrace{\frac{8\kappa_0}{7L^2} \bar{T}^{7/2}}_{\text{blue bracket}} + \frac{2}{L} F_{fl}$$

$$\tau_{rad} \equiv \frac{\frac{3}{2} \bar{p}}{\bar{n}_e^2 \Lambda(\bar{T})}$$

$$= \frac{3\bar{n}_e k_b \bar{T}}{\bar{n}_e^2 \Lambda(\bar{T})} \sim \frac{3k_b}{1.2 \times 10^{-19}} \frac{\bar{T}^{3/2}}{\bar{n}_e}$$

$$\tau_{cond} \equiv \frac{\frac{3}{2} \bar{p}}{\frac{8\kappa_0}{7L^2} \bar{T}^{7/2}}$$

$$= \frac{21k_b}{8 \times 10^{-6}} \frac{\bar{n}_e L^2}{\bar{T}^{5/2}}$$

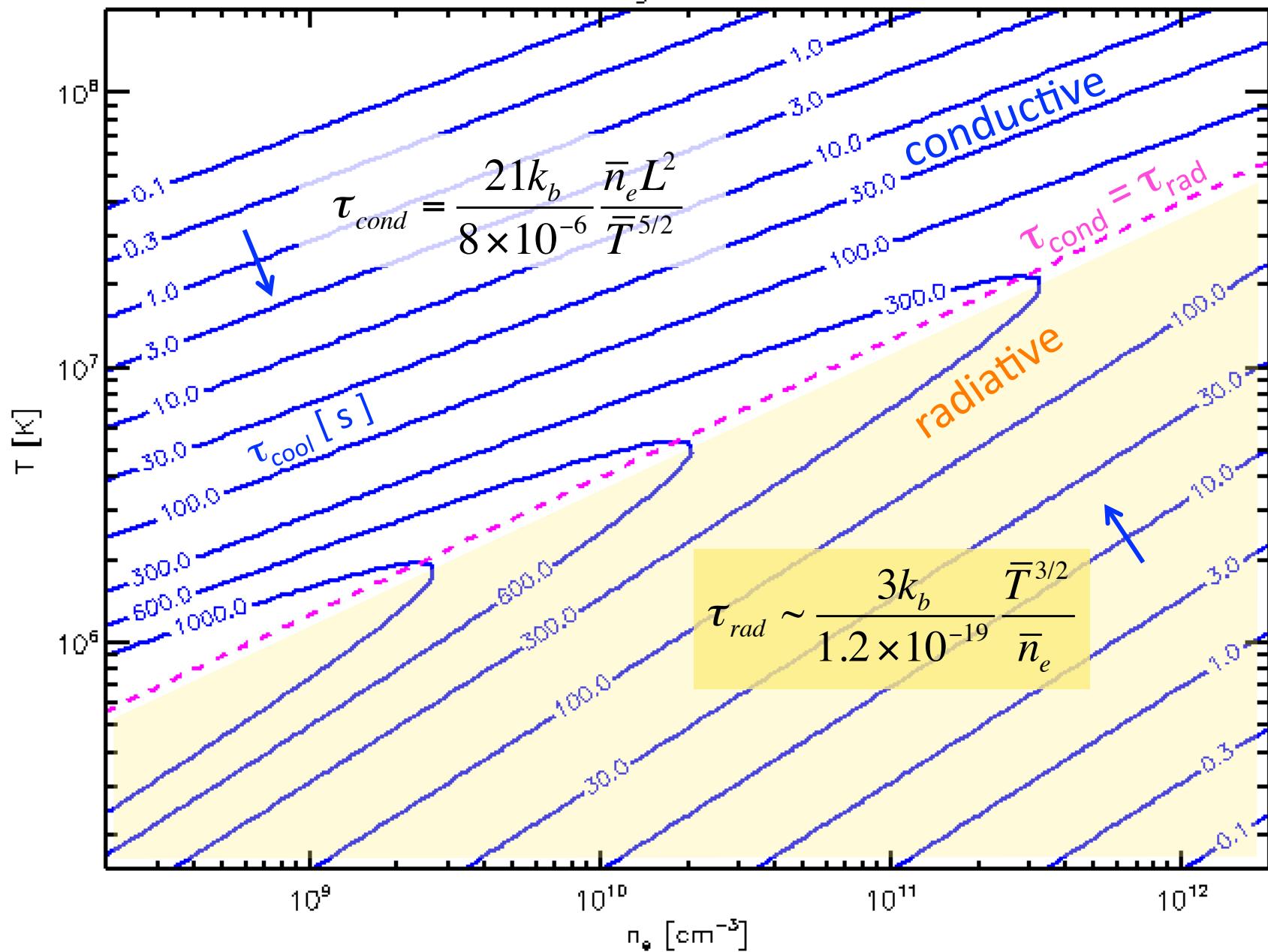
Fully-ionized H plasma

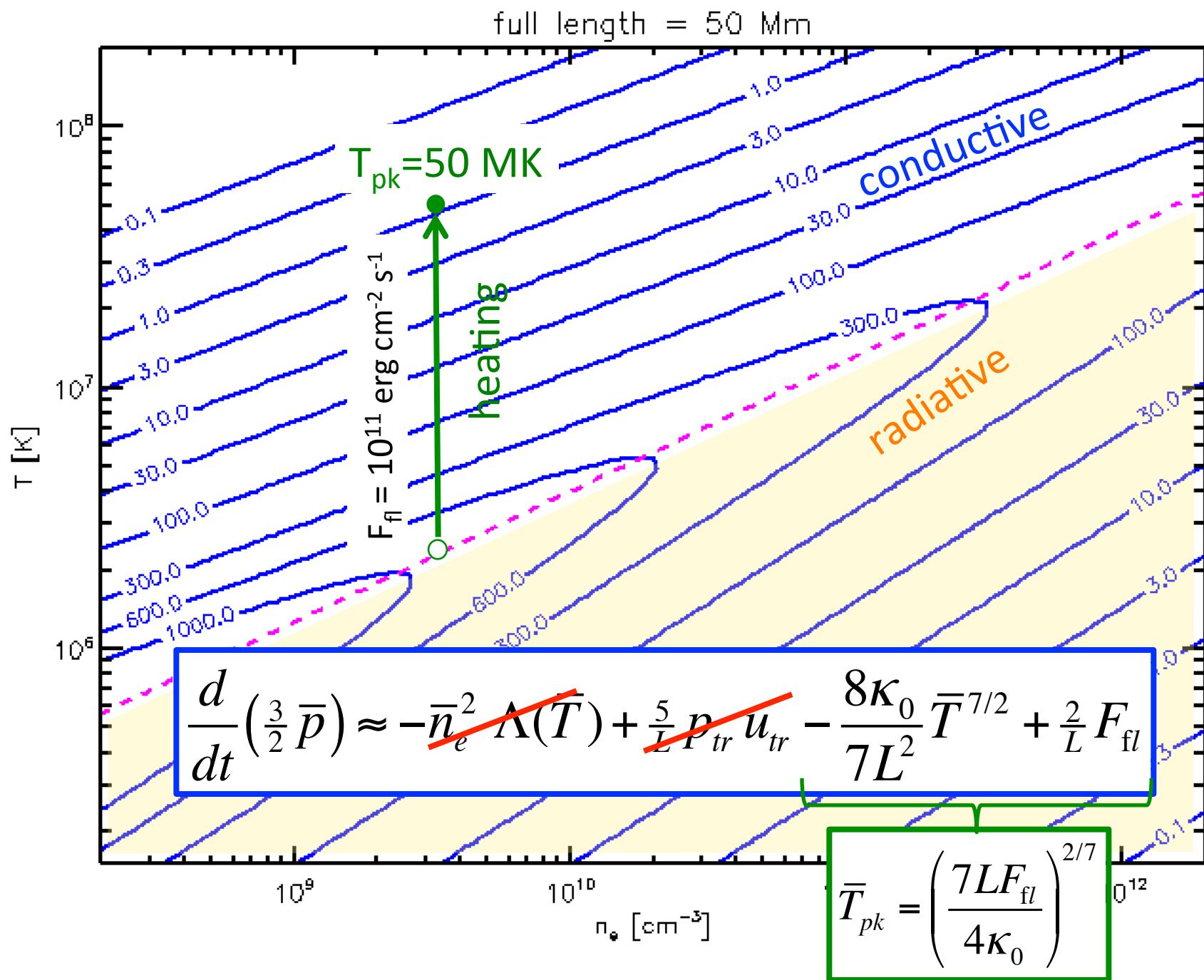
$$\bar{p} = 2\bar{n}_e k_b \bar{T}$$

Cooling rate:

$$\frac{1}{\tau_{cool}} = \frac{1}{\tau_{rad}} + \frac{1}{\tau_{cond}}$$

full length = 50 Mm





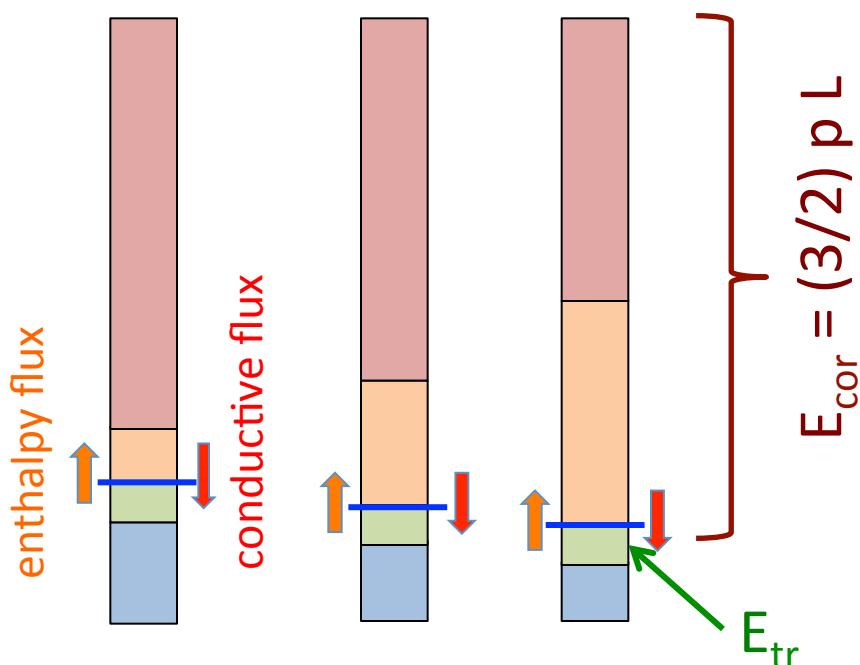
# Evaporation\*:

á la Antiochos &  
Sturrock 1978;  
Cargill *et al.* 1995

$$\frac{d\bar{n}_e}{dt} = \frac{2}{L} n_{e,tr} u_{tr} \quad \text{mass flux increases } n_e$$

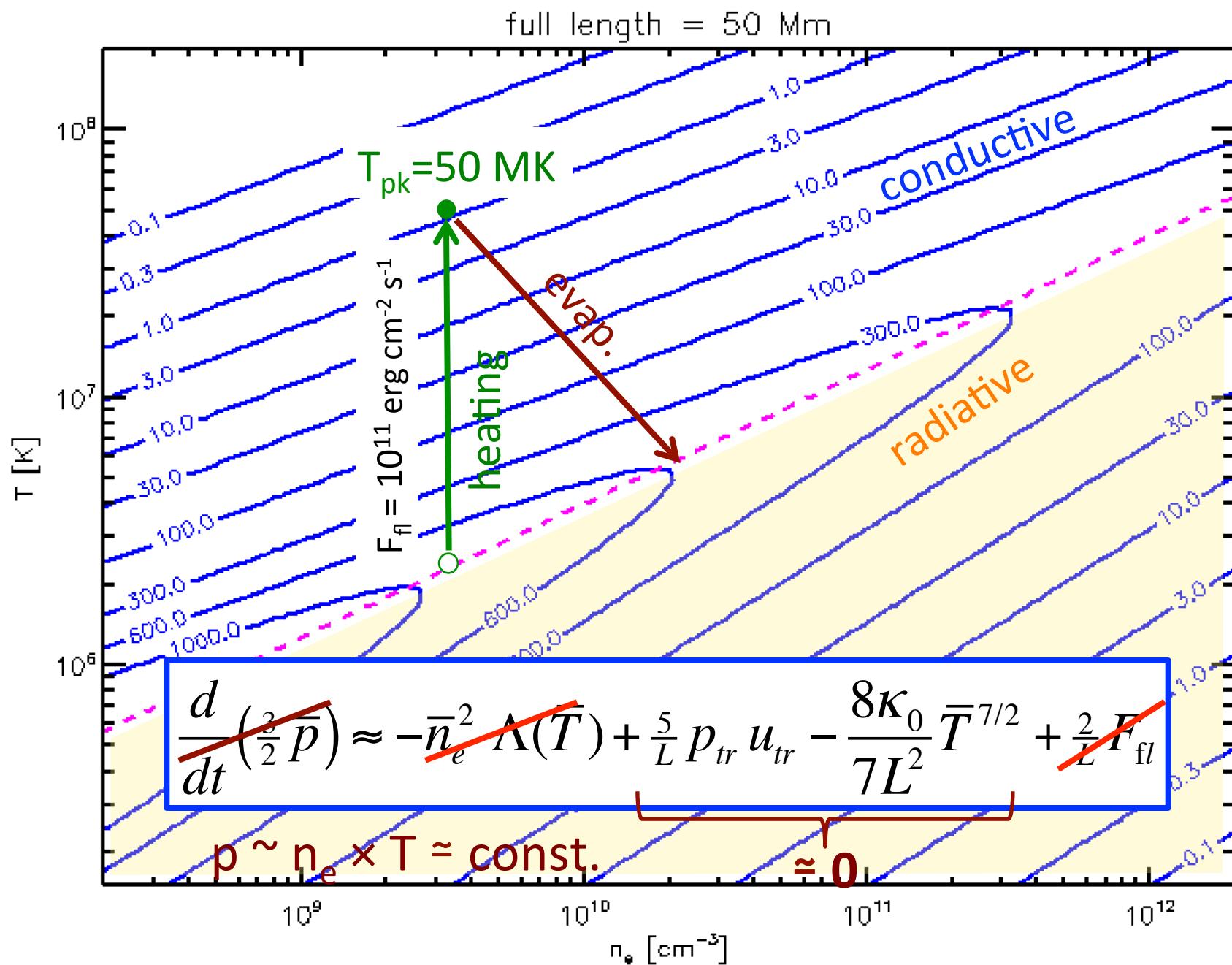
$$\frac{d}{dt} \left( \frac{3}{2} \bar{p} \right) \approx -\bar{n}_e^2 \Lambda(\bar{T}) + \frac{5}{L} p_{tr} u_{tr} - \frac{8K_0}{7L^2} \bar{T}^{7/2} + \frac{2}{L} F_{fl}$$

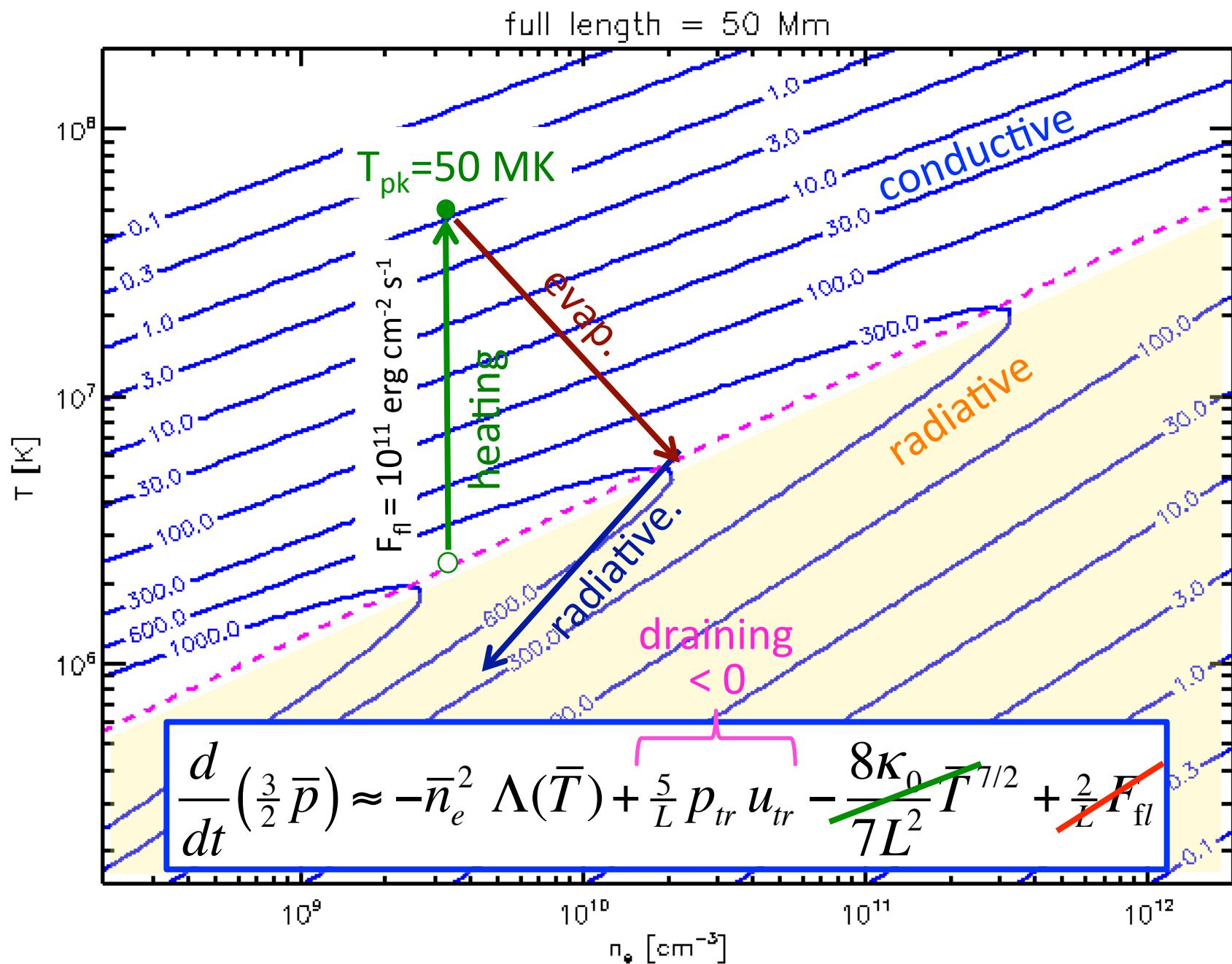
$E_{cor}$



- Heat flows into TR  
– conductive flux:  $F_c$
  - TR expands into corona – enthalpy flux:  $F_e$
  - No change in  $E_{tr}$   
& **no losses (i.e. rad)**
- No change in  $E_{cor}$
- $p \sim n_e \times T = \text{const.}$

\* Historical term based on analogy.  
Not genuine evaporation





# Evaporation:

Antiochos & Sturrock 1978;  
Cargill et al. 1995

$$\frac{d\bar{n}_e}{dt} = \frac{2}{L} u_{tr} n_{e,tr} \approx \frac{2}{L} u_{tr} \bar{n}_e$$

$$\frac{d}{dt} \left( \frac{3}{2} \bar{p} \right) \approx -\bar{n}_e^2 \Lambda(\bar{T}) + \underbrace{\frac{5}{L} p_{tr} u_{tr} - \frac{8K_0}{7L^2} \bar{T}^{7/2}}_{\simeq 0} + \frac{2}{L} F_{fl}$$

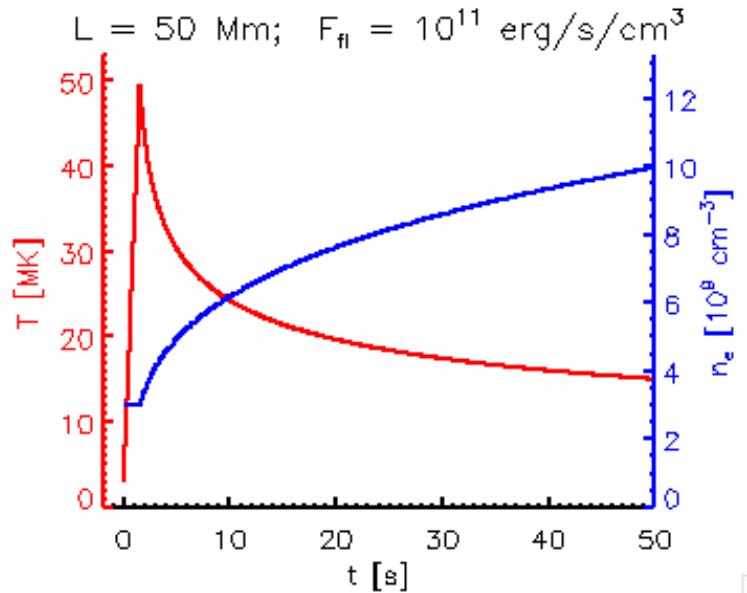
$p \sim n_e \times T \simeq \text{const.}$

$$\frac{5}{L} p_{tr} u_{tr} = \frac{5}{L} p u_{tr} = \frac{8K_0}{7L^2} \bar{T}^{7/2} = \frac{\frac{3}{2} p}{\tau_{c,0}} \left( \frac{\bar{T}}{\bar{T}_0} \right)^{7/2} = \frac{\frac{3}{2} p}{\tau_{c,0}} \left( \frac{\bar{n}_e}{\bar{n}_{e,0}} \right)^{-7/2} \rightarrow \boxed{\frac{2}{L} u_{tr} = \frac{3}{5} \frac{1}{\tau_{c,0}} \left( \frac{\bar{n}_e}{\bar{n}_{e,0}} \right)^{-7/2}}$$

$$\frac{d}{dt} \left( \frac{\bar{n}_e}{\bar{n}_{e,0}} \right) = \frac{\frac{3}{5}}{\tau_{c,0}} \left( \frac{\bar{n}_e}{\bar{n}_{e,0}} \right)^{-5/2} \rightarrow$$

$$\boxed{\bar{n}_e(t) = \bar{n}_{e,0} \left( \frac{21}{10} \frac{t - t_0}{\tau_{c,0}} + 1 \right)^{2/7}}$$

$$\boxed{\bar{T}(t) = \bar{T}_0 \left( \frac{21}{10} \frac{t - t_0}{\tau_{c,0}} + 1 \right)^{-2/7}}$$



# Radiative cooling

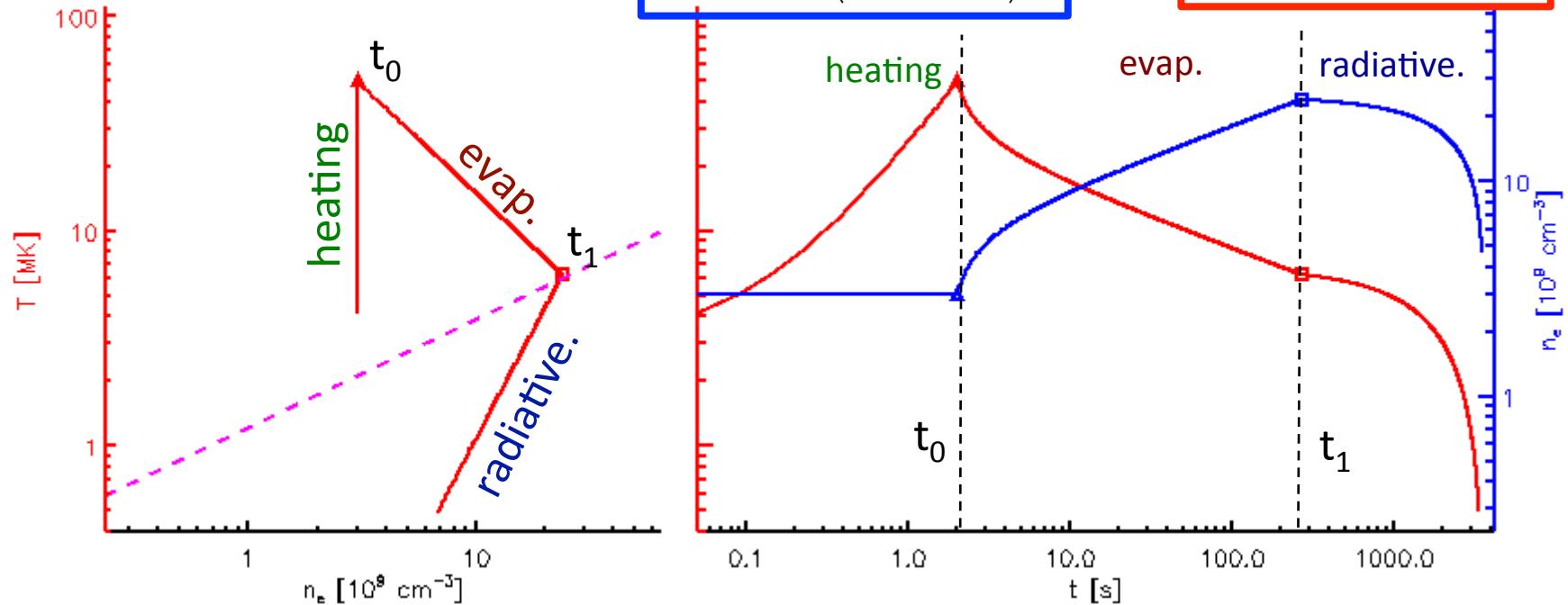
Cargill et al. 1995

$$\frac{d}{dt} \left( \frac{3}{2} \bar{p} \right) \approx -\bar{n}_e^2 \Lambda(\bar{T}) + \cancel{\frac{5}{L} p_{tr} u_{tr}} - \cancel{\frac{8K_0}{7L^2} \bar{T}^{7/2}} + \cancel{\frac{2}{L} F_{fl}}$$

I. draining  
(empirical)

$$\bar{T} \propto \bar{n}_e^2 \rightarrow \bar{p} = 2\bar{n}_e k_b \bar{T} = \bar{p}_1 \left( \frac{\bar{n}_e}{\bar{n}_{e,1}} \right)^3 \quad \tau_{rad} = \tau_{r,1} \left( \frac{\bar{n}_e}{\bar{n}_{e,1}} \right)^{-1} \left( \frac{\bar{T}}{\bar{T}_1} \right)^{3/2} = \tau_{r,1} \left( \frac{\bar{n}_e}{\bar{n}_{e,1}} \right)^2$$

$$3 \left( \frac{\bar{n}_e}{\bar{n}_{e,1}} \right)^2 \frac{d}{dt} \left( \frac{\bar{n}_e}{\bar{n}_{e,1}} \right) = -\frac{1}{\tau_{r,1}} \left( \frac{\bar{n}_e}{\bar{n}_{e,1}} \right) \rightarrow \boxed{\bar{n}_e(t) = \bar{n}_{e,1} \left( 1 - \frac{2}{3} \frac{t - t_1}{\tau_{r,1}} \right)^{1/2}} \rightarrow \boxed{\bar{T}(t) = \bar{T}_1 \left( 1 - \frac{2}{3} \frac{t - t_1}{\tau_{r,1}} \right)}$$

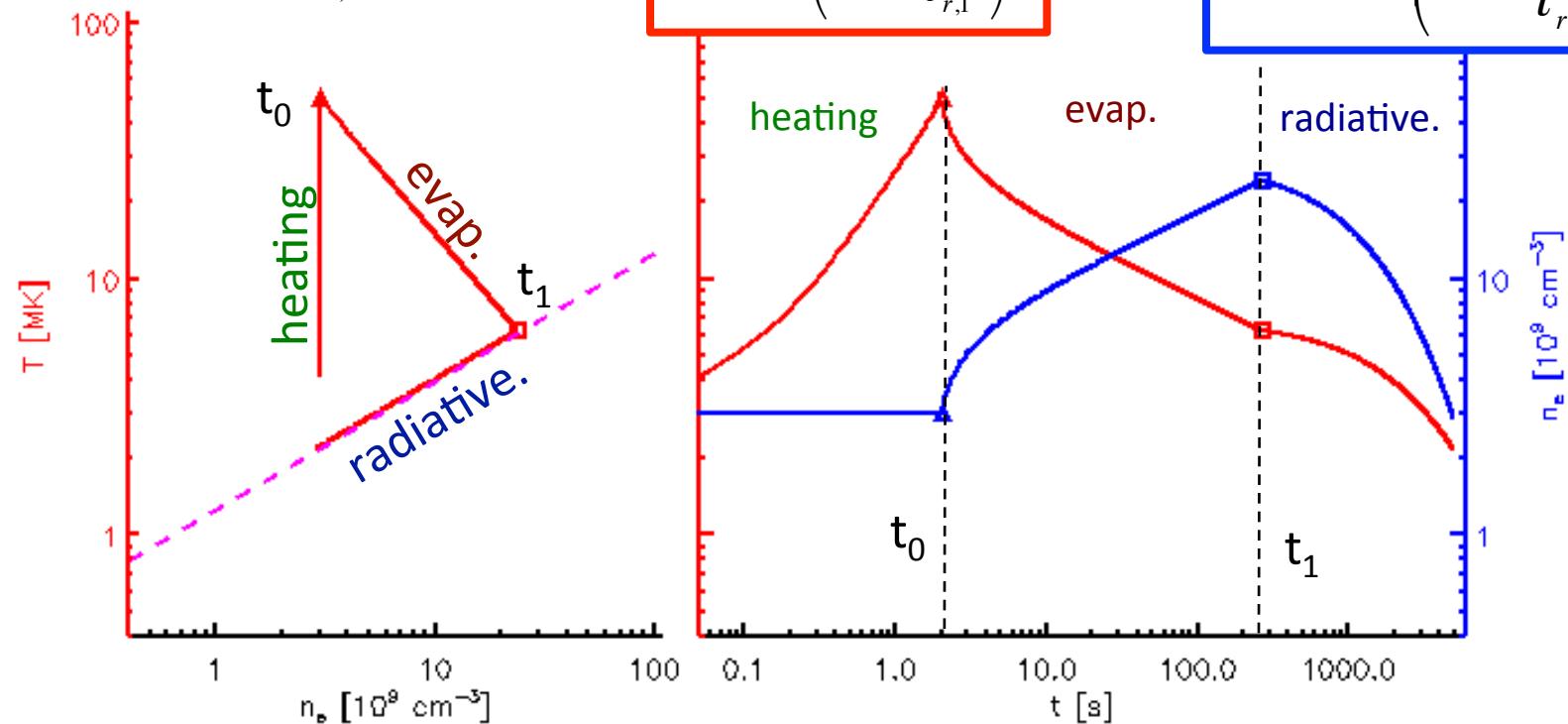


# Radiative cooling

$$\frac{d}{dt} \left( \frac{3}{2} \bar{p} \right) \approx -\bar{n}_e^2 \Lambda(\bar{T}) + \cancel{\frac{5}{L} p_{tr} u_{tr}} - \frac{8K_0}{7L^2} \bar{T}^{7/2} + \cancel{\frac{2}{L} F_{fl}}$$

**II. mechanical equilibrium**  $\bar{T} \propto \bar{n}_e^{1/2}$   $\rightarrow \bar{p} = 2\bar{n}_e k_b \bar{T} = \bar{p}_1 \left( \frac{\bar{T}}{\bar{T}_1} \right)^3$   $\tau_{rad} = \tau_{r,1} \left( \frac{\bar{n}_e}{\bar{n}_{e,1}} \right)^{-1} \left( \frac{\bar{T}}{\bar{T}_1} \right)^{3/2} = \tau_{r,1} \left( \frac{\bar{T}}{\bar{T}_1} \right)^{-1/2}$

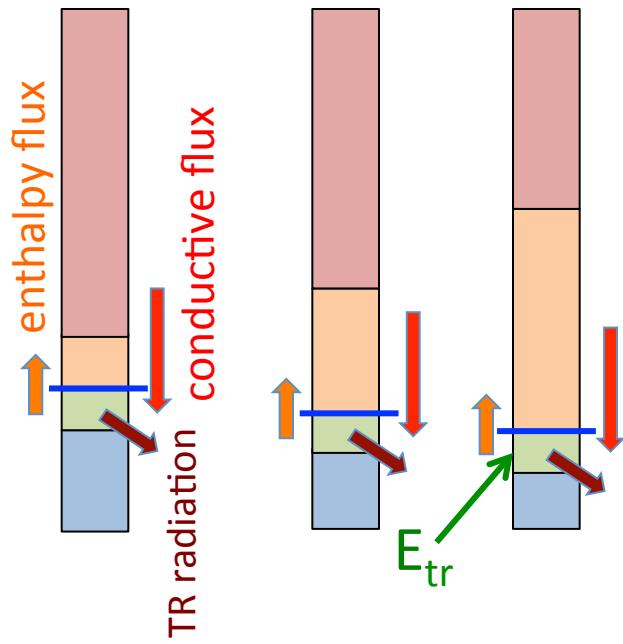
$$3 \left( \frac{\bar{T}}{\bar{T}_1} \right)^2 \frac{d}{dt} \left( \frac{\bar{T}}{\bar{T}_1} \right) = -\frac{2}{\tau_{r,1}} \left( \frac{\bar{T}}{\bar{T}_1} \right)^{7/2} \rightarrow \boxed{\bar{T}(t) = \bar{T}_1 \left( 1 + \frac{1}{3} \frac{t - t_1}{\tau_{r,1}} \right)^{-2}} \rightarrow \boxed{\bar{n}_e(t) = \bar{n}_{e,1} \left( 1 + \frac{1}{3} \frac{t - t_1}{\tau_{r,1}} \right)^4}$$



# Evaporation again:

EBTEL – Klimchuk  
*et al.* 2008

$$\frac{d}{dt} \left( \frac{3}{2} \bar{p} \right) \approx -\underbrace{\bar{n}_e^2 \Lambda(\bar{T})}_{R_{co}} + \underbrace{\frac{5}{L} p_{tr} u_{tr}}_{F_e} - \frac{8K_0}{7L^2} \bar{T}^{7/2} + \frac{2}{L} F_{fl}$$



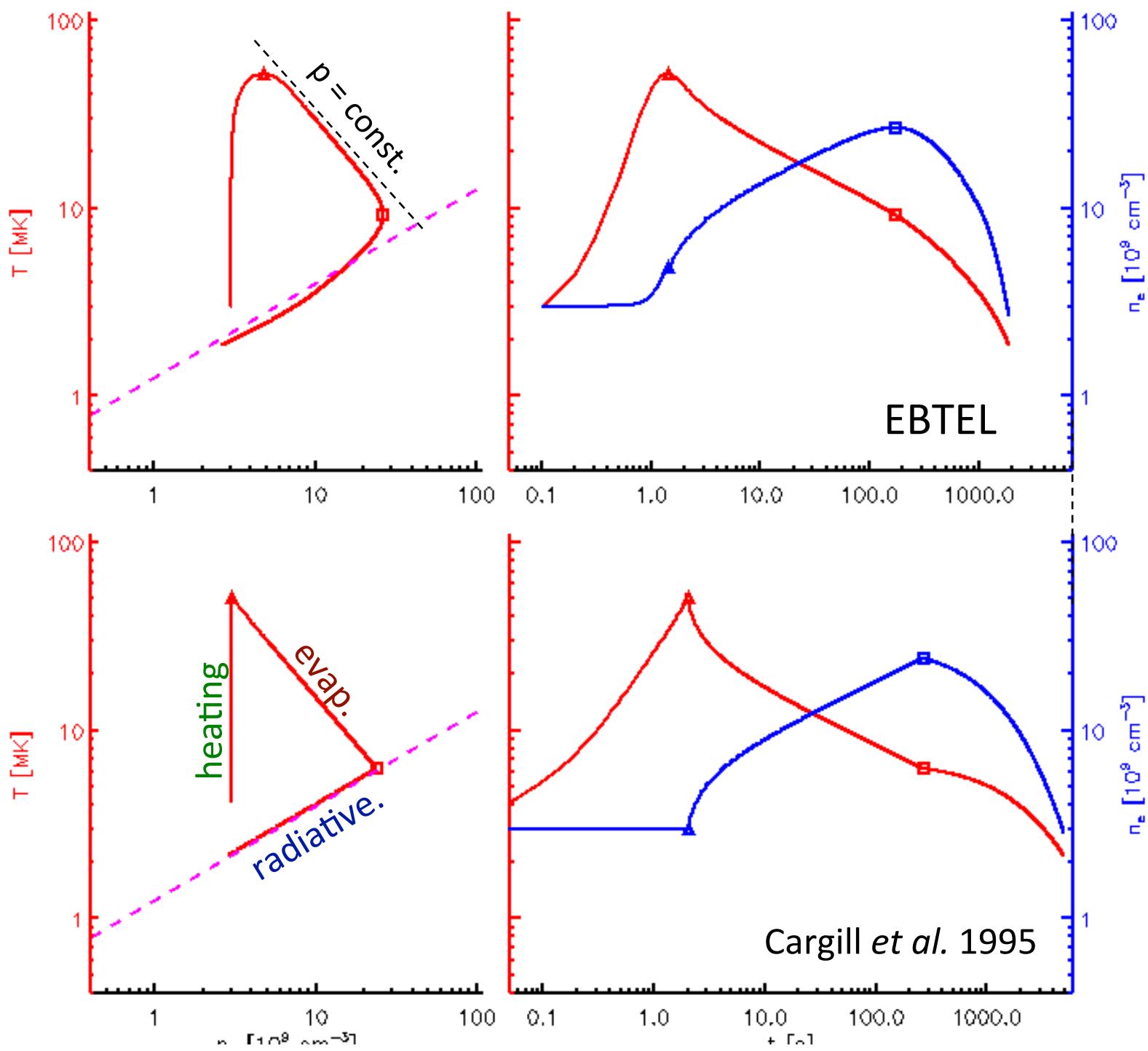
- Heat flows into TR  
– conductive flux:  $F_c$
- TR expands into corona – enthalpy flux:  $F_e$
- TR radiates  $R_{tr} = c_1 R_{co}$
- No change in  $E_{tr}$   
→  $F_e = F_c - R_{tr} = F_c - c_1 R_{co}$

$$\frac{2}{L} u_{tr} = \frac{2}{5\bar{p}} F_e = \frac{2}{5\bar{p}} \left( \frac{8K_0}{7L^2} \bar{T}^{7/2} - c_1 \bar{n}_e^2 \Lambda(\bar{T}) \right)$$

$$\frac{d}{dt} \left( \frac{3}{2} \bar{p} \right) \approx -(1 + c_1) \bar{n}_e^2 \Lambda(\bar{T}) + \frac{2}{L} F_{fl}$$

$$\frac{d\bar{n}_e}{dt} = \frac{2}{L} u_{tr} \bar{n}_e = \frac{1}{5k_b \bar{T}} \left( \frac{8K_0}{7L^2} \bar{T}^{7/2} - c_1 \bar{n}_e^2 \Lambda(\bar{T}) \right)$$

2 eqns. for unknowns  $p(t)$  &  $n_e(t)$  —  $T = p/(2k_b n_e)$



$$\sqrt{\frac{\tau_{rad}}{\tau_{cond}}} = \sqrt{\frac{8 \times 10^{-6}}{7 \times 1.2 \times 10^{-19}}} \frac{\bar{T}^2}{\bar{n}_e L} = \frac{3 \times 10^6}{(2k_b)^2} \frac{\bar{p}^2}{\bar{n}_e^3 L} = 4 \times 10^{37} \frac{\bar{p}^2}{\bar{n}_e^3 L}$$

$$\tau_{cond} = \tau_{rad}$$

$$\bar{n}_e = 3 \times 10^{12} \frac{\bar{p}^{2/3}}{L^{1/3}}$$

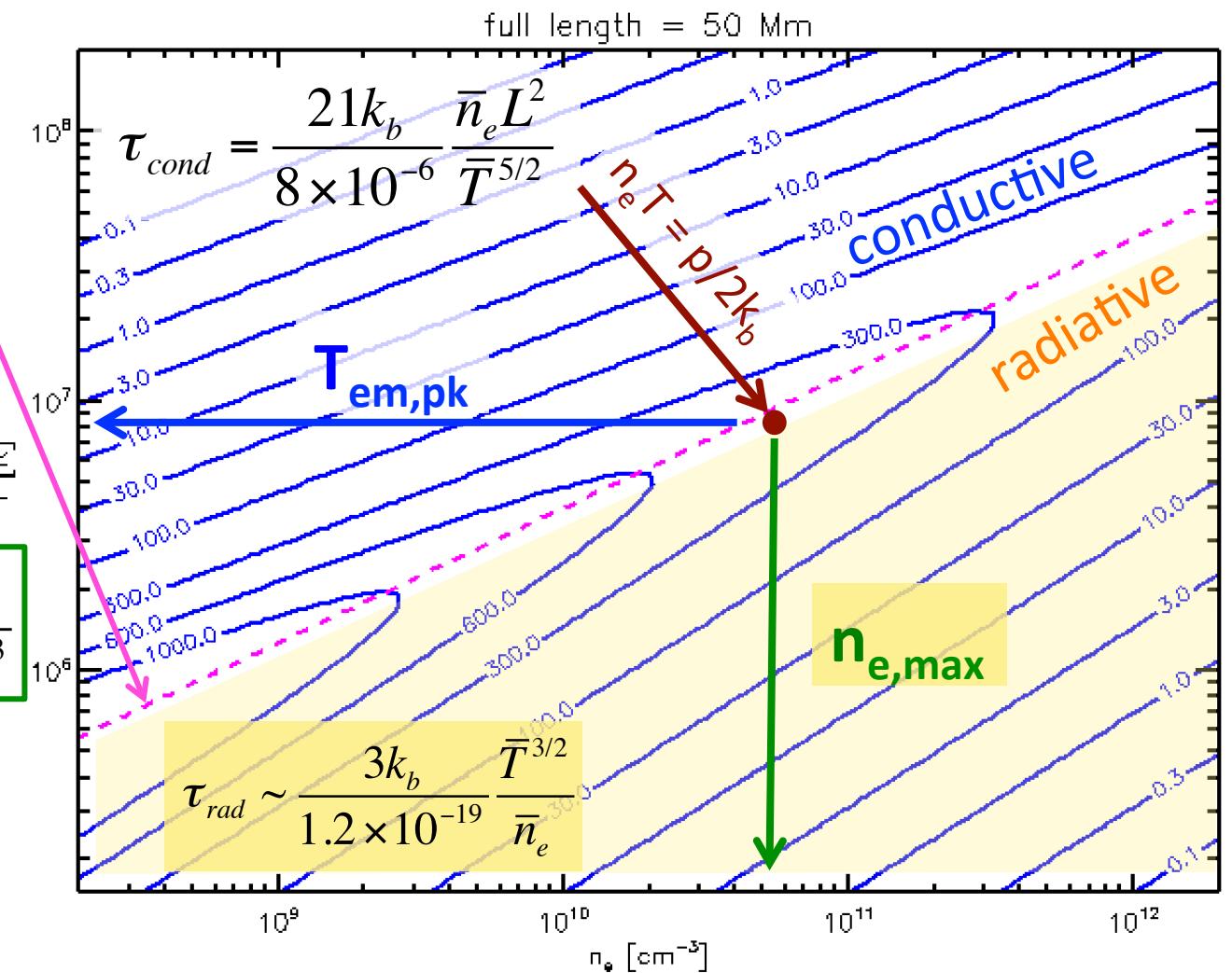
All flare energy, E,  
kept through evap  
phase

$$\bar{p} = \frac{2E}{3V}$$

$$\bar{n}_{e,max} = 2.6 \times 10^{12} \frac{E^{2/3}}{V^{2/3} L^{1/3}}$$

Warren & Antiochos 2004

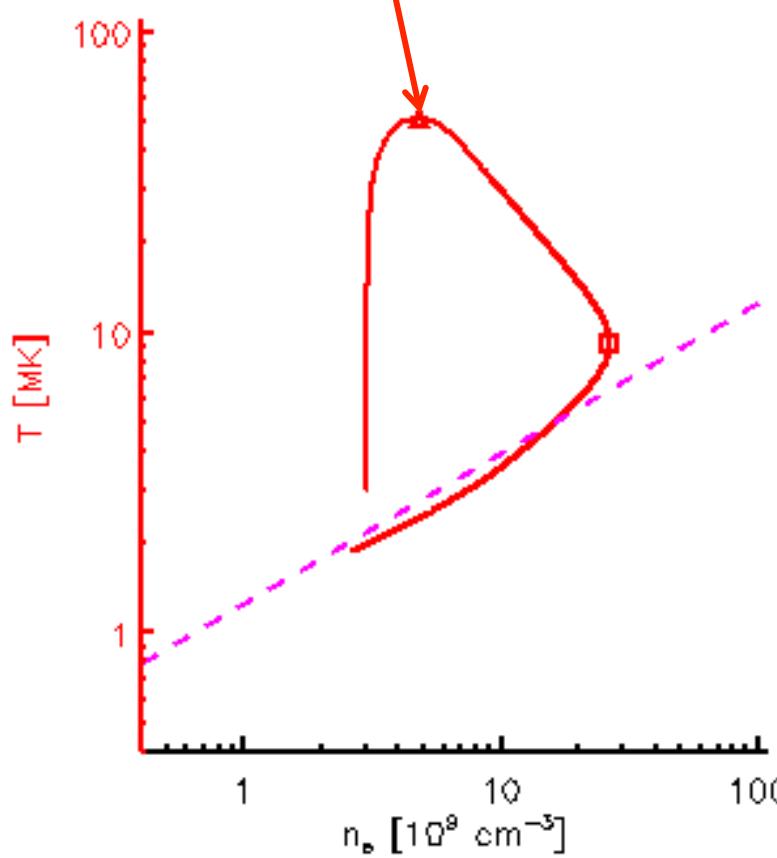
$$\bar{T}_{em,pk} = 930 \left( \frac{EL}{V} \right)^{1/3}$$



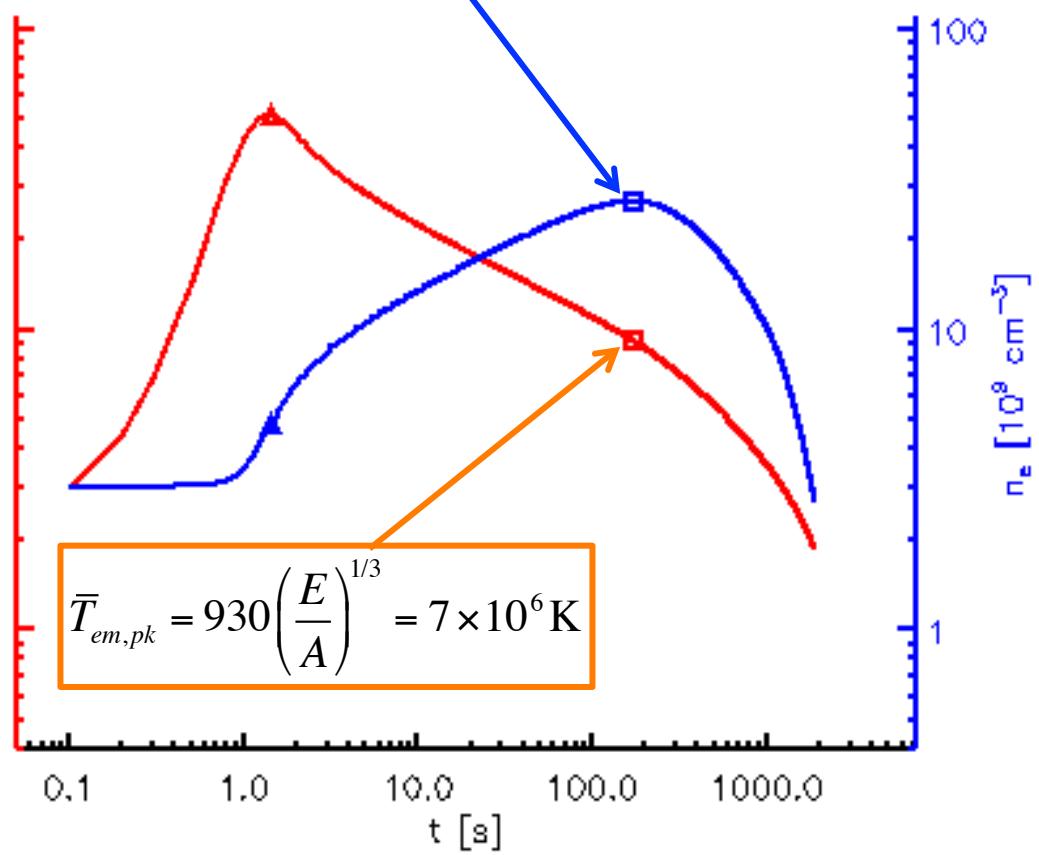
$$F_{fl} = 10^{11} \text{ erg/s/cm}^2 \quad L = 5 \times 10^9 \text{ cm} = 50 \text{ Mm}$$

$$\frac{E}{A} = 2 \int F_{fl} dt = 4 \times 10^{11} \text{ erg cm}^{-2}$$

$$\bar{T}_{pk} = \left( \frac{7LF_{fl}}{4\kappa_0} \right)^{2/7} = 5 \times 10^7 \text{ K}$$



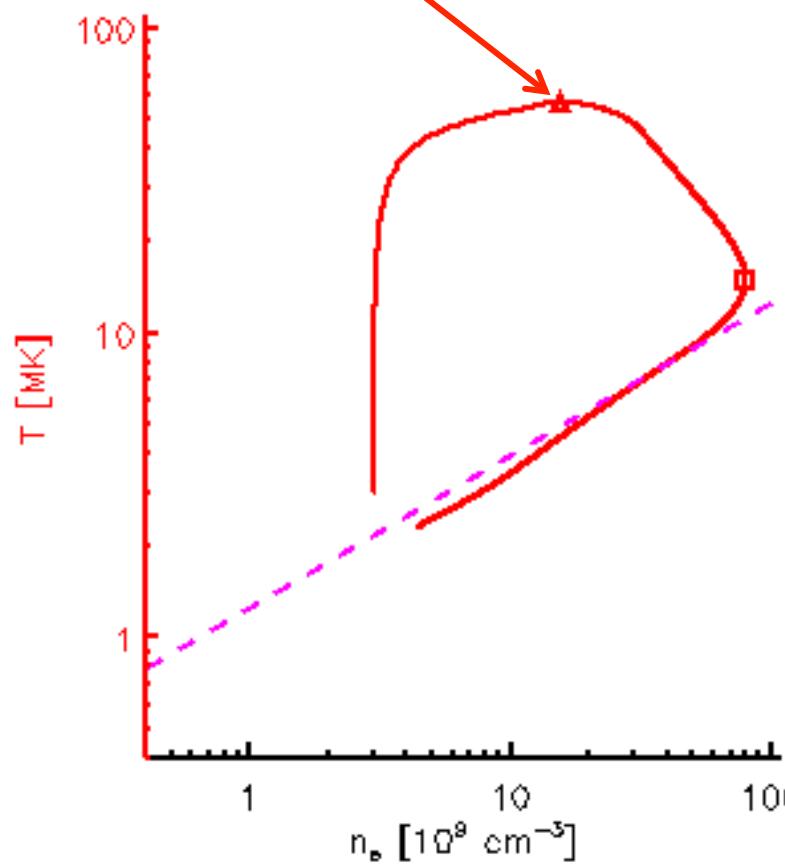
$$\bar{n}_{e,\max} = 2.6 \times 10^{12} \frac{(E / A)^{2/3}}{L} = 3 \times 10^{10} \text{ cm}^{-3}$$



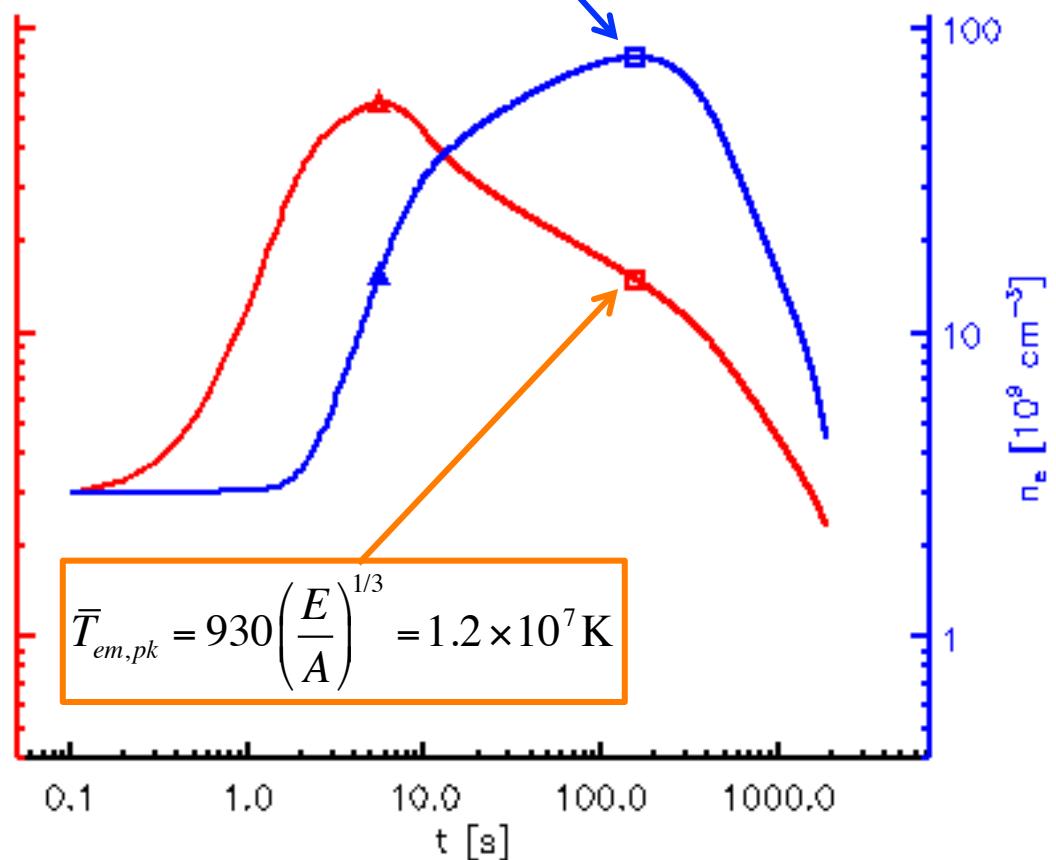
$$F_{fl} = 10^{11} \text{ erg/s/cm}^2 \quad L = 5 \times 10^9 \text{ cm} = 50 \text{ Mm}$$

$$\frac{E}{A} = 2 \int F_{fl} dt = 2 \times 10^{12} \text{ erg cm}^{-2}$$

$$\bar{T}_{pk} = \left( \frac{7LF_{fl}}{4\kappa_0} \right)^{2/7} = 5 \times 10^7 \text{ K}$$



$$\bar{n}_{e,max} = 2.6 \times 10^{12} \frac{(E / A)^{2/3}}{L} = 8 \times 10^{10} \text{ cm}^{-3}$$



$$\bar{T}_{em,pk} = 930 \left( \frac{E}{A} \right)^{1/3} = 1.2 \times 10^7 \text{ K}$$

$$\bar{n}_{e,\max} = 2.6 \times 10^{12} \frac{E^{2/3}}{V^{2/3} L^{1/3}}$$

$$\bar{T}_{em,pk} = 930 \left( \frac{EL}{V} \right)^{1/3}$$

**IF flare were a single loop**

$$\max(EM) = V \bar{n}_{e,\max}^2 = 7 \times 10^{24} \frac{E^{4/3}}{V^{1/3} L^{2/3}} = 7 \times 10^{49} \text{ cm}^3 \frac{E_{30}^{4/3}}{V_{27}^{1/3} L_9^{2/3}}$$

$$\bar{T}_{em,pk} = 930 \left( \frac{EL}{V} \right)^{1/3} = 9 \times 10^6 K \left( \frac{E_{30} L_9}{V_{27}} \right)^{1/3}$$

$E_{30} = E/10^{30} \text{ ergs}$

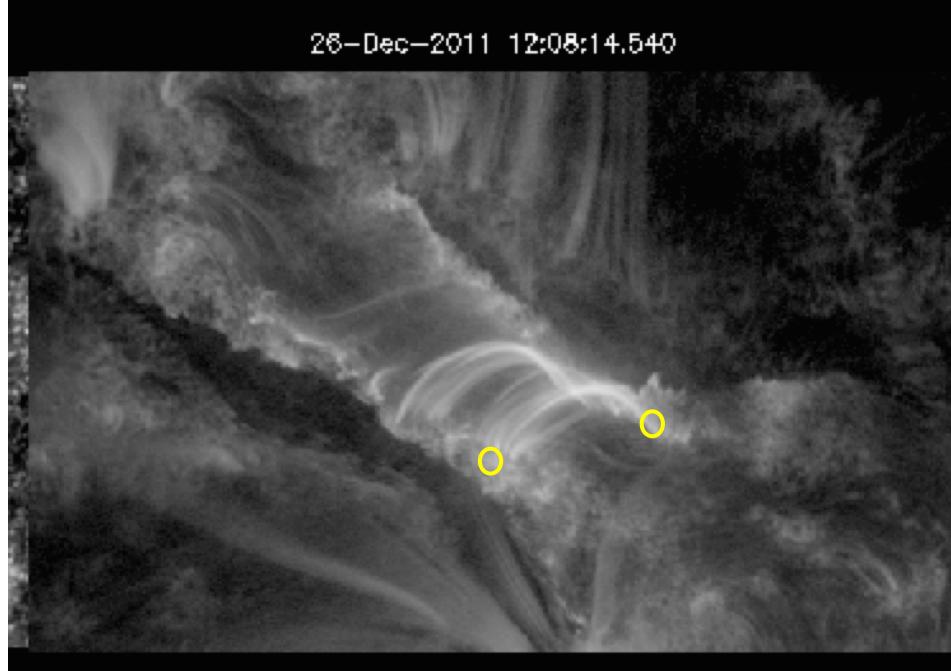
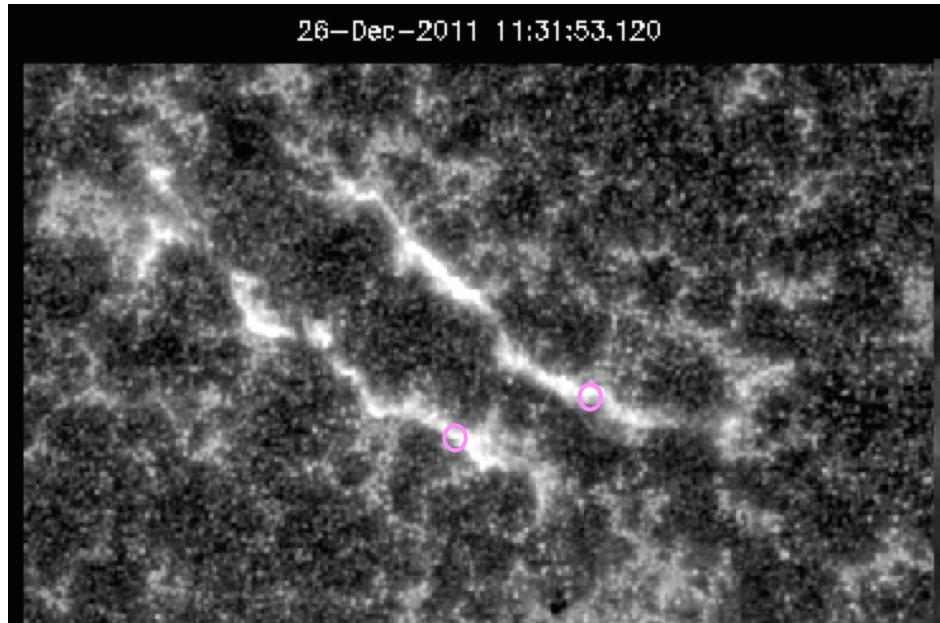
$\sim E^{7/4}$

**GOES peak:**

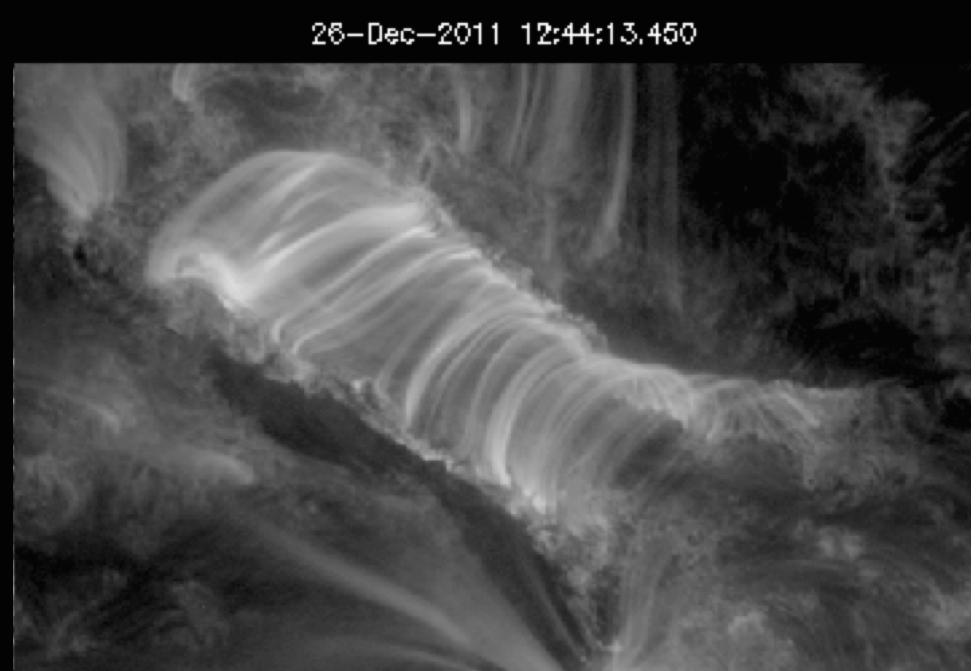
$$F_{1-8} \approx 10^{-63} \frac{\text{W}}{\text{m}^2} EM T^{5/4} = 4 \times 10^{-5} \frac{\text{W}}{\text{m}^2} \cdot \frac{E_{30}^{7/4}}{L_9^{1/4} V_{27}^{3/4}}$$

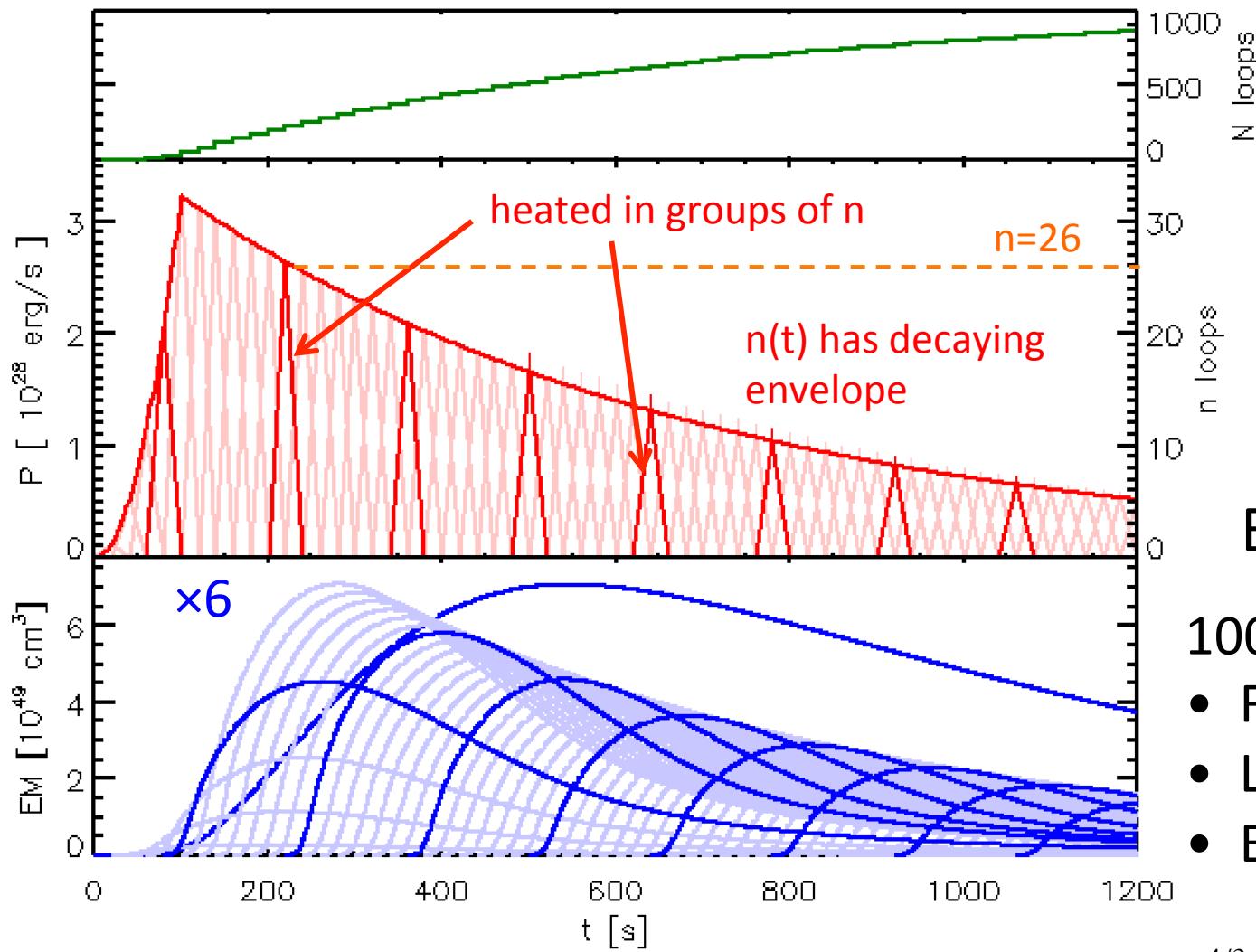
Warren & Antiochos 2004

M4 flare



**BUT** a real flare is  
built from many  
diff. loops –  
each evolving  
independently





## Example model:

Hori et al. 1997, Warren et al. 2002, Reeves & Warren 2002, Warren 2006, Qiu et al. 2012, 2013, ...

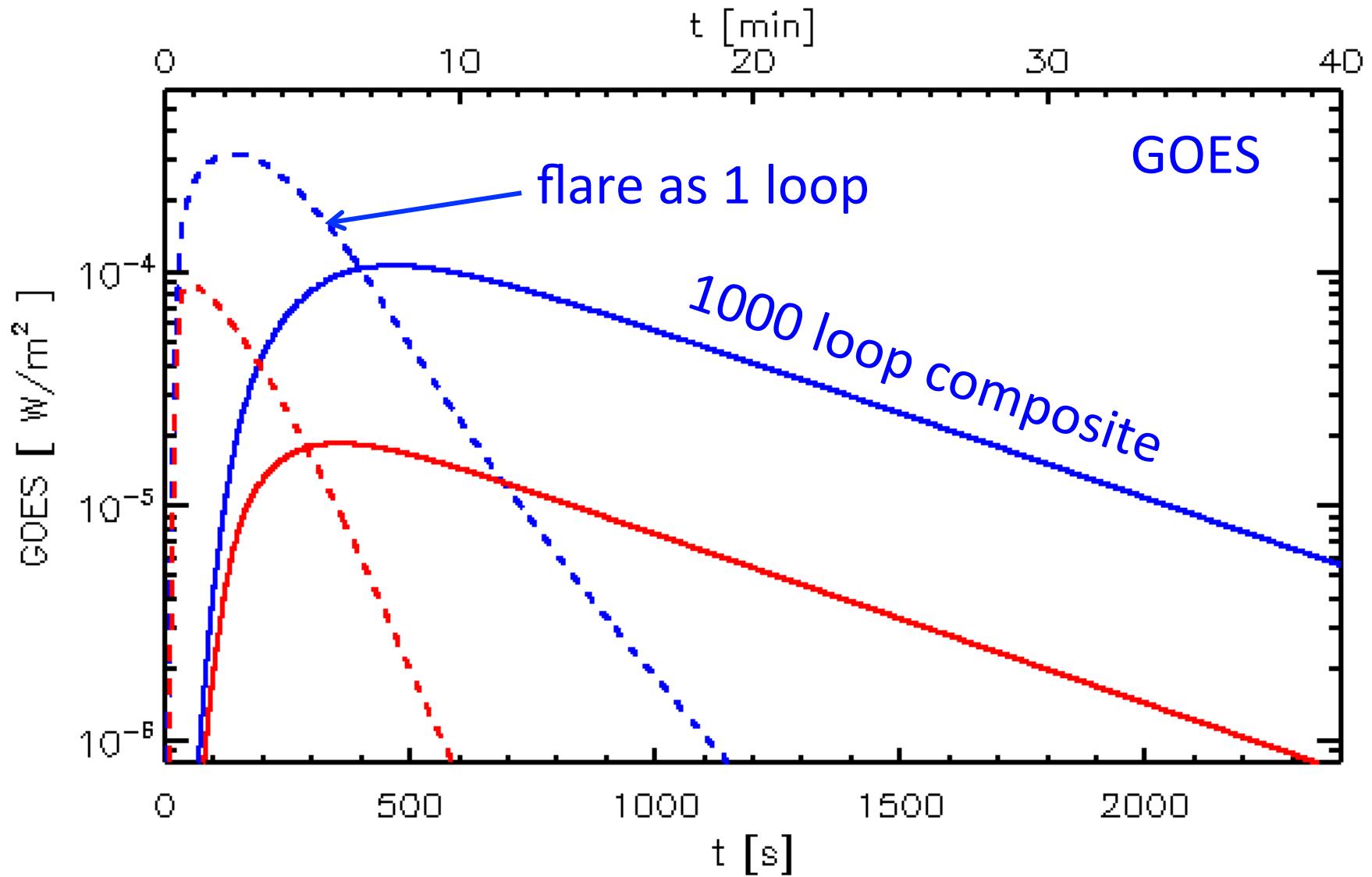
$$E = 2 \times 10^{31} \text{ erg}$$

1000 loops:

- $F_{fl} = 10^{11} \text{ erg/s/cm}^2$
- $L = 5 \times 10^9 \text{ cm}$
- $E_i = 2 \times 10^{28} \text{ erg}$

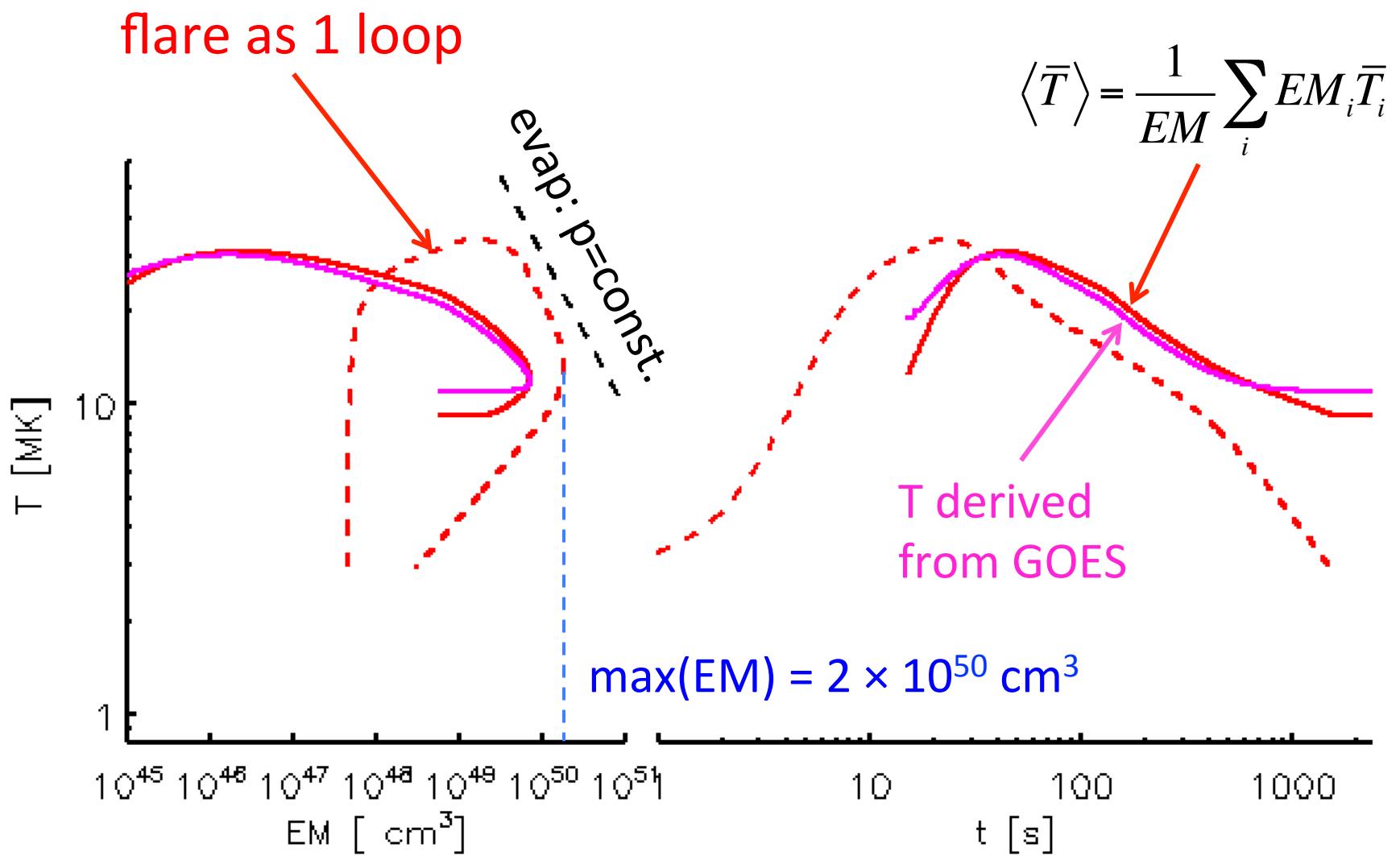
Each loop:  $\max(EM) = 7 \times 10^{49} \text{ cm}^3 \frac{E_{30}^{4/3}}{V_{27}^{1/3} L_9^{2/3}} = 0.03 \times 10^{49} \text{ cm}^3$

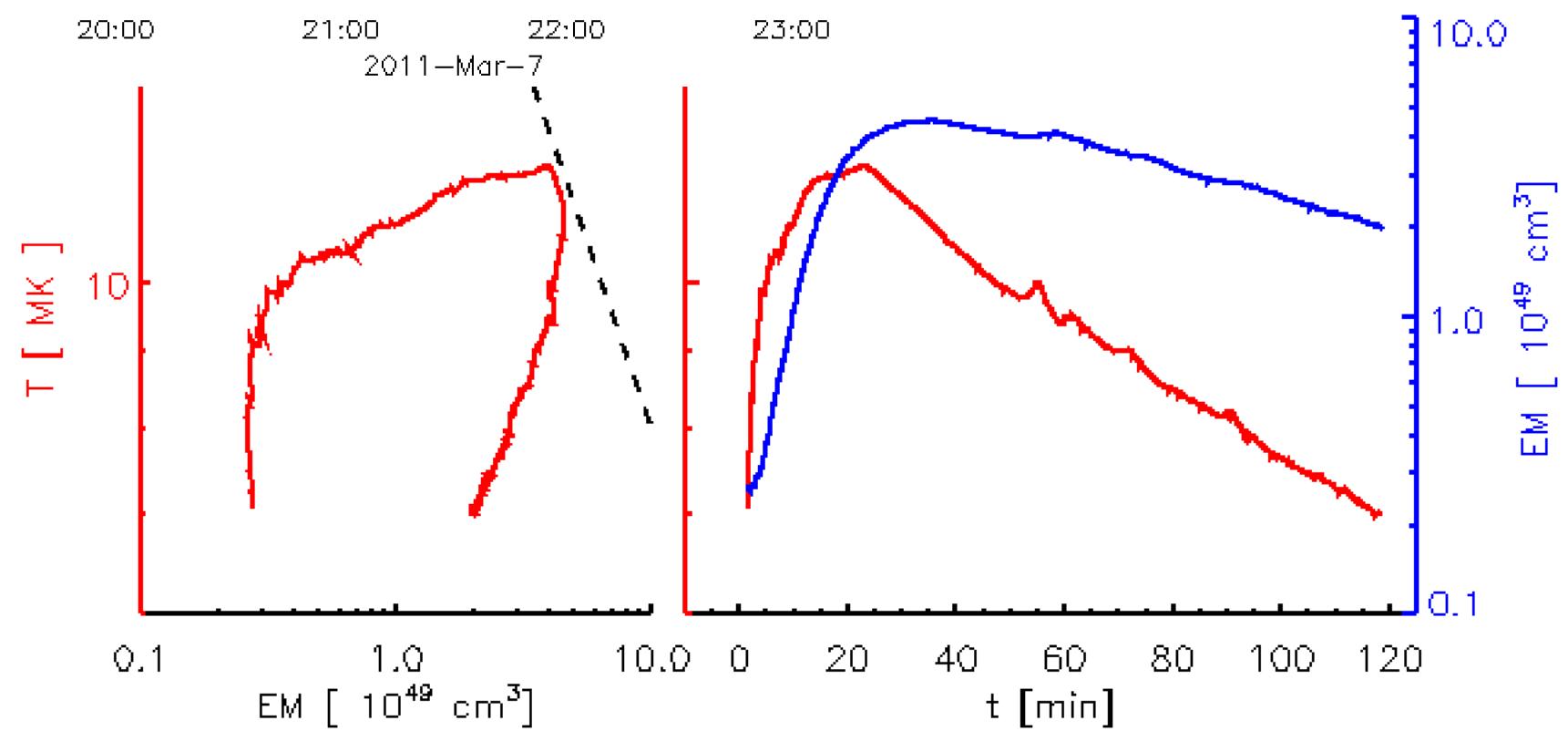
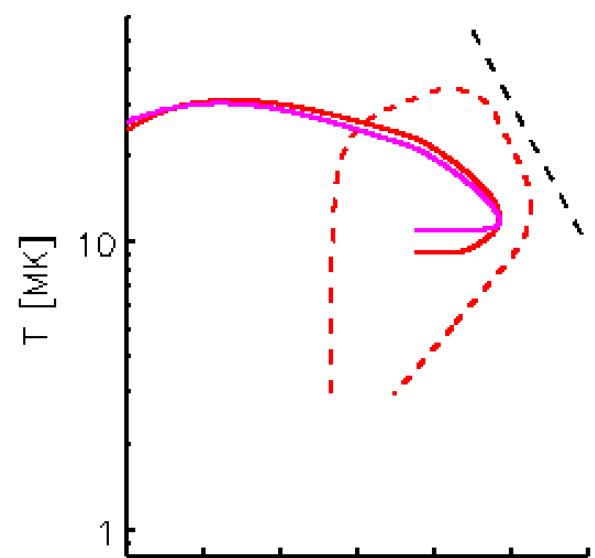
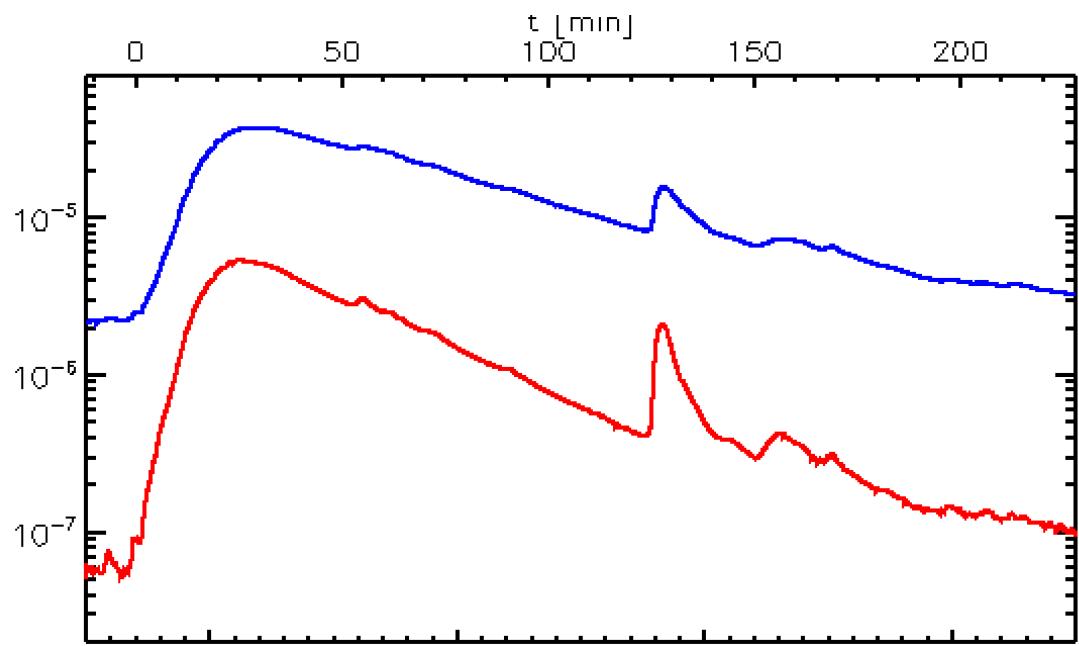
Flare as 1 loop:  $\max(EM) = 7 \times 10^{49} \text{ cm}^3 \frac{E_{30}^{4/3}}{V_{27}^{1/3} L_9^{2/3}} = 30 \times 10^{49} \text{ cm}^3$



Flare as 1 loop:

$$F_{1-8} \approx 4 \times 10^{-5} \frac{\text{W}}{\text{m}^2} \cdot \frac{E_{30}^{7/4}}{L_9^{1/4} V_{27}^{3/4}} = 3 \times 10^{-4} \frac{\text{W}}{\text{m}^2}$$





# Summary

- Evolution following energy release – governed by 1d gas dynamics
- Single loop experiences 3 phases:
  - Heating  $(T \uparrow @ \sim \text{const. } n_e)$
  - Evaporation  $(T \downarrow, n_e \uparrow, p \sim \text{const. or } \downarrow)$
  - Radiative cooling  $(T \downarrow, n_e \downarrow)$
- Real flare may be composite of many loops

**Next time:**

Evolution in one dimension