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Dirac-Fock photoionization parameters for HAXPES applications



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HIGHLIGHTS

- Photoionization parameters are presented in the photon energy range 1.5–10 keV.
- Theoretical data are intended for use in experimental studies by HAXPES spectroscopy.
- Relativistic calculations were performed by the Dirac–Fock method.
- Photoionization cross sections were calculated including all multipoles.
- The angular distribution parameters were obtained in the quadrupole approximation.

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ABSTRACT

Presented here are the photoionization cross sections and parameters of the photoelectron angular distribution for atomic subshells with binding energies lower than 1.5 keV of all elements with $1 \le Z \le 100$ in the photon energy range 1.5–10 keV. The calculations were performed in an effort to provide handy theoretical data for experimental studies by hard X-ray photoelectron spectroscopy (HAXPES). We used the relativistic treatment of atomic photoeffect and the Dirac–Fock method with proper consideration of the electron exchange for computing the electron wave functions. The photoionization cross sections were determined including all multipoles of the radiative field while the photoelectron angular distribution parameters were obtained within the quadrupole approximation. The effect of the hole resulting in the atomic subshell after photoionization was taken into account by the use of the frozen orbital model.

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1. Introduction

Theoretical values of the photoionization cross sections and the photoelectron angular distribution parameters are widely used in traditional X-ray photoelectron spectroscopy. Early extensive calculations [1–3] contain only photoionization cross sections for two photon energies associated with the Al and Mg K_{α} -line energies. More recent calculations include photoionization cross sections along with the dipole angular distribution parameters β [4,5]. Our papers [6–8] include the angular distribution parameters β , γ , and δ obtained within the quadrupole approximation to give an essential correction to photoelectron angular distribution. Calculations [1,2,6–9] were pioneered by academician Vadim I. Nefedov (1937–2008) who was deeply involved in the studies.

The present paper is a revision and extension of the calculations to provide theoretical data required for handling of data obtained by methods of the hard X-ray photoelectron spectroscopy (HAXPES). The HAXPES spectroscopy is a powerful technique for the investigation of bulk electron structure of functional materials [10] and their interfaces [11]. In particular, it was applied for investigation of the electron structure of magnetic semiconductors [12] and strongly correlated materials [13]. Investigations in this new energy region revealed some new effects in behavior of intensities of the main [14] and satellite photoelectron lines [15,16]. HAXPES is also intended for study of the valence-band density of the material buried layers because of the large analysis depth (see [11] and references therein). Theoretical photoionization parameters are required for the interpretation of HAXPES data [15]. Our previous calculations [6,7] were performed for the kinetic electron energies $E_k \leq 5$ keV what is not cover modern energy region of HAXPES spectroscopy which extends to 7 keV [13] and even to 9 keV [15].

In Table 1, we present calculations in the photon energy range 1.5 keV $\leq k \leq$ 10 keV for all elements with atomic numbers $1 \leq Z \leq$ 100. The comparatively outer atomic shells with binding energies less than 1.5 keV are taken into consideration. Although the method of calculations has been described before [6,8], we will remind below basic assumptions which provide the foundation for the calculations and will give basic expressions for the sake of convenience.

The main advantage of the present calculations over previous ones lies in the fact that electron wave functions are calculated using the Dirac–Fock (DF) method where the electron exchange interaction is considered exactly between bound electrons as well as between bound and free electrons. Previous calculations [1–9] were performed with the Dirac–Slater (DS) method where the electron exchange was considered approximately. Adequate calculations of electron wave functions may be essential for outer shells and for low photoelectron energies. As in papers [6,7], the subshell photoionization cross sections were calculated including all multipoles of the radiative field while the photoelectron angular

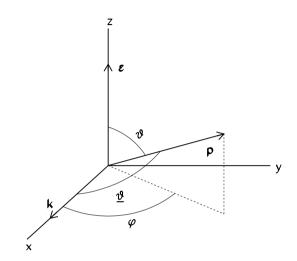


Fig. 1. Notations of angles and directions: ${\bf k}$ is the photon momentum vector; ${\bf p}$ is the direction of the photoelectron; ε is the photon polarization vector; $\underline{\theta}$ is the angle between vectors ${\bf k}$ and ${\bf p}$; θ is the angle between ${\bf p}$ and ε ; and φ is the angle between ${\bf k}$ and the plane passing through ${\bf p}$ and ε .

distribution parameters were obtained in the quadrupole approximation.

2. Basic formulas and method of calculation

The calculations were carried out for a free atom in the oneelectron approximation. The fully relativistic formalism was used in the photoeffect studies. The relativistic treatment leads to the following expressions for the differential cross section in the *i*th atomic subshell for unpolarized and circularly polarized radiation:

$$\frac{d\sigma_i}{d\Omega}(\underline{\theta}) = \frac{\sigma_i}{4\pi} \sum_n B_n P_n(\cos\underline{\theta}). \tag{1}$$

Here $P_n(\cos \underline{\theta})$ is the Legendre polynomial, $\underline{\theta}$ is the angle between the vectors of photon and photoelectron propagation. Angle designations are given in Fig. 1.

In Eq. (1), the total photoionization cross section σ_i for the *i*th subshell is written as

$$\sigma_{i} = \frac{4\pi^{2}\alpha}{k} \sum_{L} \sum_{\kappa} (2L+1)[Q_{LL}(\kappa)]^{2} + L[Q_{L+1L}(\kappa)]^{2} + (L+1)[Q_{L-1L}(\kappa)]^{2} - 2\sqrt{L(L+1)} Q_{L-1L}(\kappa)Q_{L+1L}(\kappa),$$
 (2)

the coefficient $B_0 = 1$, and coefficients B_n for $n \ge 1$ are given by

$$B_{n} = \frac{4\pi^{2}\alpha}{k\sigma_{i}} \sum_{L_{1}L_{2}} \sum_{\kappa_{1}\kappa_{2}} \sum_{\Lambda_{1}\Lambda_{2}} (-1)^{j_{1}+j_{2}+L_{1}+L_{2}+\Lambda_{1}+\Lambda_{2}+j_{i}+1/2} e^{i(\delta_{\kappa_{1}}-\delta_{\kappa_{2}})}$$

$$\times \frac{1+(-1)^{\ell_{1}+\ell_{2}+n}}{2} \cdot \frac{1+(-1)^{\ell_{1}+\Lambda_{1}+\ell_{i}+1}}{2}$$

$$\frac{1 + (-1)^{\ell_{2} + \Lambda_{2} + \ell_{i} + 1}}{2} \cdot i^{\Lambda_{1} - \Lambda_{2}} \times [j_{1}j_{2}\Lambda_{1}\Lambda_{2}]^{\frac{1}{2}} [nL_{1}L_{2}] \begin{pmatrix} j_{1} & j_{2} & n \\ 1/2 & -1/2 & 0 \end{pmatrix} \begin{pmatrix} L_{1} & L_{2} & n \\ q & -q & 0 \end{pmatrix} \times \begin{pmatrix} \Lambda_{1} & 1 & L_{1} \\ 0 & q & -q \end{pmatrix} \begin{pmatrix} \Lambda_{2} & 1 & L_{2} \\ 0 & q & -q \end{pmatrix} \begin{bmatrix} L_{1} & L_{2} & n \\ j_{2} & j_{1} & j_{i} \end{bmatrix} \times Q_{\Lambda_{1}L_{1}}(\kappa_{1})Q_{\Lambda_{2}L_{2}}(\kappa_{2}). \tag{3}$$

All formulas are presented in relativistic units, in which the Compton wavelength \hbar/m_0c is defined as the unit of length, and the electron rest mass m_0c^2 is the unit of energy. In Eqs. (2) and (3), k is the photon energy, L is the multipolarity of the radiative field, $\kappa=(\ell-j)(2j+1)$ is the relativistic quantum number, ℓ and ℓ are quantum numbers of the orbital and total angular momenta of the electron, ℓ is the fine-structure constant, $(\delta_{\kappa_1}-\delta_{\kappa_2})$ is the corresponding phase shift for two final continuum states characterized by κ_1 and κ_2 , ℓ = ℓ 1. We use the conventional notation [ℓ 1] for the expression (ℓ 2 ℓ 1). The reduced matrix element ℓ 3 ℓ 1 has the form

$$Q_{\Lambda L}(\kappa) = (-1)^{\bar{\ell}_{\kappa} - \ell_{i}} \left[\bar{\ell}_{\kappa} \ell_{i} j_{\kappa} j_{i} \Lambda 1 \right]^{1/2} \begin{pmatrix} \bar{\ell}_{\kappa} & \ell_{i} & \Lambda \\ 0 & 0 & 0 \end{pmatrix} \times \begin{cases} \bar{\ell}_{\kappa} & 1/2 & j_{\kappa} \\ \ell_{i} & 1/2 & j_{i} \\ \Lambda & 1 & L \end{cases} R_{1\Lambda} + (-1)^{\ell_{\kappa} - \bar{\ell}_{i}} \left[\ell_{\kappa} \bar{\ell}_{i} j_{\kappa} j_{i} \Lambda 1 \right]^{1/2} \begin{pmatrix} \ell_{\kappa} & \bar{\ell}_{i} & \Lambda \\ 0 & 0 & 0 \end{pmatrix} \times \begin{cases} \ell_{\kappa} & 1/2 & j_{\kappa} \\ \bar{\ell}_{i} & 1/2 & j_{i} \\ \Lambda & 1 & L \end{cases} R_{2\Lambda},$$
(4)

where $\bar{\ell}=2j-\ell$. The radial integrals $R_{1\varLambda}$ and $R_{2\varLambda}$ are written as

$$R_{1A} = \int_0^\infty G_i(r) F_{\kappa}(r) j_A(kr) dr,$$

$$R_{2A} = \int_0^\infty F_i(r) G_{\kappa}(r) j_A(kr) dr.$$
(5)

Here $j_{\Lambda}(kr)$ is the spherical Bessel function of order Λ , G(r) = rg(r) and F(r) = rf(r) are the large and small components of the Dirac radial electron wave function. Indices i and κ refer to bound and continuum states, respectively.

It was shown in paper [17] that at the moderately high photon energy, the photoelectron angular distribution is adequately described by simple expressions involving three parameters β , γ , and δ where β is the dipole parameter while γ and δ are non-dipole parameters associated with the terms of the first order O(kr) where r is the radius of the ionized atomic shell. In the case of circular polarized and unpolarized photons, the relevant equation is written as

$$\frac{d\sigma_i}{d\Omega} = \frac{\sigma_i}{4\pi} \left[1 - \frac{\beta}{2} P_2(\cos\underline{\theta}) + \left(\frac{\gamma}{2} \sin^2\underline{\theta} + \delta \right) \cos\underline{\theta} \right],\tag{6}$$

where $P_2(\cos \theta)$ is the second order Legendre polynomial.

For linear polarized photons, the angular distribution may be represented by the equation involving the same three parameters

$$\frac{d\sigma_i}{d\Omega} = \frac{\sigma_i}{4\pi} \left[1 + \beta P_2(\cos\theta) + (\delta + \gamma \cos^2\theta) \sin\theta \cos\varphi \right], \tag{7}$$

where θ is the angle between the vector \mathbf{p} and the photon polarization direction $\boldsymbol{\varepsilon}$, vector $\boldsymbol{\varepsilon}$ being coincident with the z axis; $\boldsymbol{\varphi}$ is the angle between the vector \mathbf{k} and the plane going through the z axis and the vector \mathbf{p} (see Fig. 1). Non-dipole asymmetry of the angular distribution for the case of the partially linear polarized photons

is described by the same photoionization parameters σ_i , β , γ , and δ [18].

Parameters β , γ , and δ are related with coefficients $B_n^{(q)}$, n=1,2,3 (Eq. (3)) obtained in the quadrupole approximation as follows:

$$\beta = -2B_2^{(q)}, \quad \gamma = -5B_3^{(q)}, \quad \delta = B_1^{(q)} + B_3^{(q)}.$$
 (8)

The coefficients $B_n^{(q)}$ may be expressed in the explicit form:

$$\begin{split} B_{1}^{(q)} &= \sum_{\kappa_{1}\kappa_{2}} A_{1} \left\{ 3\sqrt{6} \left\{ \begin{matrix} 1 & 1 & 1 \\ j_{2} & j_{1} & j_{1} \end{matrix} \right\} \right[\sqrt{2}Q_{01}(\kappa_{1})Q_{11}(\kappa_{2}) \\ &+ Q_{11}(\kappa_{1})Q_{21}(\kappa_{2}) \right] \\ &- 3\sqrt{2} \left\{ \begin{matrix} 1 & 2 & 1 \\ j_{2} & j_{1} & j_{1} \end{matrix} \right] \left[Q_{01}(\kappa_{1})[\sqrt{6}Q_{12}(\kappa_{2}) - 2Q_{32}(\kappa_{2})] \\ &+ \sqrt{15}Q_{11}(\kappa_{1})Q_{22}(\kappa_{2}) - Q_{21}(\kappa_{1})[\sqrt{3}Q_{12}(\kappa_{2}) \\ &- \sqrt{2}Q_{32}(\kappa_{2})] \right] \\ &- 5 \left\{ \begin{matrix} 2 & 2 & 1 \\ j_{2} & j_{1} & j_{1} \end{matrix} \right] \left[\sqrt{6}Q_{12}(\kappa_{1})Q_{22}(\kappa_{2}) \\ &+ 2Q_{22}(\kappa_{1})Q_{32}(\kappa_{2}) \right] \right\}, \end{split} \tag{9} \\ B_{2}^{(q)} &= \sum_{\kappa_{1}\kappa_{2}} A_{2} \left\{ \sqrt{\frac{3}{2}} \left\{ \begin{matrix} 1 & 1 & 2 \\ j_{2} & j_{1} & j_{1} \end{matrix} \right\} \left[2Q_{01}(\kappa_{1})[-Q_{01}(\kappa_{2}) \\ &+ \sqrt{2}Q_{21}(\kappa_{2}) \right] \\ &- 3Q_{11}(\kappa_{1})Q_{11}(\kappa_{2}) - Q_{21}(\kappa_{1})Q_{21}(\kappa_{2}) \right] \\ &- \sqrt{30} \left\{ \begin{matrix} 1 & 2 & 2 \\ j_{2} & j_{1} & j_{1} \end{matrix} \right\} \left[\sqrt{10}Q_{01}(\kappa_{1})Q_{22}(\kappa_{2}) \\ &- Q_{11}(\kappa_{1})[3Q_{12}(\kappa_{2}) - \sqrt{6}Q_{32}(\kappa_{2})] \\ &- \sqrt{5}Q_{21}(\kappa_{1})Q_{22}(\kappa_{2}) \right] - \frac{5}{\sqrt{14}} \left\{ \begin{matrix} 1 & 2 & 2 \\ j_{2} & j_{1} & j_{1} \end{matrix} \right\} \\ &\times \left[Q_{12}(\kappa_{1})[3Q_{12}(\kappa_{2}) - 2\sqrt{6}Q_{32}(\kappa_{2})] \\ &+ 5Q_{22}(\kappa_{1})Q_{22}(\kappa_{2}) + 2Q_{32}(\kappa_{1})Q_{32}(\kappa_{2}) \right] \right\}, \tag{10} \\ B_{3}^{(q)} &= \sum_{\kappa_{1}\kappa_{2}} A_{3} \left\{ -2\sqrt{3} \left\{ \begin{matrix} 1 & 2 & 3 \\ j_{2} & j_{1} & j_{1} \end{matrix} \right\} \left[Q_{01}(\kappa_{1})[\sqrt{6}Q_{12}(\kappa_{2}) \\ &- Q_{32}(\kappa_{2}) \right] \\ &+ \sqrt{15}Q_{11}(\kappa_{1})Q_{22}(\kappa_{2}) - Q_{21}(\kappa_{1})[\sqrt{3}Q_{12}(\kappa_{2}) \\ &- \sqrt{2}Q_{32}(\kappa_{2}) \right] \right] \\ &+ 10\sqrt{2} \left\{ \begin{matrix} 2 & 2 & 3 \\ j_{2} & j_{1} & j_{1} \end{matrix} \right\} \left[\sqrt{3}Q_{12}(\kappa_{1})Q_{22}(\kappa_{2}) \\ &+ \sqrt{2}Q_{22}(\kappa_{1})Q_{32}(\kappa_{2}) \right] \right\}. \tag{11} \end{aligned}$$

The factor A_n (n=1,2,3) in Eqs. (9)–(11) is written in the following form

$$A_{n} = \frac{\pi^{2}\alpha}{k\sigma_{i}} (-1)^{j_{1}+j_{2}+j_{i}-1/2} [j_{1}j_{2}n]^{1/2} \begin{pmatrix} j_{1} & j_{2} & n \\ 1/2 & -1/2 & 0 \end{pmatrix} \times \begin{cases} \sin(\delta_{\kappa_{1}} - \delta_{\kappa_{2}}) \text{ for } n = 1, 3 \\ \cos(\delta_{\kappa_{1}} - \delta_{\kappa_{2}}) \text{ for } n = 2. \end{cases}$$
(12)

Consequently, the photoionization cross section σ_i is computed including all multipoles L of the radiative field f according to

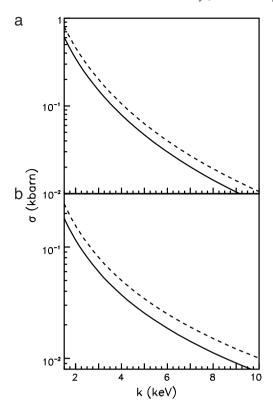


Fig. 2. Photoionization cross sections calculated by the DF (solid) and DS (dashed) methods for the $5p_{1/2}$ subshell of Sn, Z=50 (a) and for the 7s shell of Cm, Z=96 (b).

Eq. (2) while the photoelectron angular distribution parameters are computed in the quadrupole approximation, that is, taking into account terms of the first order O(kr) according to Eqs. (8)–(12). It should be noted that the influence of the second-order terms $O[(kr)^2]$ on photoelectron angular distribution in both cases of unpolarized and linearly polarized radiation was considered in paper [9]. It was shown that the inclusion of the second-order terms may contribute significantly, up to 20%–30%, into angular distribution of photoelectrons at high photon energies $k \ge 10$ keV.

As opposed to calculations [1–7,9] where the electron wave functions were computed by the DS method with the approximate consideration of the electron exchange, we used here the DF method with the proper consideration of the exchange between bound electrons as well as between bound and free electrons [19,20]. The exact consideration of the exchange is essential for outer shells for which the difference between the two calculations

$$\Delta_{\sigma} = \left[(\sigma_i^{\text{DS}} - \sigma_i^{\text{DF}}) / \sigma_i^{\text{DF}} \right] \times 100\%$$
 (13)

may be large at any photon energy. In addition, the difference Δ_{σ} may be essential for inner shells in the event that the photon energy k is close to the subshell binding energy ε_i and the photoelectron energy $E_k = k - \varepsilon_i$ turns out to be low [8].

In Fig. 2, photoionization cross sections σ_i obtained by the DF method (solid curves) and the DS method (dashed curves) are shown for the $5p_{1/2}$ subshell of Sn (Z=50) (Fig. 2(a)) and for the $7s_{1/2}$ shell of Cm (Z=96) (Fig. 2 (b)). As is seen, the difference Δ_{σ} is large and slightly increases with increasing the photon energy. It reaches \sim 40% for Sn and more than 30% for Cm in the photon energy range under consideration. Consequently, photoionization cross sections $\sigma_i^{\rm DF}$ may differ considerably from $\sigma_i^{\rm DS}$ for outer atomic shells of interest. For inner shells, both calculations are usually close to one another.

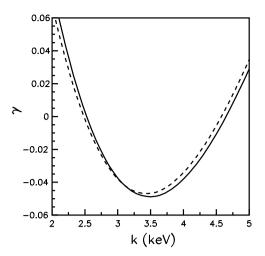


Fig. 3. The non-dipole angular distribution parameter γ calculated by the DF method (solid) and DS method (dashed) for the $5p_{3/2}$ subshell of Hg, Z=80.

The difference between the angular distribution parameters calculated by the DF and DS methods may be also considerable when the parameters become small in magnitude and change a sign. The parameter γ obtained by the two methods in the range 2 keV $\leq k \leq$ 5 keV is displayed in Fig. 3. It is seen that the DF and DS values of γ , even if small, differ considerably, being sometimes opposite in sign. As a rule, the difference between the DF and DS calculations for the β parameter is less than for γ and δ in the energy range under consideration.

Experimental values of the electron binding energies involved in the calculations were taken from work [21]. The values may differ slightly from those used in [6,7]. Binding energies for all subshells under consideration are listed in Table 1. As in our previous calculations, the hole in the atomic shell from which a photoelectron has been emitted is taken into account in the framework of the frozen orbital model. It implies that the bound wave function is calculated in the self-consistent DF field of the neutral atom while the continuum wave function is calculated in the ion field which is constructed using the bound wave functions of the neutral atom. The computational accuracy of our calculations is better than 0.1%. This accuracy does not include possible uncertainties due to the physical approximations mentioned above.

3. Relation between theoretical photoionization parameters and experimental data

Theoretical photoionization cross sections of deep atomic shells are used in traditional X-ray photoelectron spectroscopy as reliable sensitivity factors [2]. For photoionization cross sections of molecular orbitals (MO), the additive formula was proposed [22]:

$$\sigma_{\text{MO}}(\hbar\omega) = \sum_{n,i} p_{ni} \sigma_{ni}(\hbar\omega), \tag{14}$$

where the sum runs over all n atoms in a molecule and over all i valence shells of each an atom, p_{ni} is the population of atomic orbital in MO and σ_{ni} is the atomic shell photoionization cross section. This approximation was shown to be reliable for the photon energy regions in the vicinity of $k \approx 1500$ eV [23] and $k \approx 150$ eV [24]. The approximation is also used in HAXPES energy region [12].

Photoionization of the ith atomic shell is accompanied by satellite excitation of electrons from other shells j into discrete and continuum states q. Theoretical photoionization cross sections correspond to the main line i^{-1} together with shake-up and shake-off

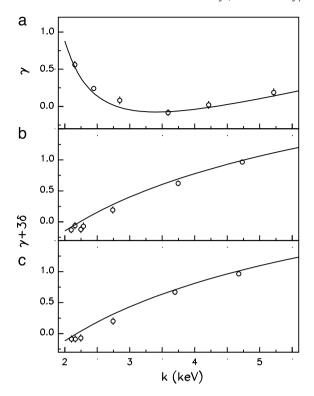


Fig. 4. The non-dipole photoelectron angular distribution parameters for inner shells of Kr versus the photon energy k. (a), the parameter γ for the 2s shell; (b) and (c), the combined parameter $\gamma + 3\delta$ for the $2p_{1/2}$ and $2p_{3/2}$ subshells, respectively. Solid curves, present DF calculations; open circles, experiment [32].

satellites $i^{-1}j^{-1}q$. Photoionization cross sections of the main line and the shake-up satellite states may be represented as:

$$\sigma_i^{\nu}(\omega) = f_i^{\nu} \sigma_i(\omega) \tag{15}$$

where $\sigma_i(\omega)$ is the photoionization cross section given in the present work and f_i^{ν} are spectroscopic factors, which were calculated in the second order of perturbation theory in papers [25–27]. The upper index ν denotes components of the satellite structure, which includes the main line also. Theoretical spectroscopic factors of all main photoelectron lines are close to 0.8 [28]. Experiments on solids generally, but not in detailed confirmed this theoretical result [29] (see also [30]). That is why one can use theoretical photoionization cross sections of the present work for estimation of relative photoionization cross section of different shells. On the other hand, some deviations from this universal value for the spectroscopic factors of the main lines were obtained in paper [14]. For the satellite excitations from the outer shell, one can use Eq. (15). On the other hand, when the satellite state is excited from the core shell, the photoionization cross section should be corrected for the satellite excitation energy [27].

The angular distribution of the core level photoemission usually reveals the atomic character. Some violations of this general rule were found for the d-orbital core-level excitations in strongly correlated materials [31].

To check a reliability of the DF non-dipole photoelectron distribution parameters our values were compared with the experimental data obtained for inner shells of Kr in the electron energy range $E_k \leq 3$ keV [32]. In Fig. 4, our calculations of the parameter γ for the 2s shell as well as the combined non-dipole asymmetry parameter $\gamma + 3\delta$ for the $2p_{1/2}$ and $2p_{3/2}$ subshells of Kr are presented along with the experimental data in the photon energy range 2 keV $\leq k \leq 5.5$ keV. As evident from Fig. 4, our DF calculations are in good agreement with experimental data [32].

4. Conclusions

We present the atomic subshell photoionization cross sections along with parameters of the photoelectron angular distribution in the photon energy range 1.5 keV $\leq k \leq$ 10 keV. The theoretical data are intended for use in experimental studies by methods of HAXPES spectroscopy which is a powerful technique for the investigation of the electron structure and interface of functional materials. Calculations were performed for subshells with binding energies lower than 1.5 keV of all atoms with $1 \leq Z \leq$ 100.

Relativistic calculations were performed within the framework of the DF method with the proper consideration of the electron exchange as distinct from previous calculations using the DS method with approximate consideration of the exchange. The subshell photoionization cross sections calculated with the DF and DS methods may differ considerably for outer atomic shells we are interested in. The difference between the angular distribution parameters obtained by the two methods may be also noticeable.

The photoionization cross sections were calculated taking into account all multipoles of the radiative field. The photoelectron angular distribution parameters were obtained using the quadrupole approximation. The hole resulting in the atomic subshell after photoionization is taken into account using the frozen orbital model.

Theoretical photoionization parameters presented here are in good agreement with available experimental data and are reliable to be used in experimental HAXPES studies.

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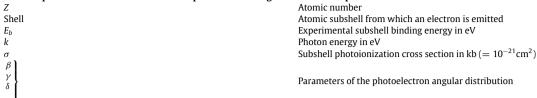
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Explanation of Tables

Table 1.

Subshell photoionization cross sections and photoelectron angular distribution parameters



Notes: The photoionization cross sections σ_i are always given for completely filled subshells. To obtain σ_i for an open atomic subshell i, the value from the Table should be divided by $2j_i + 1$ (j_i is the electron total momentum) and multiplied by the actual occupation number of the ith subshell. In the Table, the decimal order is presented to the right of an entry.

Example

In the Table, the first data block gives the parameters for the $1s_{1/2}$ shell of the hydrogen atom, whose electron configuration has one $1s_{1/2}$ electron. The experimental binding energy is equal to 13.6 eV. At the photon energy k=1500 eV, the photoionization cross section for the completely filled 1s shell is $\sigma_{1s}=5.866 \times 10^{-3}$ kb $=5.866 \times 10^{-24}$ cm², the angular distribution parameters $\beta=1.984$, $\gamma=9.11-1=0.911$, and $\delta=1.96-8=1.96\times 10^{-8}$. Because the hydrogen 1s shell is half-filled one, the real photoionization cross section is $\sigma_{1s}=2.933\times 10^{-3}$ kb.

Table 1Subshell photoionization cross sections and photoelectron angular distribution parameters.

		k (eV)									
Shell		1500	2000	3000	4000	5000	6000	7000	8000	9000	10000
1s _{1/2}	σ	5.866-3	2.223-3	5.619-4	2.110-4	9.839-5	5.270-5	3.108-5	1.966-5	1.311-5	9.123-
$E_b =$	β	1.984	1.979	1.968	1.958	1.947	1.937	1.927	1.917	1.907	1.896
13.6 eV	$\gamma \\ \delta$	9.11-1 1.96-8	1.05+0 5.98-8	1.28+0 1.17-7	1.48+0 2.30-7	1.65+0 2.14-7	1.80+0 4.26-7	1.94+0 8.87-7	2.07+0 9.82-7	2.18+0 1.41-6	2.30+0 2.21-6
Z= 2, He: 1s ₁ ²		1.90-6	J.90-0	1.17-7	2.30-7	2.14-7	4.20-7	0.07-7	9.02-7	1.41-0	2.21-0
Z= 2, He: 1S _{1,}	/2	k (eV)									
Shell		1500	2000	3000	4000	5000	6000	7000	8000	9000	10000
1s _{1/2}	σ	1.017-1	3.991-2	1.050-2	4.037-3	1.914-3	1.038-3	6.179-4	3.938-4	2.643-4	1.850-
$E_b =$	β	1.985	1.979	1.969	1.958	1.948	1.937	1.927	1.917	1.907	1.897
24.6 eV	γ	8.90 - 1	1.03+0	1.27+0	1.47+0	1.64+0	1.79+0	1.93+0	2.06+0	2.18+0	2.29+0
	δ	6.95-8	7.83-8	1.93-7	3.14-7	5.38-7	7.71–7	1.16-6	1.50-6	2.06-6	2.72-6
Z= 3, Li: 1s _{1/2}	2 2s _{1/2}										
C1 11		k (eV)	2000	2000	4000	F000		7000	0000	0000	10000
Shell		1500	2000	3000	4000	5000	6000	7000	8000	9000	10000
$1s_{1/2}$ $E_b =$	$\frac{\sigma}{\beta}$	6.613-1 1.986	2.690-1 1.980	7.391-2 1.970	2.914-2 1.959	1.406-2 1.949	7.723-3 1.938	4.640-3 1.928	2.980-3 1.918	2.014-3 1.908	1.418- 1.898
$E_b = 54.8 \text{ eV}$	γ	8.59-1	1.01+0	1.25+0	1.45+0	1.62+0	1.78+0	1.926	2.05+0	2.17+0	2.28+0
	δ	1.22-7	1.78-7	3.22-7	5.35-7	8.26-7	1.19-6	1.65-6	2.25-6	2.91-6	3.75-6
2s _{1/2}	σ	1.663-2	6.710-3	1.826-3	7.156-4	3.440-4	1.885-4	1.131-4	7.253-5	4.895-5	3.441-
$E_b = 5.4 \text{ eV}$	β	1.985 8.73-1	1.980 1.02+0	1.969 1.26+0	1.959 1.46+0	1.948 1.63+0	1.938 1.79+0	1.927 1.93+0	1.917 2.06+0	1.907 2.18+0	1.897 2.29+0
J.4 C V	δ	3.80-9	1.04-8	8.50-8	2.12-7	4.70-7	6.95-7	1.23-6	1.29-6	2.49-6	2.95-6
Z= 4, Be: 1s _{1/}	2s _{1/2}										
		k (eV)									
Shell		1500	2000	3000	4000	5000	6000	7000	8000	9000	10000
$1s_{1/2}$	σ	2.310+0	9.667 - 1	2.754-1	1.110-1	5.440-2	3.022-2	1.832-2	1.185-2	8.062-3	5.703-
$E_b = 111.9 \text{ eV}$	β	1.986	1.981 9.77-1	1.971 1.22+0	1.960 1.43+0	1.950	1.939 1.76+0	1.929 1.90+0	1.919 2.03+0	1.909 2.15+0	1.899 2.27+0
111.9 ev	$_{\delta}^{\gamma}$	8.26-1 9.85-8	2.02-7	4.16-7	7.05-7	1.60+0 1.05-6	1.53-6	2.13-6	2.84-6	3.65-6	4.55-6
2s _{1/2}	σ	7.882-2	3.292-2	9.335-3	3.753-3	1.834-3	1.017-3	6.157-4	3.979-4	2.704-4	1.911-
$E_b =$	β	1.986	1.981	1.970	1.959	1.949	1.938	1.928	1.918	1.908	1.898
9.3 eV	$\gamma \\ \delta$	8.44-1 $-8.61-9$	9.94-1 1.22-8	1.24+0 9.17-8	1.44+0 2.35-7	1.62+0 4.76-7	1.77+0 8.07-7	1.91+0 1.29-6	2.04+0 1.75-6	2.16+0 2.52-6	2.28+0 3.23-6
Z= 5, B: 1s _{1/2}			1.22 0	3.17	2.55	1.70 7	0.07	1.25	1.75 0	2.52 0	3.23
2 3, 2 . 131/2	2 231/2 2	k (eV)									
Shell		1500	2000	3000	4000	5000	6000	7000	8000	9000	10000
1s _{1/2}	σ	5.815+0	2.490+0	7.311-1	3.006-1	1.494-1	8.389-2	5.133-2	3.344-2	2.287-2	1.625-
$E_b =$	β	1.987	1.982	1.972	1.961	1.951	1.941	1.930	1.920	1.910	1.900
188.0 eV	γ	7.90-1	9.44-1	1.19+0	1.40+0	1.58+0	1.74+0	1.88+0	2.01+0	2.14+0	2.25+0
_	δ	-2.76-8	1.44-7	4.63-7	8.48-7	1.28-6	1.85-6	2.49-6	3.26-6	4.21-6	5.34-6
$2s_{1/2}$ $E_b =$	$\frac{\sigma}{\beta}$	2.366-1 1.987	1.018-1 1.981	3.003-2 1.971	1.235-2 1.960	6.139-3 1.950	3.446-3 1.940	2.107-3 1.929	1.372-3 1.919	9.381-4 1.909	6.666— 1.899
12.6 eV	γ	8.15-1	9.64-1	1.21+0	1.42+0	1.60+0	1.75+0	1.90+0	2.03+0	2.15+0	2.26+0
	δ	-3.80-9	1.75-8	1.06-7	2.83-7	5.57-7	9.38-7	1.40-6	1.95-6	2.77-6	3.67-6
$2p_{1/2}$	σ	3.894-3	1.278-3	2.552-4	7.947-5	3.179-5	1.493-5	7.854-6	4.491-6	2.740-6	1.759-
$E_b = 4.7 \text{ eV}$	β	0.145 3.32-1	0.112 3.79-1	0.077 4.61-1	0.052 5.26-1	0.030 5.79-1	0.012 6.25-1	005 $6.67-1$	020 $7.04-1$	035 7.37-1	049 7.65-1
4.7 CV	$\delta \gamma$	1.29-1	1.55-1	1.96-1	2.30-1	2.59-1	2.85-1	3.08-1	3.29-1	3.49-1	3.68-1
Z= 6, C: 1s _{1/2}	2 2s _{1/2} 2	$p_{1/2}^2$									
		k (eV)									
Shell		1500	2000	3000	4000	5000	6000	7000	8000	9000	10000
$1s_{1/2}$	σ	1.203+1	5.248+0	1.580+0	6.609-1	3.327-1	1.886-1	1.163-1	7.627-2	5.245-2	3.746-
$E_b = 284.1 \text{ eV}$	β	1.988 7.46-1	1.983 9.04-1	1.973 1.16+0	1.963 1.37+0	1.952 1.55+0	1.942 1.71+0	1.932 1.86+0	1.922 1.99+0	1.911 2.11+0	1.901 2.23+0
∠04.1 €V	δ	-2.42-7	-3.01-8	3.83-7	8.72–7	1.38-6	2.04-6	2.82-6	3.71-6	4.78–6	6.05-6
$2s_{1/2}$	σ	5.324-1	2.348-1	7.160-2	3.011-2	1.520-2	8.628-3	5.322-3	3.492-3	2.402-3	1.716-
$E_b =$	β	1.987	1.982	1.972	1.962	1.951	1.941	1.930	1.920	1.910	1.900
18.1 eV	$\gamma \\ \delta$	7.83-1 2.70-8	9.35-1 4.47-8	1.19+0 1.43-7	1.39+0 3.12-7	1.57+0 6.02-7	1.73+0 9.99-7	1.88+0 1.55-6	2.01+0 2.20-6	2.13+0 3.08-6	2.25+0 4.05-6
$2p_{1/2}$	σ	1.459-2	4.913-3	1.019-3	3.254-4	1.325-4	6.311-5	3.355-5	1.935-5	1.188-5	7.672-
-r 1/2	9				3,231 1	1.525	0.011	3,355 5		.,	

tble 1 (contin $E_b = 9.0 \text{ eV}$	β γ	0.217 3.57-1	0.163 3.98-1	0.109 4.73-1	0.077 5.37-1	0.053 5.90-1	0.031 6.36-1	0.013 6.76-1	004 7.12-1	019 7.45-1	034 7.75-1
5.0 eV	δ	1.22-1	1.47-1	1.89-1	2.23-1	2.53-1	2.79-1	3.03-1	3.25-1	3.45-1	3.63-1
= 7, N : 1s _{1/}	2 2s _{1/2} 2										
Shell		k (eV) 1500	2000	3000	4000	5000	6000	7000	8000	9000	10000
1s _{1/2}	σ	2.185+1	9.680+0	2.980+0	1.265+0	6.438-1	3.682-1	2.286-1	1.507-1	1.042-1	7.472-
$E_b =$	β	1.990	1.985	1.974	1.964	1.954	1.944	1.933	1.923	1.913	1.903
400.5 eV	$\gamma \\ \delta$	6.90-1 $-6.23-7$	8.56-1 -3.66-7	1.12+0 1.69-7	1.34+0 6.91-7	1.52+0 1.33-6	1.68+0 2.08-6	1.83+0 2.97-6	1.96+0 4.05-6	2.09+0 5.27-6	2.21+0 6.57-6
2s _{1/2}	σ	1.002+0	4.517-1	1.417-1	6.077-2	3.111-2	1.786-2	1.111-2	7.341-3	5.080-3	3.647-
$E_b =$	β	1.988	1.983	1.973	1.963	1.952	1.942	1.932	1.921	1.911	1.901
24.3 eV	$_{\delta}^{\gamma}$	7.47-1 5.73-8	9.03-1 7.18-8	1.16+0 1.56-7	1.37+0 3.62-7	1.55+0 6.60-7	1.71+0 1.10-6	1.85+0 1.71-6	1.99+0 2.39-6	2.11+0 3.32-6	2.23+0 4.41-6
$2p_{1/2}$	σ	4.103-2	1.412-2	3.026-3	9.881-4	4.090-4	1.973-4	1.060-4	6.163-5	3.811-5	2.475-
$E_b =$	β	0.310	0.232	0.155	0.111	0.080	0.055	0.034	0.015	002	017
8.9 eV	γ	3.92-1	4.28-1	4.94-1	5.53-1	6.04 - 1	6.49-1	6.90-1	7.25-1	7.57-1	7.87-1
	δ	1.13-1	1.39-1	1.81-1	2.16-1	2.47-1	2.73-1	2.97-1	3.19-1	3.40-1	3.58-1
$\begin{array}{l} 2p_{3/2} \\ E_b = \end{array}$	$\frac{\sigma}{eta}$	8.343-2 0.314	2.867-2 0.237	6.131-3 0.163	1.998-3 0.123	8.258-4 0.095	3.977-4 0.073	2.133-4 0.055	1.239-4 0.040	7.649-5 0.026	4.961- 0.013
9.7 eV	γ	3.91-1	4.27-1	4.93-1	5.51-1	6.01-1	6.45-1	6.84-1	7.19-1	7.50-1	7.78-1
	δ	1.13-1	1.39-1	1.81-1	2.16-1	2.46-1	2.72-1	2.96-1	3.18-1	3.38-1	3.57-1
Z= 8, O: 1s _{1/}	2 2s _{1/2} 2	$p_{1/2}^2 2p_{3/2}^2$									
		k (eV)									
Shell		1500	2000	3000	4000	5000	6000	7000	8000	9000	10000
$1s_{1/2}$	σ	3.583+1	1.615+1	5.078+0	2.186+0	1.124+0	6.478-1	4.047-1	2.684-1	1.863-1	1.342-
$E_b = 532.0 \text{ eV}$	β γ	1.991 6.19-1	1.986 7.99-1	1.976 1.08+0	1.966 1.30+0	1.955 1.49+0	1.945 1.65+0	1.935 1.80+0	1.925 1.94+0	1.915 2.06+0	1.905 2.18+0
	δ	-1.16-6	-8.48-7	-2.51-7	3.79-7	1.13-6	1.98-6	3.00-6	4.22-6	5.54-6	6.97-6
$2s_{1/2}$	σ	1.665+0	7.672-1	2.475-1	1.081-1	5.610-2	3.255-2	2.043-2	1.359-2	9.460-3	6.827-
$E_b =$	β	1.989	1.984	1.974	1.964	1.954	1.943	1.933	1.923	1.913	1.902
23.7 eV	$_{\delta}^{\gamma}$	7.07-1 5.38-8	8.67-1 7.35-8	1.13+0 1.94-7	1.34+0 4.35-7	1.52+0 7.87-7	1.68+0 1.27-6	1.83+0 1.91-6	1.96+0 2.68-6	2.09+0 3.67-6	2.21+0 4.83-6
$2p_{1/2}$	σ	9.557-2	3.356-2	7.396-3	2.463-3	1.035-3	5.051-4	2.738-4	1.605-4	9.993-5	6.527-
$E_b =$	β	0.413	0.316	0.211	0.153	0.113	0.083	0.059	0.037	0.018	0.001
6.8 eV	$\gamma \\ \delta$	4.32-1 1.05-1	4.65-1 1.30-1	5.22-1 1.74-1	5.75-1 2.09-1	6.23-1 2.40-1	6.67 - 1 $2.67 - 1$	7.06-1 $2.91-1$	7.41-1 3.13-1	7.73-1 3.34-1	8.02-1 3.53-1
2p _{3/2}	σ	1.920-1	6.733-2	1.480-2	4.920-3	2.063-3	1.005-3	5.441-4	3.184-4	1.980-4	1.291-
$E_b =$	β	0.417	0.321	0.220	0.164	0.128	0.101	0.079	0.061	0.045	0.031
7.4 eV	γ	4.31 - 1	4.63 - 1	5.21 - 1	5.73 - 1	6.20 - 1	6.62 - 1	7.00 - 1	7.34 - 1	7.65 - 1	7.92 - 1
	δ	1.05-1	1.30-1	1.73-1	2.09-1	2.39-1	2.66-1	2.90-1	3.12-1	3.33-1	3.52-1
Z= 9, F: 1s _{1/2}	2 2s _{1/2} 2										
Shell		k (eV) 1500	2000	3000	4000	5000	6000	7000	8000	9000	10000
1s _{1/2}	σ	5.476+1	2.509+1	8.044+0	3.505+0	1.818+0	1.056+0	6.637-1	4.423-1	3.084-1	2.230-
$E_b =$	β	1.993	1.988	1.977	1.967	1.957	1.947	1.937	1.927	1.917	1.906
685.4 eV	γ	5.35 - 1	7.29 - 1	1.03+0	1.25+0	1.45+0	1.62+0	1.77+0	1.91+0	2.03+0	2.15+0
	δ	-1.84-6	-1.49 - 6	-8.51-7	-8.73-8	7.66-7	1.72-6	2.83-6	4.14-6	5.57-6	7.20-6
$2s_{1/2}$	σ	2.572+0	1.207+0	3.985 - 1	1.769 - 1	9.286 - 2	5.438 - 2	3.438 - 2	2.302 - 2	1.611 - 2	1.168-
$E_b = 34.0 \text{ eV}$	β	1.990 6.63-1	1.985 8.27-1	1.975 1.09+0	1.965 1.30+0	1.955 1.49+0	1.945 1.65+0	1.934 1.80+0	1.924 1.94+0	1.914 2.07+0	1.904 2.18+0
34.0 ev	$\gamma \over \delta$	6.00-9	3.69-8	1.99-0	4.60-7	8.27-7	1.37-6	2.06-6	2.89-6	3.92-6	5.16-6
$2p_{1/2}$	σ	1.965-1	7.019-2	1.583-2	5.358-3	2.280-3	1.124-3	6.146-4	3.628-4	2.273-4	1.492-
$E_b =$	β	0.523	0.410	0.277	0.202	0.153	0.116	0.087	0.063	0.042	0.023
8.4 eV	γ	4.71-1	5.03-1	5.56-1	6.04-1	6.48-1	6.89-1	7.26-1	7.60-1	7.91-1	8.20-1
	δ	9.63-2	1.22-1	1.66-1	2.02-1	2.33-1	2.60-1	2.84-1	3.07-1	3.28-1	3.47-1
2p _{3/2}	σ_{β}	3.908-1 0.527	1.394—1 0.415	3.135-2 0.285	1.059-2 0.213	4.498-3 0.166	2.214-3 0.133	1.208-3 0.107	7.121-4 0.086	4.453-4 0.067	2.919- 0.051
$E_b = 8.7 \text{ eV}$	$eta \ \gamma$	4.70-1	5.03-1	5.54-1	6.01-1	6.44-1	6.84-1	7.20-1	7.53-1	7.83-1	8.09-1
	δ	9.63-2	1.22-1	1.66-1	2.01-1	2.32-1	2.59-1	2.84-1	3.06-1	3.27-1	3.46-1
Z= 10, Ne: 1s	$s_{1/2}^2 2s_{1/2}^2$										
CI II		k (eV)	2000	2000	4000	5000	5005	7000	2002	0000	1000-
Shell		7.001+1	2000	3000	4000	5000	6000	7000	8000	9000	10000
$1s_{1/2}$ $E_b =$	$\frac{\sigma}{eta}$	7.981+1 1.994	3.715+1 1.989	1.211+1 1.979	5.332+0 1.969	2.787+0 1.959	1.628+0 1.949	1.028+0 1.939	6.883-1 1.928	4.817-1 1.918	3.493- 1.908
ь — 870.1 eV	Ρ	4.23-1	6.47-1	9.64-1	1.20+0	1.555	1.545	1.555	1.520	1.510	2.12+0

		δ	-2.61-6	-2.39 - 6	-1.66-6	-8.24 - 7	5.67-8	1.05-6	2.41-6	3.64-6	5.29-6	6.96-6
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $												1.864-2
S	= 8 5 aV											1.905 2.16+0
E _j β 0.636 0.509 0.348 0.227 0.18 0.154 0.121 0.092 0.08 21 Γ eV β 0.84-2 1.14-1 1.58-1 1.94-1 2.23-1 2.77-1 7.84-1 8.13-1 2pyα β 0.339 0.533 0.68-2 2.07-2 8.89-3 0.44-0 1.14-1 1.05-1 1.94-1 2.23-1 2.77-1 2.30-1 3.00-1 3.04-1 21 Lev γ 5.08-1 5.43-1 5.91-1 6.85-1 6.73-1 7.12-1 7.43-1 7.60-1 8.04-1 2 Illev γ 5.08-1 1.57-1 1.57-1 1.93-1 2.25-1 2.52-1 2.77-1 2.89-1 3.04-1 5 Illev 5 1.18-2 1.	6.5 EV											5.42-6
Fig. = β 0.636 0.509 0.348 0.557 0.198 0.154 0.120 0.092 0.092 0.092 1.71eV y 5.588-1 5.43-1 5.84-1 0.194-1	/2	σ	3.728-1	1.348-1	3.090-2					7.398-4		3.072-4
18	=											0.046
	1.7 eV											8.41-1
δ _b β 0.639 0.513 0.396 0.267 0.211 0.170 0.139 0.114 0.093 21 for V β 0.88-1 1.14-1 1.57-1 1.93-1 225-1 2.52-1 2.77-1 2.99-1 3.00-1 Zer II.Nax [Ne/S]* ₁ KeV) Shell 1500 2000 3000 4000 5000 6000 7000 8000 9000 15/2 σ 1.085+2 5.157+1 1.720+1 7.674+0 4.086+0 2.380+0 1.512+0 1.016+0 7.141-1 5, g π 1.990 1.991 1.981 1.971 1.991 1.91												3.40-1 5.954-4
	/2 =											0.074
Tell Nation Section	1.6 eV											8.30-1
Shell 1500 2000 3000 4000 5000 6000 7000 8000 9000		δ	8.83-2	1.14-1	1.57-1	1.93-1	2.25-1	2.52-1	2.77-1	2.99-1	3.20-1	3.40-1
Shell 1500 2000 3000 4000 5000 6000 7000 8000 9000 15χ2 σ 1.058+2 5.157+1 1.720+1 7.674-0 4.046+0 2.380+0 1.512+0 1.016-0 7.141-1 1072.1 e β 1.956 1.991 1.981 1.971 1.961 1.5310 1.931 1.921 1072.1 e β 1.921 5.46-1 8.89-1 1.1440 1.3540 1.5910 1.8940 1.8910 1.970-1 28/y2 σ 5.352+0 2.60840 8.037-1 4.131-1 2.218-1 1.321-1 8.470-2 5.737-2 4.055-2 63.2 v γ 5.65-1 7.33-1 1.0140 1.2340 1.4240 1.5940 1.7540 1.8940 2.0140 63.2 v γ 5.65-1 7.33-1 1.0140 1.2340 1.4240 1.5940 1.7540 1.8940 2.0140 52.1 y 3.03 3.03 3.03 3.03 3.03	11, Na: [Ne]:	$3s_{1/2}^1$										
15												
E _j = g β 1996 1991 1981 1971 1961 1951 1941 1931 1979 1072.1 eV γ 2.21-6 -3.62-6 -3.89-0 -1.14-0 13.50 1.59-0 1.83+0 1.97-0 2.51.2 g σ 5.35-24 g -2.51-6 -2.51-6 -1.68-6 -6.22-7 4.76-7 1.74-6 3.28-6 4.85-6 2.51.2 g σ 5.35-24 g 1.58 1.978 1.98 1.98 1.978 1.98 1.978 1.96 1.93-1 1.43-1 1.23-1 1.23-1 1.83-0 1.75-7 1.91-7 1.91-7 1.91-7 1.91-7 1.91-7 1.91-7 1.91-7 1.91-7 1.91-1 1.9												10000
1072.1 V V 2.81 -1 5.46 -3.12 -6.251 -6.185 -0.217 -6.76 1.73 -0.185 1.87 0.185 0.1												5.196-1
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $	– 2.1 eV											1.911 2.09+0
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $												6.83-6
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $												2.965-2
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $	=											1.907
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	3.3 eV											2.13+0 5.81-6
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $												6.536-4
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $	/2 =											0.072
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $												8.68-1
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$			8.10 - 2	1.06 - 1	1.49 - 1	1.85 - 1	2.16 - 1	2.44 - 1	2.69 - 1	2.92 - 1	3.13 - 1	3.33 - 1
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $												1.264-3
δ 8.09-2 1.06-1 1.48-1 1.85-1 2.16-1 2.43-1 2.68-1 2.91-1 3.12-1 $31_{1/2}$ σ 1.224-1 5.933-2 2.045-2 9.331-3 5.000-3 2.975-3 1.906-3 1.291-3 9.119-4 E_p $β$ 1.992 1.987 1.977 1.967 1.957 1.49-6 1.297-0 1.89+0 2.02+0 6 $7.66-1$ 7.44-1 1.02+0 1.24+0 1.43+0 1.60+0 1.75+0 1.89+0 2.02+0 7 $7.66-1$ $7.44-1$ 1.02+0 1.24+0 1.49-6 1.59-0 1.05-0 2.02-6 3.05-6 420-6 7 7.12 7.02	=											0.098
$\frac{3s_{1/2}}{E_p} = \frac{\sigma}{\beta}$ 1,224-1 5,933-2 2,045-2 9,331-3 5,000-3 2,975-3 1,906-3 1,291-3 9,119-4 $\frac{1}{E_p} = \frac{\sigma}{\beta}$ 1,992 1,987 1,977 1,967 1,957 1,957 1,947 1,937 1,927 1,917 2,020-0 $\frac{1}{2}$ 8, $\frac{1}{2}$ 9, $\frac{1}{2}$ 8, $\frac{1}{2}$ 9, $\frac{1}{2}$ 8, $\frac{1}{2}$ 9, $\frac{1}{2}$ 8, $\frac{1}{2}$ 9, $\frac{1}{$	1.0 ev											8.57-1 3.32-1
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $												6.666-4
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $	=											1.907
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $.7 eV											2.14+0
$\begin{array}{c c c c c c c c c c c c c c c c c c c $			-8.73-8	-7.66-8	1.19-7	4.34-7	8.77-7	1.49-6	2.25-6	3.05-6	4.20-6	5.74-6
Shell 500 2000 3000 4000 5000 6000 7000 8000 9000 1s _{1/2} σ 1.419+2 6.917+1 2.359+1 1.066+1 5.665+0 3.353+0 2.141+0 1.445+0 1.019+0 $E_b = \beta$ 1.998 1.994 1.984 1.973 1.963 1.593 1.943 1.933 1.923 1305.0 eV γ 7.77-7 4.16-1 8.06-1 1.08+0 1.29+0 1.48+0 1.65+0 1.79+0 1.99+0 2s _{1/2} σ 7.384+0 3.667+0 1.299+0 6.023-1 3.266-1 1.961-1 1.265-1 8.613-2 6.115-2 E _b = β β 1.993 1.989 1.979 1.969 1.959 1.949 1.939 1.929 1.919 E _b = β β 1.993 1.989 1.979 1.960 1.959 1.949 1.939 1.929 1.919 E _b = β β 0.301-7 -2.14-7 7.80-9 3.60-7	12, Mg: [Ne]]3s _{1/2}										
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$.,			2000	2000	4000	5000	5000	7000	2000	0000	10000
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$												10000
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	/2											7.434-1 1.913
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $												2.05+0
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	-,,											6.29-6
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	/2	σ	7.384+0	3.667+0	1.299+0	6.023 - 1	3.266-1	1.961-1	1.265-1	8.613-2	6.115-2	4.489-2
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	=	β										1.909
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	9.4 eV											2.10+0
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$												6.26-6
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$												1.265-3 0.101
b 7.43-2 9.78-2 1.40-1 1.76-1 2.07-1 2.36-1 2.61-1 2.85-1 3.06-1 $2p_{3/2}$ σ 2.481+0 9.291-1 2.223-1 7.824-2 3.426-2 1.729-2 9.637-3 5.782-3 3.672-3 E_b $β$ 0.839 0.689 0.506 0.386 0.310 0.256 0.215 0.180 0.151 51.3 eV $γ$ 5.55-1 6.05-1 6.68-1 7.09-1 7.47-1 7.80-1 8.08-1 8.34-1 8.58-1 51.3 eV $γ$ 5.55-1 6.05-1 6.68-1 7.09-1 7.47-1 7.80-1 8.08-1 8.34-1 8.58-1 $δ$ 7.42-2 9.77-2 1.40-1 1.76-1 2.07-1 2.35-1 2.61-1 2.84-1 3.06-1 $δ$ 1.993 1.988 1.979 1.969 1.959 1.949 1.938 1.928 1.918 $δ$ 7.22-7 -9.96-8 7.74-8 4.52-7 9.27-7 <	– 1.5 eV											8.92-1
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$			7.43 - 2									3.26 - 1
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	/2	σ	2.481+0	9.291-1	2.223-1	7.824-2	3.426-2	1.729-2	9.637-3	5.782-3	3.672-3	2.440-3
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	=	β										0.127
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	1.3 eV											8.80-1 3.25-1
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$												
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$												1.668-3 1.908
Z= 13, Al: [Ne]3 $s_{1/2}^2$ 3 $p_{1/2}^1$ $\frac{k(eV)}{1500}$ 2000 3000 4000 5000 6000 7000 8000 9000 $2s_{1/2}$ σ 9.742+0 4.925+0 1.785+0 8.397-1 4.597-1 2.780-1 1.805-1 1.236-1 8.815-2 $E_b = \beta$ 1.994 1.990 1.981 1.971 1.961 1.951 1.941 1.931 1.921 117.7 eV γ 4.55-1 6.31-1 9.21-1 1.15+0 1.35+0 1.52+0 1.68+0 1.82+0 1.96+0		γ	5.25 - 1	6.99 - 1	9.78 - 1	1.21+0	1.40+0	1.57+0	1.72+0	1.86+0	1.99+0	2.11+0
$\frac{k (\text{eV})}{\text{Shell}} = \frac{k (\text{eV})}{1500} = \frac{k (\text{eV})}{2000} = \frac{3000}{3000} = \frac{4000}{4000} = \frac{5000}{5000} = \frac{6000}{6000} = \frac{7000}{7000} = \frac{8000}{9000} = \frac{9000}{9000}$ $\frac{2s_{1/2}}{E_b} = \frac{\beta}{\beta} = \frac{1.994}{1.994} = \frac{1.990}{1.990} = \frac{1.981}{1.981} = \frac{1.971}{1.961} = \frac{1.961}{1.951} = \frac{1.941}{1.941} = \frac{1.931}{1.921} = \frac{1.921}{117.7 \text{eV}}$ $\frac{k (\text{eV})}{\gamma} = \frac{k (\text{eV})}{1.500} = \frac{1.785 + 0}{1.981} = \frac{1.971}{1.961} = \frac{1.805 - 1}{1.951} = \frac{1.236 - 1}{1.931} = \frac{8.815 - 2}{1.921}$ $\frac{1.971}{117.7 \text{eV}} = \frac{1.964}{\gamma} = \frac{1.994}{1.951} = \frac{1.994}{1.991} = \frac{1.994}{1.9$	10 A1 F-:			-9.96-8	7.74–8	4.52-7	9.27-7	1.59-6	2.44-6	3.40-6	4.55-6	6.13-6
Shell 1500 2000 3000 4000 5000 6000 7000 8000 9000 $2s_{1/2}$ σ 9.742+0 4.925+0 1.785+0 8.397-1 4.597-1 2.780-1 1.805-1 1.236-1 8.815-2 $E_b =$ β 1.994 1.990 1.981 1.971 1.961 1.951 1.941 1.931 1.921 117.7 eV γ 4.55-1 6.31-1 9.21-1 1.15+0 1.35+0 1.52+0 1.68+0 1.82+0 1.96+0	13, AI: [Ne]3	3S _{1/2} 3	•									
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	11			2000	3000	4000	5000	6000	7000	8000	9000	10000
$E_b = \beta$ 1.994 1.990 1.981 1.971 1.961 1.951 1.941 1.931 1.921 117.7 eV γ 4.55-1 6.31-1 9.21-1 1.15+0 1.35+0 1.52+0 1.68+0 1.82+0 1.96+0												
117.7 eV γ 4.55-1 6.31-1 9.21-1 1.15+0 1.35+0 1.52+0 1.68+0 1.82+0 1.96+0												6.497-2 1.911
												2.08+0
0 -4.80-/ -3.03-/ -1.09-/ 2.91-/ 8.50-/ 1.60-6 2.53-6 3.6/-6 4.99-6		δ	-4.80 - 7	-3.63 - 7	-1.09 - 7	2.91 - 7	8.50 - 7	1.60 - 6	2.53 - 6	3.67 - 6	4.99 - 6	6.53 - 6

$\begin{array}{c c c c c c c c c c c c c c c c c c c $	0.160 0.131 9.00-1 9.25-1 2.98-1 3.17-1
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	
E _k = 0, 0,7 eV β 1.994 1.990 1.980 1.970 1.950 1.940 1.930 0.7 eV γ - 479-1 6.51-1 9.34-1 1.1740 1.38-0 1.5340 1.5340 1.5340 1.83-0 3P1/2 b, E _E = β 0.909 0.75 0.559 0.438 0.350 0.283 0.284 <td>8.91-1 9.14-1 2.97-1 3.17-1</td>	8.91-1 9.14-1 2.97-1 3.17-1
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	3 4.697-3 3.462-3 1.920 1.910 1.96+0 2.08+0 4.92-6 6.48-6
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	4 1.082-4 7.226-5 0.157 0.127 9.00-1 9.24-1 2.98-1 3.18-1
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	9000 10000
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	1 1.224-1 9.051-2 1.922 1.913 1.92+0 2.04+0 5.24-6 6.91-6
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	3 5.750-3 3.858-3 0.201 0.167 9.34-1 9.55-1
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	2.90-1 3.11-1 2 1.097-2 7.349-3 0.222 0.191
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	9.25-1 9.44-1 2.89-1 3.10-1
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	2 8.074-3 5.972-3 1.922 1.912 1.93+0 2.05+0 5.17-6 6.81-6
	4 2.499-4 1.677-4 0.195 0.163 9.34-1 9.55-1 2.90-1 3.11-1
Shell 1500 2000 3000 4000 5000 6000 7000 8000 $2s_{1/2}$ σ 1.545+1 8.069+0 3.050+0 1.474+0 8.224-1 5.048-1 3.316-1 2.292-1 E_b β 1.996 1.992 1.984 1.974 1.964 1.954 1.944 1.934 189.3 eV γ 3.47-1 5.25-1 8.20-1 1.06+0 1.27+0 1.45+0 1.61+0 1.76+0 δ -1.15-6 -8.89-7 -4.95-7 -3.59-8 5.79-7 1.43-6 2.47-6 3.74-6 $2p_{1/2}$ σ 4.801+0 1.892+0 4.826-1 1.770-1 7.988-2 4.128-2 2.346-2 1.432- E_b β 1.071 0.923 0.712 0.570 0.467 0.389 0.328 0.278 136.2 eV γ 5.79-1 6.59-1 7.57-1 8.16-1 8.58-1 8.92-1 9.22-1 9.48-1 δ 5.	
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	9000 10000
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	1 1.648-1 1.224-1 1.924 1.914 1.89+0 2.02+0 5.25-6 7.00-6
$E_b = \beta$ 1.077 0.930 0.720 0.579 0.478 0.402 0.344 0.296	2 9.228-3 6.214-3 0.237 0.202 9.72-1 9.94-1 2.81-1 3.01-1
δ 5.72-2 7.73-2 1.16-1 1.50-1 1.81-1 2.09-1 2.35-1 2.58-1	2 1.759-2 1.182-2 0.258 0.225 9.63-1 9.83-1 2.80-1 3.00-1
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	2 1.251-2 9.288-3 1.924 1.914 1.90+0 2.02+0 5.39-6 7.07-6
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	4 4.971-4 3.348-4 0.228 0.193 9.66-1 9.89-1 2.82-1 3.02-1
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	3 9.732-4 6.540-4 0.249 0.216 9.57-1 9.77-1 2.81-1 3.01-1

Table 1 (continued)

Z= 16, S: [Ne] $3s_{1/2}^2 3p_{1/2}^2 3p_{3/2}^2$

2 10,5.110	J1/2 J	k (eV)									
Shell		1500	2000	3000	4000	5000	6000	7000	8000	9000	10000
2s _{1/2}	σ	1.872+1	9.921+0	3.826+0	1.873+0	1.055+0	6.520-1	4.307-1	2.991-1	2.160-1	1.609-
$E_b =$	β	1.997	1.993	1.985	1.976	1.966	1.956	1.946	1.936	1.926	1.917
229.2 eV	γ	2.93 - 1	4.69 - 1	7.67 - 1	1.01+0	1.22+0	1.40+0	1.57+0	1.72+0	1.85+0	1.98+0
	δ	-1.74 - 6	-1.31-6	-8.52 - 7	-3.82 - 7	2.99 - 7	1.17 - 6	2.30 - 6	3.66-6	5.27 - 6	7.11-6
$2p_{1/2}$	σ	6.778+0	2.715+0	7.078-1	2.631-1	1.199-1	6.242-2	3.569-2	2.188-2	1.416-2	9.571-
$E_b =$	β	1.135	0.994	0.781	0.633	0.524	0.441	0.375	0.321	0.276	0.237
165.4 eV	γ	5.76 - 1	6.66 - 1	7.78 - 1	8.45 - 1	8.91 - 1	9.27 - 1	9.57 - 1	9.83-1	1.01+0	1.03+0
	δ	5.30-2	7.21-2	1.09-1	1.42-1	1.73-1	2.01-1	2.27-1	2.51-1	2.73-1	2.93-
$2p_{3/2}$	σ	1.315+1	5.260+0	1.368+0	5.071 - 1	2.305 - 1	1.197 - 1	6.827 - 2	4.176 - 2	2.697 - 2	1.819-
$E_b =$	β	1.141	1.001	0.789	0.642	0.535	0.455	0.391	0.339	0.296	0.259
164.2 eV	$_{\delta}^{\gamma}$	5.80-1 5.30-2	6.70-1 7.19-2	7.80-1 1.08-1	8.46-1 1.42-1	8.91-1 1.73-1	9.25 - 1 $2.01 - 1$	9.53-1 2.26-1	9.76-1 2.50-1	9.98 - 1 $2.72 - 1$	1.02+0 2.92-
$3s_{1/2}$	σ	1.607+0	8.445-1	3.234-1	1.579-1	8.883-2	5.487-2	3.624-2	2.516-2	1.816-2	1.353-
$E_b = 15.8 \text{ eV}$	β	1.996 3.40-1	1.993 5.07-1	1.984 7.94—1	1.975 1.03+0	1.965 1.24+0	1.955 1.42+0	1.945 1.58+0	1.935 1.73+0	1.925 1.86+0	1.916 1.99+0
13.6 EV	$\frac{\gamma}{\delta}$	-8.31-7	-7.86-7	-5.42-7	-7.20-8	6.12-7	1.50-6	2.59-6	3.95-6	5.54-6	7.38-6
2 n		4.069-1	1.657-1	4.384-2	1.639-2	7.493-3	3.907-3	2.236-3	1.372-3	8.888-4	6.009-
$ 3p_{1/2} \\ E_b = $	$\frac{\sigma}{eta}$	4.069—1 1.102	0.963	4.384-2 0.760	0.619	7.493-3 0.514	0.433	2.236-3 0.369	0.316	8.888-4 0.271	0.232
с _ь — 7.8 eV	γ	5.74-1	6.61-1	7.72—1	8.40-1	8.88-1	9.24-1	9.54-1	9.79—1	1.00+0	1.02+0
•	δ	5.29-2	7.25-2	1.10-1	1.44-1	1.75-1	2.03-1	2.28-1	2.52-1	2.74-1	2.95-1
$3p_{3/2}$	σ	8.054-1	3.272-1	8.619-2	3.212-2	1.463-2	7.609-3	4.344-3	2.659-3	1.718-3	1.159-
$E_b =$	β	1.110	0.972	0.769	0.629	0.526	0.447	0.385	0.334	0.291	0.254
8.2 eV	γ	5.77-1	6.64-1	7.74–1	8.40-1	8.86-1	9.21-1	9.49-1	9.72-1	9.93-1	1.01+0
	δ	5.25 - 2	7.19 - 2	1.09 - 1	1.43 - 1	1.74 - 1	2.02 - 1	2.28 - 1	2.51 - 1	2.73 - 1	2.94-
Z= 17, Cl: [Ne	2]3s _{1/2} 3	$p_{1/2}^2 3p_{3/2}^3$									
	- 1/2	k (eV)									
Shell		1500	2000	3000	4000	5000	6000	7000	8000	9000	10000
2s _{1/2}	σ	2.220+1	1.193+1	4.689+0	2.325+0	1.322+0	8.228-1	5.466-1	3.813-1	2.764-1	2.066-
$E_b =$	β	1.998	1.195+1	1.987	1.977	1.968	1.958	1.948	1.938	1.929	1.919
270.2 eV	γ	2.39-1	4.12-1	7.11-1	9.59-1	1.17+0	1.36+0	1.52+0	1.68+0	1.81+0	1.94+0
	δ	-2.38 - 6	-1.87 - 6	-1.35 - 6	-8.31 - 7	-5.94 - 8	8.39-7	1.99 - 6	3.42 - 6	5.12 - 6	7.09-6
$2p_{1/2}$	σ	9.318+0	3.786+0	1.006+0	3.788-1	1.742-1	9.130-2	5.249-2	3.234-2	2.101-2	1.425-
$E_b =$	β	1.195	1.060	0.849	0.697	0.582	0.494	0.424	0.366	0.317	0.276
201.6 eV	γ	5.70 - 1	6.69 - 1	7.95 - 1	8.71 - 1	9.23 - 1	9.62 - 1	9.93 - 1	1.02+0	1.04+0	1.06+0
	δ	4.92 - 2	6.71 - 2	1.02 - 1	1.35 - 1	1.65 - 1	1.93 - 1	2.18 - 1	2.42 - 1	2.64 - 1	2.85-1
$2p_{3/2}$	σ	1.808+1	7.335+0	1.944+0	7.298 - 1	3.347 - 1	1.750 - 1	1.004 - 1	6.167 - 2	3.998 - 2	2.705-
$E_b =$	β	1.203	1.068	0.858	0.707	0.594	0.508	0.439	0.383	0.337	0.297
200.0 eV	γ	5.75-1	6.74-1	7.98-1	8.73-1	9.23-1	9.60-1	9.90-1	1.01+0	1.03+0	1.05+0
	δ	4.92-2	6.69-2	1.02-1	1.34-1	1.64-1	1.92-1	2.17-1	2.41-1	2.63-1	2.84-
$3s_{1/2}$	σ	2.072+0	1.101+0	4.294 - 1	2.123-1	1.205 - 1	7.498-2	4.980-2	3.474-2	2.518-2	1.882-
$E_b =$	β	1.997	1.994	1.986	1.976	1.967	1.957	1.947	1.937	1.927	1.918
17.5 eV	$\frac{\gamma}{\delta}$	2.97 - 1 $-1.18 - 6$	4.60-1 $-1.14-6$	7.45-1 -9.12-7	9.86-1 -4.23-7	1.19+0 3.14-7	1.38+0 1.24-6	1.54+0 2.42-6	1.69+0 3.86-6	1.83+0 5.55-6	1.96+0 7.49-6
$3p_{1/2}$	σ	6.130-1	2.546-1	6.914-2	2.628-2	1.214-2	6.385-3	3.678-3	2.269-3	1.476-3	1.002-
$E_b = 6.7 \text{ eV}$	β	1.154 5.69-1	1.018 6.63-1	0.818 7.86-1	0.675 8.63-1	0.567 9.16-1	0.483 9.56-1	0.415 9.88-1	0.358 1.02+0	0.311 1.04+0	0.270 1.06+0
0.7 6	$_{\delta}^{\gamma}$	4.83-2	6.68-2	1.03-1	1.36-1	1.66-1	1.94-1	2.20-1	2.43-1	2.65-1	2.86-1
$3p_{3/2}$ $E_b =$	$\frac{\sigma}{\beta}$	1.202+0 1.163	4.980-1 1.026	1.346-1 0.826	5.099-2 0.686	2.349-2 0.579	1.231-2 0.497	7.075-3 0.430	4.353-3 0.376	2.825-3 0.330	1.913- 0.292
сь — 6.7 eV	γ	5.73-1	6.66-1	7.88-1	8.64-1	9.15-1	9.54-1	9.84-1	1.01+0	1.03+0	1.05+0
	δ	4.80-2	6.63-2	1.02-1	1.35-1	1.66-1	1.93-1	2.19-1	2.42-1	2.64-1	2.85
7- 10 Am [N/	e 3s ² / 2 3	3p _{1/2} 3p _{3/2}									
L- 10, AL. HIV	1/2	- 1/2 - 3/2									
2- 10, AL. [IW	-	k (eV)									
	·	k (eV)	2000	3000	4000	5000	6000	7000	8000	9000	10000
Shell	σ.	1500	2000	3000 5.668+0	4000 2.843+0	5000 1 630+0	6000 1 021+0	7000 6.820—1	8000 4 778 – 1	9000 3.476—1	10000
Shell 2s _{1/2}	σ β	1500 2.609+1	1.418+1	5.668+0	2.843+0	1.630+0	1.021+0	6.820-1	4.778-1	3.476-1	2.606-
Shell 2s _{1/2} E _b =	β	1500				1.630+0 1.970					2.606- 1.921
Shell 2s _{1/2} E _b =		1500 2.609+1 1.998	1.418+1 1.996	5.668+0 1.988	2.843+0 1.979	1.630+0	1.021+0 1.960	6.820-1 1.950	4.778-1 1.941	3.476-1 1.931	2.606- 1.921 1.90+0
Shell $2s_{1/2}$ $E_b = 326.0 \text{ eV}$	β γ	1500 2.609+1 1.998 1.84-1	1.418+1 1.996 3.55-1	5.668+0 1.988 6.54-1	2.843+0 1.979 9.04-1	1.630+0 1.970 1.12+0	1.021+0 1.960 1.31+0	6.820-1 1.950 1.48+0	4.778-1 1.941 1.63+0	3.476-1 1.931 1.77+0	2.606- 1.921 1.90+0 6.75-6
Shell $2s_{1/2}$ $E_b = 326.0 \text{ eV}$	β γ δ	1500 2.609+1 1.998 1.84-1 -3.15-6	1.418+1 1.996 3.55-1 -2.72-6	5.668+0 1.988 6.54-1 -2.04-6	2.843+0 1.979 9.04-1 -1.47-6	1.630+0 1.970 1.12+0 -6.31-7	1.021+0 1.960 1.31+0 2.95-7	6.820-1 1.950 1.48+0 1.52-6	4.778-1 1.941 1.63+0 3.00-6	3.476-1 1.931 1.77+0 4.74-6	2.606- 1.921 1.90+0 6.75-0
Shell $2s_{1/2}$ $E_b = 326.0 \text{ eV}$ $2p_{1/2}$ $E_b = 60.0 \text{ eV}$	β γ δ	1500 2.609+1 1.998 1.84-1 -3.15-6 1.263+1 1.250 5.60-1	1.418+1 1.996 3.55-1 -2.72-6 5.184+0 1.117 6.69-1	5.668+0 1.988 6.54-1 -2.04-6 1.400+0 0.912 8.08-1	2.843+0 1.979 9.04-1 -1.47-6 5.326-1 0.760 8.94-1	1.630+0 1.970 1.12+0 -6.31-7 2.468-1	1.021+0 1.960 1.31+0 2.95-7 1.302-1	6.820-1 1.950 1.48+0 1.52-6 7.520-2 0.474 1.03+0	4.778-1 1.941 1.63+0 3.00-6 4.651-2 0.412 1.06+0	3.476-1 1.931 1.77+0 4.74-6 3.033-2 0.360 1.08+0	2.606- 1.921 1.90+0 6.75-6 2.063- 0.315 1.10+0
Shell $2s_{1/2}$ $E_b = 326.0 \text{ eV}$ $2p_{1/2}$ $E_b = 6$	β γ δ σ β	1500 2.609+1 1.998 1.84-1 -3.15-6 1.263+1 1.250	1.418+1 1.996 3.55-1 -2.72-6 5.184+0 1.117	5.668+0 1.988 6.54-1 -2.04-6 1.400+0 0.912	2.843+0 1.979 9.04-1 -1.47-6 5.326-1 0.760	1.630+0 1.970 1.12+0 -6.31-7 2.468-1 0.643	1.021+0 1.960 1.31+0 2.95-7 1.302-1 0.549	6.820-1 1.950 1.48+0 1.52-6 7.520-2 0.474	4.778-1 1.941 1.63+0 3.00-6 4.651-2 0.412	3.476-1 1.931 1.77+0 4.74-6 3.033-2 0.360	2.606- 1.921 1.90+0 6.75-6 2.063- 0.315 1.10+0
Shell $2s_{1/2}$ $E_b = 326.0 \text{ eV}$ $2p_{1/2}$ $E_b = 250.6 \text{ eV}$	$\begin{array}{c} \beta \\ \gamma \\ \delta \end{array}$ $\begin{array}{c} \sigma \\ \beta \\ \gamma \end{array}$	1500 2.609+1 1.998 1.84-1 -3.15-6 1.263+1 1.250 5.60-1	1.418+1 1.996 3.55-1 -2.72-6 5.184+0 1.117 6.69-1	5.668+0 1.988 6.54-1 -2.04-6 1.400+0 0.912 8.08-1	2.843+0 1.979 9.04-1 -1.47-6 5.326-1 0.760 8.94-1	1.630+0 1.970 1.12+0 -6.31-7 2.468-1 0.643 9.52-1	1.021+0 1.960 1.31+0 2.95-7 1.302-1 0.549 9.95-1	6.820-1 1.950 1.48+0 1.52-6 7.520-2 0.474 1.03+0	4.778-1 1.941 1.63+0 3.00-6 4.651-2 0.412 1.06+0	3.476-1 1.931 1.77+0 4.74-6 3.033-2 0.360 1.08+0	2.606— 1.921 1.90+0 6.75—6 2.063—

able 1 (contin	ued)										
248.5 eV	$\delta \gamma$	5.65-1 4.55-2	6.75-1 6.18-2	8.13-1 9.53-2	8.97-1 1.27-1	9.54-1 1.56-1	9.95-1 1.83-1	1.03+0 2.09-1	1.05+0 2.32-1	1.07+0 2.54-1	1.09+0 2.75-1
3s _{1/2}	σ	2.609+0	1.399+0	5.533-1	2.766-1	1.583-1	9.913-2	6.619-2	4.637-2	3.374-2	2.530-2
$E_b = 29.2 \text{ eV}$	β γ	1.997 2.56-1	1.994 4.16-1	1.987 6.97-1	1.978 9.38-1	1.969 1.15+0	1.959 1.33+0	1.949 1.50+0	1.939 1.65+0	1.930 1.79+0	1.920 1.92+0
	δ	-1.56-6	-1.51-6	-1.32 - 6	-9.21 - 7	-1.73 - 7	8.03-7	2.04 - 6	3.56-6	5.34-6	7.38-6
$3p_{1/2}$	σ	8.876-1	3.743-1	1.039-1	4.007-2	1.871-2	9.912-3	5.744-3	3.560-3	2.326-3	1.584-3
$E_b = 15.9 \text{ eV}$	β γ	1.202 5.64-1	1.069 6.63-1	0.870 7.97-1	0.728 8.83-1	0.619 9.42-1	0.532 9.86-1	0.461 1.02+0	0.401 1.05+0	0.351 1.07+0	0.307 1.10+0
13.5 CV	δ	4.40-2	6.16-2	9.61-2	1.29-1	1.59-1	1.86-1	2.11-1	2.35-1	2.56-1	2.77-1
$3p_{3/2}$	σ	1.729+0	7.267 - 1	2.008-1	7.715-2	3.590-2	1.896-2	1.096-2	6.774-3	4.414-3	2.999-3
$E_b = 15.8 \text{ eV}$	β	1.212 5.68-1	1.078 6.68-1	0.881	0.740	0.632 9.43-1	0.546	0.477 1.02+0	0.419	0.370 1.07+0	0.329 1.09+0
13.6 EV	δ	4.37-2	6.10-2	8.01-1 9.53-2	8.85-1 1.28-1	1.58-1	9.85-1 1.85-1	2.10-1	1.04+0 2.34-1	2.55-1	2.76-1
Z= 19, K : [Ar	:]4s ¹ _{1/2}										
a		k (eV)			1000			=			10000
Shell		1500	2000	3000	4000	5000	6000	7000	8000	9000	10000
$ 2s_{1/2} \\ E_b = $	$\frac{\sigma}{\beta}$	2.990+1 1.999	1.647+1 1.997	6.699+0 1.989	3.400+0 1.981	1.967+0 1.972	1.241+0 1.962	8.332-1 1.953	5.865-1 1.943	4.283-1 1.933	3.222-1 1.923
377.1 eV	γ	1.34-1	3.03-1	5.99-1	8.51-1	1.07+0	1.26+0	1.43+0	1.58+0	1.73+0	1.86+0
	δ	-4.32-6	-3.67-6	-2.87-6	-2.17-6	-1.34-6	-3.42-7	9.12-7	2.47-6	4.31-6	6.45-6
$2p_{1/2}$	σ	1.639+1 1.291	6.823+0 1.168	1.877+0 0.963	7.236-1 0.810	3.386-1 0.693	1.799-1 0.599	1.045-1 0.523	6.495 - 2 0.460	4.252-2 0.406	2.902-2 0.359
$E_b = 296.3 \text{ eV}$	$eta \ \gamma$	5.42-1	6.63-1	0.963 8.15-1	9.09-1	0.693 9.74-1	1.02+0	1.06+0	1.09+0	1.11+0	0.359 1.14+0
	δ	4.18-2	5.79-2	8.94-2	1.20-1	1.49-1	1.76-1	2.02-1	2.25-1	2.47 - 1	2.68-1
$2p_{3/2}$	σ	3.177+1	1.319+1	3.617+0	1.390+0	6.485-1	3.435-1	1.991-1	1.234-1	8.059-2	5.488-2
$E_b = 293.6 \text{ eV}$	β γ	1.301 5.49-1	1.178 6.69-1	0.974 8.21-1	0.821 9.14-1	0.705 9.77-1	0.613 1.02+0	0.539 1.06+0	0.477 1.09+0	0.425 1.11+0	0.380 1.13+0
203.0 01	δ	4.17-2	5.77-2	8.88-2	1.19-1	1.48-1	1.75-1	2.01-1	2.24-1	2.46-1	2.67-1
3s _{1/2}	σ	3.349+0	1.811+0	7.274-1	3.677-1	2.123-1	1.338-1	8.982-2	6.322-2	4.617-2	3.474-2
$E_b = 33.9 \text{ eV}$	β	1.998 2.20-1	1.995 3.73-1	1.988 6.53-1	1.980 8.94-1	1.970 1.10+0	1.961 1.29+0	1.951 1.46+0	1.941 1.61+0	1.932 1.75+0	1.922 1.88+0
33.9 EV	$\delta \gamma$	-2.03-6	-2.04-6	-1.84-6	-1.41-6	-6.55-7	3.53-7	1.63-6	3.22-6	5.10-6	7.28-6
3p _{1/2}	σ	1.337+0	5.738-1	1.632-1	6.397-2	3.022-2	1.615-2	9.425-3	5.875-3	3.856-3	2.637-3
$E_b =$	β	1.244	1.119	0.917	0.773	0.662	0.573	0.500	0.438	0.386	0.340
18.1 eV	δ	5.55-1 $4.05-2$	6.61-1 $5.72-2$	8.04-1 $8.98-2$	8.97 - 1 $1.21 - 1$	9.63-1 1.50-1	1.01+0 1.77-1	1.05+0 2.02-1	1.08+0 2.26-1	1.11+0 2.48-1	1.13+0 2.68-1
3p _{3/2}	σ	2.603+0	1.114+0	3.151-1	1.230-1	5.792-2	3.086-2	1.796-2	1.116-2	7.306-3	4.984-3
$E_b = 17.8 \text{ eV}$	β	1.254	1.130	0.929	0.785	0.675	0.587	0.515	0.456	0.405	0.361
17.0 EV	$_{\delta}^{\gamma}$	5.59-1 4.02-2	6.65 - 1 $5.66 - 2$	8.08-1 $8.89-2$	9.01-1 1.20-1	9.65-1 1.49-1	1.01+0 1.76-1	1.05+0 2.01-1	1.08+0 2.24-1	1.10+0 2.46-1	1.12+0 2.67-1
4s _{1/2}	σ	1.262-1	6.800-2	2.718-2	1.371-2	7.902-3	4.977-3	3.339-3	2.349-3	1.715-3	1.290-3
$E_b =$	β	1.998	1.995	1.988	1.979	1.970	1.961	1.951	1.941	1.931	1.922
0.7 eV	$\frac{\gamma}{\delta}$	2.25-1 -1.83-6	3.80-1 $-1.74-6$	6.59-1 -1.71-6	8.99 - 1 $-1.28 - 6$	1.11+0 -6.33-7	1.29+0 2.89-7	1.46+0 1.48-6	1.61+0 3.16-6	1.75+0 5.15-6	1.88+0 6.81-6
Z= 20, Ca: [A:		1.03 0	1.7 1 0	1.71 0	1.20 0	0.55 7	2.03 7	1.10 0	3.10 0	3.13	0.01 0
	-/-	k (eV)									
Shell		1500	2000	3000	4000	5000	6000	7000	8000	9000	10000
2s _{1/2}	σ	3.399+1	1.894+1	7.830+0	4.019+0	2.344+0	1.488+0	1.005+0	7.104-1	5.207-1	3.930-1
$E_b = 437.8 \text{ eV}$	β	1.999 8.76-2	1.997 2.47-1	1.991 5.45-1	1.983 7.97-1	1.974 1.01+0	1.964 1.21+0	1.955 1.38+0	1.945 1.54+0	1.935 1.68+0	1.926 1.82+0
437.0 CV	δ	-5.47-6	-4.71-6	-3.85-6	-3.01-6	-2.16-6	-1.11-6	1.89-7	1.77-6	3.65-6	5.91-6
2p _{1/2}	σ	2.099+1	8.832+0	2.470+0	9.637-1	4.549-1	2.433-1	1.422-1	8.873-2	5.831-2	3.993-2
$E_b =$	β	1.330	1.216	1.014	0.866	0.750	0.654	0.575	0.508	0.451	0.401
350.0 eV	δ	5.23-1 3.92-2	6.53-1 5.37-2	8.19-1 8.37-2	9.24-1 1.14-1	9.96-1 1.42-1	1.05+0 1.69-1	1.09+0 1.93-1	1.12+0 2.17-1	1.15+0 2.38-1	1.17+0 2.59-1
2p _{3/2}	σ	4.060+1	1.704+1	4.748+0	1.846+0	8.689-1	4.634-1	2.700-1	1.681-1	1.102-1	7.525-2
$E_b =$	β	1.341	1.227	1.025	0.879	0.764	0.669	0.592	0.526	0.470	0.423
346.4 eV	$\delta \gamma$	5.30-1 3.92-2	6.60-1 $5.34-2$	8.26-1 $8.31-2$	9.30-1 1.13-1	1.00+0 1.41-1	1.05+0 1.67-1	1.09+0 1.92-1	1.12+0 2.15-1	1.15+0 2.37-1	1.17+0 2.57-1
3s _{1/2}	σ	4.202+0	2.290+0	9.314-1	4.754-1	2.766-1	1.755-1	1.184-1	8.369-2	6.135-2	4.630-2
$E_b =$	β	1.998	1.996	1.989	1.981	1.972	1.963	1.953	1.944	1.934	1.924
43.7 eV	$\delta \gamma$	1.82-1 -2.61-6	3.33-1 -2.71-6	6.08 - 1 $-2.45 - 6$	8.46-1 $-2.05-6$	1.05+0 -1.30-6	1.24+0 -3.18-7	1.41+0 1.03-6	1.57+0 2.68-6	1.71+0 4.62-6	1.84+0 6.95-6
3p _{1/2}	σ	1.908+0	8.306-1	2.415-1	9.613-2	4.592-2	2.475-2	1.454-2	9.109-3	6.004-3	4.122-3
$E_b =$	β	1.288	1.160	0.967	0.829	0.717	0.625	0.550	0.485	0.431	0.383
25.8 eV	γ	5.45-1	6.55-1	8.09-1	9.11-1	9.82-1	1.04+0	1.08+0	1.11+0	1.14+0	1.16+0
	δ	3.71-2	5.25-2	8.43-2	1.15-1	1.43-1	1.70-1	1.95-1	2.18-1	2.40-1	2.60-1

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Tа	n	le '	ш	Γ	'n	n	П	n	11	ρ	П	1

$3p_{3/2}$ $E_b =$ 25.5 eV	σ β γ δ	3.713+0 1.299 5.50-1 3.68-2	1.611+0 1.172 6.61-1 5.19-2	4.658-1 0.980 8.14-1 8.34-2	1.846-1 0.842 9.15-1 1.14-1	8.787-2 0.730 9.85-1 1.42-1	4.720-2 0.640 1.04+0 1.69-1	2.764-2 0.566 1.08+0 1.93-1	1.727-2 0.503 1.11+0 2.17-1	1.135-2 0.450 1.13+0 2.39-1	7.773-3 0.404 1.15+0 2.59-1
$4s_{1/2}$ $E_b =$ 1.8 eV	σ β γ δ	2.451-1 1.998 1.90-1 -2.34-6	1.329-1 1.996 3.41-1 -2.28-6	5.373-2 1.989 6.12-1 -2.29-6	2.736-2 1.981 8.50-1 -1.85-6	1.590-2 1.972 1.06+0 -1.16-6	1.008-2 1.963 1.25+0 -2.48-7	6.795-3 1.953 1.42+0 9.46-7	4.801-3 1.943 1.57+0 2.68-6	3.518-3 1.934 1.72+0 4.92-6	2.654-3 1.924 1.85+0 6.22-6
Z= 21, Sc: [A	r]3d _{3/2} 4										
Shell		k (eV) 1500	2000	3000	4000	5000	6000	7000	8000	9000	10000
2s _{1/2}	σ	3.830+1	2.158+1	9.054+0	4.695+0	2.759+0	1.763+0	1.196+0	8.494-1	6.249-1	4.731-1
$E_b =$	β	2.000	1.998	1.992	1.984	1.976	1.967	1.957	1.948	1.938	1.928
500.4 eV	$\gamma \\ \delta$	4.28 - 2 $-7.11 - 6$	1.94-1 $-6.28-6$	4.88 - 1 $-4.96 - 6$	7.40-1 -4.16-6	9.60-1 -3.23-6	1.15+0 -2.14-6	1.33+0 -7.86-7	1.49+0 8.17-7	1.64+0 2.77-6	1.77+0 5.15-6
2p _{1/2}	σ	2.657+1	1.129+1	3.202+0	1.262+0	6.005-1	3.232-1	1.898-1	1.190-1	7.846-2	5.390-2
$E_b =$	β	1.366	1.258	1.064	0.918	0.801	0.704	0.623	0.554	0.494	0.442
406.7 eV	γ	4.97-1	6.38-1	8.20 - 1	9.35 - 1	1.01+0	1.07+0	1.12+0	1.15+0	1.18+0	1.21+0
	δ	3.65-2	4.98-2	7.85-2	1.07-1	1.35-1	1.61-1	1.85-1	2.08-1	2.30-1	2.50-1
$\begin{array}{l} 2p_{3/2} \\ E_b = \end{array}$	$\frac{\sigma}{\beta}$	5.139+1 1.378	2.176+1 1.270	6.146+0 1.077	2.414+0 0.932	1.145+0 0.815	6.142-1 0.719	3.597-1 0.639	2.248-1 0.572	1.479-1 0.514	1.013-1 0.463
402.2 eV	γ	5.04-1	6.46 - 1	8.29 - 1	9.43-1	1.02+0	1.08+0	1.12+0	1.15+0	1.18+0	1.20+0
	δ	3.65-2	4.96-2	7.79-2	1.06-1	1.34-1	1.60-1	1.84-1	2.07-1	2.28-1	2.49-1
$3s_{1/2}$	σ	5.000+0	2.742+0	1.127+0	5.801-1	3.399-1	2.169-1	1.471-1	1.044-1	7.678-2	5.813-2
$E_b = 53.8 \text{ eV}$	$eta \gamma$	1.999 1.47-1	1.997 2.92-1	1.990 5.63-1	1.982 7.98-1	1.974 1.01+0	1.965 1.20+0	1.955 1.37+0	1.946 1.52+0	1.936 1.67+0	1.926 1.80+0
	δ	-3.33-6	-3.43-6	-3.23-6	-2.83-6	-2.12-6	-1.11-6	2.51-7	1.94-6	3.96-6	6.36-6
$\begin{array}{c} 3p_{1/2} \\ E_b = \end{array}$	σ	2.514+0	1.108+0	3.284-1	1.325-1	6.393-2	3.472-2	2.052-2	1.293-2	8.559-3	5.896-3
$E_b = 33.8 \text{ eV}$	β	1.325 5.32-1	1.201 6.49-1	1.014 8.12-1	0.875 9.21-1	0.763 9.99-1	0.671 1.06+0	0.594 1.10+0	0.528 1.14+0	0.471 1.17+0	0.422 1.19+0
33.0 EV	$\gamma \over \delta$	3.36-2	4.83-2	7.89-2	1.08-1	1.36-1	1.62-1	1.87-1	2.10-1	2.31-1	2.52-1
3p _{3/2}	σ	4.871+0	2.140+0	6.304-1	2.532-1	1.217-1	6.590-2	3.883-2	2.439-2	1.610-2	1.106-2
$E_b = 31.5 \text{ eV}$	β	1.337	1.213	1.027	0.889	0.778	0.686	0.610	0.546	0.491	0.443
31.5 eV	$\delta \gamma$	5.37-1 3.33-2	6.55 - 1 $4.77 - 2$	8.18-1 7.79-2	9.27-1 1.07-1	1.00+0 1.35-1	1.06+0 1.61-1	1.10+0 1.85-1	1.14+0 2.08-1	1.16+0 2.30-1	1.19+0 2.50-1
3d _{3/2}	σ	1.526-1	4.998-2	9.699-3	2.880-3	1.092-3	4.868-4	2.434-4	1.327-4	7.740-5	4.767-5
$E_b = 6.6 \text{ eV}$	β	0.663 5.34-1	0.566 5.85-1	0.452 6.62-1	0.377 7.12-1	0.317 7.40-1	0.265 7.53-1	0.221 7.57-1	0.181 7.54-1	0.148 7.48-1	0.116 7.36-1
0.0 6	$\frac{\gamma}{\delta}$	1.34-1	1.71-1	2.36-1	2.95-1	3.47-1	3.93-1	4.36-1	4.75—1	5.11-1	5.43-1
4s _{1/2}	σ	2.888-1	1.575-1	6.434-2	3.304-2	1.934-2	1.233-2	8.354-3	5.927-3	4.358-3	3.298-3
$E_b = 1.7 \text{ eV}$	β	1.999	1.996 3.02-1	1.990 5.69-1	1.982 8.04-1	1.974 1.01+0	1.964 1.20+0	1.955 1.38+0	1.945 1.53+0	1.936 1.68+0	1.926 1.81+0
1.7 eV	$\gamma \\ \delta$	1.56-1 $-3.02-6$	-3.00-6	-2.95-6	-2.62-6	-1.88-6	-9.83-7	2.88-7	2.00-6	4.31-6	5.85-6
Z= 22, Ti: [Aı	r]3d _{3/2} 4	ls _{1/2}									
	-,	k (eV)									
Shell		1500	2000	3000	4000	5000	6000	7000	8000	9000	10000
2s _{1/2}	σ	4.265+1	2.430+1	1.035+1	5.418+0	3.209+0	2.063+0	1.406+0	1.003+0	7.403-1	5.622-1
$E_b = 563.7 \text{ eV}$	β	2.000 4.05-3	1.999 1.43-1	1.993 4.31-1	1.986 6.83-1	1.978 9.03-1	1.969 1.10+0	1.959 1.28+0	1.950 1.44+0	1.940 1.59+0	1.931 1.73+0
303.7 EV	$\frac{\gamma}{\delta}$	-8.88-6	-7.91-6	-6.58-6	-5.60-6	-4.63-6	-3.46-6	-2.01-6	-3.55-7	1.63-6	4.09-6
2p _{1/2}	σ	3.291+1	1.413+1	4.066+0	1.620+0	7.767-1	4.207-1	2.483-1	1.564-1	1.035-1	7.133-2
$E_b =$	β	1.395	1.294	1.111	0.968	0.850	0.752	0.669	0.598	0.537	0.483
461.5 eV	$\gamma \\ \delta$	4.65-1 $3.40-2$	6.18 - 1 $4.63 - 2$	8.17-1 7.38-2	9.43-1 1.02-1	1.03+0 1.28-1	1.09+0 1.54-1	1.14+0 1.78-1	1.18+0 2.00-1	1.21+0 2.22-1	1.24+0 2.42-1
$2p_{3/2}$	σ	6.365+1	2.722+1	7.795+0	3.093+0	1.478+0	7.980-1	4.696-1	2.948-1	1.946-1	1.338-1
$E_b =$	β	1.408	1.308	1.126	0.983	0.865	0.768	0.686	0.617	0.557	0.505
455.5 eV	γ	4.73-1	6.28-1	8.27-1	9.52-1	1.04+0	1.10+0	1.15+0	1.18+0	1.21+0	1.24+0
20	δ	3.40-2	4.60-2	7.32-2	1.01-1	1.27-1	1.52-1	1.76-1	1.98-1	2.20-1	7.120 2
$3s_{1/2}$ $E_b =$	$\frac{\sigma}{\beta}$	5.813+0 1.999	3.208+0 1.997	1.331+0 1.991	6.911-1 1.984	4.077 – 1 1.975	2.616-1 1.967	1.782-1 1.957	1.270-1 1.948	9.376-2 1.938	7.120-2 1.929
60.3 eV	γ	1.13 - 1	2.53 - 1	5.17 - 1	7.51 - 1	9.60 - 1	1.15+0	1.32+0	1.48+0	1.62+0	1.76+0
	δ	-4.23-6	-4.30-6	-4.21-6	-3.77-6	-3.12-6	-2.09-6	-7.25-7	1.02-6	3.12-6	5.56-6
$3p_{1/2}$	σ_{β}	3.193+0 1.357	1.427+0	4.307 – 1 1.058	1.761-1	8.587-2 0.807	4.702-2	2.797-2	1.771-2 0.569	1.178-2	8.146-3
$E_b = 35.6 \text{ eV}$	β γ	1.357 5.16-1	1.238 6.39-1	1.058 8.12-1	0.919 9.28-1	0.807 1.01+0	0.714 1.08+0	0.636 1.12+0	0.569 1.16+0	0.511 1.20+0	0.459 1.22+0
	δ	3.04-2	4.46-2	7.39-2	1.02-1	1.29-1	1.55-1	1.79-1	2.02 - 1	2.23-1	2.43-1
3p _{3/2}	σ	6.149+0	2.737+0	8.212-1	3.343-1	1.623-1	8.856-2	5.251-2	3.315-2	2.198-2	1.516-2

Table 1 (contin	ued)										
$E_b =$	β	1.369	1.252	1.072	0.934	0.822	0.730	0.653	0.587	0.531	0.481
32.2 eV	γ	5.21-1	6.46-1	8.19-1	9.35-1	1.02+0	1.08+0	1.13+0	1.16+0	1.19+0	1.22+0
0.1	δ	3.01-2	4.40-2	7.29-2	1.01-1	1.28-1	1.53-1	1.77-1	2.00-1	2.21-1	2.42-1
$3d_{3/2}$ $E_b =$	$\frac{\sigma}{eta}$	2.580-1 0.699	8.560-2 0.595	1.698-2 0.475	5.131-3 0.398	1.971-3 0.336	8.872-4 0.285	4.470-4 0.240	2.452-4 0.200	1.437—4 0.165	8.880-5 0.132
3.7 eV	γ	5.46-1	5.99-1	6.77-1	7.30-1	7.62-1	7.80-1	7.87-1	7.87-1	7.83-1	7.74-1
	δ	1.29 - 1	1.64 - 1	2.29 - 1	2.86 - 1	3.38 - 1	3.84 - 1	4.26 - 1	4.65 - 1	5.01 - 1	5.34 - 1
4s _{1/2}	σ	3.261-1	1.788-1	7.369-2	3.814-2	2.247-2	1.440-2	9.807-3	6.985-3	5.154-3	3.913-3
$E_b =$	β	1.999	1.997	1.991	1.984	1.975	1.966	1.957	1.948	1.938	1.928
1.6 eV	$_{\delta}^{\gamma}$	1.23-1 -3.83-6	2.63-1 -3.80-6	5.25-1 -3.79-6	7.59-1 -3.48-6	9.68-1 $-2.78-6$	1.16+0 -1.86-6	1.33+0 -5.75-7	1.49+0 1.16-6	1.63+0 3.51-6	1.77+0 5.19-6
Z= 23, V : [Ar]3d _{3/2} 4	s _{1/2}									
		k (eV)									
Shell		1500	2000	3000	4000	5000	6000	7000	8000	9000	10000
$2s_{1/2}$	σ	4.700+1	2.709+1	1.170+1	6.186+0	3.690+0	2.386+0	1.635+0	1.170+0	8.671 - 1	6.605 - 1
$E_b = 628.2 \text{ eV}$	β	2.000	1.999	1.995	1.988	1.979	1.971	1.962	1.952	1.943	1.933
028.2 eV	$\gamma \\ \delta$	-2.68-2 $-1.15-5$	9.48 - 2 $-1.01 - 5$	3.73-1 -8.32-6	6.24-1 $-7.26-6$	8.46 - 1 $-6.24 - 6$	1.04+0 -5.04-6	1.22+0 -3.59-6	1.39+0 -1.88-6	1.54+0 2.03-7	1.68+0 2.67-6
2p _{1/2}	σ	4.025+1	1.745+1	5.092+0	2.048+0	9.893-1	5.390-1	3.198-1	2.022-1	1.343-1	9.286-2
$E_b =$	β	1.418	1.326	1.156	1.015	0.896	0.798	0.714	0.642	0.579	0.524
520.5 eV	γ	4.28 - 1	5.94 - 1	8.10 - 1	9.47 - 1	1.04+0	1.11+0	1.16+0	1.21+0	1.24+0	1.27+0
	δ	3.17-2	4.32-2	6.95-2	9.59-2	1.22-1	1.46-1	1.70-1	1.92-1	2.13-1	2.33-1
$2p_{3/2}$	σ	7.788+1	3.361+1	9.749+0	3.904+0	1.879+0	1.020+0	6.035-1	3.805-1	2.520-1	1.738-1
$E_b = 512.9 \text{ eV}$	β γ	1.432 4.36-1	1.342 6.05-1	1.171 8.22-1	1.031 9.58-1	0.913 1.05+0	0.815 1.12+0	0.732 1.17+0	0.661 1.21+0	0.600 1.24+0	0.546 1.27+0
312.3 CV	δ	3.17-2	4.30-2	6.88-2	9.48-2	1.20-1	1.45-1	1.68-1	1.90-1	2.11-1	2.31-1
3s _{1/2}	σ	6.658+0	3.696+0	1.548+0	8.096-1	4.807-1	3.101-1	2.122-1	1.518-1	1.125-1	8.565-2
$E_b =$	β	1.999	1.998	1.992	1.985	1.977	1.968	1.959	1.950	1.941	1.931
66.5 eV	γ	8.24-2	2.15-1	4.72-1	7.04-1	9.13-1	1.10+0	1.27+0	1.43+0	1.58+0	1.71+0
_	δ	-5.33-6	-5.34-6	-5.32-6	-4.95-6	-4.31-6	-3.30-6	-1.91-6	-1.49-7	2.00-6	4.52-6
$3p_{1/2}$ $E_b =$	$\frac{\sigma}{eta}$	3.978+0 1.387	1.799+0 1.275	5.525-1 1.099	2.288-1 0.961	1.126-1 0.848	6.213-2 0.755	3.719-2 0.676	2.367-2 0.608	1.581-2 0.549	1.097-2 0.497
40.0 eV	γ	4.97-1	6.28-1	8.10-1	9.33-1	1.02+0	1.09+0	1.14+0	1.19+0	1.22+0	1.25+0
10.0 0 1	δ	2.77-2	4.12-2	6.91-2	9.63-2	1.22-1	1.47-1	1.71-1	1.94-1	2.15-1	2.35-1
3p _{3/2}	σ	7.603+0	3.424+0	1.045+0	4.304-1	2.110-1	1.160-1	6.918-2	4.390-2	2.923-2	2.023-2
$E_b =$	β	1.400	1.289	1.115	0.977	0.865	0.772	0.694	0.627	0.569	0.519
35.0 eV	$\gamma \\ \delta$	5.04-1 2.74-2	6.36-1 $4.07-2$	8.19-1 6.80-2	9.42-1 9.49-2	1.03+0 1.21-1	1.10+0 1.46-1	1.15+0 1.69-1	1.19+0 1.91-1	1.22+0 2.13-1	1.25+0 2.33-1
3d _{3/2}		4.046-1	1.357-1	2.742-2	8.413-3	3.271-3	1.486-3	7.542-4	4.161-4	2.450-4	1.520-4
$E_b =$	0										0.149
	$\frac{\sigma}{eta}$	0.735	0.625	0.499	0.419	0.356	0.304	0.258	0.218	0.182	0.143
2.2 eV	β γ	0.735 5.58-1	6.13 - 1	6.93 - 1	7.48 - 1	7.83 - 1	8.04 - 1	8.15 - 1	8.18 - 1	8.16 - 1	8.09 - 1
	β	0.735 5.58-1 1.23-1	6.13-1 1.58-1	6.93-1 2.21-1	7.48-1 2.78-1	7.83-1 3.29-1	8.04-1 3.75-1	8.15-1 4.17-1	8.18-1 4.56-1	8.16-1 4.92-1	8.09-1 5.25-1
4s _{1/2}	β γ δ	0.735 5.58-1 1.23-1 3.603-1	6.13-1 1.58-1 1.986-1	6.93-1 2.21-1 8.256-2	7.48-1 2.78-1 4.303-2	7.83-1 3.29-1 2.550-2	8.04-1 3.75-1 1.643-2	8.15-1 4.17-1 1.124-2	8.18-1 4.56-1 8.035-3	8.16-1 4.92-1 5.949-3	8.09-1 5.25-1 4.529-3
$4s_{1/2}$ $E_b =$	β γ δ σ β	0.735 5.58-1 1.23-1 3.603-1 1.999	6.13-1 1.58-1 1.986-1 1.998	6.93-1 2.21-1 8.256-2 1.992	7.48-1 2.78-1 4.303-2 1.985	7.83-1 3.29-1 2.550-2 1.977	8.04-1 3.75-1 1.643-2 1.968	8.15-1 4.17-1 1.124-2 1.959	8.18-1 4.56-1 8.035-3 1.950	8.16-1 4.92-1 5.949-3 1.940	8.09-1 5.25-1 4.529-3 1.931
4s _{1/2}	β γ δ	0.735 5.58-1 1.23-1 3.603-1	6.13-1 1.58-1 1.986-1	6.93-1 2.21-1 8.256-2	7.48-1 2.78-1 4.303-2	7.83-1 3.29-1 2.550-2	8.04-1 3.75-1 1.643-2	8.15-1 4.17-1 1.124-2	8.18-1 4.56-1 8.035-3	8.16-1 4.92-1 5.949-3	8.09-1 5.25-1 4.529-3
$4s_{1/2}$ $E_b =$	β γ δ σ β γ δ	0.735 5.58-1 1.23-1 3.603-1 1.999 9.19-2 -4.87-6	6.13-1 1.58-1 1.986-1 1.998 2.25-1	6.93-1 2.21-1 8.256-2 1.992 4.81-1	7.48-1 2.78-1 4.303-2 1.985 7.13-1	7.83-1 3.29-1 2.550-2 1.977 9.21-1	8.04-1 3.75-1 1.643-2 1.968 1.11+0	8.15-1 4.17-1 1.124-2 1.959 1.28+0	8.18-1 4.56-1 8.035-3 1.950 1.44+0	8.16-1 4.92-1 5.949-3 1.940 1.59+0	8.09-1 5.25-1 4.529-3 1.931 1.73+0
$4s_{1/2}$ $E_b =$ 1.7 eV	β γ δ σ β γ δ	$0.735 5.58 - 1 1.23 - 1 3.603 - 1 1.999 9.19 - 2 -4.87 - 6 id_{5/2}^{1} 4s_{1/2}^{1} k \text{ (eV)}$	6.13-1 1.58-1 1.986-1 1.998 2.25-1 -4.80-6	6.93-1 2.21-1 8.256-2 1.992 4.81-1 -4.80-6	7.48-1 2.78-1 4.303-2 1.985 7.13-1 -4.52-6	7.83-1 3.29-1 2.550-2 1.977 9.21-1 -3.88-6	8.04-1 3.75-1 1.643-2 1.968 1.11+0 -2.95-6	8.15-1 4.17-1 1.124-2 1.959 1.28+0 -1.66-6	8.18-1 4.56-1 8.035-3 1.950 1.44+0 9.17-8	8.16-1 4.92-1 5.949-3 1.940 1.59+0 2.47-6	8.09-1 5.25-1 4.529-3 1.931 1.73+0 4.29-6
$4s_{1/2}$ $E_b = 1.7 \text{ eV}$ Z= 24, Cr: [And Shell	β γ δ σ β γ δ	$0.735 5.58-1 1.23-1 3.603-1 1.999 9.19-2 -4.87-6 id_{5/2}^{1} 4s_{1/2}^{1} k \text{ (eV)} 1500$	6.13-1 1.58-1 1.986-1 1.998 2.25-1 -4.80-6	6.93-1 2.21-1 8.256-2 1.992 4.81-1	7.48-1 2.78-1 4.303-2 1.985 7.13-1	7.83-1 3.29-1 2.550-2 1.977 9.21-1	8.04-1 3.75-1 1.643-2 1.968 1.11+0 -2.95-6	8.15-1 4.17-1 1.124-2 1.959 1.28+0 -1.66-6	8.18-1 4.56-1 8.035-3 1.950 1.44+0	8.16-1 4.92-1 5.949-3 1.940 1.59+0	8.09-1 5.25-1 4.529-3 1.931 1.73+0
$4s_{1/2}$ $E_b = 1.7 \text{ eV}$ Z= 24, Cr: [And Shell $2s_{1/2}$	$\frac{\beta}{\delta}$ $\frac{\gamma}{\delta}$ $\frac{\beta}{\beta}$ $\frac{\gamma}{\delta}$ $\mathbf{r}]\mathbf{3d}_{3/2}^{4} 3$	$0.735 \\ 5.58 - 1 \\ 1.23 - 1$ $3.603 - 1 \\ 1.999 \\ 9.19 - 2 \\ -4.87 - 6$ $\mathbf{dd}_{5/2}^{1} \mathbf{4s}_{1/2}^{1}$ $\frac{k \text{ (eV)}}{1500}$ $5.147 + 1$	6.13-1 1.58-1 1.986-1 1.998 2.25-1 -4.80-6 2000 3.001+1	6.93-1 2.21-1 8.256-2 1.992 4.81-1 -4.80-6 3000 1.313+1	7.48-1 2.78-1 4.303-2 1.985 7.13-1 -4.52-6 4000 7.010+0	7.83-1 3.29-1 2.550-2 1.977 9.21-1 -3.88-6 5000 4.211+0	8.04-1 3.75-1 1.643-2 1.968 1.11+0 -2.95-6 6000 2.738+0	8.15-1 4.17-1 1.124-2 1.959 1.28+0 -1.66-6 7000 1.884+0	8.18-1 4.56-1 8.035-3 1.950 1.44+0 9.17-8	8.16-1 4.92-1 5.949-3 1.940 1.59+0 2.47-6	8.09-1 5.25-1 4.529-3 1.931 1.73+0 4.29-6
$4s_{1/2}$ $E_b = 1.7 \text{ eV}$ Z= 24, Cr: [And Shell $2s_{1/2}$ $E_b = 1.7 \text{ eV}$	$ \frac{\beta}{\delta} $ $ \frac{\gamma}{\delta} $ $ \frac{\beta}{\beta} $ $ \frac{\gamma}{\delta} $ $ \frac{\delta}{\delta} $ $ \frac{\mathbf{r}}{\mathbf{3d_{3/2}^4}} = \mathbf{3d_{3/2}^4} $	0.735 5.58-1 1.23-1 3.603-1 1.999 9.19-2 -4.87-6 id ¹ _{5/2} 4s ¹ _{1/2} k (eV) 1500 5.147+1 1.999	6.13-1 1.58-1 1.986-1 1.998 2.25-1 -4.80-6 2000 3.001+1 1.999	6.93-1 2.21-1 8.256-2 1.992 4.81-1 -4.80-6 3000 1.313+1 1.996	7.48-1 2.78-1 4.303-2 1.985 7.13-1 -4.52-6 4000 7.010+0 1.989	7.83-1 3.29-1 2.550-2 1.977 9.21-1 -3.88-6 5000 4.211+0 1.981	8.04-1 3.75-1 1.643-2 1.968 1.11+0 -2.95-6 6000 2.738+0 1.973	8.15-1 4.17-1 1.124-2 1.959 1.28+0 -1.66-6 7000 1.884+0 1.964	8.18-1 4.56-1 8.035-3 1.950 1.44+0 9.17-8 8000 1.354+0 1.955	8.16-1 4.92-1 5.949-3 1.940 1.59+0 2.47-6 9000 1.006+0 1.945	8.09-1 5.25-1 4.529-3 1.931 1.73+0 4.29-6 10000 7.688-1 1.936
$4s_{1/2}$ $E_b = 1.7 \text{ eV}$ Z= 24, Cr: [An Shell $2s_{1/2}$	$\frac{\beta}{\delta}$ $\frac{\gamma}{\delta}$ $\frac{\beta}{\beta}$ $\frac{\gamma}{\delta}$ $\mathbf{r}]\mathbf{3d}_{3/2}^{4} 3$	$0.735 \\ 5.58 - 1 \\ 1.23 - 1$ $3.603 - 1 \\ 1.999 \\ 9.19 - 2 \\ -4.87 - 6$ $\mathbf{dd}_{5/2}^{1} \mathbf{4s}_{1/2}^{1}$ $\frac{k \text{ (eV)}}{1500}$ $5.147 + 1$	6.13-1 1.58-1 1.986-1 1.998 2.25-1 -4.80-6 2000 3.001+1 1.999 4.94-2	6.93-1 2.21-1 8.256-2 1.992 4.81-1 -4.80-6 3000 1.313+1 1.996 3.16-1	7.48-1 2.78-1 4.303-2 1.985 7.13-1 -4.52-6 4000 7.010+0	7.83-1 3.29-1 2.550-2 1.977 9.21-1 -3.88-6 5000 4.211+0 1.981 7.93-1	8.04-1 3.75-1 1.643-2 1.968 1.11+0 -2.95-6 6000 2.738+0	8.15-1 4.17-1 1.124-2 1.959 1.28+0 -1.66-6 7000 1.884+0	8.18-1 4.56-1 8.035-3 1.950 1.44+0 9.17-8 8000 1.354+0 1.955 1.34+0	8.16-1 4.92-1 5.949-3 1.940 1.59+0 2.47-6 9000 1.006+0 1.945 1.49+0	8.09-1 5.25-1 4.529-3 1.931 1.73+0 4.29-6
$4s_{1/2}$ $E_b = 1.7 \text{ eV}$ Z= 24, Cr: [And Shell $2s_{1/2}$ $E_b = 694.6 \text{ eV}$	β γ δ σ β γ δ r]3d ⁴ _{3/2} 3	0.735 5.58-1 1.23-1 3.603-1 1.999 9.19-2 -4.87-6 dd _{5/2} 4s _{1/2} k (eV) 1500 5.147+1 1.999 -4.86-2 -1.44-5	6.13-1 1.58-1 1.986-1 1.998 2.25-1 -4.80-6 2000 3.001+1 1.999 4.94-2 -1.25-5	3000 1.313+1 1.996 3.16-1 1.08-5	7.48-1 2.78-1 4.303-2 1.985 7.13-1 -4.52-6 4000 7.010+0 1.989 5.68-1 -9.29-6	7.83-1 3.29-1 2.550-2 1.977 9.21-1 -3.88-6 5000 4.211+0 1.981 7.93-1 -8.17-6	8.04-1 3.75-1 1.643-2 1.968 1.11+0 -2.95-6 6000 2.738+0 1.973 9.93-1 -6.93-6	8.15-1 4.17-1 1.124-2 1.959 1.28+0 -1.66-6 7000 1.884+0 1.964 1.17+0 -5.36-6	8.18-1 4.56-1 8.035-3 1.950 1.44+0 9.17-8 8000 1.354+0 1.955 1.34+0 -3.60-6	8.16-1 4.92-1 5.949-3 1.940 1.59+0 2.47-6 9000 1.006+0 1.945 1.49+0 -1.62-6	8.09-1 5.25-1 4.529-3 1.931 1.73+0 4.29-6 10000 7.688-1 1.936 1.63+0 9.05-7
$4s_{1/2}$ $E_b = 1.7 \text{ eV}$ Z= 24, Cr: [And Shell $2s_{1/2}$ $E_b = $	β γ δ σ β γ δ σ γ δ σ σ σ σ σ σ σ β γ γ σ σ σ β γ γ σ σ σ σ	0.735 5.58-1 1.23-1 3.603-1 1.999 9.19-2 -4.87-6 id _{5/2} 4s _{1/2} k (eV) 1500 5.147+1 1.999 -4.86-2	6.13-1 1.58-1 1.986-1 1.998 2.25-1 -4.80-6 2000 3.001+1 1.999 4.94-2	6.93-1 2.21-1 8.256-2 1.992 4.81-1 -4.80-6 3000 1.313+1 1.996 3.16-1	7.48-1 2.78-1 4.303-2 1.985 7.13-1 -4.52-6 4000 7.010+0 1.989 5.68-1	7.83-1 3.29-1 2.550-2 1.977 9.21-1 -3.88-6 5000 4.211+0 1.981 7.93-1	8.04-1 3.75-1 1.643-2 1.968 1.11+0 -2.95-6 6000 2.738+0 1.973 9.93-1	8.15-1 4.17-1 1.124-2 1.959 1.28+0 -1.66-6 7000 1.884+0 1.964 1.17+0	8.18-1 4.56-1 8.035-3 1.950 1.44+0 9.17-8 8000 1.354+0 1.955 1.34+0	8.16-1 4.92-1 5.949-3 1.940 1.59+0 2.47-6 9000 1.006+0 1.945 1.49+0	8.09-1 5.25-1 4.529-3 1.931 1.73+0 4.29-6 10000 7.688-1 1.936 1.63+0
$4s_{1/2}$ $E_b =$ 1.7 eV Z= 24, Cr: [And Shell $2s_{1/2}$ $E_b =$ 694.6 eV $2p_{1/2}$	β γ δ σ β γ δ δ σ β γ δ δ σ β γ γ δ δ σ β γ γ δ σ β γ γ δ σ β γ γ δ σ β γ γ δ σ β γ γ γ δ σ β γ γ γ δ σ β γ γ γ δ σ β γ γ γ δ σ β γ γ γ δ σ β γ γ γ δ σ β γ γ γ δ σ β γ γ γ δ σ β γ γ γ δ σ β γ γ γ δ σ β γ γ γ δ σ β γ γ γ δ σ β γ γ γ δ σ β γ γ γ δ σ β γ γ γ δ σ β γ γ γ δ σ γ γ γ δ σ γ γ γ δ σ γ γ γ δ σ γ γ γ δ σ γ γ γ δ σ γ γ γ γ	0.735 5.58-1 1.23-1 3.603-1 1.999 9.19-2 -4.87-6 id ¹ _{5/2} 4s ¹ _{1/2} k (eV) 1500 5.147+1 1.999 -4.86-2 -1.44-5 4.904+1 1.435 3.83-1	6.13-1 1.58-1 1.986-1 1.998 2.25-1 -4.80-6 2000 3.001+1 1.999 4.94-2 -1.25-5 2.145+1 1.359 5.66-1	6.93-1 2.21-1 8.256-2 1.992 4.81-1 -4.80-6 3000 1.313+1 1.996 3.16-1 -1.08-5 6.325+0 1.194 7.99-1	7.48-1 2.78-1 4.303-2 1.985 7.13-1 -4.52-6 4000 7.010+0 1.989 5.68-1 -9.29-6 2.564+0 1.052 9.46-1	7.83-1 3.29-1 2.550-2 1.977 9.21-1 -3.88-6 5000 4.211+0 1.981 7.93-1 -8.17-6 1.247+0 0.934 1.05+0	8.04-1 3.75-1 1.643-2 1.968 1.11+0 -2.95-6 6000 2.738+0 1.973 9.93-1 -6.93-6 6.830-1 0.835 1.12+0	8.15-1 4.17-1 1.124-2 1.959 1.28+0 -1.66-6 7000 1.884+0 1.964 1.17+0 -5.36-6 4.070-1 0.751 1.18+0	8.18-1 4.56-1 8.035-3 1.950 1.44+0 9.17-8 8000 1.354+0 1.955 1.34+0 -3.60-6 2.584-1 0.679 1.23+0	8.16-1 4.92-1 5.949-3 1.940 1.59+0 2.47-6 9000 1.006+0 1.945 1.49+0 -1.62-6 1.722-1 0.616 1.27+0	8.09-1 5.25-1 4.529-3 1.931 1.73+0 4.29-6 10000 7.688-1 1.936 1.63+0 9.05-7 1.194-1 0.560 1.30+0
$4s_{1/2}$ $E_b =$ 1.7 eV Z= 24, Cr: [An Shell $2s_{1/2}$ $E_b =$ 694.6 eV $2p_{1/2}$ $E_b =$	$ \frac{\beta}{\delta} $ $ \frac{\sigma}{\beta} $ $ \frac{\beta}{\delta} $ $ \frac{\gamma}{\delta} $ $ \frac{\sigma}{\delta} $ $ \frac{\sigma}{\delta} $ $ \frac{\sigma}{\beta} $ $ \frac{\sigma}{\delta} $ $ \frac{\sigma}{\delta} $ $ \frac{\sigma}{\delta} $	0.735 5.58-1 1.23-1 3.603-1 1.999 9.19-2 -4.87-6 id ¹ _{5/2} 4s ¹ _{1/2} k (eV) 1500 5.147+1 1.999 -4.86-2 -1.44-5 4.904+1 1.435	6.13-1 1.58-1 1.986-1 1.998 2.25-1 -4.80-6 2000 3.001+1 1.999 4.94-2 -1.25-5 2.145+1 1.359 5.66-1 4.10-2	3000 1.313+1 1.996 3.16-1 -1.08-5 6.325+0 1.194 7.99-1 6.46-2	7.48-1 2.78-1 4.303-2 1.985 7.13-1 -4.52-6 4000 7.010+0 1.989 5.68-1 -9.29-6 2.564+0 1.052 9.46-1 8.97-2	7.83-1 3.29-1 2.550-2 1.977 9.21-1 -3.88-6 5000 4.211+0 1.981 7.93-1 -8.17-6 1.247+0 0.934 1.05+0 1.15-1	8.04-1 3.75-1 1.643-2 1.968 1.11+0 -2.95-6 6000 2.738+0 1.973 9.93-1 -6.93-6 6.830-1 0.835 1.12+0 1.39-1	8.15-1 4.17-1 1.124-2 1.959 1.28+0 -1.66-6 7000 1.884+0 1.964 1.17+0 -5.36-6 4.070-1 0.751 1.18+0 1.62-1	8.18-1 4.56-1 8.035-3 1.950 1.44+0 9.17-8 8000 1.354+0 1.955 1.34+0 -3.60-6 2.584-1 0.679 1.23+0 1.84-1	8.16-1 4.92-1 5.949-3 1.940 1.59+0 2.47-6 9000 1.006+0 1.945 1.49+0 -1.62-6 1.722-1 0.616 1.27+0 2.05-1	8.09-1 5.25-1 4.529-3 1.931 1.73+0 4.29-6 10000 7.688-1 1.936 1.63+0 9.05-7 1.194-1 0.560 1.30+0 2.25-1
$4s_{1/2}$ $E_b =$ 1.7 eV Z= 24, Cr: [An Shell $2s_{1/2}$ $E_b =$ 694.6 eV $2p_{1/2}$ $E_b =$ 583.7 eV	β γ δ σ β γ δ δ σ β γ δ δ σ β γ δ δ σ β γ δ δ σ β γ δ δ σ β γ δ δ σ σ β γ δ δ σ σ β γ δ δ σ σ σ δ δ σ σ σ δ δ σ σ σ δ δ σ σ σ δ δ σ σ σ δ δ σ σ σ δ δ σ σ σ δ δ σ σ σ δ δ σ σ σ σ δ δ σ σ σ σ δ δ σ	0.735 5.58-1 1.23-1 3.603-1 1.999 9.19-2 -4.87-6 id ¹ _{5/2} 4s ¹ _{1/2} k (eV) 1500 5.147+1 1.999 -4.86-2 -1.44-5 4.904+1 1.435 3.83-1 2.94-2 9.483+1	6.13-1 1.58-1 1.986-1 1.998 2.25-1 -4.80-6 2000 3.001+1 1.999 4.94-2 -1.25-5 2.145+1 1.359 5.66-1 4.10-2 4.124+1	3000 1.313+1 1.996 3.16-1 -1.08-5 6.325+0 1.194 7.99-1 6.46-2 1.208+1	7.48-1 2.78-1 4.303-2 1.985 7.13-1 -4.52-6 4000 7.010+0 1.989 5.68-1 -9.29-6 2.564+0 1.052 9.46-1 8.97-2 4.875+0	7.83-1 3.29-1 2.550-2 1.977 9.21-1 -3.88-6 5000 4.211+0 1.981 7.93-1 -8.17-6 1.247+0 0.934 1.05+0 1.15-1 2.362+0	8.04-1 3.75-1 1.643-2 1.968 1.11+0 -2.95-6 6000 2.738+0 1.973 9.93-1 -6.93-6 6.830-1 0.835 1.12+0 1.39-1 1.289+0	8.15-1 4.17-1 1.124-2 1.959 1.28+0 -1.66-6 7000 1.884+0 1.964 1.17+0 -5.36-6 4.070-1 0.751 1.18+0 1.62-1 7.657-1	8.18-1 4.56-1 8.035-3 1.950 1.44+0 9.17-8 8000 1.354+0 1.955 1.34+0 -3.60-6 2.584-1 0.679 1.23+0 1.84-1 4.845-1	8.16-1 4.92-1 5.949-3 1.940 1.59+0 2.47-6 9000 1.006+0 1.945 1.49+0 -1.62-6 1.722-1 0.616 1.27+0 2.05-1 3.220-1	8.09-1 5.25-1 4.529-3 1.931 1.73+0 4.29-6 10000 7.688-1 1.936 1.63+0 9.05-7 1.194-1 0.560 1.30+0 2.25-1 2.226-1
$4s_{1/2}$ $E_b =$ 1.7 eV Z= 24, Cr: [And Shell $2s_{1/2}$ $E_b =$ 694.6 eV $2p_{1/2}$ $E_b =$ 583.7 eV	β γ δ σ β γ δ δ σ β γ δ δ σ β γ δ δ σ β γ δ δ σ β β γ δ δ σ β β γ δ δ σ β β β β β β β β β β β β β β β β β	0.735 $5.58-1$ $1.23-1$ $3.603-1$ 1.999 $9.19-2$ $-4.87-6$ $161_{5/2}$ $481_{1/2}$ 1500 1500 $147+1$ 1.999 $-4.86-2$ $-1.44-5$ $4.904+1$ 1.435 $3.83-1$ $2.94-2$ $9.483+1$ 1.451	6.13-1 1.58-1 1.986-1 1.998 2.25-1 -4.80-6 2000 3.001+1 1.999 4.94-2 -1.25-5 2.145+1 1.359 5.66-1 4.10-2 4.124+1 1.376	3000 1.313+1 1.98-5 6.325+0 1.194 7.99-1 6.46-2 1.208+1 1.211	7.48-1 2.78-1 4.303-2 1.985 7.13-1 -4.52-6 4000 7.010+0 1.989 5.68-1 -9.29-6 2.564+0 1.052 9.46-1 8.97-2 4.875+0 1.070	7.83-1 3.29-1 2.550-2 1.977 9.21-1 -3.88-6 5000 4.211+0 1.981 7.93-1 -8.17-6 1.247+0 0.934 1.05+0 1.15-1 2.362+0 0.952	8.04-1 3.75-1 1.643-2 1.968 1.11+0 -2.95-6 6000 2.738+0 1.973 9.93-1 -6.93-6 6.830-1 0.835 1.12+0 1.39-1 1.289+0 0.854	8.15-1 4.17-1 1.124-2 1.959 1.28+0 -1.66-6 7000 1.884+0 1.964 1.17+0 -5.36-6 4.070-1 0.751 1.18+0 1.62-1 7.657-1 0.770	8.18-1 4.56-1 8.035-3 1.950 1.44+0 9.17-8 8000 1.354+0 1.955 1.34+0 -3.60-6 2.584-1 0.679 1.23+0 1.84-1 4.845-1 0.699	8.16-1 4.92-1 5.949-3 1.940 1.59+0 2.47-6 9000 1.006+0 1.945 1.49+0 -1.62-6 1.722-1 0.616 1.27+0 2.05-1 3.220-1 0.637	8.09-1 5.25-1 4.529-3 1.931 1.73+0 4.29-6 10000 7.688-1 1.936 1.63+0 9.05-7 1.194-1 0.560 1.30+0 2.25-1 2.226-1 0.582
$4s_{1/2}$ $E_b =$ 1.7 eV Z= 24, Cr: [An Shell $2s_{1/2}$ $E_b =$ 694.6 eV $2p_{1/2}$ $E_b =$ 583.7 eV	β γ δ σ β γ δ δ σ β γ δ δ σ β γ δ δ σ β γ γ δ δ σ δ β γ γ δ δ σ δ β γ γ δ δ σ δ β γ γ δ δ σ δ β γ γ δ δ σ δ δ γ γ δ δ σ δ δ δ δ δ δ δ δ	0.735 5.58-1 1.23-1 3.603-1 1.999 9.19-2 -4.87-6 id	6.13-1 1.58-1 1.986-1 1.998 2.25-1 -4.80-6 2000 3.001+1 1.999 4.94-2 -1.25-5 2.145+1 1.359 5.66-1 4.10-2 4.124+1 1.376 5.78-1	3000 1.313+1 1.996 3.16-1 -1.08-5 6.325+0 1.194 7.99-1 6.46-2 1.208+1 1.211 8.12-1	7.48-1 2.78-1 4.303-2 1.985 7.13-1 -4.52-6 4000 7.010+0 1.989 5.68-1 -9.29-6 2.564+0 1.052 9.46-1 8.97-2 4.875+0 1.070 9.59-1	7.83-1 3.29-1 2.550-2 1.977 9.21-1 -3.88-6 5000 4.211+0 1.981 7.93-1 -8.17-6 1.247+0 0.934 1.05+0 1.15-1 2.362+0 0.952 1.06+0	8.04-1 3.75-1 1.643-2 1.968 1.11+0 -2.95-6 6000 2.738+0 1.973 9.93-1 -6.93-6 6.830-1 0.835 1.12+0 1.39-1 1.289+0 0.854 1.14+0	8.15-1 4.17-1 1.124-2 1.959 1.28+0 -1.66-6 7000 1.884+0 1.964 1.17+0 -5.36-6 4.070-1 0.751 1.18+0 1.62-1 7.657-1 0.770 1.19+0	8.18-1 4.56-1 8.035-3 1.950 1.44+0 9.17-8 8000 1.354+0 1.955 1.34+0 -3.60-6 2.584-1 0.679 1.23+0 1.84-1 4.845-1 0.699 1.24+0	8.16-1 4.92-1 5.949-3 1.940 1.59+0 2.47-6 9000 1.006+0 1.945 1.49+0 -1.62-6 1.722-1 0.616 1.27+0 2.05-1 3.220-1 0.637 1.27+0	8.09-1 5.25-1 4.529-3 1.931 1.73+0 4.29-6 10000 7.688-1 1.936 1.63+0 9.05-7 1.194-1 0.560 1.30+0 2.25-1 2.226-1 0.582 1.30+0
$4s_{1/2}$ $E_b =$ 1.7 eV Z= 24, Cr: [And Shell $2s_{1/2}$ $E_b =$ 694.6 eV $2p_{1/2}$ $E_b =$ 583.7 eV $2p_{3/2}$ $E_b =$ 574.5 eV	β γ δ σ β γ δ δ σ β γ γ δ δ σ σ β γ γ δ δ σ σ δ σ σ δ σ δ σ δ σ δ σ δ σ δ	0.735 $5.58-1$ $1.23-1$ $3.603-1$ 1.999 $9.19-2$ $-4.87-6$ $10 \frac{1}{5}$ $10 $	6.13-1 1.58-1 1.986-1 1.998 2.25-1 -4.80-6 2000 3.001+1 1.999 4.94-2 -1.25-5 2.145+1 1.359 5.66-1 4.10-2 4.124+1 1.376 5.78-1 4.08-2	3000 1.313+1 1.996 3.16-1 -1.08-5 6.325+0 1.194 7.99-1 6.46-2 1.208+1 1.211 8.12-1 6.38-2	7.48-1 2.78-1 4.303-2 1.985 7.13-1 -4.52-6 4000 7.010+0 1.989 5.68-1 -9.29-6 2.564+0 1.052 9.46-1 8.97-2 4.875+0 1.070 9.59-1 8.86-2	7.83-1 3.29-1 2.550-2 1.977 9.21-1 -3.88-6 5000 4.211+0 1.981 7.93-1 -8.17-6 1.247+0 0.934 1.05+0 1.15-1 2.362+0 0.952 1.06+0 1.13-1	8.04-1 3.75-1 1.643-2 1.968 1.11+0 -2.95-6 6000 2.738+0 1.973 9.93-1 -6.93-6 6.830-1 0.835 1.12+0 1.39-1 1.289+0 0.854 1.14+0 1.37-1	8.15-1 4.17-1 1.124-2 1.959 1.28+0 -1.66-6 7000 1.884+0 1.964 1.17+0 -5.36-6 4.070-1 0.751 1.18+0 1.62-1 7.657-1 0.770 1.19+0 1.60-1	8.18-1 4.56-1 8.035-3 1.950 1.44+0 9.17-8 8000 1.354+0 1.955 1.34+0 -3.60-6 2.584-1 0.679 1.23+0 1.84-1 4.845-1 0.699 1.24+0 1.81-1	8.16-1 4.92-1 5.949-3 1.940 1.59+0 2.47-6 9000 1.006+0 1.945 1.49+0 -1.62-6 1.722-1 0.616 1.27+0 2.05-1 3.220-1 0.637 1.27+0 2.03-1	8.09-1 5.25-1 4.529-3 1.931 1.73+0 4.29-6 10000 7.688-1 1.936 1.63+0 9.05-7 1.194-1 0.560 1.30+0 2.25-1 2.226-1 0.582 1.30+0 2.22-1
$4s_{1/2}$ $E_b =$ 1.7 eV Z= 24, Cr: [At Shell $2s_{1/2}$ $E_b =$ 694.6 eV $2p_{1/2}$ $E_b =$ 583.7 eV $2p_{3/2}$ $E_b =$ 574.5 eV	β γ δ σ β γ δ δ σ β γ δ δ σ β γ δ δ σ β γ γ δ δ σ δ β γ γ δ δ σ δ β γ γ δ δ σ δ β γ γ δ δ σ δ β γ γ δ δ σ δ δ γ γ δ δ σ δ δ δ δ δ δ δ δ	0.735 5.58-1 1.23-1 3.603-1 1.999 9.19-2 -4.87-6 id	6.13-1 1.58-1 1.986-1 1.998 2.25-1 -4.80-6 2000 3.001+1 1.999 4.94-2 -1.25-5 2.145+1 1.359 5.66-1 4.10-2 4.124+1 1.376 5.78-1	3000 1.313+1 1.996 3.16-1 -1.08-5 6.325+0 1.194 7.99-1 6.46-2 1.208+1 1.211 8.12-1	7.48-1 2.78-1 4.303-2 1.985 7.13-1 -4.52-6 4000 7.010+0 1.989 5.68-1 -9.29-6 2.564+0 1.052 9.46-1 8.97-2 4.875+0 1.070 9.59-1	7.83-1 3.29-1 2.550-2 1.977 9.21-1 -3.88-6 5000 4.211+0 1.981 7.93-1 -8.17-6 1.247+0 0.934 1.05+0 1.15-1 2.362+0 0.952 1.06+0	8.04-1 3.75-1 1.643-2 1.968 1.11+0 -2.95-6 6000 2.738+0 1.973 9.93-1 -6.93-6 6.830-1 0.835 1.12+0 1.39-1 1.289+0 0.854 1.14+0	8.15-1 4.17-1 1.124-2 1.959 1.28+0 -1.66-6 7000 1.884+0 1.964 1.17+0 -5.36-6 4.070-1 0.751 1.18+0 1.62-1 7.657-1 0.770 1.19+0	8.18-1 4.56-1 8.035-3 1.950 1.44+0 9.17-8 8000 1.354+0 1.955 1.34+0 -3.60-6 2.584-1 0.679 1.23+0 1.84-1 4.845-1 0.699 1.24+0	8.16-1 4.92-1 5.949-3 1.940 1.59+0 2.47-6 9000 1.006+0 1.945 1.49+0 -1.62-6 1.722-1 0.616 1.27+0 2.05-1 3.220-1 0.637 1.27+0	8.09-1 5.25-1 4.529-3 1.931 1.73+0 4.29-6 10000 7.688-1 1.936 1.63+0 9.05-7 1.194-1 0.560 1.30+0 2.25-1 2.226-1 0.582 1.30+0
$4s_{1/2}$ $E_b = 1.7 \text{ eV}$ Z= 24, Cr: [And Shell $2s_{1/2}$ $E_b = 694.6 \text{ eV}$ $2p_{1/2}$ $E_b = 583.7 \text{ eV}$ $2p_{3/2}$ $E_b = 574.5 \text{ eV}$	β γ δ σ β γ δ δ σ β γ γ δ δ σ δ β γ γ δ δ σ δ β γ γ δ δ σ δ δ δ σ δ δ δ δ δ δ δ δ δ δ δ	0.735 5.58-1 1.23-1 3.603-1 1.999 9.19-2 -4.87-6 6d _{5/2} 4s _{1/2} k (eV) 1500 5.147+1 1.999 -4.86-2 -1.44-5 4.904+1 1.435 3.83-1 2.94-2 9.483+1 1.451 3.93-1 2.95-2 7.446+0 1.999 5.16-2	6.13-1 1.58-1 1.986-1 1.998 2.25-1 -4.80-6 2000 3.001+1 1.999 4.94-2 -1.25-5 2.145+1 1.359 5.66-1 4.10-2 4.124+1 1.376 5.78-1 4.08-2 4.155+0 1.998 1.76-1	3000 1.313+1 1.996 3.16-1 -1.08-5 6.325+0 1.194 7.99-1 6.46-2 1.208+1 1.211 8.12-1 6.38-2 1.755+0 1.993 4.29-1	7.48-1 2.78-1 4.303-2 1.985 7.13-1 -4.52-6 4000 7.010+0 1.989 5.68-1 -9.29-6 2.564+0 1.052 9.46-1 8.97-2 4.875+0 1.070 9.59-1 8.86-2 9.242-1 1.986 6.61-1	7.83-1 3.29-1 2.550-2 1.977 9.21-1 -3.88-6 5000 4.211+0 1.981 7.93-1 -8.17-6 1.247+0 0.934 1.05+0 1.15-1 2.362+0 0.952 1.06+0 1.13-1 5.518-1 1.979 8.70-1	8.04-1 3.75-1 1.643-2 1.968 1.11+0 -2.95-6 6000 2.738+0 1.973 9.93-1 -6.93-6 6.830-1 0.835 1.12+0 1.39-1 1.289+0 0.854 1.14+0 1.37-1 3.577-1 1.970 1.06+0	8.15-1 4.17-1 1.124-2 1.959 1.28+0 -1.66-6 7000 1.884+0 1.964 1.17+0 -5.36-6 4.070-1 0.751 1.18+0 1.62-1 7.657-1 0.770 1.19+0 1.60-1 2.458-1 1.961 1.23+0	8.18-1 4.56-1 8.035-3 1.950 1.44+0 9.17-8 8000 1.354+0 1.955 1.34+0 -3.60-6 2.584-1 0.679 1.23+0 1.84-1 4.845-1 0.699 1.24+0 1.81-1 1.765-1 1.952 1.39+0	8.16-1 4.92-1 5.949-3 1.940 1.59+0 2.47-6 9000 1.006+0 1.945 1.49+0 -1.62-6 1.722-1 0.616 1.27+0 2.05-1 3.220-1 0.637 1.27+0 2.03-1 1.311-1 1.943 1.54+0	8.09-1 5.25-1 4.529-3 1.931 1.73+0 4.29-6 10000 7.688-1 1.936 1.63+0 9.05-7 1.194-1 0.560 1.30+0 2.25-1 2.226-1 0.582 1.30+0 2.22-1 1.001-1 1.933 1.67+0
$4s_{1/2}$ $E_b =$ 1.7 eV Z= 24, Cr: [And Shell $2s_{1/2}$ $E_b =$ 694.6 eV $2p_{1/2}$ $E_b =$ 583.7 eV $2p_{3/2}$ $E_b =$ 574.5 eV $3s_{1/2}$ $E_b =$ 74.1 eV	$ \begin{array}{c} \beta \\ \gamma \\ \delta \\ \hline \sigma \\ \rho \\ \gamma \\ \delta \\ \hline \sigma \\ \rho \\ \gamma \\ \delta \\ \hline \sigma \\ \rho \\ \gamma \\ \delta \\ \hline \sigma \\ \rho \\ \gamma \\ \delta \\ \delta \\ \sigma \\ \rho \\ \gamma \\ \delta \\ \delta \\ \sigma \\ \rho \\ \gamma \\ \delta \\ \delta \\ \sigma \\ \rho \\ \gamma \\ \delta \\ \delta \\ \sigma \\ \rho \\ \gamma \\ \delta \\ \delta \\ \sigma \\ \rho \\ \gamma \\ \delta \\ \delta \\ \sigma \\ \rho \\ \gamma \\ \delta \\ \delta \\ \sigma \\ \rho \\ \gamma \\ \delta \\ \delta \\ \sigma \\ \rho \\ \gamma \\ \delta \\ \delta \\ \sigma \\ \rho \\ \rho \\ \phi \\ \sigma \\ \rho \\ \rho \\ \phi \\ \sigma \\ \rho \\ \rho \\ \phi \\ \sigma \\ \rho \\ \phi \\ \phi$	0.735 5.58-1 1.23-1 3.603-1 1.999 9.19-2 -4.87-6 dd ¹ _{1/2} 4s ¹ _{1/2} k (eV) 1500 5.147+1 1.999 -4.86-2 -1.44-5 4.904+1 1.435 3.83-1 2.94-2 9.483+1 1.451 3.93-1 2.95-2 7.446+0 1.999 5.16-2 -6.64-6	6.13-1 1.58-1 1.986-1 1.998 2.25-1 -4.80-6 2000 3.001+1 1.999 4.94-2 -1.25-5 2.145+1 1.359 5.66-1 4.10-2 4.124+1 1.376 5.78-1 4.08-2 4.155+0 1.998 1.76-1 -6.73-6	3000 1.313+1 1.996 3.16-1 -1.08-5 6.325+0 1.194 7.99-1 6.46-2 1.208+1 1.211 8.12-1 6.38-2 1.755+0 1.993 4.29-1 -6.75-6	7.48-1 2.78-1 4.303-2 1.985 7.13-1 -4.52-6 4000 7.010+0 1.989 5.68-1 -9.29-6 2.564+0 1.052 9.46-1 8.97-2 4.875+0 1.070 9.59-1 8.86-2 9.242-1 1.986 6.61-1 -6.29-6	7.83-1 3.29-1 2.550-2 1.977 9.21-1 -3.88-6 5000 4.211+0 1.981 7.93-1 -8.17-6 1.247+0 0.934 1.05+0 1.15-1 2.362+0 0.952 1.06+0 1.13-1 5.518-1 1.979 8.70-1 -5.62-6	8.04-1 3.75-1 1.643-2 1.968 1.11+0 -2.95-6 6000 2.738+0 1.973 9.93-1 -6.93-6 6.830-1 0.835 1.12+0 1.39-1 1.289+0 0.854 1.14+0 1.37-1 3.577-1 1.970 1.06+0 -4.59-6	8.15-1 4.17-1 1.124-2 1.959 1.28+0 -1.66-6 7000 1.884+0 1.964 1.17+0 -5.36-6 4.070-1 0.751 1.18+0 1.62-1 7.657-1 0.770 1.19+0 1.60-1 2.458-1 1.961 1.23+0 -3.23-6	8.18-1 4.56-1 8.035-3 1.950 1.44+0 9.17-8 8000 1.354+0 1.955 1.34+0 -3.60-6 2.584-1 0.679 1.23+0 1.84-1 4.845-1 0.699 1.24+0 1.81-1 1.765-1 1.952 1.39+0 -1.49-6	8.16-1 4.92-1 5.949-3 1.940 1.59+0 2.47-6 9000 1.006+0 1.945 1.49+0 -1.62-6 1.722-1 0.616 1.27+0 2.05-1 3.220-1 0.637 1.27+0 2.03-1 1.311-1 1.943 1.54+0 6.69-7	8.09-1 5.25-1 4.529-3 1.931 1.73+0 4.29-6 10000 7.688-1 1.936 1.63+0 9.05-7 1.194-1 0.560 1.30+0 2.25-1 2.226-1 0.582 1.30+0 2.22-1 1.001-1 1.933 1.67+0 3.19-6
$4s_{1/2}$ $E_b =$ 1.7 eV Z= 24, Cr: [And Shell $2s_{1/2}$ $E_b =$ 694.6 eV $2p_{1/2}$ $E_b =$ 583.7 eV $2p_{3/2}$ $E_b =$ 574.5 eV $3s_{1/2}$ $E_b =$ 74.1 eV $3p_{1/2}$	β γ δ σ β γ δ δ σ σ β γ δ δ σ σ β γ δ δ σ σ β γ δ δ σ σ β γ δ δ σ σ β γ δ δ σ σ β γ δ δ σ σ δ β γ δ δ σ σ δ δ γ δ δ σ σ δ δ γ δ δ σ σ δ δ δ σ σ δ δ δ σ σ δ δ δ σ σ δ δ δ σ σ δ δ δ σ σ δ δ δ σ σ δ δ δ σ σ δ δ δ σ σ δ δ δ δ σ σ δ δ δ δ σ σ δ δ δ δ σ σ δ δ δ δ δ δ δ σ σ δ δ δ δ δ δ δ δ δ δ σ σ δ	0.735 5.58-1 1.23-1 3.603-1 1.999 9.19-2 -4.87-6 6d _{5/2} 4s _{1/2} k (eV) 1500 5.147+1 1.999 -4.86-2 -1.44-5 4.904+1 1.435 3.83-1 2.94-2 9.483+1 1.451 3.93-1 2.95-2 7.446+0 1.999 5.16-2 -6.64-6 4.784+0	6.13-1 1.58-1 1.986-1 1.998 2.25-1 -4.80-6 2000 3.001+1 1.999 4.94-2 -1.25-5 2.145+1 1.359 5.66-1 4.10-2 4.124+1 1.376 5.78-1 4.08-2 4.155+0 1.998 1.76-1 -6.73-6 2.187+0	3000 1.313+1 1.996 3.16-1 -1.08-5 6.325+0 1.194 7.99-1 6.46-2 1.208+1 1.211 8.12-1 6.38-2 1.755+0 1.993 4.29-1 -6.75-6 6.812-1	7.48-1 2.78-1 4.303-2 1.985 7.13-1 -4.52-6 4000 7.010+0 1.989 5.68-1 -9.29-6 2.564+0 1.052 9.46-1 8.97-2 4.875+0 1.070 9.59-1 8.86-2 9.242-1 1.986 6.61-1 -6.29-6 2.851-1	7.83-1 3.29-1 2.550-2 1.977 9.21-1 -3.88-6 5000 4.211+0 1.981 7.93-1 -8.17-6 1.247+0 0.934 1.05+0 1.15-1 2.362+0 0.952 1.06+0 1.13-1 5.518-1 1.979 8.70-1 -5.62-6 1.415-1	8.04-1 3.75-1 1.643-2 1.968 1.11+0 -2.95-6 6000 2.738+0 1.973 9.93-1 -6.93-6 6.830-1 0.835 1.12+0 1.39-1 1.289+0 0.854 1.14+0 1.37-1 3.577-1 1.970 1.06+0 -4.59-6 7.862-2	8.15-1 4.17-1 1.124-2 1.959 1.28+0 -1.66-6 7000 1.884+0 1.964 1.17+0 -5.36-6 4.070-1 0.751 1.18+0 1.62-1 7.657-1 0.770 1.19+0 1.60-1 2.458-1 1.961 1.23+0 -3.23-6 4.733-2	8.18-1 4.56-1 8.035-3 1.950 1.44+0 9.17-8 8000 1.354+0 1.955 1.34+0 -3.60-6 2.584-1 0.679 1.23+0 1.84-1 4.845-1 0.699 1.24+0 1.81-1 1.765-1 1.952 1.39+0 -1.49-6 3.027-2	8.16-1 4.92-1 5.949-3 1.940 1.59+0 2.47-6 9000 1.006+0 1.945 1.49+0 -1.62-6 1.722-1 0.616 1.27+0 2.05-1 3.220-1 0.637 1.27+0 2.03-1 1.943 1.54+0 6.69-7 2.030-2	8.09-1 5.25-1 4.529-3 1.931 1.73+0 4.29-6 10000 7.688-1 1.936 1.63+0 9.05-7 1.194-1 0.560 1.30+0 2.25-1 2.226-1 0.582 1.30+0 2.22-1 1.001-1 1.933 1.67+0 3.19-6 1.414-2
$4s_{1/2}$ $E_b =$ 1.7 eV Z= 24, Cr: [And Shell $2s_{1/2}$ $E_b =$ 694.6 eV $2p_{1/2}$ $E_b =$ 583.7 eV $2p_{3/2}$ $E_b =$ 574.5 eV $3s_{1/2}$ $E_b =$ 74.1 eV	$ \begin{array}{c} \beta \\ \gamma \\ \delta \\ \hline \sigma \\ \rho \\ \gamma \\ \delta \\ \hline \sigma \\ \rho \\ \gamma \\ \delta \\ \hline \sigma \\ \rho \\ \gamma \\ \delta \\ \hline \sigma \\ \rho \\ \gamma \\ \delta \\ \delta \\ \sigma \\ \rho \\ \gamma \\ \delta \\ \delta \\ \sigma \\ \rho \\ \gamma \\ \delta \\ \delta \\ \sigma \\ \rho \\ \gamma \\ \delta \\ \delta \\ \sigma \\ \rho \\ \gamma \\ \delta \\ \delta \\ \sigma \\ \rho \\ \gamma \\ \delta \\ \delta \\ \sigma \\ \rho \\ \gamma \\ \delta \\ \delta \\ \sigma \\ \rho \\ \gamma \\ \delta \\ \delta \\ \sigma \\ \rho \\ \gamma \\ \delta \\ \delta \\ \sigma \\ \rho \\ \rho \\ \phi \\ \sigma \\ \rho \\ \rho \\ \phi \\ \sigma \\ \rho \\ \rho \\ \phi \\ \sigma \\ \rho \\ \phi \\ \phi$	0.735 5.58-1 1.23-1 3.603-1 1.999 9.19-2 -4.87-6 dd ¹ _{1/2} 4s ¹ _{1/2} k (eV) 1500 5.147+1 1.999 -4.86-2 -1.44-5 4.904+1 1.435 3.83-1 2.94-2 9.483+1 1.451 3.93-1 2.95-2 7.446+0 1.999 5.16-2 -6.64-6	6.13-1 1.58-1 1.986-1 1.998 2.25-1 -4.80-6 2000 3.001+1 1.999 4.94-2 -1.25-5 2.145+1 1.359 5.66-1 4.10-2 4.124+1 1.376 5.78-1 4.08-2 4.155+0 1.998 1.76-1 -6.73-6	3000 1.313+1 1.996 3.16-1 -1.08-5 6.325+0 1.194 7.99-1 6.46-2 1.208+1 1.211 8.12-1 6.38-2 1.755+0 1.993 4.29-1 -6.75-6	7.48-1 2.78-1 4.303-2 1.985 7.13-1 -4.52-6 4000 7.010+0 1.989 5.68-1 -9.29-6 2.564+0 1.052 9.46-1 8.97-2 4.875+0 1.070 9.59-1 8.86-2 9.242-1 1.986 6.61-1 -6.29-6	7.83-1 3.29-1 2.550-2 1.977 9.21-1 -3.88-6 5000 4.211+0 1.981 7.93-1 -8.17-6 1.247+0 0.934 1.05+0 1.15-1 2.362+0 0.952 1.06+0 1.13-1 5.518-1 1.979 8.70-1 -5.62-6	8.04-1 3.75-1 1.643-2 1.968 1.11+0 -2.95-6 6000 2.738+0 1.973 9.93-1 -6.93-6 6.830-1 0.835 1.12+0 1.39-1 1.289+0 0.854 1.14+0 1.37-1 3.577-1 1.970 1.06+0 -4.59-6	8.15-1 4.17-1 1.124-2 1.959 1.28+0 -1.66-6 7000 1.884+0 1.964 1.17+0 -5.36-6 4.070-1 0.751 1.18+0 1.62-1 7.657-1 0.770 1.19+0 1.60-1 2.458-1 1.961 1.23+0 -3.23-6	8.18-1 4.56-1 8.035-3 1.950 1.44+0 9.17-8 8000 1.354+0 1.955 1.34+0 -3.60-6 2.584-1 0.679 1.23+0 1.84-1 4.845-1 0.699 1.24+0 1.81-1 1.765-1 1.952 1.39+0 -1.49-6	8.16-1 4.92-1 5.949-3 1.940 1.59+0 2.47-6 9000 1.006+0 1.945 1.49+0 -1.62-6 1.722-1 0.616 1.27+0 2.05-1 3.220-1 0.637 1.27+0 2.03-1 1.311-1 1.943 1.54+0 6.69-7	8.09-1 5.25-1 4.529-3 1.931 1.73+0 4.29-6 10000 7.688-1 1.936 1.63+0 9.05-7 1.194-1 0.560 1.30+0 2.25-1 2.226-1 0.582 1.30+0 2.22-1 1.001-1 1.933 1.67+0 3.19-6

	able 1 (contin	,										
		δ	2.55-2	3.75-2	6.38-2	9.01-2		1.40-1	1.63-1	1.85-1	2.06-1	2.26-1
Section Sec	$3p_{3/2}$											2.601-2 0.551
\$\frac{\delta}{2}, \text{of} \frac{\delta}{2}, \text{of} \frac{\delta}{2}, \text{of} \frac{\delta}{2}, \text{of} \frac{\delta}{2} \de	$E_b = 39.9 \text{ eV}$											1.28+0
= β 0.777 0.665 0.524 0.438 0.373 0.321 0.275 0.234 0.198 0.192 0.296 0.571 1.62-1 7.62-1 7.62-1 7.62-1 3.62												2.24 - 1
28 eV y 5,71 1 6,29 7,109 7,09 7,05 1 3,00 1 3,00 1 3,60 1 3,60 1 4,07 1 4,07 1 4,07 1 5,00	3d _{3/2}	σ										2.102-4
1.19-1 1.53-1 2.15-1 2.70-1 3.20-1 3.66-1 4.08-1 4.47-1 4.83-1 4.95-2 2.50-1 5.11-2 1.581-2 2.28-3 1.44-1 7.077-4 0.28-3 1.28-2 2.28 7.48-1 2.50-1 5.12-1 7.72-1 7.72-1 3.20-1 3.66-1 4.06-1 4.44-1 4.79-1 5.89-2 2.28 7.70-1 3.20-1 3.65-1 4.06-1 4.44-1 4.79-1 5.89-2 3.69-2 3.65-1 4.06-1 4.44-1 4.79-1 5.89-2 3.69-2 3.65-1 4.06-1 4.44-1 4.79-1 5.89-2 3.69-2 3.69-2 3.65-1 4.06-1 4.44-1 4.79-1 5.89-2 3.69-2 3.69-2 3.65-1 4.06-1 4.44-1 4.79-1 5.89-2 3.69-2 3.	$E_b =$											0.165
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	2.9 eV											8.42-1 5.16-1
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	3d= /2											2.927-4
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $	$E_b =$											0.210
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	2.2 eV											8.78-1
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$												5.13-1
1.0 eV y 6.13-2 1.88-1 4.40-1 6.70-1 8.77-1 1.00+0 1.23+0 1.33+0 1.54-0 1.23+0 1.33+0 1.54-0 1.23+0 1.43-6 5.45-7 2.23+0.55-1 1.23+0 1.43-6 5.45-7 2.23+0.55-1 1.23+0 1.43-6 5.45-7 2.23+0.55-1 1.23+0	4s _{1/2}											3.815-3 1.933
$\begin{array}{c c c c c c c c c c c c c c c c c c c $												1.68+0
Relation			-6.22 - 6	-6.12 - 6	-6.03 - 6	-5.80 - 6	-5.16 - 6	-4.44 - 6	-3.18 - 6	-1.43 - 6	9.54 - 7	2.92 - 6
rell 100 2000 3000 4000 5000 6000 7000 8000 9000 1	Z= 25, Mn: [<i>A</i>	\r]3d _{3/2}	3d _{5/2} 4s _{1/2}									
$ \begin{array}{c} i_{12} \\ = \\ \beta \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0$			k (eV)									
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	Shell		1500	2000	3000	4000	5000	6000	7000	8000	9000	10000
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	2s _{1/2}											8.859-1
S	$E_b = 760.0 \text{ eV}$											1.939 1.58+0
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	703.0 CV											-1.24-0
$\begin{array}{c} = & \beta & 1.448 & 1.382 & 1.234 & 1.098 & 0.981 & 0.882 & 0.797 & 0.723 & 0.659 & 0.811 \\ 1.144 & y & 3.37 - 1 & 5.32 - 1 & 7.84 - 1 & 1.05 + 0 & 1.14 + 0 & 1.20 + 0 & 1.25 + 0 & 1.29 + 0 & 1.2$	$2p_{1/2}$	σ	5.833+1	2.576+1	7.705+0	3.152+0	1.544+0	8.505-1	5.093-1	3.246-1	2.171-1	1.510-1
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$E_b =$	β				1.098						0.602
$\begin{array}{c} g_{2/2} \\ g_{1/2} \\$	651.4 eV											1.32+0 2.17-1
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	2n											2.807-1
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	$E_b =$											0.625
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	640.3 eV	γ						1.15+0				1.33+0
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$		δ										2.14-1
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$3s_{1/2}$											1.190-1
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$E_b = 83.9 \text{ eV}$											1.936 1.63+0
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$												1.52-6
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	3p _{1/2}	σ										1.867-2
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	$E_b =$											0.568
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	53.1 eV											1.30+0 2.18-1
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	3p _{3/2}											3.401-2
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$E_b =$								0.771			0.591
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	46.4 eV											1.30+0
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	2.4											2.16-1
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$E_b =$											3.807-4 0.181
$\begin{array}{cccccccccccccccccccccccccccccccccccc$												8.75-1
$\begin{array}{cccccccccccccccccccccccccccccccccccc$		δ	1.14-1	1.47-1	2.08-1	2.63-1	3.13-1	3.58-1	3.99-1	4.37-1	4.73-1	5.06-1
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	3d _{5/2}											5.375-4
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$E_b = 2.7 \text{ eV}$											0.226 9.10-1
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	2.7 C V											5.03-1
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	4s _{1/2}	σ										5.827-3
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$E_b =$	β	2.000	1.998	1.994	1.987			1.963	1.954	1.945	1.935
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	1.9 eV											1.64+0 1.58-6
$\frac{k (\text{eV})}{1500} \qquad \frac{k (\text{eV})}{1500}$	7= 26 Fe: [A			7.00 0	7.55 0	7.10 0	0.00	3.32 0	1.00 0	2.51	1.00 7	1.50 0
The left of the l	_ =0,1C.[A	- J-u3/2										
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	Shell			2000	3000	4000	5000	6000	7000	8000	9000	10000
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	2s _{1/2}	σ										1.013+0
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	$E_b =$		1.998	1.999	1.997	1.992	1.985	1.977	1.969	1.960	1.951	1.941
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	846.1 eV											1.53+0
$\beta=$ β 1.454 1.404 1.267 1.135 1.019 0.921 0.836 0.762 0.697 0 21.1 eV γ 2.85 -1 4.93 -1 7.64 -1 9.35 -1 1.06+0 1.14+0 1.21+0 1.27+0 1.31+0 1.	n											-3.80-0
21.1 eV γ 2.85 -1 4.93 -1 7.64 -1 9.35 -1 1.06+0 1.14+0 1.21+0 1.27+0 1.31+0 1	$\begin{array}{l} 2p_{1/2} \\ E_b = \end{array}$											1.890-1 0.639
	721.1 eV											1.35+0
			2.59-2	3.58-2	5.75-2	8.02-2	1.03-1	1.26-1	1.48-1	1.69-1	1.89-1	2.09-1

able 1 (contin	ued)										
$2p_{3/2}$	σ	1.335+2	5.907+1	1.773+1	7.270+0	3.567+0	1.968+0	1.179+0	7.518 - 1	5.030 - 1	3.497 - 1
$E_b =$	β	1.473	1.423	1.287	1.155	1.040	0.942	0.858	0.784	0.720	0.663
708.1 eV	γ	2.94 - 1	5.06 - 1	7.80 - 1	9.52 - 1	1.07+0	1.16+0	1.23+0	1.28+0	1.32+0	1.36+0
	δ	2.61-2	3.58-2	5.68-2	7.89-2	1.01-1	1.24-1	1.45-1	1.66-1	1.86-1	2.06-1
$3s_{1/2}$	σ	9.411+0	5.316+0	2.282+0	1.217+0	7.342-1	4.802-1	3.326-1	2.405-1	1.797-1	1.380-1
$E_b =$	β	2.000	1.999	1.995	1.989	1.982	1.974	1.965	1.956	1.947	1.938
92.9 eV	γ	1.89-3	1.07-1	3.42-1	5.67-1	7.73-1	9.61-1	1.13+0	1.29+0	1.44+0	1.58+0
	δ	-1.02-5	-1.02-5	-1.03-5	-1.01-5	-9.41-6	-8.45-6	-7.05-6	-5.32-6	-3.11-6	-4.63-7
$3p_{1/2}$ $E_b =$	σ_{ρ}	6.920+0 1.466	3.241+0 1.371	1.042+0 1.205	4.457-1 1.070	2.250-1 0.960	1.268-1 0.867	7.721-2 0.787	4.987-2 0.718	3.372-2 0.657	2.366-2 0.602
58.1 eV	β γ	4.30-1	5.78-1	7.89-1	9.35-1	1.04+0	1.13+0	1.19+0	1.24+0	1.29+0	1.33+0
30.1 CV	δ	2.09-2	3.20-2	5.54-2	7.97-2	1.04-1	1.27-1	1.49-1	1.70-1	1.91-1	2.10-1
$3p_{3/2}$	σ	1.316+1	6.130+0	1.954+0	8.308-1	4.174-1	2.341-1	1.420-1	9.139-2	6.159-2	4.308-2
$E_b =$	β	1.483	1.389	1.224	1.090	0.980	0.887	0.808	0.740	0.680	0.626
52.0 eV	γ	4.37 - 1	5.87 - 1	8.01 - 1	9.47 - 1	1.05+0	1.14+0	1.20+0	1.25+0	1.29+0	1.33+0
	δ	2.09-2	3.15-2	5.43-2	7.81-2	1.02-1	1.24-1	1.46-1	1.68-1	1.88-1	2.07 - 1
$3d_{3/2}$	σ	1.214+0	4.179 - 1	8.804 - 2	2.798 - 2	1.121 - 2	5.220-3	2.704 - 3	1.517 - 3	9.058 - 4	5.686 - 4
$E_b =$	β	0.848	0.730	0.580	0.485	0.415	0.359	0.311	0.269	0.232	0.197
3.9 eV	γ	5.84-1	6.53-1	7.42-1	8.01-1	8.42-1	8.71-1	8.90-1	9.01-1	9.06-1	9.06-1
	δ	1.09-1	1.42-1	2.02-1	2.56-1	3.05-1	3.49-1	3.90-1	4.28-1	4.64-1	4.97-1
3d _{5/2}	σ_{ρ}	1.764+0	6.047-1 0.728	1.268-1	4.014-2 0.497	1.603-2 0.434	7.446-3 0.384	3.847-3 0.341	2.154-3	1.283-3	8.039-4
$E_b = 3.1 \text{ eV}$	β	0.842 5.82-1	0.728 6.52-1	0.586 7.44-1	0.497 8.06-1	0.434 8.52-1	0.384 8.85-1	0.341 9.09-1	0.304 9.25-1	0.271 9.35-1	0.241 9.40-1
J.1 CV	$_{\delta}^{\gamma}$	1.11-1	1.43-1	2.03-1	2.56-1	3.05-1	3.48-1	3.89-1	4.26-1	4.61–1	4.93-1
4s _{1/2}	σ	4.569-1	2.560-1	1.089-1	5.780-2	3.479-2	2.272-2	1.572-2	1.136-2	8.487-3	6.515-3
$E_b =$	β	2.000	1.999	1.995	1.989	1.981	1.973	1.965	1.956	1.947	1.938
2.1 eV	γ	1.17-2	1.20-1	3.55-1	5.78-1	7.82-1	9.69-1	1.14+0	1.30+0	1.45+0	1.59+0
	δ	-9.45 - 6	-9.43 - 6	-9.46 - 6	-9.29 - 6	-8.77 - 6	-7.88 - 6	-6.62 - 6	-4.91 - 6	-2.50-6	-3.33-7
Z= 27, Co: [A	r]3d _{3/2} 3	3d _{5/2} 4s _{1/2}									
		k (eV)									
Shell		1500	2000	3000	4000	5000	6000	7000	8000	9000	10000
2s _{1/2}	σ	6.420+1	3.879+1	1.770+1	9.702+0	5.945+0	3.927+0	2.738+0	1.990+0	1.493+0	1.150+0
$E_b =$	β	1.996	1.999	1.998	1.993	1.987	1.979	1.971	1.962	1.953	1.944
925.6 eV	γ	-2.56-2	-4.74-2	1.54 - 1	3.92 - 1	6.16 - 1	8.19 - 1	1.00+0	1.17+0	1.33+0	1.47+0
	δ	-2.66-5	-2.32-5	-2.04-5	-1.86-5	-1.69-5	-1.52-5	-1.36-5	-1.16-5	-9.35-6	-6.87 - 6
$2p_{1/2}$	σ	8.089+1	3.642+1	1.115+1	4.638+0	2.300+0	1.280+0	7.734-1	4.966 - 1	3.343-1	2.339-1
$E_b =$	β	1.454	1.421	1.296	1.169	1.056	0.959	0.874	0.800	0.734	0.676
793.6 eV	$_{\delta}^{\gamma}$	2.27-1 2.40-2	4.49-1 3.36-2	7.39-1 5.40-2	9.24-1 7.55-2	1.05+0 9.76-2	1.15+0 1.19-1	1.22+0 1.41-1	1.28+0 1.62-1	1.33+0 1.81-1	1.37+0 2.01-1
2n	σ	1.562+2	6.975+1	2.116+1	8.745+0	4.316+0	2.392+0	1.440+0	9.210-1	6.180-1	4.309-1
$\begin{array}{l} 2p_{3/2} \\ E_b = \end{array}$	β	1.474	1.442	1.318	1.191	1.078	0.981	0.897	0.824	0.758	0.701
778.6 eV	γ	2.37-1	4.62-1	7.56-1	9.42-1	1.07+0	1.17+0	1.24+0	1.30+0	1.34+0	1.38+0
	δ	2.44-2	3.37-2	5.33-2	7.42 - 2	9.57 - 2	1.17 - 1	1.38-1	1.59-1	1.78 - 1	1.98 - 1
3s _{1/2}	σ	1.037+1	5.894+0	2.551+0	1.368+0	8.296-1	5.449-1	3.788-1	2.747-1	2.059-1	1.585-1
$E_b =$	β	1.999	1.999	1.996	1.990	1.983	1.975	1.967	1.959	1.950	1.941
100.7 eV	γ	-1.87 - 2	7.63 - 2	3.01 - 1	5.22 - 1	7.27 - 1	9.15 - 1	1.09+0	1.25+0	1.40+0	1.54+0
	δ	-1.22-5	-1.24-5	-1.27-5	-1.25-5	-1.18-5	-1.08-5	-9.40-6	-7.66-6	-5.48-6	-2.82-6
$3p_{1/2}$	σ	8.071+0	3.825+0	1.248+0	5.393-1	2.745-1	1.556-1	9.530-2	6.183-2	4.198-2	2.956-2
$E_b =$	β	1.488	1.397	1.235	1.103	0.994	0.902	0.822	0.753	0.691	0.636
63.2 eV	$_{\delta}^{\gamma}$	4.03-1 1.90-2	5.56-1	7.77-1	9.31-1	1.04+0 9.79-2	1.13+0 1.20-1	1.20+0 1.42-1	1.26+0	1.31+0	1.35+0 2.02-1
•			2.91-2	5.14-2	7.47-2				1.63-1	1.83-1	
$3p_{3/2}$	σ	1.539+1	7.249+0	2.344+0	1.006+0	5.094-1	2.874-1	1.753-1	1.133-1	7.664-2	5.378-2
$E_b = 57.7 \text{ eV}$	β	1.505 4.10-1	1.416 5.66-1	1.255 7.90-1	1.124 9.44-1	1.016 1.06+0	0.924 1.15+0	0.845 1.21+0	0.776 1.27+0	0.715 1.32+0	0.660 1.35+0
37.7 CV	δ	1.90-2	2.88-2	5.03-2	7.31–2	9.58-2	1.18-1	1.39-1	1.60-1	1.80-1	1.99-1
3d _{3/2}	σ	1.646+0	5.714-1	1.219-1	3.912-2	1.581-2	7.415-3	3.865-3	2.180-3	1.308-3	8.240-4
$E_b =$	β	0.885	0.766	0.608	0.507	0.435	0.377	0.328	0.286	0.247	0.212
2.7 eV	$_{\delta}^{\gamma}$	5.87-1 1.06-1	6.63-1 1.37-1	7.57-1 1.96-1	8.18-1 2.48-1	8.61-1 2.97-1	8.92-1 3.41-1	9.13-1 3.82-1	9.27-1 4.19-1	9.34-1 4.55-1	9.35-1 4.88-1
	σ	2.399+0	8.297-1	1.760-1	5.624-2	2.265-2	1.059-2	5.508-3	3.099-3	1.855-3	1.166-3
3d= /2		0.878	0.762	0.612	0.518	0.452	0.400	0.357	0.320	0.286	0.256
			· · · · · · ·	J.J.2		8.70-1	9.05-1	9.31-1	9.49-1	9.62-1	9.69-1
$E_b =$	β		6.61 - 1	7.58 - 1	8.22-1	0./U-1					9.09-1
$3d_{5/2}$ $E_b =$ 3.3 eV		5.85-1 1.07-1	6.61-1 1.39-1	7.58-1 1.97-1	8.22-1 2.49-1	2.97-1	3.40-1	3.80-1	4.18-1	4.52 - 1	4.84-1
$E_b =$ 3.3 eV	β γ δ	5.85-1 1.07-1	1.39-1	1.97-1	2.49-1	2.97-1	3.40-1	3.80-1	4.18-1	4.52-1	4.84-1
$E_b = 3.3 \text{ eV}$ $4s_{1/2}$	β γ	5.85 - 1									
$E_b = 3.3 \text{ eV}$	$\begin{array}{c} \beta \\ \gamma \\ \delta \end{array}$ $\begin{array}{c} \sigma \\ \beta \\ \gamma \end{array}$	5.85-1 1.07-1 4.871-1 1.999 -9.69-3	1.39-1 2.745-1 1.999 8.89-2	1.97-1 1.176-1 1.995 3.15-1	2.49-1 6.278-2 1.990 5.34-1	2.97-1 3.796-2 1.983 7.37-1	3.40-1 2.489-2 1.975 9.23-1	3.80-1 1.728-2 1.967 1.09+0	4.18-1 1.252-2 1.958 1.25+0	4.52-1 9.383-3 1.949 1.40+0	4.84-1 7.221-3 1.940 1.54+0
$E_b = 3.3 \text{ eV}$ $4s_{1/2}$ $E_b =$	β γ δ σ β	5.85-1 1.07-1 4.871-1 1.999	1.39-1 2.745-1 1.999	1.97-1 1.176-1 1.995	2.49-1 6.278-2 1.990	2.97-1 3.796-2 1.983	3.40-1 2.489-2 1.975	3.80-1 1.728-2 1.967	4.18-1 1.252-2 1.958	4.52-1 9.383-3 1.949	4.84-1 7.221-3 1.940

Table 1 (continued)

Z= 28, Ni: [Ar] $3d_{3/2}^4 3d_{5/2}^4 4s_{1/2}^2$

Shell		1500	2000	3000	4000	5000	6000	7000	8000	9000	10000
$2s_{1/2}$	σ	6.817+1	4.171+1	1.931+1	1.067+1	6.582+0	4.369+0	3.059+0	2.231+0	1.679+0	1.297+0
$E_b =$	β	1.995	1.998	1.999	1.995	1.988	1.981	1.973	1.965	1.956	1.947
1008.1 eV	γ	2.51-2	-6.15 - 2	1.05 - 1	3.35 - 1	5.57 - 1	7.61 - 1	9.47 - 1	1.12+0	1.28+0	1.42+0
	δ	-2.98 - 5	-2.72 - 5	-2.46-5	-2.27 - 5	-2.08 - 5	-1.90-5	-1.73 - 5	-1.52 - 5	-1.30-5	-1.03-
$2p_{1/2}$	σ	9.410+1	4.278+1	1.325+1	5.550+0	2.769+0	1.549+0	9.392 - 1	6.051 - 1	4.087 - 1	2.866-
$E_b =$	β	1.446	1.434	1.323	1.201	1.092	0.996	0.912	0.837	0.771	0.712
871.9 eV	γ	1.62-1	4.00-1	7.10-1	9.09-1	1.05+0	1.15+0	1.23+0	1.30+0	1.35+0	1.39+0
	δ	2.19-2	3.15-2	5.06-2	7.12-2	9.25-2	1.14-1	1.34-1	1.55-1	1.74-1	1.93-1
$2p_{3/2}$	σ	1.816+2	8.180+1	2.508+1	1.043+1	5.178+0	2.883+0	1.741+0	1.118+0	7.523-1	5.258-
E _b = 854.7 eV	β	1.467 1.72-1	1.456 4.13-1	1.346 7.28-1	1.225 9.29-1	1.116 1.07+0	1.020 1.17+0	0.937 1.25+0	0.863 1.31+0	0.797 1.36+0	0.738 1.40+0
334.7 EV	$_{\delta}^{\gamma}$	2.24-2	3.17-2	5.00-2	6.99-2	9.06-2	1.17+0	1.32-1	1.52-1	1.71-1	1.40+0
$3s_{1/2}$	σ	1.137+1	6.500+0	2.835+0	1.529+0	9.312-1	6.139-1	4.282-1	3.115-1	2.341-1	1.806-
$E_b =$	β	1.999	1.999	1.996	1.991	1.985	1.977	1.969	1.961	1.952	1.943
111.8 eV	γ	-3.66-2	4.71-2	2.61-1	4.78-1	6.81-1	8.68-1	1.04+0	1.20+0	1.35+0	1.49+0
	δ	-1.43-5	-1.49 - 5	-1.54 - 5	-1.52 - 5	-1.46 - 5	-1.36 - 5	-1.22 - 5	-1.04 - 5	-8.23 - 6	-5.55-
$3p_{1/2}$	σ	9.330+0	4.473+0	1.481+0	6.459-1	3.312-1	1.889-1	1.163-1	7.577-2	5.163-2	3.648-
$E_b =$	β	1.507	1.420	1.263	1.135	1.028	0.937	0.857	0.787	0.725	0.669
71.2 eV	γ	3.73 - 1	5.32 - 1	7.64 - 1	9.25 - 1	1.04+0	1.14+0	1.21+0	1.27+0	1.32+0	1.37+0
	δ	1.71-2	2.65-2	4.76-2	7.01-2	9.26-2	1.14-1	1.36-1	1.56-1	1.76-1	1.95-1
$3p_{3/2}$	σ	1.790+1	8.520+0	2.791+0	1.208+0	6.159-1	3.495-1	2.141-1	1.389-1	9.433-2	6.640-2
$E_b =$	β	1.526	1.441	1.286	1.158	1.051	0.960	0.881	0.812	0.750	0.695
69.7 eV	$_{\delta}^{\gamma}$	3.81-1 1.73-2	5.42-1 2.62-2	7.77-1 4.66-2	9.40-1 6.85-2	1.06+0 9.04-2	1.15+0 1.12-1	1.23+0 1.33-1	1.29+0 1.53-1	1.33+0 1.72-1	1.37+0 1.91-1
$3d_{3/2}$ $E_b =$	$\frac{\sigma}{\beta}$	2.190+0 0.921	7.669-1 0.800	1.654-1 0.635	5.353-2 0.530	2.179-2 0.454	1.029-2 0.395	5.395-3 0.345	3.058-3 0.302	1.842-3 0.263	1.165- 0.228
3.9 eV	γ	5.88-1	6.70-1	7.71-1	8.35-1	8.80-1	9.13-1	9.36-1	9.51-1	9.60-1	9.64-1
5.5 01	δ	1.02-1	1.33-1	1.89-1	2.41-1	2.89-1	3.32-1	3.73-1	4.10-1	4.45-1	4.78-1
3d _{5/2}	σ	3.187+0	1.112+0	2.387-1	7.695-2	3.122-2	1.470-2	7.687-3	4.347-3	2.613-3	1.649-
$E_b =$	β	0.912	0.795	0.637	0.539	0.470	0.417	0.373	0.335	0.301	0.270
$E_b = 3.3 \text{ eV}$	γ	5.85 - 1	6.68 - 1	7.71 - 1	8.38 - 1	8.88 - 1	9.25 - 1	9.53 - 1	9.73 - 1	9.87 - 1	9.96 - 1
	δ	1.03 - 1	1.34 - 1	1.91 - 1	2.42 - 1	2.89 - 1	3.32 - 1	3.72 - 1	4.09 - 1	4.43 - 1	4.75 - 1
4s _{1/2}	σ	5.162-1	2.926-1	1.263-1	6.778-2	4.116-2	2.709-2	1.887-2	1.371-2	1.030-2	7.945-
$E_b =$	β	1.999	1.999	1.996	1.991	1.984	1.977	1.969	1.960	1.951	1.942
2.2 eV	γ	-2.83-2	6.00-2	2.76-1	4.91 - 1	6.92 - 1	8.77 - 1	1.05+0	1.21+0	1.36+0	1.50+0
2.2 eV	δ	-1.34-5	6.00-2 -1.40-5	2.76-1 -1.44-5							
2.2 eV Z= 29, Cu: [A i	δ	-1.34-5			4.91 - 1	6.92 - 1	8.77 - 1	1.05+0	1.21+0	1.36+0	1.50+0
2.2 eV	δ	-1.34-5			4.91 - 1	6.92 - 1	8.77 - 1	1.05+0	1.21+0	1.36+0	1.50+0
2.2 eV	δ	$ \begin{array}{r} -1.34 - 5 \\ \mathbf{3d_{5/2}^6 4s_{1/2}^1} \end{array} $			4.91 - 1	6.92 - 1	8.77 - 1	1.05+0	1.21+0	1.36+0	1.50+0
2.2 eV Z= 29, Cu: [A r Shell	$\frac{\delta}{r]3d_{3/2}^4}$	$ \begin{array}{r} -1.34 - 5 \\ 3d_{5/2}^{6} 4s_{1/2}^{1} \\ \underline{k \text{ (eV)}} \\ 1500 \end{array} $	-1.40-5 2000	-1.44-5 3000	4.91-1 -1.42-5	6.92-1 -1.37-5 5000	8.77-1 -1.29-5	1.05+0 -1.17-5	1.21+0 -9.98-6 8000	1.36+0 -7.74-6	1.50+0 -5.40-
2.2 eV Z= 29, Cu: [An Shell 2s _{1/2}	$\frac{\delta}{r]3d_{3/2}^4}$	$ \begin{array}{r} -1.34-5 \\ \mathbf{3d_{5/2}^6 4s_{1/2}^1} \\ k \text{ (eV)} \end{array} $	-1.40-5	-1.44-5	4.91-1 -1.42-5	6.92-1 -1.37-5	8.77-1 -1.29-5	1.05+0 -1.17-5	1.21+0 -9.98-6	1.36+0 -7.74-6	1.50+0 -5.40-
2.2 eV Z= 29, Cu: [A r Shell	$\frac{\delta}{r]3d_{3/2}^4}$ $\frac{\sigma}{\beta}$ γ	$ \begin{array}{r} -1.34-5 \\ 3d_{5/2}^{6} 4s_{1/2}^{1} \\ \hline $	2000 4.476+1 1.997 -6.29-2	3000 2.101+1 1.999 5.85-2	4.91-1 -1.42-5 4000 1.171+1 1.996 2.77-1	5000 7.259+0 1.990 4.94-1	6000 4.841+0 1.983 6.96-1	7000 3.403+0 1.975 8.83-1	8000 2.489+0 1.967 1.06+0	1.36+0 -7.74-6 9000 1.879+0 1.959 1.22+0	1.50+0 -5.40- 10000 1.455+0 1.950 1.37+0
2.2 eV Z= 29, Cu: [And Shell 2s _{1/2} E _b =	$\frac{\delta}{r]3d_{3/2}^4}$ $\frac{\sigma}{\beta}$	$ \begin{array}{r} -1.34-5 \\ 3d_{5/2}^{6} 4s_{1/2}^{1} \\ \hline k \text{ (eV)} \\ \hline 1500 \\ 7.216+1 \\ 1.992 \end{array} $	-1.40-5 2000 4.476+1 1.997	3000 2.101+1 1.999	4.91-1 -1.42-5 4000 1.171+1 1.996	5000 7.259+0 1.990	8.77-1 -1.29-5 6000 4.841+0 1.983	7000 3.403+0 1.975	1.21+0 -9.98-6 8000 2.489+0 1.967	1.36+0 -7.74-6 9000 1.879+0 1.959	1.50+0 -5.40- 10000 1.455+0 1.950
2.2 eV Z= 29, Cu: [And Shell 2s _{1/2} E _b =	$\frac{\delta}{\mathbf{r}]\mathbf{3d}_{3/2}^{4}}$ $\frac{\sigma}{\beta}$ $\frac{\gamma}{\delta}$ σ	$ \begin{array}{r} -1.34-5 \\ 3d_{5/2}^{6} 4s_{1/2}^{1} \\ \underline{k (eV)} \\ 1500 \\ 7.216+1 \\ 1.992 \\ 1.15-1 \\ -2.66-5 \\ 1.092+2 \end{array} $	2000 4.476+1 1.997 -6.29-2 -3.04-5 5.008+1	3000 2.101+1 1.999 5.85-2 -2.90-5 1.567+1	4.91-1 -1.42-5 4000 1.171+1 1.996 2.77-1 -2.70-5 6.609+0	5000 7.259+0 1.990 4.94-1 -2.55-5 3.315+0	8.77-1 -1.29-5 6000 4.841+0 1.983 6.96-1 -2.38-5 1.862+0	7000 3.403+0 1.975 8.83-1 -2.18-5 1.133+0	8000 2.489+0 1.967 1.06+0 -1.97-5 7.323-1	1.36+0 -7.74-6 9000 1.879+0 1.959 1.22+0 -1.70-5 4.959-1	1.50+0 -5.40- 10000 1.455+0 1.950 1.37+0 -1.45- 3.486-
2.2 eV Z= 29, Cu: [An Shell $2s_{1/2}$ $E_b = 1096.1$ eV $2p_{1/2}$ $E_b = 1096.1$	$\frac{\delta}{\mathbf{r}]\mathbf{3d_{3/2}^4}}$ $\frac{\sigma}{\beta}$ $\frac{\gamma}{\delta}$ $\frac{\sigma}{\beta}$	$ \begin{array}{r} -1.34-5 \\ 3d_{5/2}^{6} 4s_{1/2}^{1} \\ \underline{k \text{ (eV)}} \\ 1500 \\ 7.216+1 \\ 1.992 \\ 1.15-1 \\ -2.66-5 \\ 1.092+2 \\ 1.427 \end{array} $	2000 4.476+1 1.997 -6.29-2 -3.04-5 5.008+1 1.443	3000 2.101+1 1.999 5.85-2 -2.90-5 1.567+1 1.346	4.91-1 -1.42-5 4000 1.171+1 1.996 2.77-1 -2.70-5 6.609+0 1.236	5000 7.259+0 1.990 4.94-1 -2.55-5 3.315+0 1.132	8.77-1 -1.29-5 6000 4.841+0 1.983 6.96-1 -2.38-5 1.862+0 1.038	1.05+0 -1.17-5 7000 3.403+0 1.975 8.83-1 -2.18-5 1.133+0 0.955	8000 2.489+0 1.967 1.06+0 -1.97-5 7.323-1 0.880	1.36+0 -7.74-6 9000 1.879+0 1.959 1.22+0 -1.70-5 4.959-1 0.813	1.50+0 -5.40- 10000 1.455+0 1.950 1.37+0 -1.45- 3.486- 0.751
2.2 eV Z= 29, Cu: [At Shell $2s_{1/2}$ $E_b = 1096.1 \text{ eV}$	$ \frac{\delta}{\mathbf{r}]\mathbf{3d_{3/2}^4}} $ $ \frac{\sigma}{\beta}$ $ \frac{\gamma}{\delta}$ $ \frac{\sigma}{\beta}$ $ \frac{\sigma}{\beta}$ $ \frac{\sigma}{\gamma}$	$-1.34-5$ $3d_{5/2}^{6} 4s_{1/2}^{1}$ $k \text{ (eV)}$ 1500 $7.216+1$ 1.992 $1.15-1$ $-2.66-5$ $1.092+2$ 1.427 $9.26-2$	2000 4.476+1 1.997 -6.29-2 -3.04-5 5.008+1 1.443 3.44-1	3000 2.101+1 1.999 5.85-2 -2.90-5 1.567+1 1.346 6.78-1	4.91-1 -1.42-5 4000 1.171+1 1.996 2.77-1 -2.70-5 6.609+0 1.236 8.92-1	5000 7.259+0 1.990 4.94-1 -2.55-5 3.315+0 1.132 1.04+0	8.77-1 -1.29-5 6000 4.841+0 1.983 6.96-1 -2.38-5 1.862+0 1.038 1.15+0	7000 3.403+0 1.975 8.83-1 -2.18-5 1.133+0 0.955 1.24+0	8000 2.489+0 1.967 1.06+0 -1.97-5 7.323-1 0.880 1.31+0	1.36+0 -7.74-6 9000 1.879+0 1.959 1.22+0 -1.70-5 4.959-1 0.813 1.36+0	1.50+0 -5.40- 10000 1.455+0 1.950 1.37+0 -1.45- 3.486- 0.751 1.41+0
2.2 eV Z= 29, Cu: [An Shell $2s_{1/2}$ $E_b = 1096.1$ eV $2p_{1/2}$ $E_b = 951.0$ eV	$\frac{\sigma}{\beta}$	$\begin{array}{c} -1.34-5 \\ \hline 3d_{5/2}^6 4s_{1/2}^1 \\ \hline k (\text{eV}) \\ \hline 1500 \\ \hline 7.216+1 \\ 1.992 \\ 1.15-1 \\ -2.66-5 \\ \hline 1.092+2 \\ 1.427 \\ 9.26-2 \\ 1.97-2 \\ \end{array}$	-1.40-5 2000 4.476+1 1.997 -6.29-2 -3.04-5 5.008+1 1.443 3.44-1 2.96-2	3000 2.101+1 1.999 5.85-2 -2.90-5 1.567+1 1.346 6.78-1 4.80-2	4.91-1 -1.42-5 4000 1.171+1 1.996 2.77-1 -2.70-5 6.609+0 1.236 8.92-1 6.82-2	5000 7.259+0 1.990 4.94-1 -2.55-5 3.315+0 1.132 1.04+0 8.86-2	8.77-1 -1.29-5 6000 4.841+0 1.983 6.96-1 -2.38-5 1.862+0 1.038 1.15+0 1.09-1	1.05+0 -1.17-5 7000 3.403+0 1.975 8.83-1 -2.18-5 1.133+0 0.955 1.24+0 1.29-1	1.21+0 -9.98-6 8000 2.489+0 1.967 1.06+0 -1.97-5 7.323-1 0.880 1.31+0 1.49-1	1.36+0 -7.74-6 9000 1.879+0 1.959 1.22+0 -1.70-5 4.959-1 0.813 1.36+0 1.68-1	1.50+0 -5.40- 10000 1.455+0 1.950 1.37+0 -1.45- 3.486- 0.751 1.41+0 1.86-1
2.2 eV Z= 29, Cu: [An Shell $2s_{1/2}$ $E_b = 1096.1$ eV $2p_{1/2}$ $E_b = 951.0$ eV	$ \begin{array}{c} \delta \\ \mathbf{r}]\mathbf{3d}_{3/2}^{4} \\ \sigma \\ \beta \\ \gamma \\ \delta \\ \sigma \\ \beta \\ \gamma \\ \delta \\ \sigma \end{array} $	$\begin{array}{c} -1.34-5 \\ \hline {\bf 3d_{5/2}^6 4s_{1/2}^1} \\ \hline {\it k (eV)} \\ \hline 1500 \\ \hline {\it 7.216+1} \\ 1.992 \\ 1.15-1 \\ -2.66-5 \\ \hline 1.092+2 \\ 1.427 \\ 9.26-2 \\ 1.97-2 \\ \hline 2.101+2 \\ \end{array}$	-1.40-5 2000 4.476+1 1.997 -6.29-2 -3.04-5 5.008+1 1.443 3.44-1 2.96-2 9.547+1	3000 2.101+1 1.999 5.85-2 -2.90-5 1.567+1 1.346 6.78-1 4.80-2 2.955+1	4.91-1 -1.42-5 4000 1.171+1 1.996 2.77-1 -2.70-5 6.609+0 1.236 8.92-1 6.82-2 1.238+1	5000 7.259+0 1.990 4.94-1 -2.55-5 3.315+0 1.132 1.04+0 8.86-2 6.173+0	8.77-1 -1.29-5 6000 4.841+0 1.983 6.96-1 -2.38-5 1.862+0 1.038 1.15+0 1.09-1 3.451+0	7000 3.403+0 1.975 8.83-1 -2.18-5 1.133+0 0.955 1.24+0 1.29-1 2.091+0	8000 2.489+0 1.967 1.06+0 -1.97-5 7.323-1 0.880 1.31+0 1.49-1 1.346+0	9000 1.879+0 1.959 1.22+0 -1.70-5 4.959-1 0.813 1.36+0 1.68-1 9.084-1	1.50+0 -5.40- 10000 1.455+0 1.37+0 -1.45- 3.486- 0.751 1.41+0 1.86-1 6.364-
2.2 eV Z= 29, Cu: [And Shell $2s_{1/2}$ $E_b = 1096.1$ eV $2p_{1/2}$ $E_b = 951.0$ eV	$ \begin{array}{c} \delta \\ \mathbf{r}]\mathbf{3d}_{3/2}^{4} \\ \hline \sigma \\ \beta \\ \gamma \\ \delta \\ \hline \sigma \\ \beta \\ \gamma \\ \delta \\ \hline \sigma \\ \beta \end{array} $	$\begin{array}{c} -1.34-5 \\ \mathbf{3d_{5/2}^6 4s_{1/2}^1} \\ \hline k (\text{eV}) \\ \hline 1500 \\ 7.216+1 \\ 1.992 \\ 1.15-1 \\ -2.66-5 \\ 1.092+2 \\ 1.427 \\ 9.26-2 \\ 1.97-2 \\ 2.101+2 \\ 1.451 \end{array}$	2000 4.476+1 1.997 -6.29-2 -3.04-5 5.008+1 1.443 3.44-1 2.96-2 9.547+1 1.466	3000 2.101+1 1.999 5.85-2 -2.90-5 1.567+1 1.346 6.78-1 4.80-2 2.955+1 1.372	4.91-1 -1.42-5 4000 1.171+1 1.996 2.77-1 -2.70-5 6.609+0 1.236 8.92-1 6.82-2 1.238+1 1.262	5000 7.259+0 1.990 4.94-1 -2.55-5 3.315+0 1.132 1.04+0 8.86-2 6.173+0 1.158	8.77-1 -1.29-5 6000 4.841+0 1.983 6.96-1 -2.38-5 1.862+0 1.038 1.15+0 1.09-1 3.451+0 1.065	7000 3.403+0 1.975 8.83-1 -2.18-5 1.133+0 0.955 1.24+0 1.29-1 2.091+0 0.982	8000 2.489+0 1.967 1.06+0 -1.97-5 7.323-1 0.880 1.31+0 1.49-1 1.346+0 0.907	9000 1.879+0 1.959 1.22+0 -1.70-5 4.959-1 0.813 1.36+0 1.68-1 9.084-1 0.840	1.50+0 -5.40- 10000 1.455+0 1.950 1.37+0 -1.45- 3.486- 0.751 1.41+0 1.86-1 6.364- 0.779
2.2 eV Z= 29, Cu: [An Shell $2s_{1/2}$ $E_b = 1096.1$ eV $2p_{1/2}$ $E_b = 951.0$ eV	$ \begin{array}{c} \delta \\ \mathbf{r}]\mathbf{3d}_{3/2}^{4} \\ \sigma \\ \beta \\ \gamma \\ \delta \\ \sigma \\ \beta \\ \gamma \\ \delta \\ \sigma \end{array} $	$\begin{array}{c} -1.34-5 \\ \hline {\bf 3d_{5/2}^6 4s_{1/2}^1} \\ \hline {\it k (eV)} \\ \hline 1500 \\ \hline {\it 7.216+1} \\ 1.992 \\ 1.15-1 \\ -2.66-5 \\ \hline 1.092+2 \\ 1.427 \\ 9.26-2 \\ 1.97-2 \\ \hline 2.101+2 \\ \end{array}$	-1.40-5 2000 4.476+1 1.997 -6.29-2 -3.04-5 5.008+1 1.443 3.44-1 2.96-2 9.547+1	3000 2.101+1 1.999 5.85-2 -2.90-5 1.567+1 1.346 6.78-1 4.80-2 2.955+1	4.91-1 -1.42-5 4000 1.171+1 1.996 2.77-1 -2.70-5 6.609+0 1.236 8.92-1 6.82-2 1.238+1	5000 7.259+0 1.990 4.94-1 -2.55-5 3.315+0 1.132 1.04+0 8.86-2 6.173+0	8.77-1 -1.29-5 6000 4.841+0 1.983 6.96-1 -2.38-5 1.862+0 1.038 1.15+0 1.09-1 3.451+0	7000 3.403+0 1.975 8.83-1 -2.18-5 1.133+0 0.955 1.24+0 1.29-1 2.091+0	8000 2.489+0 1.967 1.06+0 -1.97-5 7.323-1 0.880 1.31+0 1.49-1 1.346+0	9000 1.879+0 1.959 1.22+0 -1.70-5 4.959-1 0.813 1.36+0 1.68-1 9.084-1	1.50+0 -5.40- 10000 1.455+0 1.37+0 -1.45- 3.486- 0.751 1.41+0 1.86-1 6.364-
2.2 eV Z= 29, Cu: [An Shell $2s_{1/2}$ $E_b = 1096.1$ eV $2p_{1/2}$ $E_b = 951.0$ eV $2p_{3/2}$ $E_b = 931.1$ eV	δ r]3d ⁴ _{3/2} σ β γ δ σ β γ δ	$\begin{array}{c} -1.34-5 \\ \hline {\bf 3d_{5/2}^6 4s_{1/2}^1} \\ \hline {\it k (eV)} \\ \hline 1500 \\ \hline {\it 7.216+1} \\ 1.992 \\ 1.15-1 \\ -2.66-5 \\ \hline 1.092+2 \\ 1.427 \\ 9.26-2 \\ 1.97-2 \\ \hline 2.101+2 \\ 1.451 \\ 1.04-1 \\ 2.03-2 \\ \end{array}$	2000 4.476+1 1.997 -6.29-2 -3.04-5 5.008+1 1.443 3.44-1 2.96-2 9.547+1 1.466 3.58-1 2.99-2	3000 2.101+1 1.999 5.85-2 -2.90-5 1.567+1 1.346 6.78-1 4.80-2 2.955+1 1.372 6.98-1 4.76-2	4.91-1 -1.42-5 4000 1.171+1 1.996 2.77-1 -2.70-5 6.609+0 1.236 8.92-1 6.82-2 1.238+1 1.262 9.14-1 6.69-2	5000 7.259+0 1.990 4.94-1 -2.55-5 3.315+0 1.132 1.04+0 8.86-2 6.173+0 1.158 1.07+0 8.67-2	8.77-1 -1.29-5 6000 4.841+0 1.983 6.96-1 -2.38-5 1.862+0 1.038 1.15+0 1.09-1 3.451+0 1.065 1.18+0 1.07-1	7000 3.403+0 1.975 8.83-1 -2.18-5 1.133+0 0.955 1.24+0 1.29-1 2.091+0 0.982 1.26+0 1.26-1	1.21+0 -9.98-6 8000 2.489+0 1.967 1.06+0 -1.97-5 7.323-1 0.880 1.31+0 1.49-1 1.346+0 0.907 1.33+0 1.46-1	9000 1.879+0 1.959 1.22+0 -1.70-5 4.959-1 0.813 1.36+0 1.68-1 9.084-1 0.840 1.38+0 1.64-1	1.50+0 -5.40- 10000 1.455+6 1.950 1.37+0 -1.45- 0.751 1.41+0 1.86-1 6.364- 0.779 1.43+0 1.82-1
2.2 eV Z= 29, Cu: [And Shell $2s_{1/2}$ $E_b = 1096.1$ eV $2p_{1/2}$ $E_b = 951.0$ eV	$ \begin{array}{c} \delta \\ \mathbf{r}]\mathbf{3d}_{3/2}^{4} \\ \hline \sigma \\ \beta \\ \gamma \\ \delta \\ \hline \sigma \\ \beta \\ \gamma \\ \delta \\ \hline \sigma \\ \beta \\ \gamma \\ \gamma \end{array} $	$\begin{array}{c} -1.34-5 \\ \hline {\bf 3d_{5/2}^6 4s_{1/2}^1} \\ \hline {\it k (eV)} \\ \hline {\it 1500} \\ \hline {\it 7.216+1} \\ {\it 1.992} \\ {\it 1.15-1} \\ {\it -2.66-5} \\ \hline {\it 1.092+2} \\ {\it 1.427} \\ {\it 9.26-2} \\ {\it 1.97-2} \\ \hline {\it 2.101+2} \\ {\it 1.451} \\ {\it 1.04-1} \\ \end{array}$	2000 4.476+1 1.997 -6.29-2 -3.04-5 5.008+1 1.443 3.44-1 2.96-2 9.547+1 1.466 3.58-1	3000 2.101+1 1.999 5.85-2 -2.90-5 1.567+1 1.346 6.78-1 4.80-2 2.955+1 1.372 6.98-1	4.91-1 -1.42-5 4000 1.171+1 1.996 2.77-1 -2.70-5 6.609+0 1.236 8.92-1 6.82-2 1.238+1 1.262 9.14-1	5000 7.259+0 1.990 4.94-1 -2.55-5 3.315+0 1.132 1.04+0 8.86-2 6.173+0 1.158 1.07+0	8.77-1 -1.29-5 6000 4.841+0 1.983 6.96-1 -2.38-5 1.862+0 1.038 1.15+0 1.09-1 3.451+0 1.065 1.18+0	7000 3.403+0 1.975 8.83-1 -2.18-5 1.133+0 0.955 1.24+0 1.29-1 2.091+0 0.982 1.26+0	8000 2.489+0 1.967 1.06+0 -1.97-5 7.323-1 0.880 1.31+0 1.49-1 1.346+0 0.907 1.33+0	9000 1.879+0 1.959 1.22+0 -1.70-5 4.959-1 0.813 1.36+0 1.68-1 9.084-1 0.840 1.38+0	1.50+0 -5.40- 10000 1.455+6 1.950 1.37+0 -1.45- 0.751 1.41+0 1.86-1 6.364- 0.779 1.43+0 1.82-1
2.2 eV Z= 29, Cu: [And Shell $2s_{1/2}$ $E_b = 1096.1$ eV $2p_{1/2}$ $E_b = 951.0$ eV $2p_{3/2}$ $E_b = 931.1$ eV	δ r]3d ⁴ _{3/2} σ β γ δ σ β γ δ σ β γ δ σ β γ δ σ σ β σ σ σ σ σ σ σ σ σ σ σ σ σ σ σ σ	$\begin{array}{c} -1.34-5 \\ \hline {\bf 3d_{5/2}^6 4s_{1/2}^1} \\ \hline {\it k (eV)} \\ \hline 1500 \\ \hline {\it 7.216+1} \\ 1.992 \\ 1.15-1 \\ -2.66-5 \\ \hline 1.092+2 \\ 1.427 \\ 9.26-2 \\ 1.97-2 \\ \hline 2.101+2 \\ 1.451 \\ 1.04-1 \\ 2.03-2 \\ \hline 1.226+1 \\ \hline \end{array}$	2000 4.476+1 1.997 -6.29-2 -3.04-5 5.008+1 1.443 3.44-1 2.96-2 9.547+1 1.466 3.58-1 2.99-2 7.056+0 1.999 2.01-2	3000 2.101+1 1.999 5.85-2 -2.90-5 1.567+1 1.346 6.78-1 4.80-2 2.955+1 1.372 6.98-1 4.76-2 3.101+0	4.91-1 -1.42-5 4000 1.171+1 1.996 2.77-1 -2.70-5 6.609+0 1.236 8.92-1 6.82-2 1.238+1 1.262 9.14-1 6.69-2 1.680+0	5000 7.259+0 1.990 4.94-1 -2.55-5 3.315+0 1.132 1.04+0 8.86-2 6.173+0 1.158 1.07+0 8.67-2 1.027+0	8.77-1 -1.29-5 6000 4.841+0 1.983 6.96-1 -2.38-5 1.862+0 1.038 1.15+0 1.09-1 3.451+0 1.065 1.18+0 1.07-1 6.799-1	7000 3.403+0 1.975 8.83-1 -2.18-5 1.133+0 0.955 1.24+0 1.29-1 2.091+0 0.982 1.26+0 1.26-1 4.757-1	1.21+0 -9.98-6 8000 2.489+0 1.967 1.06+0 -1.97-5 7.323-1 0.880 1.31+0 1.49-1 1.346+0 0.907 1.33+0 1.46-1 3.470-1	9000 1.879+0 1.959 1.22+0 -1.70-5 4.959-1 0.813 1.36+0 1.68-1 9.084-1 0.840 1.38+0 1.64-1 2.615-1	1.50+0 -5.40- 10000 1.455+(1.950 1.37+0 -1.45- 3.486- 0.751 1.41+0 1.86-1 0.779 1.43+0 1.82-1 2.023-
2.2 eV Z= 29, Cu: [And Shell $2s_{1/2}$ $E_b = 1096.1$ eV $2p_{1/2}$ $E_b = 951.0$ eV $2p_{3/2}$ $E_b = 931.1$ eV $3s_{1/2}$ $E_b = 1000.0$ eV	$ \begin{array}{c} \delta \\ \mathbf{r}]\mathbf{3d}_{3/2}^{4} \\ \\ \sigma \\ \beta \\ \gamma \\ \delta \\ \\ \sigma \\ \beta \\ \gamma \\ \delta \\ \\ \sigma \\ \beta \\ \beta \\ \\ \sigma \\ \beta \\ \beta \\ \rho \\ \delta \\ \\ \sigma \\ \beta \\ \beta \\ \rho \\ \delta \\ \sigma \\ \beta \\ \rho \\ \delta \\ \sigma \\ \beta \\ \rho \\ \delta \\ \sigma \\ \beta \\ \rho \\ \rho \\ \delta \\ \sigma \\ \beta \\ \rho \\ \delta \\ \sigma \\ \beta \\ \rho \\ \delta \\ \sigma \\ \beta \\ \rho \\ \rho \\ \delta \\ \sigma \\ \beta \\ \rho \\ \rho \\ \delta \\ \sigma \\ \beta \\ \rho \\ \rho \\ \delta \\ \sigma \\ \rho \\ \rho \\ \rho \\ \delta \\ \sigma \\ \rho \\ \rho \\ \delta \\ \sigma \\ \rho \\ \rho \\ \delta \\ \sigma \\ \rho \\ \rho \\ \rho \\ \delta \\ \sigma \\ \rho \\ \rho \\ \rho \\ \sigma \\ \rho \\ \rho \\ \rho \\ \sigma \\ \rho \\ \rho$	$\begin{array}{c} -1.34-5 \\ \hline {\bf 3d_{5/2}^6 ds_{1/2}^1} \\ \hline {\it k (eV)} \\ \hline 1500 \\ \hline {\it 7.216+1} \\ 1.992 \\ 1.15-1 \\ -2.66-5 \\ \hline 1.092+2 \\ 1.427 \\ 9.26-2 \\ 1.97-2 \\ \hline 2.101+2 \\ 1.451 \\ 1.04-1 \\ 2.03-2 \\ \hline 1.226+1 \\ 1.999 \\ \end{array}$	2000 4.476+1 1.997 -6.29-2 -3.04-5 5.008+1 1.443 3.44-1 2.96-2 9.547+1 1.466 3.58-1 2.99-2 7.056+0 1.999	3000 2.101+1 1.999 5.85-2 -2.90-5 1.567+1 1.346 6.78-1 4.80-2 2.955+1 1.372 6.98-1 4.76-2 3.101+0 1.997	4.91-1 -1.42-5 4000 1.171+1 1.996 2.77-1 -2.70-5 6.609+0 1.236 8.92-1 6.82-2 1.238+1 1.262 9.14-1 6.69-2 1.680+0 1.992	5000 7.259+0 1.990 4.94-1 -2.55-5 3.315+0 1.132 1.04+0 8.86-2 6.173+0 1.158 1.07+0 8.67-2 1.027+0 1.986	8.77-1 -1.29-5 6000 4.841+0 1.983 6.96-1 -2.38-5 1.862+0 1.038 1.15+0 1.09-1 3.451+0 1.065 1.18+0 1.07-1 6.799-1 1.979	7000 3.403+0 1.975 8.83-1 -2.18-5 1.133+0 0.955 1.24+0 1.29-1 2.091+0 0.982 1.26+0 1.26-1 4.757-1 1.971	1.21+0 -9.98-6 8000 2.489+0 1.967 1.06+0 -1.97-5 7.323-1 0.880 1.31+0 1.49-1 1.346+0 0.907 1.33+0 1.46-1 3.470-1 1.963	9000 1.879+0 1.959 1.22+0 -1.70-5 4.959-1 0.813 1.36+0 1.68-1 9.084-1 0.840 1.38+0 1.64-1 2.615-1 1.954	1.50+0 -5.40- 10000 1.455+(1.950 1.37+0 -1.45- 0.751 1.41+0 1.86-1 6.364- 0.79 1.43+0 1.82-1 2.023- 1.945 1.44+0
2.2 eV Z= 29, Cu: [And Shell $2s_{1/2}$ $E_b = 1096.1$ eV $2p_{1/2}$ $E_b = 951.0$ eV $2p_{3/2}$ $E_b = 931.1$ eV $3s_{1/2}$ $E_b = 119.8$ eV	δ r]3d ⁴ _{3/2} σ β γ δ σ β γ δ σ β γ δ σ β γ δ σ β γ δ σ β γ δ σ β σ δ σ σ β σ σ σ σ σ σ σ σ σ σ σ σ σ	$\begin{array}{c} -1.34-5 \\ \hline 3d_{5/2}^6 4s_{1/2}^1 \\ \hline k (\text{eV}) \\ \hline 1500 \\ \hline 7.216+1 \\ 1.992 \\ 1.15-1 \\ -2.66-5 \\ \hline 1.092+2 \\ 1.427 \\ 9.26-2 \\ 1.97-2 \\ \hline 2.101+2 \\ 1.451 \\ 1.04-1 \\ 2.03-2 \\ \hline 1.226+1 \\ 1.999 \\ -5.19-2 \\ -1.64-5 \\ \hline 1.053+1 \\ \hline \end{array}$	2000 4.476+1 1.997 -6.29-2 -3.04-5 5.008+1 1.443 3.44-1 2.96-2 9.547+1 1.466 3.58-1 2.99-2 7.056+0 1.999 2.01-2 -1.75-5 5.109+0	3000 2.101+1 1.999 5.85-2 -2.90-5 1.567+1 1.346 6.78-1 4.80-2 2.955+1 1.372 6.98-1 4.76-2 3.101+0 1.997 2.21-1 -1.84-5 1.715+0	4.91-1 -1.42-5 4000 1.171+1 1.996 2.77-1 -2.70-5 6.609+0 1.236 8.92-1 6.82-2 1.238+1 1.262 9.14-1 6.69-2 1.680+0 1.992 4.30-1 -1.86-5 7.552-1	6.92-1 -1.37-5 5000 7.259+0 1.990 4.94-1 -2.55-5 3.315+0 1.132 1.04+0 8.86-2 6.173+0 1.158 1.07+0 8.67-2 1.027+0 1.986 6.30-1 -1.81-5 3.899-1	8.77-1 -1.29-5 6000 4.841+0 1.983 6.96-1 -2.38-5 1.862+0 1.038 1.15+0 1.09-1 3.451+0 1.065 1.18+0 1.07-1 6.799-1 1.979 8.16-1 -1.71-5 2.237-1	1.05+0 -1.17-5 7000 3.403+0 1.975 8.83-1 -2.18-5 1.133+0 0.955 1.24+0 1.29-1 2.091+0 0.982 1.26+0 1.26-1 4.757-1 1.971 9.89-1 -1.56-5 1.383-1	1.21+0 -9.98-6 8000 2.489+0 1.967 1.06+0 -1.97-5 7.323-1 0.880 1.31+0 1.49-1 1.346+0 0.907 1.33+0 1.46-1 3.470-1 1.963 1.15+0 -1.38-5 9.049-2	1.36+0 -7.74-6 9000 1.879+0 1.959 1.22+0 -1.70-5 4.959-1 0.813 1.36+0 1.68-1 9.084-1 0.840 1.38+0 1.64-1 2.615-1 1.954 1.30+0 -1.15-5 6.188-2	1.50+0 -5.40- 10000 1.455+(1.950 1.37+0 -1.45- 0.751 1.41+0 1.86-1 6.364- 0.79 1.43+0 1.82-1 2.023- 1.945 1.44+0 -8.68- 4.385-
2.2 eV Z= 29, Cu: [An Shell $2s_{1/2}$ $E_b = 1096.1$ eV $2p_{1/2}$ $E_b = 951.0$ eV $2p_{3/2}$ $E_b = 119.8$ eV $3s_{1/2}$ $E_b = 119.8$ eV	$\begin{array}{c} \delta \\ \hline \kappa \\ \hline r] 3d_{3/2}^4 \\ \hline \\ \sigma \\ \beta \\ \gamma \\ \delta \\ \hline \\ \sigma \\ \beta \\ \gamma \\ \delta \\ \hline \\ \sigma \\ \beta \\ \gamma \\ \delta \\ \hline \\ \sigma \\ \beta \\ \gamma \\ \delta \\ \hline \\ \sigma \\ \beta \\ \gamma \\ \delta \\ \hline \\ \sigma \\ \beta \\ \gamma \\ \delta \\ \hline \\ \sigma \\ \beta \\ \gamma \\ \delta \\ \hline \\ \sigma \\ \beta \\ \gamma \\ \delta \\ \hline \\ \sigma \\ \beta \\ \gamma \\ \delta \\ \hline \\ \sigma \\ \beta \\ \gamma \\ \delta \\ \hline \\ \sigma \\ \beta \\ \gamma \\ \delta \\ \hline \\ \sigma \\ \beta \\ \gamma \\ \delta \\ \hline \\ \sigma \\ \beta \\ \gamma \\ \delta \\ \hline \\ \sigma \\ \beta \\ \gamma \\ \delta \\ \hline \\ \sigma \\ \beta \\ \gamma \\ \delta \\ \hline \\ \sigma \\ \beta \\ \gamma \\ \delta \\ \hline \\ \sigma \\ \sigma \\ \beta \\ \gamma \\ \delta \\ \hline \\ \sigma \\ \sigma \\ \beta \\ \gamma \\ \delta \\ \hline \\ \sigma \\ \sigma \\ \rho \\ \gamma \\ \delta \\ \hline \\ \sigma \\ \sigma \\ \rho \\ \gamma \\ \delta \\ \hline \\ \sigma \\ \sigma \\ \rho \\ \gamma \\ \delta \\ \hline \\ \sigma \\ \sigma \\ \sigma \\ \rho \\ \gamma \\ \delta \\ \sigma \\ \sigma$	$\begin{array}{c} -1.34-5 \\ \hline {\bf 3d_{5/2}^6 4s_{1/2}^1} \\ \hline k (\text{eV}) \\ \hline 1500 \\ \hline 7.216+1 \\ 1.992 \\ 1.15-1 \\ -2.66-5 \\ 1.092+2 \\ 1.427 \\ 9.26-2 \\ 1.97-2 \\ \hline 2.101+2 \\ 1.451 \\ 1.04-1 \\ 2.03-2 \\ \hline 1.226+1 \\ 1.999 \\ -5.19-2 \\ -1.64-5 \\ \hline 1.053+1 \\ 1.524 \\ \hline \end{array}$	-1.40-5 2000 4.476+1 1.997 -6.29-2 -3.04-5 5.008+1 1.443 3.44-1 2.96-2 9.547+1 1.466 3.58-1 2.99-2 7.056+0 1.999 2.01-2 -1.75-5 5.109+0 1.441	3000 2.101+1 1.999 5.85-2 -2.90-5 1.567+1 1.346 6.78-1 4.80-2 2.955+1 1.372 6.98-1 4.76-2 3.101+0 1.997 2.21-1 -1.84-5 1.715+0 1.295	4.91-1 -1.42-5 4000 1.171+1 1.996 2.77-1 -2.70-5 6.609+0 1.236 8.92-1 6.82-2 1.238+1 1.262 9.14-1 6.69-2 1.680+0 1.992 4.30-1 -1.86-5 7.552-1 1.172	6.92-1 -1.37-5 5000 7.259+0 1.990 4.94-1 -2.55-5 3.315+0 1.132 1.04+0 8.86-2 6.173+0 1.158 1.07+0 1.986 6.30-1 -1.81-5 3.899-1 1.067	8.77-1 -1.29-5 6000 4.841+0 1.983 6.96-1 -2.38-5 1.862+0 1.038 1.15+0 1.09-1 3.451+0 1.065 1.18+0 1.07-1 6.799-1 1.979 8.16-1 -1.71-5 2.237-1 0.977	1.05+0 -1.17-5 7000 3.403+0 1.975 8.83-1 -2.18-5 1.133+0 0.955 1.24+0 1.29-1 2.091+0 0.982 1.26+0 1.26-1 4.757-1 1.971 9.89-1 -1.56-5 1.383-1 0.898	1.21+0 -9.98-6 8000 2.489+0 1.967 1.06+0 -1.97-5 7.323-1 0.880 1.31+0 1.49-1 1.346+0 0.907 1.33+0 1.46-1 3.470-1 1.963 1.15+0 -1.38-5 9.049-2 0.827	1.36+0 -7.74-6 9000 1.879+0 1.959 1.22+0 -1.70-5 4.959-1 0.813 1.36+0 1.68-1 9.084-1 0.840 1.38+0 1.64-1 2.615-1 1.954 1.30+0 -1.15-5 6.188-2 0.763	1.50+0 -5.40- 10000 1.455+1 1.950 1.37+0 -1.45- 0.751 1.41+0 1.86-1 6.364- 0.779 1.43+0 1.82-1 2.023- 1.945 1.44+0 -8.68- 4.385- 0.706
2.2 eV Z= 29, Cu: [And Shell $2s_{1/2}$ $E_b = 1096.1$ eV $2p_{1/2}$ $E_b = 951.0$ eV $2p_{3/2}$ $E_b = 931.1$ eV $3s_{1/2}$ $E_b = 119.8$ eV	δ r]3d ⁴ _{3/2} σ β γ δ σ β γ δ σ β γ δ σ β γ δ σ β γ δ σ β γ δ σ β γ δ σ σ σ σ σ σ σ σ σ σ σ σ σ	$\begin{array}{c} -1.34-5 \\ \hline {\bf 3d_{5/2}^6 4s_{1/2}^1} \\ \hline k (\text{eV}) \\ \hline 1500 \\ \hline 7.216+1 \\ 1.992 \\ 1.15-1 \\ -2.66-5 \\ \hline 1.092+2 \\ 1.427 \\ 9.26-2 \\ 1.97-2 \\ \hline 2.101+2 \\ 1.451 \\ 1.04-1 \\ 2.03-2 \\ \hline 1.226+1 \\ 1.999 \\ -5.19-2 \\ -1.64-5 \\ \hline 1.053+1 \\ 1.524 \\ 3.42-1 \\ \hline \end{array}$	2000 4.476+1 1.997 -6.29-2 -3.04-5 5.008+1 1.443 3.44-1 2.96-2 9.547+1 1.466 3.58-1 2.99-2 7.056+0 1.999 2.01-2 -1.75-5 5.109+0 1.441 5.07-1	3000 2.101+1 1.999 5.85-2 -2.90-5 1.567+1 1.346 6.78-1 4.80-2 2.955+1 1.372 6.98-1 4.76-2 3.101+0 1.997 2.21-1 -1.84-5 1.715+0 1.295 7.49-1	4.91-1 -1.42-5 4000 1.171+1 1.996 2.77-1 -2.70-5 6.609+0 1.236 8.92-1 6.82-2 1.238+1 1.262 9.14-1 6.69-2 1.680+0 1.992 4.30-1 -1.86-5 7.552-1 1.172 9.18-1	6.92-1 -1.37-5 5000 7.259+0 1.990 4.94-1 -2.55-5 3.315+0 1.132 1.04+0 8.86-2 6.173+0 1.158 1.07+0 8.67-2 1.027+0 1.986 6.30-1 -1.81-5 3.899-1 1.067 1.04+0	8.77-1 -1.29-5 6000 4.841+0 1.983 6.96-1 -2.38-5 1.862+0 1.038 1.15+0 1.09-1 3.451+0 1.065 1.18+0 1.07-1 6.799-1 1.979 8.16-1 -1.71-5 2.237-1 0.977 1.14+0	1.05+0 -1.17-5 7000 3.403+0 1.975 8.83-1 -2.18-5 1.133+0 0.955 1.24+0 1.29-1 2.091+0 0.982 1.26+0 1.26-1 4.757-1 1.971 9.89-1 -1.56-5 1.383-1 0.898 1.22+0	1.21+0 -9.98-6 8000 2.489+0 1.967 1.06+0 -1.97-5 7.323-1 0.880 1.31+0 1.49-1 1.346+0 0.907 1.33+0 1.46-1 3.470-1 1.963 1.15+0 -1.38-5 9.049-2 0.827 1.29+0	1.36+0 -7.74-6 9000 1.879+0 1.959 1.22+0 -1.70-5 4.959-1 0.813 1.36+0 1.68-1 9.084-1 0.840 1.38+0 1.64-1 2.615-1 1.954 1.30+0 -1.15-5 6.188-2 0.763 1.34+0	1.50+0 -5.40- 10000 1.455+(1.950 1.37+0 -1.45- 0.751 1.41+0 1.86-1 6.364- 0.779 1.43+0 1.82-1 2.023- 1.945 1.44+0 -8.68- 4.385- 0.706 1.38+0
2.2 eV Z= 29, Cu: [Ar Shell $2s_{1/2}$ $E_b = 1096.1$ eV $2p_{1/2}$ $E_b = 931.1$ eV $3s_{1/2}$ $E_b = 119.8$ eV $3p_{1/2}$ $a_{1/2}$	δ r]3d ⁴ _{3/2} σ β γ δ σ β γ δ σ β γ δ σ β γ δ σ β γ δ σ β γ δ σ β γ δ δ σ β γ δ δ σ σ δ δ σ σ δ δ δ δ δ δ δ δ δ δ δ δ δ	$\begin{array}{c} -1.34-5 \\ \hline {\bf 3d_{5/2}^6 4s_{1/2}^1} \\ \hline k (\text{eV}) \\ \hline 1500 \\ \hline 7.216+1 \\ 1.992 \\ 1.15-1 \\ -2.66-5 \\ \hline 1.092+2 \\ 1.427 \\ 9.26-2 \\ 1.97-2 \\ \hline 2.101+2 \\ 1.451 \\ 1.04-1 \\ 2.03-2 \\ \hline 1.226+1 \\ 1.999 \\ -5.19-2 \\ -1.64-5 \\ \hline 1.053+1 \\ 1.524 \\ 3.42-1 \\ 1.51-2 \\ \hline \end{array}$	2000 4.476+1 1.997 -6.29-2 -3.04-5 5.008+1 1.443 3.44-1 2.96-2 9.547+1 1.466 3.58-1 2.99-2 7.056+0 1.999 2.01-2 -1.75-5 5.109+0 1.441 5.07-1 2.43-2	3000 2.101+1 1.999 5.85-2 -2.90-5 1.567+1 1.346 6.78-1 4.80-2 2.955+1 1.372 6.98-1 4.76-2 3.101+0 1.997 2.21-1 -1.84-5 1.715+0 1.295 7.49-1 4.49-2	4.91-1 -1.42-5 4000 1.171+1 1.996 2.77-1 -2.70-5 6.609+0 1.236 8.92-1 6.82-2 1.238+1 1.262 9.14-1 6.69-2 1.680+0 1.992 4.30-1 -1.86-5 7.552-1 1.172 9.18-1 6.65-2	6.92-1 -1.37-5 5000 7.259+0 1.990 4.94-1 -2.55-5 3.315+0 1.132 1.04+0 8.86-2 6.173+0 1.158 1.07+0 8.67-2 1.027+0 1.986 6.30-1 -1.81-5 3.899-1 1.067 1.04+0 8.82-2	8.77-1 -1.29-5 6000 4.841+0 1.983 6.96-1 -2.38-5 1.862+0 1.038 1.15+0 1.09-1 3.451+0 1.065 1.18+0 1.07-1 6.799-1 1.979 8.16-1 -1.71-5 2.237-1 0.977 1.14+0 1.10-1	1.05+0 -1.17-5 7000 3.403+0 1.975 8.83-1 -2.18-5 1.133+0 0.955 1.24+0 1.29-1 2.091+0 0.982 1.26+0 1.26-1 4.757-1 1.971 9.89-1 -1.56-5 1.383-1 0.898 1.22+0 1.30-1	1.21+0 -9.98-6 8000 2.489+0 1.967 1.06+0 -1.97-5 7.323-1 0.880 1.31+0 1.49-1 1.346+0 0.907 1.33+0 1.46-1 3.470-1 1.963 1.15+0 -1.38-5 9.049-2 0.827 1.29+0 1.50-1	1.36+0 -7.74-6 9000 1.879+0 1.959 1.22+0 -1.70-5 4.959-1 0.813 1.36+0 1.68-1 9.084-1 0.840 1.38+0 1.64-1 2.615-1 1.954 1.30+0 -1.15-5 6.188-2 0.763 1.34+0 1.69-1	1.50+0 -5.40- 10000 1.455+(1.950 1.37+0 -1.45- 0.751 1.41+0 1.86-1 6.364- 0.779 1.43+0 1.82-1 2.023- 1.945 1.44+0 -8.68- 0.706 1.38+0 1.88-1
2.2 eV Z= 29, Cu: [And Shell $2s_{1/2}$ $E_b = 1096.1$ eV $2p_{1/2}$ $E_b = 951.0$ eV $2p_{3/2}$ $E_b = 931.1$ eV $3s_{1/2}$ $E_b = 119.8$ eV $3p_{1/2}$ $E_b = 75.3$ eV	δ r]3d ⁴ _{3/2} σ β γ δ σ β γ δ σ β γ δ σ β γ δ σ β γ δ σ β γ δ σ β γ δ σ β γ δ σ β γ δ σ β γ δ σ σ β γ δ σ σ σ σ σ σ σ σ σ σ σ σ	$\begin{array}{c} -1.34-5 \\ \hline {\bf 3d_{5/2}^6 4s_{1/2}^1} \\ \hline k (\text{eV}) \\ \hline 1500 \\ \hline 7.216+1 \\ 1.992 \\ 1.15-1 \\ -2.66-5 \\ \hline 1.092+2 \\ 1.427 \\ 9.26-2 \\ 1.97-2 \\ \hline 2.101+2 \\ 1.451 \\ 1.04-1 \\ 2.03-2 \\ \hline 1.226+1 \\ 1.999 \\ -5.19-2 \\ -1.64-5 \\ \hline 1.053+1 \\ 1.524 \\ 3.42-1 \\ 1.51-2 \\ \hline 2.028+1 \\ \hline \end{array}$	2000 4.476+1 1.997 -6.29-2 -3.04-5 5.008+1 1.443 3.44-1 2.96-2 9.547+1 1.466 3.58-1 2.99-2 7.056+0 1.999 2.01-2 -1.75-5 5.109+0 1.441 5.07-1 2.43-2 9.761+0	3000 2.101+1 1.999 5.85-2 -2.90-5 1.567+1 1.346 6.78-1 4.80-2 2.955+1 1.372 6.98-1 4.76-2 3.101+0 1.997 2.21-1 -1.84-5 1.715+0 1.295 7.49-1 4.49-2 3.243+0	4.91-1 -1.42-5 4000 1.171+1 1.996 2.77-1 -2.70-5 6.609+0 1.236 8.92-1 6.82-2 1.238+1 1.262 9.14-1 6.69-2 1.680+0 1.992 4.30-1 -1.86-5 7.552-1 1.172 9.18-1 6.65-2 1.417+0	6.92-1 -1.37-5 5000 7.259+0 1.990 4.94-1 -2.55-5 3.315+0 1.132 1.04+0 8.86-2 6.173+0 1.158 1.07+0 8.67-2 1.027+0 1.986 6.30-1 -1.81-5 3.899-1 1.067 1.04+0 8.82-2 7.268-1	8.77-1 -1.29-5 6000 4.841+0 1.983 6.96-1 -2.38-5 1.862+0 1.038 1.15+0 1.09-1 3.451+0 1.065 1.18+0 1.07-1 6.799-1 1.979 8.16-1 -1.71-5 2.237-1 0.977 1.14+0 1.10-1 4.147-1	1.05+0 -1.17-5 7000 3.403+0 1.975 8.83-1 -2.18-5 1.133+0 0.955 1.24+0 1.29-1 2.091+0 0.982 1.26+0 1.26-1 4.757-1 1.971 9.89-1 -1.56-5 1.383-1 0.898 1.22+0 1.30-1 2.552-1	1.21+0 -9.98-6 8000 2.489+0 1.967 1.06+0 -1.97-5 7.323-1 0.880 1.31+0 1.49-1 1.346+0 0.907 1.33+0 1.46-1 3.470-1 1.963 1.15+0 -1.38-5 9.049-2 0.827 1.29+0 1.50-1	1.36+0 -7.74-6 9000 1.879+0 1.959 1.22+0 -1.70-5 4.959-1 0.813 1.36+0 1.68-1 9.084-1 0.840 1.38+0 1.64-1 2.615-1 1.954 1.30+0 -1.15-5 6.188-2 0.763 1.34+0 1.69-1 1.133-1	1.50+0 -5.40- 10000 1.455+0 1.950 1.37+0 -1.45- 3.486- 0.751 1.41+0 1.86-1 6.364- 0.779 1.43+0 1.82-1 2.023- 1.945 1.44+0 -8.68- 4.385- 0.706 1.38+0 1.88-1 7.997-
2.2 eV Z= 29, Cu: [And Shell $2s_{1/2}$ $E_b = 1096.1$ eV $2p_{1/2}$ $E_b = 951.0$ eV $2p_{3/2}$ $E_b = 931.1$ eV $3s_{1/2}$ $E_b = 119.8$ eV $3p_{1/2}$ $E_b = 75.3$ eV	$\begin{array}{c} \delta \\ \hline \delta \\ \hline r] 3d_{3/2}^4 \\ \hline \\ \sigma \\ \beta \\ \gamma \\ \delta \\ \hline \\ \sigma \\ \delta \\ \sigma \\ \rho \\ \delta \\ \sigma \\ \delta \\ \sigma \\ \delta \\ \sigma \\ \delta \\ \sigma \\ \delta \\ \delta$	$\begin{array}{c} -1.34-5 \\ \hline {\bf 3d_{5/2}^6 4s_{1/2}^1} \\ \hline k (\text{eV}) \\ \hline 1500 \\ \hline 7.216+1 \\ 1.992 \\ 1.15-1 \\ -2.66-5 \\ \hline 1.092+2 \\ 1.427 \\ 9.26-2 \\ 1.97-2 \\ \hline 2.101+2 \\ 1.451 \\ 1.04-1 \\ 2.03-2 \\ \hline 1.226+1 \\ 1.999 \\ -5.19-2 \\ -1.64-5 \\ \hline 1.053+1 \\ 1.524 \\ 3.42-1 \\ 1.51-2 \\ \hline 2.028+1 \\ 1.543 \\ \hline \end{array}$	2000 4.476+1 1.997 -6.29-2 -3.04-5 5.008+1 1.443 3.44-1 2.96-2 9.547+1 1.466 3.58-1 2.99-2 7.056+0 1.999 2.01-2 -1.75-5 5.109+0 1.441 5.07-1 2.43-2 9.761+0 1.463	3000 2.101+1 1.999 5.85-2 -2.90-5 1.567+1 1.346 6.78-1 4.80-2 2.955+1 1.372 6.98-1 4.76-2 3.101+0 1.997 2.21-1 -1.84-5 1.715+0 1.295 7.49-1 4.49-2 3.243+0 1.319	4.91-1 -1.42-5 4000 1.171+1 1.996 2.77-1 -2.70-5 6.609+0 1.236 8.92-1 6.82-2 1.238+1 1.262 9.14-1 6.69-2 1.680+0 1.992 4.30-1 -1.86-5 7.552-1 1.172 9.18-1 6.65-2 1.417+0 1.197	6.92-1 -1.37-5 5000 7.259+0 1.990 4.94-1 -2.55-5 3.315+0 1.132 1.04+0 8.86-2 6.173+0 1.158 1.07+0 8.67-2 1.027+0 1.986 6.30-1 -1.81-5 3.899-1 1.067 1.04+0 8.82-2 7.268-1 1.093	8.77-1 -1.29-5 6000 4.841+0 1.983 6.96-1 -2.38-5 1.862+0 1.038 1.15+0 1.09-1 3.451+0 1.065 1.18+0 1.07-1 6.799-1 1.979 8.16-1 -1.71-5 2.237-1 0.977 1.14+0 1.10-1 4.147-1 1.003	1.05+0 -1.17-5 7000 3.403+0 1.975 8.83-1 -2.18-5 1.133+0 0.955 1.24+0 1.29-1 2.091+0 0.982 1.26+0 1.26-1 4.757-1 1.971 9.89-1 -1.56-5 1.383-1 0.898 1.22+0 1.30-1 2.552-1 0.924	1.21+0 -9.98-6 8000 2.489+0 1.967 1.06+0 -1.97-5 7.323-1 0.880 1.31+0 1.49-1 1.346+0 0.907 1.33+0 1.46-1 3.470-1 1.963 1.15+0 -1.38-5 9.049-2 0.827 1.29+0 1.50-1 1.663-1 0.854	1.36+0 -7.74-6 9000 1.879+0 1.959 1.22+0 -1.70-5 4.959-1 0.813 1.36+0 1.68-1 9.084-1 0.840 1.38+0 1.64-1 2.615-1 1.954 1.30+0 -1.15-5 6.188-2 0.763 1.34+0 1.69-1 1.133-1 0.790	1.50+0 -5.40- 10000 1.455+0 1.950 1.37+0 -1.45- 3.486- 0.751 1.41+0 1.86-1 6.364- 0.779 1.43+0 1.82-1 2.023- 1.945 1.44+0 -8.68- 4.385- 0.706 1.38+0 1.88-1 7.997- 0.733
2.2 eV Z= 29, Cu: [And Shell $2s_{1/2}$ $E_b = 1096.1$ eV $2p_{1/2}$ $E_b = 951.0$ eV $2p_{3/2}$ $E_b = 931.1$ eV $3s_{1/2}$ $E_b = 119.8$ eV $3p_{1/2}$ $E_b = 75.3$ eV	δ r]3d ⁴ _{3/2} σ β γ δ σ β γ δ σ β γ δ σ β γ δ σ β γ δ σ β γ δ σ β γ δ σ β γ δ σ σ σ σ σ σ σ σ σ σ σ σ σ	$\begin{array}{c} -1.34-5 \\ \hline {\bf 3d_{5/2}^6 4s_{1/2}^1} \\ \hline k (\text{eV}) \\ \hline 1500 \\ \hline 7.216+1 \\ 1.992 \\ 1.15-1 \\ -2.66-5 \\ \hline 1.092+2 \\ 1.427 \\ 9.26-2 \\ 1.97-2 \\ \hline 2.101+2 \\ 1.451 \\ 1.04-1 \\ 2.03-2 \\ \hline 1.226+1 \\ 1.999 \\ -5.19-2 \\ -1.64-5 \\ \hline 1.053+1 \\ 1.524 \\ 3.42-1 \\ 1.51-2 \\ \hline 2.028+1 \\ 1.543 \\ 3.50-1 \\ \hline \end{array}$	2000 4.476+1 1.997 -6.29-2 -3.04-5 5.008+1 1.443 3.44-1 2.96-2 9.547+1 1.466 3.58-1 2.99-2 7.056+0 1.999 2.01-2 -1.75-5 5.109+0 1.441 5.07-1 2.43-2 9.761+0 1.463 5.18-1	3000 2.101+1 1.999 5.85-2 -2.90-5 1.567+1 1.346 6.78-1 4.80-2 2.955+1 1.372 6.98-1 4.76-2 3.101+0 1.997 2.21-1 -1.84-5 1.715+0 1.295 7.49-1 4.49-2 3.243+0 1.319 7.63-1	4.91-1 -1.42-5 4000 1.171+1 1.996 2.77-1 -2.70-5 6.609+0 1.236 8.92-1 6.82-2 1.238+1 1.262 9.14-1 6.69-2 1.680+0 1.992 4.30-1 -1.86-5 7.552-1 1.172 9.18-1 6.65-2 1.417+0 1.197 9.35-1	6.92-1 -1.37-5 5000 7.259+0 1.990 4.94-1 -2.55-5 3.315+0 1.132 1.04+0 8.86-2 6.173+0 1.158 1.07+0 8.67-2 1.027+0 1.986 6.30-1 -1.81-5 3.899-1 1.067 1.04+0 8.82-2 7.268-1 1.093 1.06+0	8.77-1 -1.29-5 6000 4.841+0 1.983 6.96-1 -2.38-5 1.862+0 1.038 1.15+0 1.09-1 3.451+0 1.065 1.18+0 1.07-1 6.799-1 1.979 8.16-1 -1.71-5 2.237-1 0.977 1.14+0 1.10-1 4.147-1 1.003 1.16+0	1.05+0 -1.17-5 7000 3.403+0 1.975 8.83-1 -2.18-5 1.133+0 0.955 1.24+0 1.29-1 2.091+0 0.982 1.26+0 1.26-1 4.757-1 1.971 9.89-1 -1.56-5 1.383-1 0.898 1.22+0 1.30-1 2.552-1 0.924 1.24+0	1.21+0 -9.98-6 8000 2.489+0 1.967 1.06+0 -1.97-5 7.323-1 0.880 1.31+0 1.49-1 1.346+0 0.907 1.33+0 1.46-1 3.470-1 1.963 1.15+0 -1.38-5 9.049-2 0.827 1.29+0 1.50-1 1.663-1 0.854 1.30+0	1.36+0 -7.74-6 9000 1.879+0 1.959 1.22+0 -1.70-5 4.959-1 0.813 1.36+0 1.68-1 9.084-1 0.840 1.38+0 1.64-1 2.615-1 1.954 1.30+0 -1.15-5 6.188-2 0.763 1.34+0 1.69-1 1.133-1 0.790 1.35+0	1.50+0 -5.40- 10000 1.455+0 1.950 1.37+0 -1.45- 0.751 1.41+0 1.86-1 6.364- 0.779 1.43+0 1.82-1 2.023- 1.945 1.44+0 -8.68- 4.385- 0.706 1.38+0 1.38+0 1.38+0 1.397- 0.733 1.40+0
2.2 eV Z= 29, Cu: [And Shell $2s_{1/2}$ $E_b = 1096.1$ eV $2p_{1/2}$ $E_b = 951.0$ eV $2p_{3/2}$ $E_b = 931.1$ eV $3s_{1/2}$ $E_b = 119.8$ eV $3p_{1/2}$ $E_b = 75.3$ eV	$\begin{array}{c} \delta \\ \hline \delta \\ \hline r] 3d_{3/2}^4 \\ \hline \\ \sigma \\ \beta \\ \gamma \\ \delta \\ \hline \\ \sigma \\ \delta \\ \sigma \\ \rho \\ \delta \\ \sigma \\ \delta \\ \sigma \\ \delta \\ \sigma \\ \delta \\ \sigma \\ \delta \\ \delta$	$\begin{array}{c} -1.34-5 \\ \hline {\bf 3d_{5/2}^6 4s_{1/2}^1} \\ \hline k (\text{eV}) \\ \hline 1500 \\ \hline 7.216+1 \\ 1.992 \\ 1.15-1 \\ -2.66-5 \\ \hline 1.092+2 \\ 1.427 \\ 9.26-2 \\ 1.97-2 \\ \hline 2.101+2 \\ 1.451 \\ 1.04-1 \\ 2.03-2 \\ \hline 1.226+1 \\ 1.999 \\ -5.19-2 \\ -1.64-5 \\ \hline 1.053+1 \\ 1.524 \\ 3.42-1 \\ 1.51-2 \\ \hline 2.028+1 \\ 1.543 \\ \hline \end{array}$	2000 4.476+1 1.997 -6.29-2 -3.04-5 5.008+1 1.443 3.44-1 2.96-2 9.547+1 1.466 3.58-1 2.99-2 7.056+0 1.999 2.01-2 -1.75-5 5.109+0 1.441 5.07-1 2.43-2 9.761+0 1.463	3000 2.101+1 1.999 5.85-2 -2.90-5 1.567+1 1.346 6.78-1 4.80-2 2.955+1 1.372 6.98-1 4.76-2 3.101+0 1.997 2.21-1 -1.84-5 1.715+0 1.295 7.49-1 4.49-2 3.243+0 1.319	4.91-1 -1.42-5 4000 1.171+1 1.996 2.77-1 -2.70-5 6.609+0 1.236 8.92-1 6.82-2 1.238+1 1.262 9.14-1 6.69-2 1.680+0 1.992 4.30-1 -1.86-5 7.552-1 1.172 9.18-1 6.65-2 1.417+0 1.197	6.92-1 -1.37-5 5000 7.259+0 1.990 4.94-1 -2.55-5 3.315+0 1.132 1.04+0 8.86-2 6.173+0 1.158 1.07+0 8.67-2 1.027+0 1.986 6.30-1 -1.81-5 3.899-1 1.067 1.04+0 8.82-2 7.268-1 1.093	8.77-1 -1.29-5 6000 4.841+0 1.983 6.96-1 -2.38-5 1.862+0 1.038 1.15+0 1.09-1 3.451+0 1.065 1.18+0 1.07-1 6.799-1 1.979 8.16-1 -1.71-5 2.237-1 0.977 1.14+0 1.10-1 4.147-1 1.003	1.05+0 -1.17-5 7000 3.403+0 1.975 8.83-1 -2.18-5 1.133+0 0.955 1.24+0 1.29-1 2.091+0 0.982 1.26+0 1.26-1 4.757-1 1.971 9.89-1 -1.56-5 1.383-1 0.898 1.22+0 1.30-1 2.552-1 0.924	1.21+0 -9.98-6 8000 2.489+0 1.967 1.06+0 -1.97-5 7.323-1 0.880 1.31+0 1.49-1 1.346+0 0.907 1.33+0 1.46-1 3.470-1 1.963 1.15+0 -1.38-5 9.049-2 0.827 1.29+0 1.50-1 1.663-1 0.854	1.36+0 -7.74-6 9000 1.879+0 1.959 1.22+0 -1.70-5 4.959-1 0.813 1.36+0 1.68-1 9.084-1 0.840 1.38+0 1.64-1 2.615-1 1.954 1.30+0 -1.15-5 6.188-2 0.763 1.34+0 1.69-1 1.133-1 0.790	1.50+0 -5.40- 10000 1.455+0 1.950 1.37+0 -1.45- 3.486- 0.751 1.41+0 1.86-1 6.364- 0.779 1.43+0 1.82-1 2.023- 1.945 1.44+0 -8.68- 4.385- 0.706 1.38+0 1.88-1 7.997- 0.733

Table 1 (contin	ued)										
1.8 eV	γ δ	5.85-1 9.85-2	6.74-1 1.27-1	7.85-1 1.83-1	8.54-1 2.34-1	9.02-1 2.81-1	9.37-1 3.24-1	9.62-1 3.63-1	9.78 - 1 $4.01 - 1$	9.88-1 4.35-1	9.93-1 4.68-1
3d _{5/2}	σ	3.820+0	1.343+0	2.909-1	9.449-2	3.858-2	1.826-2	9.596-3	5.450-3	3.289-3	2.083-3
$E_b = 1.5 \text{ eV}$	β	0.943 5.83-1	0.821 6.72-1	0.663 7.85-1	0.563 8.57-1	0.492 9.09-1	0.436 9.48-1	0.390 9.77-1	0.350 9.99-1	0.315 1.01+0	0.283 1.02+0
1.5 ev	$\gamma \\ \delta$	9.97-2	1.29-1	1.85-1	2.36-1	2.82-1	3.24-1	3.63-1	3.99-1	4.33-1	4.66-1
4s _{1/2}	σ	3.946-1	2.252-1	9.798-2	5.285-2	3.224-2	2.130-2	1.488-2	1.084-2	8.162-3	6.309-3
$E_b =$	β	1.999	1.999	1.997	1.992	1.985	1.978	1.970	1.962	1.954	1.945
1.2 eV	γ	-4.50-2	3.26-2	2.36-1	4.46-1	6.45-1	8.32-1	1.00+0	1.16+0	1.31+0	1.45+0
	δ	-1.53-5	-1.63-5	-1.72-5	-1.72-5	-1.67-5	-1.58-5	-1.46-5	-1.30-5	-1.08-5	-8.71-6
Z= 30, Zn: [A	r]3d _{3/2}										
Shell		k (eV) 1500	2000	3000	4000	5000	6000	7000	8000	9000	10000
2s _{1/2}	σ	7.551+1	4.758+1	2.266+1	1.274+1	7.949+0	5.326+0	3.758+0	2.758+0	2.088+0	1.621+0
$E_b =$	β	1.990	1.996	1.999	1.997	1.991	1.985	1.978	1.970	1.961	1.952
1193.6 eV	$\gamma \\ \delta$	2.49-1 $-2.82-5$	-4.64-2 $-3.48-5$	1.75-2 -3.47-5	2.23-1 -3.29-5	4.37 - 1 $-3.09 - 5$	6.39 - 1 $-2.89 - 5$	8.27 - 1 $-2.68 - 5$	1.00+0 -2.46-5	1.16+0 -2.21-5	1.31+0 1.945
		1.245+2	5.776+1	1.829+1	7.770+0	3.918+0	2.211+0	1.351+0	8.758-1	5.948-1	4.193-1
$\begin{array}{l} 2p_{1/2} \\ E_b = \end{array}$	$\frac{\sigma}{\beta}$	1.245+2	1.446	1.829+1	1.261	1.159	1.068	0.985	0.911	0.844	4.193—1 0.784
1042.8 eV	γ	2.09-2	2.83-1	6.38 - 1	8.68-1	1.03+0	1.15+0	1.24+0	1.32+0	1.38+0	1.43+0
	δ	1.69-2	2.74-2	4.48-2	6.38-2	8.36-2	1.03-1	1.23-1	1.42-1	1.60-1	1.78-1
$2p_{3/2}$	σ	2.399+2	1.101+2	3.443+1	1.452+1	7.277+0	4.085+0	2.485+0	1.605+0	1.086+0	7.625 - 1
$E_b = 1019.7 \text{ eV}$	β	1.423 3.31-2	1.471 2.99-1	1.395 6.59-1	1.288 8.92-1	1.187 1.05+0	1.096 1.17+0	1.014 1.27+0	0.940 1.34+0	0.873 1.40+0	0.813 1.45+0
1019.7 ev	$\frac{\gamma}{\delta}$	1.77-2	2.79-1	4.44-2	6.26-2	8.16-2	1.01-1	1.20-1	1.34-0	1.57-1	1.74-1
$3s_{1/2}$	σ	1.341+1	7.764+0	3.440+0	1.874+0	1.151+0	7.642-1	5.363-1	3.922-1	2.963-1	2.297-1
$E_b = 135.9 \text{ eV}$	β	1.998 -6.24-2	1.999 -3.45-3	1.997 1.85-1	1.993 3.90-1	1.987 5.87-1	1.980 7.71-1	1.973 9.44-1	1.965 1.11+0	1.956 1.26+0	1.948 1.40+0
155.9 eV	$\gamma \\ \delta$	-0.24-2 $-1.90-5$	-3.43-3 -2.08-5	-2.21-5	-2.22-5	-2.17-5	-2.08-5	-1.93-5	-1.75-5	-1.53-5	-1.26-5
3p _{1/2}	σ	1.210+1	5.939+0	2.023+0	8.993-1	4.676-1	2.698-1	1.676-1	1.101-1	7.561-2	5.376-2
$E_b =$	β	1.540	1.461	1.317	1.196	1.093	1.004	0.925	0.856	0.793	0.735
88.6 eV	γ	3.12-1	4.78 - 1	7.29-1	9.07 - 1	1.04+0	1.14+0	1.23+0	1.29+0	1.35+0	1.40+0
	δ	1.37-2	2.18-2	4.11-2	6.20-2	8.29-2	1.04-1	1.24-1	1.43-1	1.62-1	1.80-1
$3p_{3/2}$	σ	2.329+1	1.134+1 1.485	3.820+0 1.343	1.684+0 1.223	8.698-1 1.120	4.990-1 1.032	3.085-1 0.953	2.018-1 0.883	1.380-1 0.821	9.771-2
$E_b = 85.6 \text{ eV}$	$eta \ \gamma$	1.560 3.20-1	4.89-1	7.45–1	9.25—1	1.120	1.052	1.24+0	1.31+0	1.37+0	0.764 1.41+0
	δ	1.41-2	2.18-2	4.03-2	6.04 - 2	8.07-2	1.01 - 1	1.20 - 1	1.40 - 1	1.58 - 1	1.76 - 1
3d _{3/2}	σ	3.676+0	1.310+0	2.884-1	9.481-2	3.910-2	1.868-2	9.894-3	5.660-3	3.437-3	2.190-3
$E_b = 7.9 \text{ eV}$	β	0.986	0.864 6.78-1	0.690	0.577 8.68-1	0.496	0.432 9.55-1	0.380 9.81-1	0.334 1.00+0	0.294 1.01+0	0.257
7.9 eV	$\gamma \\ \delta$	5.81-1 9.57-2	1.24-1	7.96-1 1.77-1	2.27-1	9.18-1 2.73-1	3.16-1	3.56-1	3.92-1	4.27-1	1.02+0 4.60-1
3d _{5/2}	σ	5.350+0	1.901+0	4.166-1	1.364-1	5.606-2	2.670-2	1.410-2	8.046-3	4.875-3	3.099-3
$E_b =$	β	0.975	0.856	0.689	0.583	0.509	0.452	0.405	0.365	0.330	0.298
8.0 eV	γ	5.78-1	6.75 - 1	7.94-1	8.70-1	9.24-1	9.65-1	9.96-1	1.02+0	1.04+0	1.05+0
	δ	9.70-2	1.25-1	1.79-1	2.29-1	2.75-1	3.17-1	3.56-1	3.92-1	4.25-1	4.58-1
$4s_{1/2}$	σ	5.706-1 1.999	3.273-1 1.999	1.435-1 1.997	7.781-2 1.993	4.763-2 1.987	3.156-2 1.980	2.212-2 1.972	1.616-2 1.964	1.220-2 1.956	9.451-3 1.947
$E_b = 1.3 \text{ eV}$	$eta \ \gamma$	-5.63-2	9.86-3	2.02-1	4.06-1	6.02-1	7.85-1	9.56-1	1.11+0	1.26+0	1.40+0
	δ	-1.79 - 5	-1.95 - 5	-2.08 - 5	-2.09 - 5	-2.04-5	-1.97 - 5	-1.86 - 5	-1.69 - 5	-1.48 - 5	-1.24 - 5
Z= 31, Ga: [A	r]3d _{3/2}	3d _{5/2} 4s _{1/2} 4p _{1/}	2								
Chall		k (eV)	2000	2000	4000	F000	C000	7000	9000	0000	10000
Shell		1500	2000	3000	4000	5000	6000	7000	8000	9000	10000
$2s_{1/2} \\ E_b =$	$\frac{\sigma}{\beta}$	7.822+1 1.987	5.030+1 1.994	2.433+1 1.999	1.379+1 1.997	8.655+0 1.993	5.825+0 1.987	4.126+0 1.980	3.038+0 1.972	2.306+0 1.964	1.795+0 1.955
ь = 1297.7 eV	γ	4.43-1	-1.08-2	-1.72-2	1.69-1	3.76–1	5.76-1	7.63-1	9.37—1	1.904	1.955
	δ	-2.67 - 5	-3.97 - 5	-4.13-5	-3.94-5	-3.72-5	-3.53-5	-3.33-5	-3.11-5	-2.85-5	-2.58-5
2p _{1/2}	σ	1.407+2	6.616+1	2.120+1	9.076+0	4.601+0	2.607+0	1.599+0	1.040+0	7.083-1	5.005-1
$E_b =$	β	1.344	1.443	1.388	1.291	1.194	1.103	1.021	0.948	0.880	0.820
1142.3 eV	$_{\delta}^{\gamma}$	-5.18-2 1.35-2	2.17-1 2.52-2	5.98-1 4.28-2	8.41-1 $6.08-2$	1.01+0 7.93-2	1.14+0 9.83-2	1.24+0 1.17-1	1.32+0 1.36-1	1.38+0 1.54-1	1.44+0 1.72-1
2n _{2 (2}		2.715+2	1.260+2	3.985+1	1.692+1	8.520+0	4.802+0	2.931+0	1.898+0	1.288+0	9.066-1
$2p_{3/2} E_b =$	$\frac{\sigma}{eta}$	2.715+2 1.376	1.260+2 1.470	3.985+1 1.416	1.692+1	8.520+0 1.223	4.802+0 1.133	2.931+0 1.051	0.978	0.911	9.066—1 0.852
1115.4 eV	γ	-3.89-2	2.33 - 1	6.20 - 1	8.66 - 1	1.04+0	1.17+0	1.27+0	1.35+0	1.41+0	1.46+0
	δ	1.46-2	2.59-2	4.26-2	5.95-2	7.74-2	9.56-2	1.14-1	1.32-1	1.50-1	1.67-1
3s _{1/2}	σ	1.464+1	8.527+0	3.805+0	2.083+0	1.284+0	8.553-1	6.020-1	4.415-1	3.342-1	2.596-1
$E_b = 158.1 \text{ eV}$	β	1.998	1.999	1.998	1.994	1.988	1.982	1.975	1.967	1.959	1.950
158.1 eV	$_{\delta}^{\gamma}$	-7.08-2 $-2.25-5$	-2.43-2 $-2.42-5$	1.48 - 1 $-2.61 - 5$	3.44-1 -2.67-5	5.38 - 1 $-2.65 - 5$	7.21-1 -2.57-5	8.93-1 -2.44-5	1.05+0 -2.26-5	1.20+0 -2.04-5	1.34+0 1.78-5
	U	2,23-3	2,72-3	2.01-3	2.07-3	2.05-5	2.51-5	2,44-3	2,20-3	2,04−3	1.70-3

Table I (continued)	Tab	le 1 (continued)
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$3p_{1/2}$ $E_b = 106.8 \text{ eV}$	$egin{array}{c} \sigma \ eta \ \gamma \ \delta \end{array}$	1.385+1 1.552 2.83-1 1.23-2	6.882+0 1.481 4.51-1 2.02-2	2.379+0 1.346 7.09-1 3.83-2	1.067+0 1.228 8.93-1 5.79-2	5.587-1 1.125 1.03+0 7.79-2	3.241-1 1.036 1.14+0 9.79-2	2.023-1 0.957 1.23+0 1.18-1	1.335-1 0.887 1.30+0 1.37-1	9.196-2 0.825 1.36+0 1.55-1	6.559-2 0.769 1.41+0 1.73-1
$ 3p_{3/2} E_b = 102.9 eV $	σ	2.662+1	1.312+1	4.481+0	1.993+0	1.036+0	5.973-1	3.710-1	2.436-1	1.671-1	1.187-1
	β	1.574	1.505	1.373	1.256	1.153	1.065	0.986	0.917	0.855	0.799
	γ	2.91-1	4.62-1	7.25-1	9.13-1	1.05+0	1.16+0	1.25+0	1.32+0	1.38+0	1.43+0
	δ	1.29-2	2.04-2	3.75-2	5.63-2	7.56-2	9.51-2	1.14-1	1.33-1	1.51-1	1.69-1
$3d_{3/2}$ $E_b =$ 20.7 eV	σ	5.009+0	1.803+0	4.015-1	1.330-1	5.518-2	2.650-2	1.410-2	8.103-3	4.939-3	3.158-3
	β	1.010	0.893	0.722	0.607	0.523	0.456	0.402	0.355	0.313	0.275
	γ	5.73-1	6.78-1	8.08-1	8.86-1	9.39-1	9.77-1	1.00+0	1.02+0	1.04+0	1.05+0
	δ	9.19-2	1.19-1	1.72-1	2.22-1	2.67-1	3.09-1	3.48-1	3.85-1	4.19-1	4.51-1
$3d_{5/2}$ $E_b =$ 15.7 eV	σ	7.255+0	2.608+0	5.792-1	1.912-1	7.913-2	3.790-2	2.012-2	1.153-2	7.012-3	4.473-3
	β	0.997	0.882	0.718	0.611	0.533	0.474	0.425	0.384	0.347	0.314
	γ	5.70-1	6.74-1	8.05-1	8.86-1	9.42-1	9.85-1	1.02+0	1.04+0	1.06+0	1.07+0
	δ	9.32-2	1.21-1	1.74-1	2.24-1	2.69-1	3.10-1	3.49-1	3.84-1	4.18-1	4.49-1
$4s_{1/2}$ $E_b = 5.6 \text{ eV}$	σ	8.343-1	4.814-1	2.127-1	1.158-1	7.114-2	4.728-2	3.323-2	2.434-2	1.842-2	1.430-2
	β	1.998	1.999	1.998	1.994	1.988	1.981	1.974	1.966	1.958	1.949
	γ	-6.51-2	-1.04-2	1.68-1	3.65-1	5.56-1	7.37-1	9.06-1	1.07+0	1.21+0	1.36+0
	δ	-2.09-5	-2.33-5	-2.47-5	-2.48-5	-2.45-5	-2.39-5	-2.26-5	-2.10-5	-1.88-5	-1.61-5
$ \begin{array}{c} 4p_{1/2} \\ E_b = \\ 0.8 \text{ eV} \end{array} $	σ	3.670-1	1.822-1	6.290-2	2.820-2	1.476-2	8.565-3	5.349-3	3.530-3	2.432-3	1.735-3
	β	1.555	1.479	1.342	1.223	1.121	1.033	0.956	0.887	0.825	0.769
	γ	2.98-1	4.63-1	7.17-1	8.99-1	1.04+0	1.14+0	1.23+0	1.30+0	1.36+0	1.41+0
	δ	1.16-2	1.96-2	3.79-2	5.78-2	7.81-2	9.83-2	1.18-1	1.38-1	1.56-1	1.74-1

Z= 32, Ge: [Ar] $3d_{3/2}^4 3d_{5/2}^6 4s_{1/2}^2 4p_{1/2}^2$

		k (eV)									
Shell		1500	2000	3000	4000	5000	6000	7000	8000	9000	10000
2s _{1/2}	σ	7.948+1	5.300+1	2.604+1	1.489+1	9.400+0	6.356+0	4.518+0	3.336+0	2.539+0	1.981+0
$E_b =$	β	1.983	1.992	1.999	1.998	1.994	1.988	1.982	1.974	1.966	1.958
1414.3 eV	γ	7.53 - 1	5.53 - 2	-4.58 - 2	1.18 - 1	3.18 - 1	5.16 - 1	7.02 - 1	8.75 - 1	1.04+0	1.19+0
	δ	-1.48 - 5	-4.39-5	-4.84 - 5	-4.65 - 5	-4.42 - 5	-4.20-5	-3.98 - 5	-3.76-5	-3.50-5	-3.22 - 5
$2p_{1/2}$	σ	1.570+2	7.529+1	2.442+1	1.053+1	5.366+0	3.054+0	1.879+0	1.226+0	8.374 - 1	5.932 - 1
$E_b =$	β	1.258	1.433	1.403	1.313	1.221	1.135	1.056	0.984	0.918	0.858
1247.8 eV	γ	-1.21-1	1.48 - 1	5.51 - 1	8.11-1	9.94 - 1	1.13+0	1.24+0	1.32+0	1.39+0	1.45+0
	δ	8.80-3	2.30-2	4.03-2	5.77-2	7.58-2	9.42-2	1.13-1	1.31-1	1.48-1	1.66-1
$2p_{3/2}$	σ	3.041+2	1.433+2	4.581+1	1.958+1	9.909+0	5.607+0	3.433+0	2.230+0	1.517+0	1.070+0
$E_b =$	β	1.300	1.462	1.433	1.344	1.253	1.167	1.089	1.017	0.951	0.891
1216.7 eV	γ	-1.09-1	1.65 - 1	5.74 - 1	8.38 - 1	1.02+0	1.16+0	1.27+0	1.35+0	1.42+0	1.48+0
	δ	1.03-2	2.40-2	4.02-2	5.66-2	7.39-2	9.15-2	1.09-1	1.27-1	1.44-1	1.61-1
$3s_{1/2}$	σ	1.592+1	9.328+0	4.195+0	2.308+0	1.428+0	9.544 - 1	6.735 - 1	4.951 - 1	3.757 - 1	2.924 - 1
$E_b =$	β	1.997	1.999	1.998	1.995	1.990	1.983	1.976	1.969	1.961	1.952
180.0 eV	γ	-7.50-2	-4.19 - 2	1.15 - 1	3.04 - 1	4.93 - 1	6.73 - 1	8.43 - 1	1.00+0	1.15+0	1.29+0
	δ	-2.60-5	-2.86-5	-3.07 - 5	-3.15 - 5	-3.13-5	-3.07 - 5	-2.94-5	-2.76-5	-2.56-5	-2.29-5
$3p_{1/2}$	σ	1.578+1	7.937+0	2.784+0	1.260+0	6.642 - 1	3.874 - 1	2.429 - 1	1.609 - 1	1.112 - 1	7.955 - 2
$E_b =$	β	1.565	1.498	1.368	1.254	1.155	1.069	0.992	0.923	0.861	0.804
127.9 eV	γ	2.51 - 1	4.21 - 1	6.87 - 1	8.80 - 1	1.02+0	1.14+0	1.23+0	1.31+0	1.37+0	1.42+0
	δ	1.09-2	1.83-2	3.56-2	5.46-2	7.42-2	9.37-2	1.13-1	1.32-1	1.50-1	1.67-1
$3p_{3/2}$	σ	3.022+1	1.507+1	5.221+0	2.342+0	1.226+0	7.104 - 1	4.431 - 1	2.920 - 1	2.010 - 1	1.432 - 1
$E_b =$	β	1.587	1.523	1.396	1.283	1.186	1.100	1.023	0.955	0.893	0.836
120.8 eV	γ	2.60-1	4.33-1	7.04-1	9.00-1	1.05+0	1.16+0	1.25+0	1.33+0	1.39+0	1.44+0
	δ	1.17-2	1.86-2	3.50-2	5.31-2	7.19-2	9.07-2	1.09-1	1.28-1	1.45-1	1.63-1
$3d_{3/2}$	σ	6.595+0	2.402+0	5.422 - 1	1.811 - 1	7.563 - 2	3.652 - 2	1.953 - 2	1.127 - 2	6.896 - 3	4.424 - 3
$E_b =$	β	1.036	0.920	0.746	0.628	0.541	0.473	0.417	0.369	0.327	0.289
29.2 eV	γ	5.63-1	6.75-1	8.14-1	8.98-1	9.54-1	9.95-1	1.03+0	1.05+0	1.06+0	1.07+0
	δ	8.87-2	1.15-1	1.66-1	2.14-1	2.59 - 1	3.01-1	3.39-1	3.75-1	4.09-1	4.41 - 1
$3d_{5/2}$	σ	9.640+0	3.502+0	7.869 - 1	2.617 - 1	1.089 - 1	5.242 - 2	2.795 - 2	1.608 - 2	9.817 - 3	6.283 - 3
$E_b =$	β	1.023	0.909	0.742	0.630	0.550	0.489	0.440	0.397	0.361	0.327
28.5 eV	γ	5.61-1	6.72-1	8.12-1	8.97-1	9.58-1	1.00+0	1.04+0	1.06+0	1.08+0	1.10+0
	δ	9.01-2	1.17-1	1.69-1	2.17-1	2.61-1	3.02-1	3.40-1	3.75-1	4.08-1	4.39-1
$4s_{1/2}$	σ	1.106+0	6.412 - 1	2.852-1	1.560-1	9.620-2	6.415-2	4.521-2	3.320-2	2.517-2	1.958-2
$E_b =$	β	1.998	1.999	1.998	1.994	1.989	1.983	1.976	1.968	1.960	1.952
9.0 eV	$\gamma \\ \delta$	-7.17-2 $-2.44-5$	-2.77-2 $-2.69-5$	1.35-1 $-2.92-5$	3.26-1 $-2.98-5$	5.15-1 -2.95-5	6.95 - 1 $-2.86 - 5$	8.65 - 1 $-2.73 - 5$	1.02+0 -2.55-5	1.17+0 -2.33-5	1.31+0 -2.06-5
1n		5.863-1	2.947-1	1.033-1	4.677-2	2.466-2	1.439-2	9.026-3	5.980-3	4.135-3	2.959-3
$4p_{1/2} E_b =$	$\frac{\sigma}{eta}$	5.863—1 1.569	2.947—1 1.495	1.033-1	4.677—2 1.244	2.466-2 1.145	1.439-2 1.059	9.026—3 0.982	5.980-3 0.914	4.135—3 0.851	2.959-3 0.795
$E_b = 2.3 \text{ eV}$		2.69—1	4.35-1	6.97—1	8.86—1	1.145	1.059	1.23+0	1.31+0	1.37+0	0.795 1.42+0
2.3 C V	$\gamma \\ \delta$	1.01-2	1.73-2	3.47 - 1	5.40-2	7.37-2	9.34-2	1.13-1	1.31-1	1.49-1	1.42+0
		1,01 2	1.7.5 2	J. 17 2	J, 10 2	,,,,, 2	3,31 2	1,10 1	1,51 1	1, 10 1	1.07

Table 1 (continued)

Z= 33, As: [Ar] $3d_{3/2}^4 3d_{5/2}^6 4s_{1/2}^2 4p_{1/2}^2 4p_{3/2}^1$

	- 3/2	k (eV)	2 13/2								
Shell		1500	2000	3000	4000	5000	6000	7000	8000	9000	10000
2p _{1/2}	σ	1.705+2	8.503+1	2.794+1	1.213+1	6.217+0	3.552+0	2.194+0	1.436+0	9.829-1	6.979-1
$E_b =$	β	1.098	1.414	1.416	1.335	1.246	1.161	1.083	1.012	0.946	0.886
1358.6 eV	γ	-1.67-1	7.30-2	4.98-1	7.75-1	9.70-1	1.12+0	1.23+0	1.32+0	1.40+0	1.46+0
	δ	3.60-3	2.03-2	3.79-2	5.45-2	7.17-2	8.93-2	1.07-1	1.25-1	1.42-1	1.59-1
$2p_{3/2}$ $E_b =$	$\frac{\sigma}{\beta}$	3.345+2 1.169	1.620+2 1.445	5.236+1 1.448	2.252+1 1.368	1.145+1 1.280	6.504+0 1.195	3.995+0 1.117	2.602+0 1.046	1.774+0 0.981	1.254+0 0.921
1323.1 eV	γ	-1.64-1	9.21 - 2	5.23 - 1	8.04 - 1	1.00+0	1.15+0	1.26+0	1.35+0	1.43+0	1.49+0
	δ	4.65-3	2.17-2	3.81-2	5.36-2	6.98-2	8.66-2	1.04-1	1.21-1	1.37-1	1.54-1
$3s_{1/2}$	σ	1.726+1	1.017+1	4.608+0	2.548+0	1.583+0	1.061+0	7.508-1	5.532-1	4.207-1	3.281-1
$E_b = 203.5 \text{ eV}$	$eta \ \gamma$	1.997 -7.59-2	1.998 -5.65-2	1.998 8.36-2	1.995 2.65-1	1.991 4.51-1	1.985 6.29-1	1.978 7.98-1	1.971 9.57-1	1.963 1.11+0	1.955 1.25+0
200.0 01	δ	-3.05-5	-3.33-5	-3.59-5	-3.71-5	-3.68-5	-3.61-5	-3.50-5	-3.32-5	-3.10-5	-2.82-5
3p _{1/2}	σ	1.778+1	9.052+0	3.224+0	1.473+0	7.816-1	4.583-1	2.887-1	1.919-1	1.331-1	9.552-2
$E_b =$	β	1.576	1.514	1.388	1.277	1.179	1.093	1.016	0.949	0.887	0.831
146.4 eV	$\gamma \\ \delta$	2.22-1 9.73-3	3.91-1 1.66-2	6.63-1 3.28-2	8.62 - 1 $5.08 - 2$	1.01+0 6.96-2	1.13+0 8.84-2	1.23+0 1.07-1	1.31+0 1.25-1	1.38+0 1.43-1	1.43+0 1.60-1
3p _{3/2}	σ	3.414+1	1.722+1	6.049+0	2.737+0	1.441+0	8.395-1	5.258-1	3.478-1	2.401-1	1.715-1
$E_b =$	β	1.598	1.540	1.418	1.308	1.211	1.125	1.049	0.982	0.920	0.864
140.5 eV	γ	2.30-1	4.03-1	6.81-1	8.84-1	1.04+0	1.16+0	1.25+0	1.33+0	1.40+0	1.46+0
	δ	1.06-2	1.71-2	3.23-2	4.94-2	6.73-2	8.55-2	1.03-1	1.21-1	1.39-1	1.55-1
$3d_{3/2}$ $E_b =$	$\frac{\sigma}{\beta}$	8.552+0 1.061	3.150+0 0.948	7.202-1 0.774	2.424-1 0.652	1.018-1 0.563	4.943-2 0.493	2.655-2 0.435	1.538-2 0.385	9.446-3 0.342	6.080-3 0.303
41.7 eV	γ	5.52-1	6.71-1	8.21-1	9.10-1	9.70-1	1.01+0	1.04+0	1.07+0	1.08+0	1.10+0
	δ	8.60-2	1.11-1	1.61 - 1	2.08 - 1	2.52 - 1	2.93 - 1	3.32 - 1	3.67 - 1	4.01 - 1	4.32 - 1
$3d_{5/2}$	σ	1.248+1	4.584+0	1.043+0	3.496-1	1.463-1	7.078-2	3.790-2	2.189-2	1.341-2	8.609-3
$E_b = 40.9 \text{ eV}$	β	1.047 5.50-1	0.936 6.68-1	0.768 8.17-1	0.653 9.09-1	0.570 9.72-1	0.507 1.02+0	0.455 1.05+0	0.412 1.08+0	0.374 1.10+0	0.340 1.12+0
40.5 CV	$\frac{\gamma}{\delta}$	8.74-2	1.13-1	1.64-1	2.11-1	2.55-1	2.95-1	3.33-1	3.68-1	4.01-1	4.31-1
4s _{1/2}	σ	1.386+0	8.080-1	3.619-1	1.989-1	1.230-1	8.226-2	5.811-2	4.277-2	3.250-2	2.533-2
$E_b =$	β	1.997	1.999	1.998	1.995	1.990	1.984	1.977	1.970	1.962	1.954
12.5 eV	$\gamma \\ \delta$	-7.57-2 $-2.84-5$	-4.26-2 $-3.12-5$	1.05 - 1 $-3.40 - 5$	2.87-1 -3.53-5	4.70-1 $-3.52-5$	6.47 - 1 $-3.46 - 5$	8.14-1 $-3.36-5$	9.72-1 -3.19-5	1.12+0 -2.98-5	1.26+0 -2.71-5
$4p_{1/2}$	σ	8.431-1	4.290-1	1.528-1	6.984-2	3.708-2	2.176-2	1.371-2	9.122-3	6.330-3	4.544-3
$E_b =$	β	1.581	1.512	1.383	1.270	1.172	1.085	1.009	0.940	0.878	0.822
2.5 eV	γ	2.43-1	4.08-1	6.73-1	8.69-1	1.02+0	1.13+0	1.23+0	1.31+0	1.37+0	1.43+0
4	δ	8.98-3	1.56-2	3.17-2	4.99-2	6.88-2	8.77-2	1.06-1	1.25-1	1.43-1	1.60-1
$\begin{array}{l} 4p_{3/2} \\ E_b = \end{array}$	$\frac{\sigma}{\beta}$	1.632+0 1.604	8.225-1 1.539	2.890-1 1.413	1.308-1 1.301	6.891-2 1.204	4.016-2 1.118	2.517-2 1.041	1.666-2 0.973	1.150-2 0.911	8.222-3 0.855
2.5 eV	γ	2.51-1	4.19-1	6.91-1	8.90-1	1.04+0	1.16+0	1.26+0	1.33+0	1.40+0	1.45+0
	δ	9.79-3	1.60-2	3.12-2	4.84-2	6.64-2	8.46-2	1.03-1	1.21-1	1.38-1	1.55-1
Z= 34, Se: [A:	r]3d _{3/2} 3	$3d_{5/2}^6 4s_{1/2}^2 4p_{1/2}^2$	$_{2}$ $4p_{3/2}^{2}$								
		k (eV)									
Shell		1500	2000	3000	4000	5000	6000	7000	8000	9000	10000
$2p_{1/2}$	σ	1.611+2	9.549+1	3.181+1	1.391+1	7.164+0	4.110+0	2.546+0	1.671+0	1.147+0	8.162 - 1
$E_b = 1476.2 \text{ eV}$	β	0.628 -1.25-1	1.381 -5.99-3	1.426 4.40-1	1.355 7.35-1	1.271 9.43-1	1.188 1.10+0	1.112 1.22+0	1.041 1.32+0	0.976 1.40+0	0.916 1.46+0
1470.2 ev	$_{\delta}^{\gamma}$	1.76–2	-3.99-3 1.71-2	3.56-2	5.16-2	6.80-2	8.47-2	1.02-1	1.32+0	1.40+0	1.52-1
2p _{3/2}	σ	3.463+2	1.821+2	5.956+1	2.577+1	1.316+1	7.503+0	4.622+0	3.019+0	2.063+0	1.461+0
$E_b =$	β	0.866	1.417	1.459	1.390	1.306	1.224	1.148	1.077	1.012	0.953
1435.8 eV	$\gamma \\ \delta$	-1.56-1 4.76-3	1.32-2 1.88-2	4.66-1 3.61-2	7.66-1 $5.09-2$	9.77 - 1 $6.63 - 2$	1.13+0 8.20-2	1.26+0 9.82-2	1.35+0 1.14-1	1.43+0 1.31-1	1.50+0 1.47-1
3s _{1/2}	σ	1.867+1	1.106+1	5.047+0	2.805+0	1.748+0	1.175+0	8.337-1	6.156-1	4.691-1	3.665-1
$E_b =$	β	1.996	1.998	1.998	1.996	1.992	1.175+0	1.980	1.973	1.965	1.957
231.5 eV	γ	-7.35-2	-6.81 - 2	5.40 - 2	2.26 - 1	4.07 - 1	5.83 - 1	7.51 - 1	9.09 - 1	1.06+0	1.20+0
	δ	-3.47-5	-3.83-5	-4.18-5	-4.34-5	-4.35-5	-4.30-5	-4.20-5	-4.02-5	-3.80-5	-3.52-5
$3p_{1/2}$	σ_{β}	1.992+1 1.585	1.026+1 1.528	3.710+0 1.409	1.711+0 1.300	9.138-1 1.203	5.386-1 1.118	3.407-1 1.042	2.274-1 0.974	1.582-1 0.913	1.139-1 0.856
$E_b = 168.2 \text{ eV}$	$eta \ \gamma$	1.585	3.59—1	6.37-1	8.43-1	1.203	1.118	1.042	0.974 1.31+0	1.38+0	0.856 1.44+0
	δ	8.62-3	1.50-2	3.02-2	4.74-2	6.52-2	8.33-2	1.01-1	1.19-1	1.36-1	1.53-1
3p _{3/2}	σ	3.833+1	1.955+1	6.964+0	3.178+0	1.684+0	9.854-1	6.197-1	4.113-1	2.848-1	2.040-1
$E_b =$	β	1.609	1.556	1.441	1.333	1.237	1.153	1.077	1.009	0.948	0.891
161.9 eV	$_{\delta}^{\gamma}$	2.00-1 $9.68-3$	3.72-1 1.56-2	6.56-1 2.99-2	8.66-1 $4.60-2$	1.03+0 6.30-2	1.15+0 8.03-2	1.25+0 9.76-2	1.34+0 1.15-1	1.41+0 1.32-1	1.47+0 1.48-1
3d _{3/2}	σ	1.091+1	4.064+0	9.407-1	3.189-1	1.348-1	6.571-2	3.544-2	2.061-2	1.270-2	8.197-3
$E_b =$	β	1.085	0.977	0.802	0.678	0.587	0.515	0.456	0.405	0.360	0.320

Table 1 (contin	ued)										
57.4 eV	γ δ	5.40-1 8.37-2	6.66-1 1.08-1	8.26-1 1.56-1	9.22-1 2.02-1	9.86-1 2.46-1	1.03+0 2.87-1	1.06+0 3.25-1	1.09+0 3.60-1	1.11+0 3.93-1	1.12+0 4.25-1
3d _{5/2}	σ	1.589+1	5.903+0	1.360+0	4.591-1	1.932-1	9.389-2	5.048-2	2.926-2	1.798-2	1.158-2
$E_b = 56.4 \text{ eV}$	β γ	1.070 5.39-1	0.963 6.63-1	0.794 8.22-1	0.677 9.20-1	0.592 9.87-1	0.527 1.04+0	0.474 1.07+0	0.430 1.10+0	0.390 1.13+0	0.356 1.14+0
	δ	8.50-2	1.10-1	1.59-1	2.05-1	2.49-1	2.89-1	3.26-1	3.61-1	3.94-1	4.24-1
$4s_{1/2}$	σ	1.681+0 1.997	9.839-1 1.998	4.437-1 1.998	2.450-1 1.996	1.521-1 1.991	1.020-1 1.985	7.220-2 1.979	5.325-2 1.972	4.054-2 1.964	3.165-2 1.956
$E_b = 16.2 \text{ eV}$	β γ	-7.74-2	-5.50-2	7.79–2	2.51-1	4.30-1	6.04–1	7.69–1	9.25-1	1.964	1.21+0
	δ	-3.23-5	-3.60-5	-3.94 - 5	-4.11-5	-4.12 - 5	-4.06 - 5	-3.95 - 5	-3.79 - 5	-3.61-5	-3.34-5
$4p_{1/2}$	σ	1.131+0 1.592	5.826-1 1.528	2.107-1 1.404	9.724-2	5.198-2 1.200	3.066-2 1.116	1.941-2 1.041	1.296-2 0.973	9.025-3 0.912	6.498-3 0.856
$E_b = 5.6 \text{ eV}$	$eta \ \gamma \ \delta$	2.17 - 1	3.80 - 1	6.50 - 1	1.295 8.52-1	1.01+0	1.13+0	1.23+0	1.31+0	1.38+0	1.44+0
4p _{3/2}	σ	7.83-3 2.174+0	1.40-2 1.108+0	2.93-2 3.949-1	4.68-2 1.804-1	6.52-2 9.563-2	8.37-2 5.602-2	1.02-1 3.525-2	1.20-1 2.341-2	1.37-1 1.622-2	1.54-1 1.163-2
$E_b =$	β	1.616	1.555	1.436	1.329	1.234	1.151	1.076	1.009	0.947	0.891
5.6 eV	$\gamma \\ \delta$	2.25-1 8.80-3	3.92-1 1.45-2	6.68-1 $2.88-2$	8.75-1 4.54-2	1.03+0 6.28-2	1.16+0 8.05-2	1.26+0 9.80-2	1.34+0 1.15-1	1.41+0 1.32-1	1.47+0 1.49-1
7= 35 Rr· [A		$\frac{3d_{5/2}^6 4s_{1/2}^2 4p_{1/2}^2}{3d_{5/2}^6 4s_{1/2}^2 4p_{1/2}^2}$		2.00-2	4.34-2	0.20-2	8.03-2	9.60-2	1,13-1	1.32-1	1.49-1
Z- 33, BI. [A	1 JJu _{3/2}	k (eV)	2 ⁴ P _{3/2}								
Shell		1500	2000	3000	4000	5000	6000	7000	8000	9000	10000
3s _{1/2}	σ	2.008+1	1.196+1	5.499+0	3.071+0	1.921+0	1.295+0	9.210-1	6.817-1	5.204-1	4.074-1
$E_b =$	β	1.995	1.997	1.998	1.996	1.993	1.987	1.981	1.974	1.967	1.959
256.5 eV	δ	-6.78-2 $-4.01-5$	-7.62-2 $-4.33-5$	2.74-2 -4.82-5	1.90-1 -5.05-5	3.65-1 -5.09-5	5.37-1 -5.07-5	7.02 - 1 $-4.96 - 5$	8.59-1 -4.84-5	1.01+0 -4.61-5	1.15+0 -4.35-5
$3p_{1/2}$	σ	2.213+1	1.154+1	4.236+0	1.972+0	1.060+0	6.281-1	3.991-1	2.673-1	1.866-1	1.347-1
$E_b = 189.3 \text{ eV}$	β γ	1.594 1.63-1	1.542 3.28-1	1.429 6.09-1	1.323 8.22-1	1.228 9.85-1	1.144 1.11+0	1.070 1.22+0	1.003 1.31+0	0.941 1.38+0	0.886 1.44+0
103.3 € 1	δ	7.56-3	1.34-2	2.79-2	4.42-2	6.12-2	7.86-2	9.61-2	1.13-1	1.30-1	1.47-1
3p _{3/2}	σ	4.266+1	2.200+1	7.951+0	3.661+0	1.951+0	1.148+0	7.247-1	4.827-1	3.353-1	2.408-1
$E_b = 181.5 \text{ eV}$	β γ	1.618 1.71-1	1.570 3.40-1	1.462 6.29-1	1.357 8.47-1	1.264 1.01+0	1.180 1.14+0	1.106 1.25+0	1.039 1.34+0	0.978 1.41+0	0.922 1.47+0
101.5 € 1	δ	8.76-3	1.43-2	2.77-2	4.30-2	5.90-2	7.56–2	9.24-2	1.09-1	1.26-1	1.42-1
3d _{3/2}	σ	1.361+1	5.130+0	1.204+0	4.116-1	1.750-1	8.572-2	4.643-2	2.709-2	1.675-2	1.085-2
$E_b = 70.1 \text{ eV}$	β γ	1.107 5.27-1	1.004 6.59-1	0.830 8.29-1	0.704 9.32-1	0.610 1.00+0	0.537 1.05+0	0.477 1.08+0	0.425 1.11+0	0.379 1.13+0	0.338 1.14+0
	δ	8.14-2	1.05-1	1.51-1	1.96-1	2.39-1	2.80-1	3.17-1	3.52-1	3.85-1	4.16-1
$3d_{5/2}$	σ	1.979+1 1.092	7.442+0 0.989	1.738+0 0.819	5.915-1 0.700	2.504-1	1.223-1 0.547	6.599-2 0.493	3.839-2 0.447	2.367-2 0.407	1.529-2 0.372
$E_b = 69.0 \text{ eV}$	β γ	5.26-1	6.55-1	8.24-1	9.29-1	0.614 1.00+0	1.05+0	1.09+0	1.12+0	1.15+0	1.17+0
	δ	8.27-2	1.07-1	1.54-1	2.00-1	2.42-1	2.82-1	3.19-1	3.54-1	3.86-1	4.17-1
$4s_{1/2}$	σ	1.997+0	1.173+0	5.319-1	2.949-1	1.836-1	1.234-1	8.759-2	6.473-2	4.936-2	3.861-2
$E_b = 27.3 \text{ eV}$	β γ	1.996 -7.75-2	1.998 -6.59-2	1.998 5.15-2	1.996 2.16-1	1.992 3.90-1	1.987 5.61-1	1.980 7.26-1	1.973 8.82-1	1.966 1.03+0	1.958 1.17+0
	δ	-3.63-5	-4.10-5	-4.55 - 5	-4.78-5	-4.81-5	-4.77 - 5	-4.65 - 5	-4.49-5	-4.27 - 5	-4.01-5
$4p_{1/2}$	σ	1.444+0	7.526-1	2.765-1	1.289-1	6.937-2	4.114-2	2.616-2	1.754-2	1.225-2	8.846-3
$E_b = 5.2 \text{ eV}$	β γ	1.603 1.93-1	1.541 3.53-1	1.423 6.25-1	1.318 8.34-1	1.224 9.94-1	1.141 1.12+0	1.066 1.23+0	1.000 1.31+0	0.938 1.38+0	0.883 1.45+0
	δ	6.80-3	1.25-2	2.69-2	4.38-2	6.15-2	7.94-2	9.72-2	1.15-1	1.32-1	1.48-1
$4p_{3/2}$	σ	2.759+0	1.422+0	5.145-1	2.372-1	1.266-1	7.453-2	4.710-2	3.139-2	2.182-2	1.568-2
$E_b = 4.6 \text{ eV}$	β γ	1.627 2.01-1	1.570 3.65-1	1.456 6.44-1	1.353 8.57-1	1.260 1.02+0	1.178 1.15+0	1.104 1.26+0	1.037 1.34+0	0.976 1.41+0	0.920 1.48+0
	δ	7.91-3	1.32-2	2.66-2	4.24-2	5.92-2	7.63-2	9.34-2	1.10-1	1.27-1	1.43-1
Z= 36, Kr: [A	r]3d _{3/2}	$3d_{5/2}^6 \ 4s_{1/2}^2 \ 4p_{1/2}^2$	4p _{3/2}								
Shall		k (eV)	2000	3000	4000	5000	6000	7000	9000	0000	10000
Shell 3s _{1/2}	~	1500 2.162+1	2000 1.293+1	3000 5.986+0	4000 3.358+0	5000 2.107+0	6000 1.425+0	1.015+0	8000 7.528-1	9000 5.758-1	10000 4.514-1
$E_b =$	$\frac{\sigma}{eta}$	1.994	1.293+1	1.998	3.338+0 1.997	1.993	1.425+0	1.015+0	1.976	1.969	1.961
292.1 eV	γ δ	-5.89-2 -4.51-5	-8.21-2 $-4.98-5$	2.23-3 -5.55-5	1.53-1 -5.82-5	3.22-1 -5.92-5	4.91-1 -5.93-5	6.54-1 -5.86-5	8.09-1 -5.74-5	9.57-1 -5.54-5	1.10+0 -5.29-5
$3p_{1/2}$	σ	2.463+1	1.298+1	4.829+0	2.267+0	1.226+0	7.299-1	4.656-1	3.129-1	2.191-1	1.585-1
$E_b =$	β	1.601	1.554	1.448	1.346	1.253	1.170	1.097	1.031	0.971	0.915
222.1 eV	$_{\delta}^{\gamma}$	1.33-1 $6.50-3$	2.94-1 1.19-2	5.79-1 2.55-2	7.99-1 4.12-2	9.69-1 5.76-2	1.10+0 7.43-2	1.21+0 9.12-2	1.31+0 1.08-1	1.38+0 1.25-1	1.45+0 1.41-1
3p _{3/2}	σ	4.765+1	2.481+1	9.079+0	4.213+0	2.258+0	1.334+0	8.450-1	5.645-1	3.931-1	2.831-1
$E_b =$	β	1.626	1.584	1.482	1.382	1.290	1.208	1.135	1.069	1.010	0.954
214.4 eV	$\gamma \\ \delta$	1.40-1 $7.86-3$	3.07-1 1.29-2	5.99-1 2.55-2	8.25 - 1 $4.01 - 2$	9.99-1 5.55-2	1.14+0 7.13-2	1.25+0 8.74-2	1.34+0 1.04-1	1.42+0 1.20-1	1.48+0 1.36-1
	U	,.50 5	1.23 2	2.33 2	1.01 2	J.JJ 2	,.15 2	5.74 Z	1.54 1	1.20 1	1.50 - 1

Ta	h	۱۵.	1	(~	^*	ı f	in	.,	n	ď	١

2.1		1.701.1	C 4C0 · 0	1.524.0	5 250 4	2.252 4	1.100 1	6.000	2.525. 2	2.405. 2	1 110 2
$3d_{3/2}$	σ	1.701+1	6.468+0	1.534+0	5.278 - 1	2.253 - 1	1.108 - 1	6.022 - 2	3.525 - 2	2.185 - 2	1.418 - 2
$E_b =$	β	1.129	1.031	0.859	0.730	0.634	0.559	0.497	0.444	0.397	0.355
$E_b = 95.0 \text{ eV}$	γ	5.12 - 1	6.50 - 1	8.32 - 1	9.41 - 1	1.01+0	1.07+0	1.11+0	1.13+0	1.15+0	1.17+0
	δ	7.90 - 2	1.02 - 1	1.47 - 1	1.91 - 1	2.33 - 1	2.73 - 1	3.10 - 1	3.44 - 1	3.77 - 1	4.08 - 1
$3d_{5/2}$	σ	2.471+1	9.372+0	2.212+0	7.573 - 1	3.220 - 1	1.578 - 1	8.545 - 2	4.986 - 2	3.082 - 2	1.995 - 2
$E_b =$	β	1.114	1.015	0.847	0.724	0.635	0.567	0.511	0.464	0.423	0.387
93.8 eV	γ	5.11 - 1	6.47 - 1	8.27 - 1	9.37 - 1	1.01+0	1.07+0	1.11+0	1.14+0	1.17+0	1.19+0
	δ	8.03-2	1.04-1	1.50-1	1.94-1	2.36-1	2.76-1	3.12-1	3.46-1	3.78-1	4.08-1
$4s_{1/2}$	σ	2.316+0	1.365+0	6.232 - 1	3.471 - 1	2.169 - 1	1.462 - 1	1.040 - 1	7.702 - 2	5.885 - 2	4.610 - 2
$E_b =$	β	1.996	1.997	1.998	1.996	1.993	1.988	1.982	1.975	1.968	1.960
27.5 eV	γ	-7.58 - 2	-7.36-2	2.87 - 2	1.83 - 1	3.52 - 1	5.20 - 1	6.82 - 1	8.37 - 1	9.84 - 1	1.12+0
	δ	-4.13-5	-4.68 - 5	-5.23-5	-5.56-5	-5.59-5	-5.60-5	-5.47 - 5	-5.33-5	-5.11-5	-4.84-5
$4p_{1/2}$	σ	1.797+0	9.456 - 1	3.523 - 1	1.657 - 1	8.975 - 2	5.349 - 2	3.415 - 2	2.297 - 2	1.610 - 2	1.165 - 2
$E_b =$	β	1.613	1.555	1.441	1.339	1.247	1.165	1.090	1.023	0.962	0.906
14.7 eV	γ	1.69 - 1	3.26 - 1	5.99 - 1	8.13 - 1	9.79 - 1	1.11+0	1.22+0	1.31+0	1.39+0	1.45+0
	δ	5.83-3	1.10-2	2.45-2	4.06-2	5.77-2	7.50-2	9.21-2	1.09-1	1.26-1	1.42-1
	0										
$4p_{3/2}$	σ	3.419+0	1.779+0	6.521 - 1	3.032 - 1	1.627 - 1	9.625 - 2	6.104 - 2	4.082 - 2	2.845 - 2	2.050 - 2
$E_b =$	β	1.638	1.584	1.475	1.376	1.285	1.203	1.129	1.062	1.002	0.946
14.0 eV	γ	1.76 - 1	3.38 - 1	6.18 - 1	8.38 - 1	1.01+0	1.14+0	1.25+0	1.34+0	1.42+0	1.48+0
1 1.0 C V	δ	7.09-3	1.19-2	2.44-2	3.94-2	5.55-2	7.19-2	8.83-2	1.05-1	1.20-1	1.36-1
	0	7.05-5	1.13-2	2,44-2	3.34-2	3.33-2	7.13-2	0.05-2	1.05-1	1.20-1	1.50-1
Z= 37, Rb: [Ki	rl5s.										
2 37, 10. [10	1001/2										
		k (eV)									
Shall		1500	2000	3000	4000	5000	6000	7000	8000	0000	10000
Shell		1500				5000	6000	/000		9000	10000
$3s_{1/2}$	σ	2.307+1	1.387+1	6.465+0	3.644+0	2.295+0	1.556+0	1.112+0	8.266 - 1	6.335 - 1	4.976 - 1
$E_b =$	β	1.993	1.996	1.998	1.997	1.994	1.990	1.984	1.978	1.971	1.963
322.1 eV	γ	-4.91-2	-8.44-2	-1.87 - 2	1.20-1	2.81-1	4.44-1	6.05-1	7.59-1	9.07-1	1.05+0
J22.1 CV											
	δ	-5.05 - 5	-5.60-5	-6.37 - 5	-6.75 - 5	-6.91-5	-6.91-5	-6.85 - 5	-6.71 - 5	-6.50 - 5	-6.24 - 5
$3p_{1/2}$	σ	2.694+1	1.437+1	5.427+0	2.573+0	1.402+0	8.394 - 1	5.378 - 1	3.628 - 1	2.548 - 1	1.849 - 1
$E_b =$	β	1.606	1.564	1.463	1.366	1.278	1.199	1.127	1.061	1.001	0.945
247.4 eV		1.09-1	2.65-1	5.49-1	7.73-1	9.49-1	1.09+0	1.21+0	1.30+0	1.38+0	1.45+0
247.4 CV	γ										
	δ	5.65-3	1.07 - 2	2.30-2	3.77 - 2	5.39-2	7.06-2	8.75-2	1.04 - 1	1.20 - 1	1.36 - 1
$3p_{3/2}$	σ	5.220+1	2.748+1	1.020+1	4.776+0	2.578+0	1.531+0	9.738-1	6.528-1	4.560-1	3.292-1
$E_b =$	β	1.631	1.595	1.499	1.404	1.318	1.239	1.168	1.102	1.042	0.986
220 5 -14											
238.5 eV	γ	1.17-1	2.78-1	5.69-1	8.00-1	9.81-1	1.13+0	1.24+0	1.34+0	1.42+0	1.49+0
	δ	7.17 - 3	1.19 - 2	2.32 - 2	3.68 - 2	5.19 - 2	6.76 - 2	8.36 - 2	9.94 - 2	1.15 - 1	1.30 - 1
3d _{3/2}	σ	2.047+1	7.891+0	1.904+0	6.610-1	2.840-1	1.403-1	7.656-2	4.497-2	2.797-2	1.821-2
	β	1.144	1.052	0.888	0.760	0.661	0.581	0.515	0.459	0.411	0.368
$E_b =$											
111.8 eV	γ	4.95 - 1	6.38 - 1	8.31 - 1	9.49 - 1	1.03+0	1.08+0	1.12+0	1.15+0	1.17+0	1.19+0
	δ	7.63 - 2	9.86 - 2	1.43 - 1	1.86 - 1	2.27 - 1	2.65 - 1	3.01 - 1	3.35 - 1	3.68 - 1	3.98 - 1
3d _{5/2}	σ	2.972+1	1.142+1	2.742+0	9.476-1	4.055-1	1.996-1	1.085-1	6.353-2	3.939-2	2.557-2
$E_b =$	β	1.128	1.035	0.874	0.752	0.660	0.587	0.528	0.478	0.435	0.398
110.3 eV	γ	4.95 - 1	6.36 - 1	8.25 - 1	9.45 - 1	1.03+0	1.08+0	1.13+0	1.16+0	1.19+0	1.21+0
	δ	7.75 - 2	1.01 - 1	1.46 - 1	1.90 - 1	2.31 - 1	2.69 - 1	3.05 - 1	3.38 - 1	3.70 - 1	3.99 - 1
1c	σ	2.784+0	1.646+0	7.562-1	4.231-1	2.653-1	1.793-1	1.279-1	9.487-2	7.262-2	5.699-2
$4s_{1/2}$		1.995	1.997	1.998	1.997		1.989	1.983	1.977		
$E_b =$	β					1.993				1.970	1.962
29.3 eV	γ	-7.29-2	-7.87 - 2	8.84 - 3	1.54 - 1	3.15 - 1	4.77 - 1	6.35 - 1	7.87 - 1	9.33 - 1	1.07+0
	δ	-4.65 - 5	-5.29 - 5	-6.01 - 5	-6.43 - 5	-6.53 - 5	-6.58 - 5	-6.50 - 5	-6.38 - 5	-6.18 - 5	-5.93 - 5
4p _{1/2}	σ	2.357+0	1.254+0	4.743-1	2.253-1	1.230-1	7.370-2	4.728-2	3.192-2	2.245-2	1.630-2
		1.622	1.567	1.455	1.354	1.265	1.185	1.113	1.047	0.988	0.933
$E_b =$	β										
14.8 eV	γ	1.49-1	3.01-1	5.74-1	7.90-1	9.61 - 1	1.10+0	1.21+0	1.30+0	1.38+0	1.45+0
	δ	5.14 - 3	9.82 - 3	2.22 - 2	3.71 - 2	5.32 - 2	6.98 - 2	8.65 - 2	1.03 - 1	1.20 - 1	1.36 - 1
						2.240 1	4 000 4	0.400.0	5.693-2	3.980-2	2.876-2
$4n_{2/2}$	ď	4517+0	2 373+0	8 820_1	4 144-1	/ /411— 1	1 337-1	8 48 4 /		J.JUU-2	2.070-2
$4p_{3/2}$	σ	4.517+0 1.647	2.373+0	8.829-1	4.144-1 1.303	2.240-1	1.332-1	8.483-2 1.153		1 020	0.072
$E_b =$	β	1.647	1.597	1.491	1.393	1.304	1.225	1.153	1.088	1.029	0.973
	β γ	1.647 1.56-1	1.597 3.12-1	1.491 5.94-1	1.393 8.16-1	1.304 9.91-1	1.225 1.13+0	1.153 1.25+0	1.088 1.34+0	1.42+0	1.49+0
$E_b =$	β	1.647	1.597	1.491	1.393	1.304	1.225	1.153	1.088		
$E_b = 14.0 \text{ eV}$	$eta \ \gamma \ \delta$	1.647 1.56-1 6.54-3	1.597 3.12-1 1.09-2	1.491 5.94-1 2.24-2	1.393 8.16-1 3.61-2	1.304 9.91-1 5.11-2	1.225 1.13+0 6.67-2	1.153 1.25+0 8.26-2	1.088 1.34+0 9.85-2	1.42+0 1.14-1	1.49+0 1.30-1
$E_b = 14.0 \text{ eV}$ $5s_{1/2}$	β γ δ	1.647 1.56-1 6.54-3 1.261-1	1.597 3.12-1 1.09-2 7.433-2	1.491 5.94-1 2.24-2 3.400-2	1.393 8.16-1 3.61-2 1.898-2	1.304 9.91-1 5.11-2 1.189-2	1.225 1.13+0 6.67-2 8.029-3	1.153 1.25+0 8.26-2 5.722-3	1.088 1.34+0 9.85-2 4.244-3	1.42+0 1.14-1 3.247-3	1.49+0 1.30-1 2.548-3
$E_b = 14.0 \text{ eV}$ $5s_{1/2}$ $E_b =$	β γ δ σ β	1.647 1.56-1 6.54-3 1.261-1 1.995	1.597 3.12-1 1.09-2 7.433-2 1.997	1.491 5.94-1 2.24-2 3.400-2 1.998	1.393 8.16-1 3.61-2 1.898-2 1.997	1.304 9.91-1 5.11-2 1.189-2 1.993	1.225 1.13+0 6.67-2 8.029-3 1.989	1.153 1.25+0 8.26-2 5.722-3 1.983	1.088 1.34+0 9.85-2 4.244-3 1.976	1.42+0 1.14-1 3.247-3 1.970	1.49+0 1.30-1 2.548-3 1.962
$E_b = 14.0 \text{ eV}$ $5s_{1/2}$	$\begin{array}{c} \beta \\ \gamma \\ \delta \end{array}$ $\begin{array}{c} \sigma \\ \beta \\ \gamma \end{array}$	1.647 1.56-1 6.54-3 1.261-1 1.995 -7.47-2	1.597 3.12-1 1.09-2 7.433-2 1.997 -7.97-2	1.491 5.94-1 2.24-2 3.400-2 1.998 9.60-3	1.393 8.16-1 3.61-2 1.898-2 1.997 1.55-1	1.304 9.91-1 5.11-2 1.189-2 1.993 3.15-1	1.225 1.13+0 6.67-2 8.029-3 1.989 4.78-1	1.153 1.25+0 8.26-2 5.722-3 1.983 6.38-1	1.088 1.34+0 9.85-2 4.244-3 1.976 7.91-1	1.42+0 1.14-1 3.247-3 1.970 9.38-1	1.49+0 1.30-1 2.548-3 1.962 1.08+0
$E_b = 14.0 \text{ eV}$ $5s_{1/2}$ $E_b =$	β γ δ σ β	1.647 1.56-1 6.54-3 1.261-1 1.995	1.597 3.12-1 1.09-2 7.433-2 1.997	1.491 5.94-1 2.24-2 3.400-2 1.998	1.393 8.16-1 3.61-2 1.898-2 1.997	1.304 9.91-1 5.11-2 1.189-2 1.993	1.225 1.13+0 6.67-2 8.029-3 1.989	1.153 1.25+0 8.26-2 5.722-3 1.983	1.088 1.34+0 9.85-2 4.244-3 1.976	1.42+0 1.14-1 3.247-3 1.970	1.49+0 1.30-1 2.548-3 1.962
$E_b = 14.0 \text{ eV}$ $5s_{1/2}$ $E_b = 4.0 \text{ eV}$	β γ δ σ β γ δ	1.647 1.56-1 6.54-3 1.261-1 1.995 -7.47-2	1.597 3.12-1 1.09-2 7.433-2 1.997 -7.97-2	1.491 5.94-1 2.24-2 3.400-2 1.998 9.60-3	1.393 8.16-1 3.61-2 1.898-2 1.997 1.55-1	1.304 9.91-1 5.11-2 1.189-2 1.993 3.15-1	1.225 1.13+0 6.67-2 8.029-3 1.989 4.78-1	1.153 1.25+0 8.26-2 5.722-3 1.983 6.38-1	1.088 1.34+0 9.85-2 4.244-3 1.976 7.91-1	1.42+0 1.14-1 3.247-3 1.970 9.38-1	1.49+0 1.30-1 2.548-3 1.962 1.08+0
$E_b = 14.0 \text{ eV}$ $5s_{1/2}$ $E_b =$	β γ δ σ β γ δ	1.647 1.56-1 6.54-3 1.261-1 1.995 -7.47-2	1.597 3.12-1 1.09-2 7.433-2 1.997 -7.97-2	1.491 5.94-1 2.24-2 3.400-2 1.998 9.60-3	1.393 8.16-1 3.61-2 1.898-2 1.997 1.55-1	1.304 9.91-1 5.11-2 1.189-2 1.993 3.15-1	1.225 1.13+0 6.67-2 8.029-3 1.989 4.78-1	1.153 1.25+0 8.26-2 5.722-3 1.983 6.38-1	1.088 1.34+0 9.85-2 4.244-3 1.976 7.91-1	1.42+0 1.14-1 3.247-3 1.970 9.38-1	1.49+0 1.30-1 2.548-3 1.962 1.08+0
$E_b = 14.0 \text{ eV}$ $5s_{1/2}$ $E_b = 4.0 \text{ eV}$	β γ δ σ β γ δ	1.647 1.56-1 6.54-3 1.261-1 1.995 -7.47-2 -4.60-5	1.597 3.12-1 1.09-2 7.433-2 1.997 -7.97-2	1.491 5.94-1 2.24-2 3.400-2 1.998 9.60-3	1.393 8.16-1 3.61-2 1.898-2 1.997 1.55-1	1.304 9.91-1 5.11-2 1.189-2 1.993 3.15-1	1.225 1.13+0 6.67-2 8.029-3 1.989 4.78-1	1.153 1.25+0 8.26-2 5.722-3 1.983 6.38-1	1.088 1.34+0 9.85-2 4.244-3 1.976 7.91-1	1.42+0 1.14-1 3.247-3 1.970 9.38-1	1.49+0 1.30-1 2.548-3 1.962 1.08+0
$E_b = 14.0 \text{ eV}$ $5s_{1/2} = E_b = 4.0 \text{ eV}$ $Z= 38, \text{ Sr: [Kr]}$	β γ δ σ β γ δ	1.647 1.56-1 6.54-3 1.261-1 1.995 -7.47-2 -4.60-5 k (eV)	1.597 3.12-1 1.09-2 7.433-2 1.997 -7.97-2 -5.26-5	1.491 5.94-1 2.24-2 3.400-2 1.998 9.60-3 -6.05-5	1.393 8.16-1 3.61-2 1.898-2 1.997 1.55-1 -6.36-5	1.304 9.91-1 5.11-2 1.189-2 1.993 3.15-1 -6.47-5	1.225 1.13+0 6.67-2 8.029-3 1.989 4.78-1 -6.47-5	1.153 1.25+0 8.26-2 5.722-3 1.983 6.38-1 -6.39-5	1.088 1.34+0 9.85-2 4.244-3 1.976 7.91-1 -6.21-5	1.42+0 1.14-1 3.247-3 1.970 9.38-1 -6.03-5	1.49+0 1.30-1 2.548-3 1.962 1.08+0 -5.66-5
$E_b = 14.0 \text{ eV}$ $5s_{1/2}$ $E_b = 4.0 \text{ eV}$	β γ δ σ β γ δ	1.647 1.56-1 6.54-3 1.261-1 1.995 -7.47-2 -4.60-5	1.597 3.12-1 1.09-2 7.433-2 1.997 -7.97-2	1.491 5.94-1 2.24-2 3.400-2 1.998 9.60-3	1.393 8.16-1 3.61-2 1.898-2 1.997 1.55-1	1.304 9.91-1 5.11-2 1.189-2 1.993 3.15-1	1.225 1.13+0 6.67-2 8.029-3 1.989 4.78-1	1.153 1.25+0 8.26-2 5.722-3 1.983 6.38-1	1.088 1.34+0 9.85-2 4.244-3 1.976 7.91-1	1.42+0 1.14-1 3.247-3 1.970 9.38-1	1.49+0 1.30-1 2.548-3 1.962 1.08+0
$E_b = 14.0 \text{ eV}$ $5s_{1/2}$ $E_b = 4.0 \text{ eV}$ $Z= 38, \text{ Sr: [Kr]}$ Shell	$ \begin{array}{c} \beta \\ \gamma \\ \delta \\ \hline \sigma \\ \beta \\ \gamma \\ \delta \\ r]5s_{1/2}^2 \end{array} $	1.647 1.56-1 6.54-3 1.261-1 1.995 -7.47-2 -4.60-5 k (eV) 1500	1.597 3.12-1 1.09-2 7.433-2 1.997 -7.97-2 -5.26-5	1.491 5.94-1 2.24-2 3.400-2 1.998 9.60-3 -6.05-5	1.393 8.16-1 3.61-2 1.898-2 1.997 1.55-1 -6.36-5	1.304 9.91-1 5.11-2 1.189-2 1.993 3.15-1 -6.47-5	1.225 1.13+0 6.67-2 8.029-3 1.989 4.78-1 -6.47-5	1.153 1.25+0 8.26-2 5.722-3 1.983 6.38-1 -6.39-5	1.088 1.34+0 9.85-2 4.244-3 1.976 7.91-1 -6.21-5	1.42+0 1.14-1 3.247-3 1.970 9.38-1 -6.03-5	1.49+0 1.30-1 2.548-3 1.962 1.08+0 -5.66-5
$E_b = 14.0 \text{ eV}$ $5s_{1/2}$ $E_b = 4.0 \text{ eV}$ $Z= 38, \text{ Sr: [Kr]}$ Shell $3s_{1/2}$	$\frac{\beta}{\delta}$ $\frac{\gamma}{\delta}$ $\frac{\sigma}{\beta}$ $\frac{\gamma}{\delta}$ $r]5s_{1/2}^{2}$	1.647 1.56-1 6.54-3 1.261-1 1.995 -7.47-2 -4.60-5 k (eV) 1500 2.458+1	1.597 3.12-1 1.09-2 7.433-2 1.997 -7.97-2 -5.26-5 2000 1.485+1	1.491 5.94-1 2.24-2 3.400-2 1.998 9.60-3 -6.05-5	1.393 8.16-1 3.61-2 1.898-2 1.997 1.55-1 -6.36-5 4000 3.949+0	1.304 9.91-1 5.11-2 1.189-2 1.993 3.15-1 -6.47-5 5000 2.496+0	1.225 1.13+0 6.67-2 8.029-3 1.989 4.78-1 -6.47-5	1.153 1.25+0 8.26-2 5.722-3 1.983 6.38-1 -6.39-5 7000 1.216+0	1.088 1.34+0 9.85-2 4.244-3 1.976 7.91-1 -6.21-5	1.42+0 1.14-1 3.247-3 1.970 9.38-1 -6.03-5 9000 6.950-1	1.49+0 1.30-1 2.548-3 1.962 1.08+0 -5.66-5 10000 5.468-1
$E_b = 14.0 \text{ eV}$ $5s_{1/2}$ $E_b = 4.0 \text{ eV}$ Z= 38, Sr: [Kr Shell $3s_{1/2}$ $E_b = 6$	$ \begin{array}{c} \beta \\ \gamma \\ \delta \\ \sigma \\ \beta \\ \gamma \\ \delta \\ r]5s_{1/2}^{2} \end{array} $	1.647 1.56-1 6.54-3 1.261-1 1.995 -7.47-2 -4.60-5 k (eV) 1500 2.458+1 1.992	1.597 3.12-1 1.09-2 7.433-2 1.997 -7.97-2 -5.26-5 2000 1.485+1 1.995	1.491 5.94-1 2.24-2 3.400-2 1.998 9.60-3 -6.05-5 3000 6.972+0 1.997	1.393 8.16-1 3.61-2 1.898-2 1.997 1.55-1 -6.36-5 4000 3.949+0 1.997	1.304 9.91-1 5.11-2 1.189-2 1.993 3.15-1 -6.47-5 5000 2.496+0 1.995	1.225 1.13+0 6.67-2 8.029-3 1.989 4.78-1 -6.47-5 6000 1.697+0 1.991	1.153 1.25+0 8.26-2 5.722-3 1.983 6.38-1 -6.39-5 7000 1.216+0 1.985	1.088 1.34+0 9.85-2 4.244-3 1.976 7.91-1 -6.21-5 8000 9.053-1 1.979	1.42+0 1.14-1 3.247-3 1.970 9.38-1 -6.03-5 9000 6.950-1 1.973	1.49+0 1.30-1 2.548-3 1.962 1.08+0 -5.66-5 10000 5.468-1 1.966
$E_b = 14.0 \text{ eV}$ $5s_{1/2}$ $E_b = 4.0 \text{ eV}$ $Z= 38, \text{ Sr: [Kr]}$ Shell $3s_{1/2}$	$\frac{\beta}{\delta}$ $\frac{\gamma}{\delta}$ $\frac{\sigma}{\beta}$ $\frac{\gamma}{\delta}$ $r]5s_{1/2}^{2}$	1.647 1.56-1 6.54-3 1.261-1 1.995 -7.47-2 -4.60-5 k (eV) 1500 2.458+1	1.597 3.12-1 1.09-2 7.433-2 1.997 -7.97-2 -5.26-5 2000 1.485+1	1.491 5.94-1 2.24-2 3.400-2 1.998 9.60-3 -6.05-5	1.393 8.16-1 3.61-2 1.898-2 1.997 1.55-1 -6.36-5 4000 3.949+0	1.304 9.91-1 5.11-2 1.189-2 1.993 3.15-1 -6.47-5 5000 2.496+0	1.225 1.13+0 6.67-2 8.029-3 1.989 4.78-1 -6.47-5	1.153 1.25+0 8.26-2 5.722-3 1.983 6.38-1 -6.39-5 7000 1.216+0	1.088 1.34+0 9.85-2 4.244-3 1.976 7.91-1 -6.21-5	1.42+0 1.14-1 3.247-3 1.970 9.38-1 -6.03-5 9000 6.950-1	1.49+0 1.30-1 2.548-3 1.962 1.08+0 -5.66-5 10000 5.468-1
$E_b = 14.0 \text{ eV}$ $5s_{1/2}$ $E_b = 4.0 \text{ eV}$ Z= 38, Sr: [Kr Shell $3s_{1/2}$ $E_b = 4.0 \text{ eV}$	$ \begin{array}{c} \beta \\ \gamma \\ \delta \\ \sigma \\ \beta \\ \gamma \\ \delta \\ r]5s_{1/2}^{2} \end{array} $	1.647 1.56-1 6.54-3 1.261-1 1.995 -7.47-2 -4.60-5 k (eV) 1500 2.458+1 1.992	1.597 3.12-1 1.09-2 7.433-2 1.997 -7.97-2 -5.26-5 2000 1.485+1 1.995	1.491 5.94-1 2.24-2 3.400-2 1.998 9.60-3 -6.05-5 3000 6.972+0 1.997	1.393 8.16-1 3.61-2 1.898-2 1.997 1.55-1 -6.36-5 4000 3.949+0 1.997	1.304 9.91-1 5.11-2 1.189-2 1.993 3.15-1 -6.47-5 5000 2.496+0 1.995	1.225 1.13+0 6.67-2 8.029-3 1.989 4.78-1 -6.47-5 6000 1.697+0 1.991	1.153 1.25+0 8.26-2 5.722-3 1.983 6.38-1 -6.39-5 7000 1.216+0 1.985	1.088 1.34+0 9.85-2 4.244-3 1.976 7.91-1 -6.21-5 8000 9.053-1 1.979	1.42+0 1.14-1 3.247-3 1.970 9.38-1 -6.03-5 9000 6.950-1 1.973	1.49+0 1.30-1 2.548-3 1.962 1.08+0 -5.66-5 10000 5.468-1 1.966
$E_b = 14.0 \text{ eV}$ $5s_{1/2}$ $E_b = 4.0 \text{ eV}$ Z= 38, Sr: [Kr Shell $3s_{1/2}$ $E_b = 4.0 \text{ eV}$	$ \frac{\beta}{\delta} $ $ \frac{\gamma}{\delta} $ $ \frac{\sigma}{\beta} $ $ \frac{\gamma}{\delta} $ $ \tau]5s_{1/2}^{2} $ $ \frac{\sigma}{\beta} $ $ \gamma $	1.647 1.56-1 6.54-3 1.261-1 1.995 -7.47-2 -4.60-5 k (eV) 1500 2.458+1 1.992 -3.51-2	1.597 3.12-1 1.09-2 7.433-2 1.997 -7.97-2 -5.26-5 2000 1.485+1 1.995 -8.43-2	1.491 5.94-1 2.24-2 3.400-2 1.998 9.60-3 -6.05-5 3000 6.972+0 1.997 -3.78-2	1.393 8.16-1 3.61-2 1.898-2 1.997 1.55-1 -6.36-5 4000 3.949+0 1.997 8.99-2	1.304 9.91-1 5.11-2 1.189-2 1.993 3.15-1 -6.47-5 5000 2.496+0 1.995 2.44-1	1.225 1.13+0 6.67-2 8.029-3 1.989 4.78-1 -6.47-5 6000 1.697+0 1.991 4.04-1	1.153 1.25+0 8.26-2 5.722-3 1.983 6.38-1 -6.39-5 7000 1.216+0 1.985 5.62-1	1.088 1.34+0 9.85-2 4.244-3 1.976 7.91-1 -6.21-5 8000 9.053-1 1.979 7.16-1	1.42+0 1.14-1 3.247-3 1.970 9.38-1 -6.03-5 9000 6.950-1 1.973 8.63-1	1.49+0 1.30-1 2.548-3 1.962 1.08+0 -5.66-5 10000 5.468-1 1.966 1.00+0

$E_b = 279.8 \text{ eV}$	$eta \ \gamma$	1.611 8.38-2	1.574 2.35-1	1.477 5.20-1	1.384 7.49-1	1.297 9.30-1	1.218 1.08+0	1.147 1.19+0	1.081 1.29+0	1.021 1.38+0	0.965 1.45+0
	δ	4.86-3	9.41-3	2.12-2	3.55-2	5.09-2	6.67-2	8.27-2	9.86-2	1.14-1	1.30-1
$3p_{3/2}$	σ	5.711+1	3.036+1	1.143+1	5.399+0	2.931+0	1.749+0	1.117+0	7.510-1	5.260-1	3.806-
$E_b = 269.1 \text{ eV}$	β	1.636 9.11-2	1.605 2.47-1	1.515 5.42-1	1.424 7.77-1	1.339 9.63-1	1.261 1.11+0	1.189 1.23+0	1.124 1.33+0	1.064 1.42+0	1.008 1.49+0
209.1 EV	$\frac{\gamma}{\delta}$	6.51-3	1.08-2	2.17-2	3.48-2	4.91-2	6.39-2	7.89-2	9.40-2	1.09-1	1.24-1
3d _{3/2}	σ	2.457+1	9.576+0	2.343+0	8.209-1	3.548-1	1.762-1	9.647-2	5.686-2	3.547-2	2.316-2
$E_b =$	β	1.162	1.074	0.908	0.780	0.679	0.599	0.533	0.477	0.428	0.385
135.0 eV	$_{\delta}^{\gamma}$	4.78-1 7.45-2	6.25-1 9.51-2	8.26-1 1.38-1	9.52-1 1.80-1	1.04+0 2.20-1	1.10+0 2.58-1	1.14+0 2.94-1	1.17+0 3.28-1	1.19+0 3.61-1	1.21+0 3.91-1
3d _{5/2}	σ	3.563+1	1.385+1	3.372+0	1.176+0	5.060-1	2.502-1	1.365-1	8.020-2	4.988-2	3.247-
$E_b =$	β	1.146	1.055	0.892	0.770	0.676	0.603	0.543	0.494	0.451	0.413
133.1 eV	γ	4.79-1	6.23-1	8.21-1	9.47-1	1.03+0	1.09+0	1.14+0	1.18+0	1.21+0	1.23+0
Ac.	δ	7.57-2 3.300+0	9.71-2 1.957+0	1.41-1 9.036-1	1.84-1 5.076-1	2.24-1 3.193-1	2.62-1 2.164-1	2.98-1 1.546-1	3.31-1 1.149-1	3.63-1 8.812-2	3.93-1 6.926-
$4s_{1/2} E_b =$	$\frac{\sigma}{\beta}$	1.994	1.937+0	1.998	1.997	1.994	1.990	1.984	1.149-1	1.971	1.964
37.7 eV	γ	-6.83 - 2	-8.34-2	-9.95 - 3	1.24-1	2.79-1	4.38-1	5.94-1	7.45-1	8.90-1	1.03+0
	δ	-5.20-5	-5.99-5	-6.82-5	-7.31-5	-7.44-5	-7.52-5	-7.46-5	-7.33-5	-7.12-5	-6.86-
$4p_{1/2}$	σ	2.965+0	1.593+0	6.113-1	2.932-1	1.611-1	9.709-2	6.255-2	4.239-2	2.990-2	2.177
$E_b = 20.7 \text{ eV}$	β γ	1.631 1.29-1	1.577 2.77-1	1.471 5.49-1	1.376 7.69-1	1.289 9.44-1	1.210 1.09+0	1.140 1.20+0	1.074 1.30+0	1.015 1.38+0	0.960 1.45+0
20.7 CV	δ	4.33-3	8.65-3	2.07-2	3.51-2	5.07-2	6.68-2	8.30-2	9.92-2	1.15-1	1.31-1
$4p_{3/2}$	σ	5.705+0	3.026+0	1.141+0	5.404-1	2.940-1	1.757-1	1.123-1	7.565-2	5.304-2	3.842-
$E_b =$	β	1.656	1.609	1.509	1.416	1.331	1.253	1.182	1.118	1.059	1.004
19.5 eV	δ	1.35-1 5.86-3	2.88-1 9.94-3	5.70-1 2.10-2	7.96-1 3.43-2	9.76-1 4.87-2	1.12+0 6.38-2	1.24+0 7.92-2	1.34+0 9.45-2	1.42+0 1.10-1	1.49+0 1.25-1
5s _{1/2}	σ	2.259-1	1.334-1	6.130-2	3.436-2	2.159-2	1.461-2	1.043-2	7.751-3	5.940-3	4.667-
$E_b =$	β	1.994	1.996	1.998	1.997	1.994	1.989	1.984	1.978	1.971	1.964
5.0 eV	γ	-7.08-2	-8.36-2	-8.58 - 3	1.26 - 1	2.82 - 1	4.42 - 1	5.99 - 1	7.49 - 1	8.93 - 1	1.03+0
	δ	-5.14-5	-5.94-5	-6.81-5	-7.22-5	-7.38-5	-7.45-5	-7.43-5	-7.25-5	-7.18-5	-6.69-
Z= 39, Y : [Ki	r]4d _{3/2} 5	*									
		k (eV)									
		1500	2000	3000	4000	5000	6000	7000	8000	9000	10000
Shell 3s _{1/2}	σ	1500 2.613+1	1.586+1	7.492+0	4.263+0	2.704+0	1.844+0	1.323+0	9.875-1	7.594-1	5.983-
$3s_{1/2}$ $E_b =$	β	1500 2.613+1 1.991	1.586+1 1.994	7.492+0 1.997	4.263+0 1.997	2.704+0 1.995	1.844+0 1.991	1.323+0 1.987	9.875-1 1.981	7.594-1 1.974	5.983- 1.967
$3s_{1/2}$ $E_b =$		1500 2.613+1	1.586+1	7.492+0	4.263+0	2.704+0	1.844+0	1.323+0	9.875-1	7.594-1	5.983- 1.967 9.52-1
3s _{1/2}	$eta \ \gamma$	1500 2.613+1 1.991 -1.84-2	1.586+1 1.994 -8.14-2 -7.27-5 1.745+1	7.492+0 1.997 -5.44-2 -8.30-5 6.783+0	4.263+0 1.997 6.08-2 -8.82-5 3.276+0	2.704+0 1.995 2.07-1	1.844+0 1.991 3.62-1 -9.17-5 1.094+0	1.323+0 1.987 5.17-1 -9.15-5 7.065-1	9.875-1 1.981 6.68-1 -9.06-5 4.799-1	7.594-1 1.974 8.13-1 -8.90-5 3.391-1	5.983— 1.967 9.52—1 —8.67— 2.473—
$3s_{1/2}$ $E_b =$ 393.6 eV $3p_{1/2}$ $E_b =$	β γ δ σ β	1500 2.613+1 1.991 -1.84-2 -6.34-5 3.202+1 1.614	1.586+1 1.994 -8.14-2 -7.27-5 1.745+1 1.583	7.492+0 1.997 -5.44-2 -8.30-5 6.783+0 1.492	4.263+0 1.997 6.08-2 -8.82-5 3.276+0 1.401	2.704+0 1.995 2.07-1 -9.08-5 1.809+0 1.317	1.844+0 1.991 3.62-1 -9.17-5 1.094+0 1.239	1.323+0 1.987 5.17-1 -9.15-5 7.065-1 1.169	9.875-1 1.981 6.68-1 -9.06-5 4.799-1 1.104	7.594-1 1.974 8.13-1 -8.90-5 3.391-1 1.045	5.983- 1.967 9.52-1 -8.67- 2.473- 0.990
$3s_{1/2}$ $E_b =$ 393.6 eV $3p_{1/2}$ $E_b =$	β γ δ σ β γ	1500 2.613+1 1.991 -1.84-2 -6.34-5 3.202+1 1.614 6.07-2	1.586+1 1.994 -8.14-2 -7.27-5 1.745+1 1.583 2.05-1	7.492+0 1.997 -5.44-2 -8.30-5 6.783+0 1.492 4.89-1	4.263+0 1.997 6.08-2 -8.82-5 3.276+0 1.401 7.21-1	2.704+0 1.995 2.07-1 -9.08-5 1.809+0 1.317 9.07-1	1.844+0 1.991 3.62-1 -9.17-5 1.094+0 1.239 1.06+0	1.323+0 1.987 5.17-1 -9.15-5 7.065-1 1.169 1.18+0	9.875-1 1.981 6.68-1 -9.06-5 4.799-1 1.104 1.29+0	7.594-1 1.974 8.13-1 -8.90-5 3.391-1 1.045 1.37+0	5.983— 1.967 9.52—1 —8.67— 2.473— 0.990 1.45+0
$3s_{1/2}$ $E_b =$ 393.6 eV $3p_{1/2}$ $E_b =$ 312.4 eV	β γ δ σ β γ δ	2.613+1 1.991 -1.84-2 -6.34-5 3.202+1 1.614 6.07-2 4.11-3	1.586+1 1.994 -8.14-2 -7.27-5 1.745+1 1.583 2.05-1 8.32-3	7.492+0 1.997 -5.44-2 -8.30-5 6.783+0 1.492 4.89-1 1.93-2	4.263+0 1.997 6.08-2 -8.82-5 3.276+0 1.401 7.21-1 3.26-2	2.704+0 1.995 2.07-1 -9.08-5 1.809+0 1.317 9.07-1 4.73-2	1.844+0 1.991 3.62-1 -9.17-5 1.094+0 1.239 1.06+0 6.25-2	1.323+0 1.987 5.17-1 -9.15-5 7.065-1 1.169 1.18+0 7.79-2	9.875-1 1.981 6.68-1 -9.06-5 4.799-1 1.104 1.29+0 9.33-2	7.594-1 1.974 8.13-1 -8.90-5 3.391-1 1.045 1.37+0 1.09-1	5.983- 1.967 9.52-1 -8.67- 2.473- 0.990 1.45+0 1.24-1
$3s_{1/2}$ $E_b =$ 393.6 eV $3p_{1/2}$ $E_b =$ 312.4 eV	$\begin{array}{c} \beta \\ \gamma \\ \delta \\ \hline \sigma \\ \beta \\ \gamma \\ \delta \\ \hline \sigma \\ \end{array}$	2.613+1 1.991 -1.84-2 -6.34-5 3.202+1 1.614 6.07-2 4.11-3 6.225+1	1.586+1 1.994 -8.14-2 -7.27-5 1.745+1 1.583 2.05-1 8.32-3 3.342+1	7.492+0 1.997 -5.44-2 -8.30-5 6.783+0 1.492 4.89-1 1.93-2 1.274+1	4.263+0 1.997 6.08-2 -8.82-5 3.276+0 1.401 7.21-1 3.26-2 6.070+0	2.704+0 1.995 2.07-1 -9.08-5 1.809+0 1.317 9.07-1 4.73-2 3.316+0	1.844+0 1.991 3.62-1 -9.17-5 1.094+0 1.239 1.06+0 6.25-2 1.987+0	1.323+0 1.987 5.17-1 -9.15-5 7.065-1 1.169 1.18+0 7.79-2 1.274+0	9.875-1 1.981 6.68-1 -9.06-5 4.799-1 1.104 1.29+0 9.33-2 8.593-1	7.594-1 1.974 8.13-1 -8.90-5 3.391-1 1.045 1.37+0 1.09-1 6.035-1	5.983- 1.967 9.52-1 -8.67- 2.473- 0.990 1.45+0 1.24-1 4.378-
$3s_{1/2}$ $E_b = 393.6 \text{ eV}$ $3p_{1/2}$ $E_b = 312.4 \text{ eV}$ $3p_{3/2}$ $E_b = 6$	$\begin{array}{c} \beta \\ \gamma \\ \delta \\ \\ \sigma \\ \beta \\ \\ \gamma \\ \delta \\ \\ \sigma \\ \beta \end{array}$	2.613+1 1.991 -1.84-2 -6.34-5 3.202+1 1.614 6.07-2 4.11-3	1.586+1 1.994 -8.14-2 -7.27-5 1.745+1 1.583 2.05-1 8.32-3 3.342+1 1.614	7.492+0 1.997 -5.44-2 -8.30-5 6.783+0 1.492 4.89-1 1.93-2	4.263+0 1.997 6.08-2 -8.82-5 3.276+0 1.401 7.21-1 3.26-2	2.704+0 1.995 2.07-1 -9.08-5 1.809+0 1.317 9.07-1 4.73-2 3.316+0 1.360	1.844+0 1.991 3.62-1 -9.17-5 1.094+0 1.239 1.06+0 6.25-2	1.323+0 1.987 5.17-1 -9.15-5 7.065-1 1.169 1.18+0 7.79-2 1.274+0 1.213	9.875-1 1.981 6.68-1 -9.06-5 4.799-1 1.104 1.29+0 9.33-2	7.594-1 1.974 8.13-1 -8.90-5 3.391-1 1.045 1.37+0 1.09-1	5.983- 1.967 9.52-1 -8.67- 2.473- 0.990 1.45+0 1.24-1
$3s_{1/2}$ $E_b =$ 393.6 eV $3p_{1/2}$ $E_b =$ 312.4 eV	$\begin{array}{c} \beta \\ \gamma \\ \delta \\ \hline \sigma \\ \beta \\ \gamma \\ \delta \\ \hline \sigma \\ \end{array}$	2.613+1 1.991 -1.84-2 -6.34-5 3.202+1 1.614 6.07-2 4.11-3 6.225+1 1.640 6.73-2 5.87-3	1.586+1 1.994 -8.14-2 -7.27-5 1.745+1 1.583 2.05-1 8.32-3 3.342+1	7.492+0 1.997 -5.44-2 -8.30-5 6.783+0 1.492 4.89-1 1.93-2 1.274+1 1.531	4.263+0 1.997 6.08-2 -8.82-5 3.276+0 1.401 7.21-1 3.26-2 6.070+0 1.443 7.50-1 3.21-2	2.704+0 1.995 2.07-1 -9.08-5 1.809+0 1.317 9.07-1 4.73-2 3.316+0 1.360 9.42-1 4.56-2	1.844+0 1.991 3.62-1 -9.17-5 1.094+0 1.239 1.06+0 6.25-2 1.987+0 1.284 1.10+0 5.97-2	1.323+0 1.987 5.17-1 -9.15-5 7.065-1 1.169 1.18+0 7.79-2 1.274+0 1.213 1.22+0 7.42-2	9.875-1 1.981 6.68-1 -9.06-5 4.799-1 1.104 1.29+0 9.33-2 8.593-1 1.149	7.594-1 1.974 8.13-1 -8.90-5 3.391-1 1.045 1.37+0 1.09-1 6.035-1 1.090	5.983— 1.967 9.52—1 —8.67— 2.473— 0.990 1.45+0 1.24—1 4.378— 1.035 1.49+0 1.18—1
$3s_{1/2}$ $E_b = 393.6 \text{ eV}$ $3p_{1/2}$ $E_b = 312.4 \text{ eV}$ $3p_{3/2}$ $E_b = 300.3 \text{ eV}$	β γ δ σ β γ δ σ β γ δ σ σ σ σ σ σ σ σ σ σ σ σ σ σ σ σ σ σ	1500 2.613+1 1.991 -1.84-2 -6.34-5 3.202+1 1.614 6.07-2 4.11-3 6.225+1 1.640 6.73-2 5.87-3 2.933+1	1.586+1 1.994 -8.14-2 -7.27-5 1.745+1 1.583 2.05-1 8.32-3 3.342+1 1.614 2.17-1 9.97-3 1.155+1	7.492+0 1.997 -5.44-2 -8.30-5 6.783+0 1.492 4.89-1 1.93-2 1.274+1 1.531 5.10-1 1.99-2 2.866+0	4.263+0 1.997 6.08-2 -8.82-5 3.276+0 1.401 7.21-1 3.26-2 6.070+0 1.443 7.50-1 3.21-2 1.012+0	2.704+0 1.995 2.07-1 -9.08-5 1.809+0 1.317 9.07-1 4.73-2 3.316+0 1.360 9.42-1 4.56-2 4.401-1	1.844+0 1.991 3.62-1 -9.17-5 1.094+0 1.239 1.06+0 6.25-2 1.987+0 1.284 1.10+0 5.97-2 2.194-1	1.323+0 1.987 5.17-1 -9.15-5 7.065-1 1.169 1.18+0 7.79-2 1.274+0 1.213 1.22+0 7.42-2 1.206-1	9.875-1 1.981 6.68-1 -9.06-5 4.799-1 1.104 1.29+0 9.33-2 8.593-1 1.149 1.33+0 8.87-2 7.130-2	7.594-1 1.974 8.13-1 -8.90-5 3.391-1 1.045 1.37+0 1.09-1 6.035-1 1.090 1.42+0 1.03-1 4.460-2	5.983— 1.967 9.52—1 -8.67— 2.473— 0.990 1.45+0 1.24—1 4.378— 1.035 1.49+0 1.18—1 2.919—
$3s_{1/2}$ $E_b = 393.6 \text{ eV}$ $3p_{1/2}$ $E_b = 312.4 \text{ eV}$ $3p_{3/2}$ $E_b = 300.3 \text{ eV}$ $3d_{3/2}$ $E_b = 3d_{3/2}$	β γ δ σ β γ δ δ σ β γ δ σ β β γ	2.613+1 1.991 -1.84-2 -6.34-5 3.202+1 1.614 6.07-2 4.11-3 6.225+1 1.640 6.73-2 5.87-3 2.933+1 1.177	1.586+1 1.994 -8.14-2 -7.27-5 1.745+1 1.583 2.05-1 8.32-3 3.342+1 1.614 2.17-1 9.97-3 1.155+1 1.094	7.492+0 1.997 -5.44-2 -8.30-5 6.783+0 1.492 4.89-1 1.93-2 1.274+1 1.531 5.10-1 1.99-2 2.866+0 0.934	4.263+0 1.997 6.08-2 -8.82-5 3.276+0 1.401 7.21-1 3.26-2 6.070+0 1.443 7.50-1 3.21-2 1.012+0 0.805	2.704+0 1.995 2.07-1 -9.08-5 1.809+0 1.317 9.07-1 4.73-2 3.316+0 1.360 9.42-1 4.56-2 4.401-1 0.704	1.844+0 1.991 3.62-1 -9.17-5 1.094+0 1.239 1.06+0 6.25-2 1.987+0 1.284 1.10+0 5.97-2 2.194-1 0.623	1.323+0 1.987 5.17-1 -9.15-5 7.065-1 1.169 1.18+0 7.79-2 1.274+0 1.213 1.22+0 7.42-2 1.206-1 0.556	9.875-1 1.981 6.68-1 -9.06-5 4.799-1 1.104 1.29+0 9.33-2 8.593-1 1.149 1.33+0 8.87-2 7.130-2 0.498	7.594-1 1.974 8.13-1 -8.90-5 3.391-1 1.045 1.37+0 1.09-1 6.035-1 1.090 1.42+0 1.03-1 4.460-2 0.449	5.983- 1.967 9.52-1 -8.67- 2.473- 0.990 1.45+0 1.24-1 4.378- 1.035 1.49+0 1.18-1 2.919- 0.405
$3s_{1/2}$ $E_b = 393.6 \text{ eV}$ $3p_{1/2}$ $E_b = 312.4 \text{ eV}$ $3p_{3/2}$ $E_b = 300.3 \text{ eV}$ $3d_{3/2}$ $E_b = 3d_{3/2}$	β γ δ σ β γ δ σ β γ δ σ β γ δ	2.613+1 1.991 -1.84-2 -6.34-5 3.202+1 1.614 6.07-2 4.11-3 6.225+1 1.640 6.73-2 5.87-3 2.933+1 1.177 4.60-1	1.586+1 1.994 -8.14-2 -7.27-5 1.745+1 1.583 2.05-1 8.32-3 3.342+1 1.614 2.17-1 9.97-3 1.155+1 1.094 6.11-1	7.492+0 1.997 -5.44-2 -8.30-5 6.783+0 1.492 4.89-1 1.93-2 1.274+1 1.531 5.10-1 1.99-2 2.866+0 0.934 8.22-1	4.263+0 1.997 6.08-2 -8.82-5 3.276+0 1.401 7.21-1 3.26-2 6.070+0 1.443 7.50-1 3.21-2 1.012+0 0.805 9.56-1	2.704+0 1.995 2.07-1 -9.08-5 1.809+0 1.317 9.07-1 4.73-2 3.316+0 1.360 9.42-1 4.56-2 4.401-1 0.704 1.05+0	1.844+0 1.991 3.62-1 -9.17-5 1.094+0 1.239 1.06+0 6.25-2 1.987+0 1.284 1.10+0 5.97-2 2.194-1 0.623 1.11+0	1.323+0 1.987 5.17-1 -9.15-5 7.065-1 1.169 1.18+0 7.79-2 1.274+0 1.213 1.22+0 7.42-2 1.206-1 0.556 1.16+0	9.875-1 1.981 6.68-1 -9.06-5 4.799-1 1.104 1.29+0 9.33-2 8.593-1 1.149 1.33+0 8.87-2 7.130-2 0.498 1.19+0	7.594-1 1.974 8.13-1 -8.90-5 3.391-1 1.045 1.37+0 1.09-1 6.035-1 1.090 1.42+0 1.03-1 4.460-2 0.449 1.22+0	5.983— 1.967 9.52—1 -8.67— 2.473— 0.990 1.45+0 1.24—1 4.378— 1.035 1.49+0 1.18—1 2.919— 0.405 1.24+0
$3s_{1/2}$ $E_b = 393.6 \text{ eV}$ $3p_{1/2}$ $E_b = 312.4 \text{ eV}$ $3p_{3/2}$ $E_b = 300.3 \text{ eV}$ $3d_{3/2}$ $E_b = 159.6 \text{ eV}$	β γ δ σ β γ δ σ β γ δ σ β γ δ σ β γ δ σ β γ δ	2.613+1 1.991 -1.84-2 -6.34-5 3.202+1 1.614 6.07-2 4.11-3 6.225+1 1.640 6.73-2 5.87-3 2.933+1 1.177 4.60-1 7.22-2	1.586+1 1.994 -8.14-2 -7.27-5 1.745+1 1.583 2.05-1 8.32-3 3.342+1 1.614 2.17-1 9.97-3 1.155+1 1.094 6.11-1 9.22-2	7.492+0 1.997 -5.44-2 -8.30-5 6.783+0 1.492 4.89-1 1.93-2 1.274+1 1.531 5.10-1 1.99-2 2.866+0 0.934 8.22-1 1.34-1	4.263+0 1.997 6.08-2 -8.82-5 3.276+0 1.401 7.21-1 3.26-2 6.070+0 1.443 7.50-1 3.21-2 1.012+0 0.805 9.56-1 1.75-1	2.704+0 1.995 2.07-1 -9.08-5 1.809+0 1.317 9.07-1 4.73-2 3.316+0 1.360 9.42-1 4.56-2 4.401-1 0.704 1.05+0 2.14-1	1.844+0 1.991 3.62-1 -9.17-5 1.094+0 1.239 1.06+0 6.25-2 1.987+0 1.284 1.10+0 5.97-2 2.194-1 0.623 1.11+0 2.52-1	1.323+0 1.987 5.17-1 -9.15-5 7.065-1 1.169 1.18+0 7.79-2 1.274+0 1.213 1.22+0 7.42-2 1.206-1 0.556 1.16+0 2.88-1	9.875-1 1.981 6.68-1 -9.06-5 4.799-1 1.104 1.29+0 9.33-2 8.593-1 1.149 1.33+0 8.87-2 7.130-2 0.498 1.19+0 3.21-1	7.594-1 1.974 8.13-1 -8.90-5 3.391-1 1.045 1.37+0 1.09-1 6.035-1 1.090 1.42+0 1.03-1 4.460-2 0.449 1.22+0 3.53-1	5.983- 1.967 9.52-1 -8.67- 2.473- 0.990 1.45+0 1.24-1 4.378- 1.035 1.49+0 1.18-1 2.919- 0.405 1.24+0 3.83-1
$3s_{1/2}$ $E_b =$ 393.6 eV $3p_{1/2}$ $E_b =$ 312.4 eV $3p_{3/2}$ $E_b =$ 300.3 eV $3d_{3/2}$ $E_b =$ 159.6 eV	β γ δ σ β γ δ σ β γ δ σ β γ δ	2.613+1 1.991 -1.84-2 -6.34-5 3.202+1 1.614 6.07-2 4.11-3 6.225+1 1.640 6.73-2 5.87-3 2.933+1 1.177 4.60-1	1.586+1 1.994 -8.14-2 -7.27-5 1.745+1 1.583 2.05-1 8.32-3 3.342+1 1.614 2.17-1 9.97-3 1.155+1 1.094 6.11-1	7.492+0 1.997 -5.44-2 -8.30-5 6.783+0 1.492 4.89-1 1.93-2 1.274+1 1.531 5.10-1 1.99-2 2.866+0 0.934 8.22-1	4.263+0 1.997 6.08-2 -8.82-5 3.276+0 1.401 7.21-1 3.26-2 6.070+0 1.443 7.50-1 3.21-2 1.012+0 0.805 9.56-1	2.704+0 1.995 2.07-1 -9.08-5 1.809+0 1.317 9.07-1 4.73-2 3.316+0 1.360 9.42-1 4.56-2 4.401-1 0.704 1.05+0	1.844+0 1.991 3.62-1 -9.17-5 1.094+0 1.239 1.06+0 6.25-2 1.987+0 1.284 1.10+0 5.97-2 2.194-1 0.623 1.11+0	1.323+0 1.987 5.17-1 -9.15-5 7.065-1 1.169 1.18+0 7.79-2 1.274+0 1.213 1.22+0 7.42-2 1.206-1 0.556 1.16+0	9.875-1 1.981 6.68-1 -9.06-5 4.799-1 1.104 1.29+0 9.33-2 8.593-1 1.149 1.33+0 8.87-2 7.130-2 0.498 1.19+0	7.594-1 1.974 8.13-1 -8.90-5 3.391-1 1.045 1.37+0 1.09-1 6.035-1 1.090 1.42+0 1.03-1 4.460-2 0.449 1.22+0	5.983- 1.967 9.52-1 -8.67- 2.473- 0.990 1.45+0 1.24-1 4.378- 1.035 1.49+0 1.18-1 2.919- 0.405 1.24+0 3.83-1
$3s_{1/2}$ $E_b = 393.6 \text{ eV}$ $3p_{1/2}$ $E_b = 312.4 \text{ eV}$ $3p_{3/2}$ $E_b = 300.3 \text{ eV}$ $3d_{3/2}$ $E_b = 159.6 \text{ eV}$ $3d_{5/2}$ $E_b = 6$	β γ δ σ β γ δ δ σ β γ δ σ β γ δ σ β γ γ δ σ β γ γ δ σ β γ γ δ σ β γ γ δ σ β γ γ δ σ β γ γ δ σ β γ γ δ	2.613+1 1.991 -1.84-2 -6.34-5 3.202+1 1.614 6.07-2 4.11-3 6.225+1 1.640 6.73-2 5.87-3 2.933+1 1.177 4.60-1 7.22-2 4.246+1 1.161 4.61-1	1.586+1 1.994 -8.14-2 -7.27-5 1.745+1 1.583 2.05-1 8.32-3 3.342+1 1.614 2.17-1 9.97-3 1.155+1 1.094 6.11-1 9.22-2 1.667+1 1.075 6.09-1	7.492+0 1.997 -5.44-2 -8.30-5 6.783+0 1.492 4.89-1 1.93-2 1.274+1 1.531 5.10-1 1.99-2 2.866+0 0.934 8.22-1 1.34-1 4.115+0 0.917 8.16-1	4.263+0 1.997 6.08-2 -8.82-5 3.276+0 1.401 7.21-1 3.26-2 6.070+0 1.443 7.50-1 3.21-2 1.012+0 0.805 9.56-1 1.75-1 1.446+0 0.793 9.50-1	2.704+0 1.995 2.07-1 -9.08-5 1.809+0 1.317 9.07-1 4.73-2 3.316+0 1.360 9.42-1 4.56-2 4.401-1 0.704 1.05+0 2.14-1 6.261-1 0.699 1.04+0	1.844+0 1.991 3.62-1 -9.17-5 1.094+0 1.239 1.06+0 6.25-2 1.987+0 1.284 1.10+0 5.97-2 2.194-1 0.623 1.11+0 2.52-1 3.109-1 0.624 1.11+0	1.323+0 1.987 5.17-1 -9.15-5 7.065-1 1.169 1.18+0 7.79-2 1.274+0 1.213 1.22+0 7.42-2 1.206-1 0.556 1.16+0 2.88-1 1.703-1 0.563 1.16+0	9.875-1 1.981 6.68-1 -9.06-5 4.799-1 1.104 1.29+0 9.33-2 8.593-1 1.149 1.33+0 8.87-2 7.130-2 0.498 1.19+0 3.21-1 1.003-1 0.512 1.20+0	7.594-1 1.974 8.13-1 -8.90-5 3.391-1 1.045 1.37+0 1.09-1 6.035-1 1.090 1.42+0 1.03-1 4.460-2 0.449 1.22+0 3.53-1 6.255-2 0.469 1.23+0	5.983- 1.967 9.52-1 -8.67- 2.473- 0.990 1.45+0 1.24-1 4.378- 1.035 1.49+0 1.18-1 2.919- 0.405 1.24+0 3.83-1 4.081- 0.430 1.25+0
$3s_{1/2}$ $E_b = 393.6 \text{ eV}$ $3p_{1/2}$ $E_b = 312.4 \text{ eV}$ $3p_{3/2}$ $E_b = 300.3 \text{ eV}$ $3d_{3/2}$ $E_b = 159.6 \text{ eV}$ $3d_{5/2}$ $E_b = 157.4 \text{ eV}$	β γ δ σ β γ δ δ σ β γ δ σ β γ δ σ β γ δ σ β γ δ σ β γ δ σ β γ δ σ β γ δ σ β γ δ σ β γ δ	2.613+1 1.991 -1.84-2 -6.34-5 3.202+1 1.614 6.07-2 4.11-3 6.225+1 1.640 6.73-2 5.87-3 2.933+1 1.177 4.60-1 7.22-2 4.246+1 1.161 4.61-1 7.34-2	1.586+1 1.994 -8.14-2 -7.27-5 1.745+1 1.583 2.05-1 8.32-3 3.342+1 1.614 2.17-1 9.97-3 1.155+1 1.094 6.11-1 9.22-2 1.667+1 1.075 6.09-1 9.42-2	7.492+0 1.997 -5.44-2 -8.30-5 6.783+0 1.492 4.89-1 1.93-2 1.274+1 1.531 5.10-1 1.99-2 2.866+0 0.934 8.22-1 1.34-1 4.115+0 0.917 8.16-1 1.37-1	4.263+0 1.997 6.08-2 -8.82-5 3.276+0 1.401 7.21-1 3.26-2 6.070+0 1.443 7.50-1 3.21-2 1.012+0 0.805 9.56-1 1.75-1 1.446+0 0.793 9.50-1 1.79-1	2.704+0 1.995 2.07-1 -9.08-5 1.809+0 1.317 9.07-1 4.73-2 3.316+0 1.360 9.42-1 4.56-2 4.401-1 0.704 1.05+0 2.14-1 6.261-1 0.699 1.04+0 2.19-1	1.844+0 1.991 3.62-1 -9.17-5 1.094+0 1.239 1.06+0 6.25-2 1.987+0 1.284 1.10+0 5.97-2 2.194-1 0.623 1.11+0 2.52-1 3.109-1 0.624 1.11+0 2.56-1	1.323+0 1.987 5.17-1 -9.15-5 7.065-1 1.169 1.18+0 7.79-2 1.274+0 1.213 1.22+0 7.42-2 1.206-1 0.556 1.16+0 2.88-1 1.703-1 0.563 1.16+0 2.92-1	9.875-1 1.981 6.68-1 -9.06-5 4.799-1 1.104 1.29+0 9.33-2 8.593-1 1.149 1.33+0 8.87-2 7.130-2 0.498 1.19+0 3.21-1 1.003-1 0.512 1.20+0 3.25-1	7.594-1 1.974 8.13-1 -8.90-5 3.391-1 1.045 1.37+0 1.09-1 6.035-1 1.090 1.42+0 1.03-1 4.460-2 0.449 1.22+0 3.53-1 6.255-2 0.469 1.23+0 3.56-1	5.983- 1.967 9.52-1 -8.67- 2.473- 0.990 1.45+0 1.24-1 4.378- 1.035 1.49+0 1.18-1 2.919- 0.405 1.24+0 3.83-1 4.081- 0.430 1.25+0 3.86-1
$3s_{1/2}$ $E_b = 393.6 \text{ eV}$ $3p_{1/2}$ $E_b = 312.4 \text{ eV}$ $3p_{3/2}$ $E_b = 300.3 \text{ eV}$ $3d_{3/2}$ $E_b = 159.6 \text{ eV}$ $3d_{5/2}$ $E_b = 157.4 \text{ eV}$	β γ δ σ β γ δ δ σ β γ δ σ β γ δ σ β γ δ σ β γ δ σ σ β γ δ σ σ σ σ σ σ σ σ σ σ σ σ σ σ σ σ σ σ	2.613+1 1.991 -1.84-2 -6.34-5 3.202+1 1.614 6.07-2 4.11-3 6.225+1 1.640 6.73-2 5.87-3 2.933+1 1.177 4.60-1 7.22-2 4.246+1 1.161 4.61-1 7.34-2 3.783+0	1.586+1 1.994 -8.14-2 -7.27-5 1.745+1 1.583 2.05-1 8.32-3 3.342+1 1.614 2.17-1 9.97-3 1.155+1 1.094 6.11-1 9.22-2 1.667+1 1.075 6.09-1 9.42-2 2.247+0	7.492+0 1.997 -5.44-2 -8.30-5 6.783+0 1.492 4.89-1 1.93-2 1.274+1 1.531 5.10-1 1.99-2 2.866+0 0.934 8.22-1 1.34-1 4.115+0 0.917 8.16-1 1.37-1 1.042+0	4.263+0 1.997 6.08-2 -8.82-5 3.276+0 1.401 7.21-1 3.26-2 6.070+0 1.443 7.50-1 3.21-2 1.012+0 0.805 9.56-1 1.75-1 1.446+0 0.793 9.50-1 1.79-1 5.878-1	2.704+0 1.995 2.07-1 -9.08-5 1.809+0 1.317 9.07-1 4.73-2 3.316+0 1.360 9.42-1 4.56-2 4.401-1 0.704 1.05+0 2.14-1 6.261-1 0.699 1.04+0 2.19-1 3.709-1	1.844+0 1.991 3.62-1 -9.17-5 1.094+0 1.239 1.06+0 6.25-2 1.987+0 1.284 1.10+0 5.97-2 2.194-1 0.623 1.11+0 2.52-1 3.109-1 0.624 1.11+0 2.56-1 2.520-1	1.323+0 1.987 5.17-1 -9.15-5 7.065-1 1.169 1.18+0 7.79-2 1.274+0 1.213 1.22+0 7.42-2 1.206-1 0.556 1.16+0 2.88-1 1.703-1 0.563 1.16+0 2.92-1 1.804-1	9.875-1 1.981 6.68-1 -9.06-5 4.799-1 1.104 1.29+0 9.33-2 8.593-1 1.149 1.33+0 8.87-2 7.130-2 0.498 1.19+0 3.21-1 1.003-1 0.512 1.20+0 3.25-1 1.344-1	7.594-1 1.974 8.13-1 -8.90-5 3.391-1 1.045 1.37+0 1.09-1 6.035-1 1.090 1.42+0 1.03-1 4.460-2 0.449 1.22+0 3.53-1 6.255-2 0.469 1.23+0 3.56-1 1.032-1	5.983— 1.967 9.52—1 -8.67— 2.473— 0.990 1.45+0 1.24—1 4.378— 1.035 1.49+0 1.18—1 2.919— 0.405 1.24+0 3.83—1 4.081— 0.430 1.25+0 3.86—1 8.121—
$3s_{1/2}$ $E_b = 393.6 \text{ eV}$ $3p_{1/2}$ $E_b = 312.4 \text{ eV}$ $3p_{3/2}$ $E_b = 300.3 \text{ eV}$ $3d_{3/2}$ $E_b = 159.6 \text{ eV}$ $3d_{5/2}$ $E_b = 157.4 \text{ eV}$	β γ δ σ β γ δ δ σ β γ δ σ β γ δ σ β γ δ σ β γ δ σ β γ δ σ β γ δ σ β γ δ σ β γ δ σ β γ δ	2.613+1 1.991 -1.84-2 -6.34-5 3.202+1 1.614 6.07-2 4.11-3 6.225+1 1.640 6.73-2 5.87-3 2.933+1 1.177 4.60-1 7.22-2 4.246+1 1.161 4.61-1 7.34-2	1.586+1 1.994 -8.14-2 -7.27-5 1.745+1 1.583 2.05-1 8.32-3 3.342+1 1.614 2.17-1 9.97-3 1.155+1 1.094 6.11-1 9.22-2 1.667+1 1.075 6.09-1 9.42-2	7.492+0 1.997 -5.44-2 -8.30-5 6.783+0 1.492 4.89-1 1.93-2 1.274+1 1.531 5.10-1 1.99-2 2.866+0 0.934 8.22-1 1.34-1 4.115+0 0.917 8.16-1 1.37-1	4.263+0 1.997 6.08-2 -8.82-5 3.276+0 1.401 7.21-1 3.26-2 6.070+0 1.443 7.50-1 3.21-2 1.012+0 0.805 9.56-1 1.75-1 1.446+0 0.793 9.50-1 1.79-1	2.704+0 1.995 2.07-1 -9.08-5 1.809+0 1.317 9.07-1 4.73-2 3.316+0 1.360 9.42-1 4.56-2 4.401-1 0.704 1.05+0 2.14-1 6.261-1 0.699 1.04+0 2.19-1	1.844+0 1.991 3.62-1 -9.17-5 1.094+0 1.239 1.06+0 6.25-2 1.987+0 1.284 1.10+0 5.97-2 2.194-1 0.623 1.11+0 2.52-1 3.109-1 0.624 1.11+0 2.56-1	1.323+0 1.987 5.17-1 -9.15-5 7.065-1 1.169 1.18+0 7.79-2 1.274+0 1.213 1.22+0 7.42-2 1.206-1 0.556 1.16+0 2.88-1 1.703-1 0.563 1.16+0 2.92-1	9.875-1 1.981 6.68-1 -9.06-5 4.799-1 1.104 1.29+0 9.33-2 8.593-1 1.149 1.33+0 8.87-2 7.130-2 0.498 1.19+0 3.21-1 1.003-1 0.512 1.20+0 3.25-1	7.594-1 1.974 8.13-1 -8.90-5 3.391-1 1.045 1.37+0 1.09-1 6.035-1 1.090 1.42+0 1.03-1 4.460-2 0.449 1.22+0 3.53-1 6.255-2 0.469 1.23+0 3.56-1	5.983— 1.967 9.52—1 -8.67— 2.473— 0.990 1.45+0 1.24—1 4.378— 1.035 1.49+0 1.18—1 2.919— 0.405 1.24+0 3.83—1 4.081— 0.430 1.25+0 3.86—1 8.121— 1.966
$3s_{1/2}$ $E_b =$ 393.6 eV $3p_{1/2}$ $E_b =$ 312.4 eV $3p_{3/2}$ $E_b =$ 300.3 eV $3d_{3/2}$ $E_b =$ 159.6 eV $3d_{5/2}$ $E_b =$ 157.4 eV $4s_{1/2}$ $E_b =$	β γ δ σ β γ δ σ β γ δ σ β γ δ σ β γ δ σ β γ δ σ β γ δ σ β γ δ σ β γ δ σ β γ δ σ β γ δ	2.613+1 1.991 -1.84-2 -6.34-5 3.202+1 1.614 6.07-2 4.11-3 6.225+1 1.640 6.73-2 5.87-3 2.933+1 1.177 4.60-1 7.22-2 4.246+1 1.161 4.61-1 7.34-2 3.783+0 1.994	1.586+1 1.994 -8.14-2 -7.27-5 1.745+1 1.583 2.05-1 8.32-3 3.342+1 1.614 2.17-1 9.97-3 1.155+1 1.094 6.11-1 9.22-2 1.667+1 1.075 6.09-1 9.42-2 2.247+0 1.995	7.492+0 1.997 -5.44-2 -8.30-5 6.783+0 1.492 4.89-1 1.93-2 1.274+1 1.531 5.10-1 1.99-2 2.866+0 0.934 8.22-1 1.34-1 4.115+0 0.917 8.16-1 1.37-1 1.042+0 1.997	4.263+0 1.997 6.08-2 -8.82-5 3.276+0 1.401 7.21-1 3.26-2 6.070+0 1.443 7.50-1 3.21-2 1.012+0 0.805 9.56-1 1.75-1 1.446+0 0.793 9.50-1 1.79-1 5.878-1 1.997	2.704+0 1.995 2.07-1 -9.08-5 1.809+0 1.317 9.07-1 4.73-2 3.316+0 1.360 9.42-1 4.56-2 4.401-1 0.704 1.05+0 2.14-1 6.261-1 0.699 1.04+0 2.19-1 3.709-1 1.994	1.844+0 1.991 3.62-1 -9.17-5 1.094+0 1.239 1.06+0 6.25-2 1.987+0 1.284 1.10+0 5.97-2 2.194-1 0.623 1.11+0 2.52-1 3.109-1 0.624 1.11+0 2.56-1 2.520-1 1.990	1.323+0 1.987 5.17-1 -9.15-5 7.065-1 1.169 1.18+0 7.79-2 1.274+0 1.213 1.22+0 7.42-2 1.206-1 0.556 1.16+0 2.88-1 1.703-1 0.563 1.16+0 2.92-1 1.804-1 1.985 5.53-1 -8.62-5	9.875-1 1.981 6.68-1 -9.06-5 4.799-1 1.104 1.29+0 9.33-2 8.593-1 1.149 1.33+0 8.87-2 7.130-2 0.498 1.19+0 3.21-1 1.003-1 0.512 1.20+0 3.25-1 1.344-1 1.980	7.594-1 1.974 8.13-1 -8.90-5 3.391-1 1.045 1.37+0 1.09-1 6.035-1 1.090 1.42+0 1.03-1 4.460-2 0.449 1.22+0 3.53-1 6.255-2 0.469 1.23+0 3.56-1 1.032-1 1.973	5.983- 1.967 9.52-1 -8.67- 2.473- 0.990 1.45+0 1.24-1 4.378- 1.035 1.49+0 1.18-1 2.919- 0.405 1.24+0 3.83-1 4.081- 0.435 1.25+0 9.83-1 -8.08-
$3s_{1/2}$ $E_b = 393.6 \text{ eV}$ $3p_{1/2}$ $E_b = 312.4 \text{ eV}$ $3p_{3/2}$ $E_b = 300.3 \text{ eV}$ $3d_{3/2}$ $E_b = 159.6 \text{ eV}$ $3d_{5/2}$ $E_b = 45.4 \text{ eV}$ $4p_{1/2}$	β γ δ σ β γ δ δ σ β γ δ σ β γ δ σ β γ δ σ β γ δ σ β γ δ σ σ β γ δ σ σ β γ δ σ σ β γ δ σ σ σ σ σ σ σ σ σ σ σ σ σ σ σ σ σ σ	2.613+1 1.991 -1.84-2 -6.34-5 3.202+1 1.614 6.07-2 4.11-3 6.225+1 1.640 6.73-2 5.87-3 2.933+1 1.177 4.60-1 7.22-2 4.246+1 1.161 4.61-1 7.34-2 3.783+0 1.994 -6.29-2 -5.86-5 3.508+0	1.586+1 1.994 -8.14-2 -7.27-5 1.745+1 1.583 2.05-1 8.32-3 3.342+1 1.614 2.17-1 9.97-3 1.155+1 1.094 6.11-1 9.22-2 1.667+1 1.075 6.09-1 9.42-2 2.247+0 1.995 -8.58-2 -6.76-5 1.901+0	7.492+0 1.997 -5.44-2 -8.30-5 6.783+0 1.492 4.89-1 1.93-2 1.274+1 1.531 5.10-1 1.99-2 2.866+0 0.934 8.22-1 1.34-1 4.115+0 0.917 8.16-1 1.37-1 1.042+0 1.997 -2.70-2 -7.77-5 7.397-1	4.263+0 1.997 6.08-2 -8.82-5 3.276+0 1.401 7.21-1 3.26-2 6.070+0 1.443 7.50-1 3.21-2 1.012+0 0.805 9.56-1 1.75-1 1.446+0 0.793 9.50-1 1.79-1 5.878-1 1.997 9.71-2 -8.36-5 3.582-1	2.704+0 1.995 2.07-1 -9.08-5 1.809+0 1.317 9.07-1 4.73-2 3.316+0 1.360 9.42-1 4.56-2 4.401-1 0.704 1.05+0 2.14-1 6.261-1 0.699 1.04+0 2.19-1 3.709-1 1.994 2.45-1 -8.56-5 1.982-1	1.844+0 1.991 3.62-1 -9.17-5 1.094+0 1.239 1.06+0 6.25-2 1.987+0 1.284 1.10+0 5.97-2 2.194-1 0.623 1.11+0 2.52-1 3.109-1 0.624 1.11+0 2.56-1 2.520-1 1.990 4.00-1 -8.66-5 1.201-1	1.323+0 1.987 5.17-1 -9.15-5 7.065-1 1.169 1.18+0 7.79-2 1.274+0 1.213 1.22+0 7.42-2 1.206-1 0.556 1.16+0 2.88-1 1.703-1 0.563 1.16+0 2.92-1 1.804-1 1.985 5.53-1 -8.62-5 7.767-2	9.875-1 1.981 6.68-1 -9.06-5 4.799-1 1.104 1.29+0 9.33-2 8.593-1 1.149 1.33+0 8.87-2 7.130-2 0.498 1.19+0 3.21-1 1.003-1 0.512 1.20+0 3.25-1 1.344-1 1.980 7.02-1 -8.52-5 5.283-2	7.594-1 1.974 8.13-1 -8.90-5 3.391-1 1.045 1.37+0 1.09-1 6.035-1 1.090 1.42+0 1.03-1 4.460-2 0.449 1.22+0 3.53-1 6.255-2 0.469 1.23+0 3.56-1 1.032-1 1.973 8.46-1 -8.31-5 3.737-2	5.983— 1.967 9.52—1 -8.67— 2.473— 0.990 1.45+0 1.24—1 4.378— 1.035 1.49+0 1.18—1 2.919— 0.405 1.24+0 3.83—1 4.081— 0.430 1.25+0 3.86—1 8.121— 1.966 9.83—1 -8.08—
$3s_{1/2}$ $E_b = 393.6 \text{ eV}$ $3p_{1/2}$ $E_b = 312.4 \text{ eV}$ $3p_{3/2}$ $E_b = 300.3 \text{ eV}$ $3d_{3/2}$ $E_b = 159.6 \text{ eV}$ $4s_{1/2}$ $E_b = 45.4 \text{ eV}$	β γ δ σ β γ δ δ σ β γ δ σ β σ β γ δ σ β γ δ σ β γ δ σ β γ δ σ β γ δ σ β γ δ σ β γ δ σ β γ δ σ β γ δ σ β γ δ σ β γ δ σ β γ δ σ β γ δ σ β γ δ σ β σ β σ β σ β σ β σ β σ β σ β σ β σ	1500 2.613+1 1.991 -1.84-2 -6.34-5 3.202+1 1.614 6.07-2 4.11-3 6.225+1 1.640 6.73-2 5.87-3 2.933+1 1.177 4.60-1 7.22-2 4.246+1 1.161 4.61-1 7.34-2 3.783+0 1.994 -6.29-2 -5.86-5 3.508+0 1.639	1.586+1 1.994 -8.14-2 -7.27-5 1.745+1 1.583 2.05-1 8.32-3 3.342+1 1.614 2.17-1 9.97-3 1.155+1 1.094 6.11-1 9.22-2 1.667+1 1.075 6.09-1 9.42-2 2.247+0 1.995 -8.58-2 -6.76-5 1.901+0 1.588	7.492+0 1.997 -5.44-2 -8.30-5 6.783+0 1.492 4.89-1 1.93-2 1.274+1 1.531 5.10-1 1.99-2 2.866+0 0.934 8.22-1 1.34-1 4.115+0 0.917 8.16-1 1.37-1 1.042+0 1.997 -2.70-2 -7.77-5 7.397-1 1.486	4.263+0 1.997 6.08-2 -8.82-5 3.276+0 1.401 7.21-1 3.26-2 6.070+0 1.443 7.50-1 3.21-2 1.012+0 0.805 9.56-1 1.75-1 1.446+0 0.793 9.50-1 1.79-1 5.878-1 1.997 9.71-2 -8.36-5 3.582-1 1.392	2.704+0 1.995 2.07-1 -9.08-5 1.809+0 1.317 9.07-1 4.73-2 3.316+0 1.360 9.42-1 4.56-2 4.401-1 0.704 1.05+0 2.14-1 6.261-1 0.699 1.04+0 2.19-1 3.709-1 1.994 2.45-1 -8.56-5 1.982-1 1.307	1.844+0 1.991 3.62-1 -9.17-5 1.094+0 1.239 1.06+0 6.25-2 1.987+0 1.284 1.10+0 5.97-2 2.194-1 0.623 1.11+0 2.52-1 3.109-1 0.624 1.11+0 2.56-1 1.990 4.00-1 -8.66-5 1.201-1 1.229	1.323+0 1.987 5.17-1 -9.15-5 7.065-1 1.169 1.18+0 7.79-2 1.274+0 1.213 1.22+0 7.42-2 1.206-1 0.556 1.16+0 2.88-1 1.703-1 0.563 1.16+0 2.92-1 1.804-1 1.985 5.53-1 -8.62-5 7.767-2 1.159	9.875-1 1.981 6.68-1 -9.06-5 4.799-1 1.104 1.29+0 9.33-2 8.593-1 1.149 1.33+0 8.87-2 7.130-2 0.498 1.19+0 3.21-1 1.003-1 0.512 1.20+0 3.25-1 1.344-1 1.980 7.02-1 -8.52-5 5.283-2 1.094	7.594-1 1.974 8.13-1 -8.90-5 3.391-1 1.045 1.37+0 1.09-1 6.035-1 1.090 1.42+0 1.03-1 4.460-2 0.449 1.22+0 3.53-1 6.255-2 0.469 1.23+0 3.56-1 1.032-1 1.973 8.46-1 -8.31-5 3.737-2 1.035	5.983— 1.967 9.52—1 -8.67— 2.473— 0.990 1.45+0 1.24—1 4.378— 1.035 1.49+0 1.18—1 0.405 1.24+0 3.83—1 4.081— 0.430 1.25+0 3.86—1 8.121— 1.966 9.83—1 -8.08—
$3s_{1/2}$ $E_b = 393.6 \text{ eV}$ $3p_{1/2}$ $E_b = 312.4 \text{ eV}$ $3p_{3/2}$ $E_b = 300.3 \text{ eV}$ $3d_{3/2}$ $E_b = 159.6 \text{ eV}$ $3d_{5/2}$ $E_b = 45.4 \text{ eV}$ $4s_{1/2}$	β γ δ σ β γ δ δ σ β γ δ σ β γ δ σ β γ δ σ β γ δ σ β γ δ σ σ β γ δ σ σ β γ δ σ σ β γ δ σ σ σ σ σ σ σ σ σ σ σ σ σ σ σ σ σ σ	2.613+1 1.991 -1.84-2 -6.34-5 3.202+1 1.614 6.07-2 4.11-3 6.225+1 1.640 6.73-2 5.87-3 2.933+1 1.177 4.60-1 7.22-2 4.246+1 1.161 4.61-1 7.34-2 3.783+0 1.994 -6.29-2 -5.86-5 3.508+0	1.586+1 1.994 -8.14-2 -7.27-5 1.745+1 1.583 2.05-1 8.32-3 3.342+1 1.614 2.17-1 9.97-3 1.155+1 1.094 6.11-1 9.22-2 1.667+1 1.075 6.09-1 9.42-2 2.247+0 1.995 -8.58-2 -6.76-5 1.901+0 1.588 2.52-1	7.492+0 1.997 -5.44-2 -8.30-5 6.783+0 1.492 4.89-1 1.93-2 1.274+1 1.531 5.10-1 1.99-2 2.866+0 0.934 8.22-1 1.34-1 4.115+0 0.917 8.16-1 1.37-1 1.042+0 1.997 -2.70-2 -7.77-5 7.397-1 1.486 5.22-1	4.263+0 1.997 6.08-2 -8.82-5 3.276+0 1.401 7.21-1 3.26-2 6.070+0 1.443 7.50-1 3.21-2 1.012+0 0.805 9.56-1 1.75-1 1.446+0 0.793 9.50-1 1.79-1 5.878-1 1.997 9.71-2 -8.36-5 3.582-1 1.392 7.45-1	2.704+0 1.995 2.07-1 -9.08-5 1.809+0 1.317 9.07-1 4.73-2 3.316+0 1.360 9.42-1 4.56-2 4.401-1 0.704 1.05+0 2.14-1 6.261-1 0.699 1.04+0 2.19-1 3.709-1 1.994 2.45-1 -8.56-5 1.982-1 1.307 9.24-1	1.844+0 1.991 3.62-1 -9.17-5 1.094+0 1.239 1.06+0 6.25-2 1.987+0 1.284 1.10+0 5.97-2 2.194-1 0.623 1.11+0 2.52-1 3.109-1 0.624 1.11+0 2.56-1 2.520-1 1.990 4.00-1 -8.66-5 1.201-1 1.229 1.07+0	1.323+0 1.987 5.17-1 -9.15-5 7.065-1 1.169 1.18+0 7.79-2 1.274+0 1.213 1.22+0 7.42-2 1.206-1 0.556 1.16+0 2.88-1 1.703-1 0.563 1.16+0 2.92-1 1.804-1 1.985 5.53-1 -8.62-5 7.767-2 1.159 1.19+0	9.875-1 1.981 6.68-1 -9.06-5 4.799-1 1.104 1.29+0 9.33-2 8.593-1 1.149 1.33+0 8.87-2 7.130-2 0.498 1.19+0 3.21-1 1.003-1 0.512 1.20+0 3.25-1 1.344-1 1.980 7.02-1 -8.52-5 5.283-2 1.094 1.29+0	7.594-1 1.974 8.13-1 -8.90-5 3.391-1 1.045 1.37+0 1.09-1 6.035-1 1.090 1.42+0 1.03-1 4.460-2 0.449 1.22+0 3.53-1 6.255-2 0.469 1.23+0 3.56-1 1.032-1 1.973 8.46-1 -8.31-5 3.737-2 1.035 1.38+0	5.983-1 1.967 9.52-1 -8.67-2 2.473-0.990 1.45+0 1.24-1 4.378-1 1.035 1.49+0 1.18-1 2.919-0.405 1.24+0 3.83-1 4.081-0.430 1.25+0 3.86-1 8.121-1 1.966 9.83-1 -8.08-2 2.729-0.981 1.45+0
$3s_{1/2}$ $E_b = 393.6 \text{ eV}$ $3p_{1/2}$ $E_b = 312.4 \text{ eV}$ $3p_{3/2}$ $E_b = 300.3 \text{ eV}$ $3d_{3/2}$ $E_b = 159.6 \text{ eV}$ $3d_{5/2}$ $E_b = 45.4 \text{ eV}$ $4p_{1/2}$ $E_b = 25.1 \text{ eV}$	β γ δ σ β γ δ δ σ β γ δ σ β σ β γ δ σ β γ δ σ β γ δ σ β γ δ σ β γ δ σ β γ δ σ β γ δ σ β γ δ σ β γ δ σ β γ δ σ β σ β γ δ σ β γ δ σ β γ δ σ β σ β σ β σ β σ β σ β σ β σ β σ β σ	1500 2.613+1 1.991 -1.84-2 -6.34-5 3.202+1 1.614 6.07-2 4.11-3 6.225+1 1.640 6.73-2 5.87-3 2.933+1 1.177 4.60-1 7.22-2 4.246+1 1.161 4.61-1 7.34-2 3.783+0 1.994 -6.29-2 -5.86-5 3.508+0 1.639 1.10-1	1.586+1 1.994 -8.14-2 -7.27-5 1.745+1 1.583 2.05-1 8.32-3 3.342+1 1.614 2.17-1 9.97-3 1.155+1 1.094 6.11-1 9.22-2 1.667+1 1.075 6.09-1 9.42-2 2.247+0 1.995 -8.58-2 -6.76-5 1.901+0 1.588	7.492+0 1.997 -5.44-2 -8.30-5 6.783+0 1.492 4.89-1 1.93-2 1.274+1 1.531 5.10-1 1.99-2 2.866+0 0.934 8.22-1 1.34-1 4.115+0 0.917 8.16-1 1.37-1 1.042+0 1.997 -2.70-2 -7.77-5 7.397-1 1.486	4.263+0 1.997 6.08-2 -8.82-5 3.276+0 1.401 7.21-1 3.26-2 6.070+0 1.443 7.50-1 3.21-2 1.012+0 0.805 9.56-1 1.75-1 1.446+0 0.793 9.50-1 1.79-1 5.878-1 1.997 9.71-2 -8.36-5 3.582-1 1.392	2.704+0 1.995 2.07-1 -9.08-5 1.809+0 1.317 9.07-1 4.73-2 3.316+0 1.360 9.42-1 4.56-2 4.401-1 0.704 1.05+0 2.14-1 6.261-1 0.699 1.04+0 2.19-1 3.709-1 1.994 2.45-1 -8.56-5 1.982-1 1.307	1.844+0 1.991 3.62-1 -9.17-5 1.094+0 1.239 1.06+0 6.25-2 1.987+0 1.284 1.10+0 5.97-2 2.194-1 0.623 1.11+0 2.52-1 3.109-1 0.624 1.11+0 2.56-1 1.990 4.00-1 -8.66-5 1.201-1 1.229 1.07+0 6.27-2	1.323+0 1.987 5.17-1 -9.15-5 7.065-1 1.169 1.18+0 7.79-2 1.274+0 1.213 1.22+0 7.42-2 1.206-1 0.556 1.16+0 2.88-1 1.703-1 0.563 1.16+0 2.92-1 1.804-1 1.985 5.53-1 -8.62-5 7.767-2 1.159	9.875-1 1.981 6.68-1 -9.06-5 4.799-1 1.104 1.29+0 9.33-2 8.593-1 1.149 1.33+0 8.87-2 7.130-2 0.498 1.19+0 3.21-1 1.003-1 0.512 1.20+0 3.25-1 1.344-1 1.980 7.02-1 -8.52-5 5.283-2 1.094	7.594-1 1.974 8.13-1 -8.90-5 3.391-1 1.045 1.37+0 1.09-1 6.035-1 1.090 1.42+0 1.03-1 4.460-2 0.449 1.22+0 3.53-1 6.255-2 0.469 1.23+0 3.56-1 1.032-1 1.973 8.46-1 -8.31-5 3.737-2 1.035	5.983—1.967 9.52—1 -8.67—2.473—0.990 1.45+0 1.24—1 4.378—1.035 1.49+0 1.18—1 2.919—0.405 1.24+0 3.83—1 4.081—0.430 1.25+0 3.86—1 8.121—1.966 9.83—1 -8.08—2.729—0.981 1.45+0 1.25—1
$3s_{1/2}$ $E_b = 393.6 \text{ eV}$ $3p_{1/2}$ $E_b = 312.4 \text{ eV}$ $3p_{3/2}$ $E_b = 300.3 \text{ eV}$ $3d_{3/2}$ $E_b = 159.6 \text{ eV}$ $4s_{1/2}$ $E_b = 45.4 \text{ eV}$ $4p_{1/2}$ $E_b = 25.1 \text{ eV}$	β γ δ σ σ β γ δ σ σ σ β γ δ σ σ σ β γ δ σ σ σ σ σ σ σ σ σ σ σ σ σ σ σ σ σ σ	1500 2.613+1 1.991 -1.84-2 -6.34-5 3.202+1 1.614 6.07-2 4.11-3 6.225+1 1.640 6.73-2 5.87-3 2.933+1 1.177 4.60-1 7.22-2 4.246+1 1.161 4.61-1 7.34-2 3.783+0 1.994 -6.29-2 -5.86-5 3.508+0 1.639 1.10-1 3.64-3 6.828+0 1.665	1.586+1 1.994 -8.14-2 -7.27-5 1.745+1 1.583 2.05-1 8.32-3 3.342+1 1.614 2.17-1 9.97-3 1.155+1 1.094 6.11-1 9.22-2 1.667+1 1.075 6.09-1 9.42-2 2.247+0 1.995 -8.58-2 -6.76-5 1.901+0 1.588 2.52-1 7.59-3 3.651+0 1.621	7.492+0 1.997 -5.44-2 -8.30-5 6.783+0 1.492 4.89-1 1.93-2 1.274+1 1.531 5.10-1 1.99-2 2.866+0 0.934 8.22-1 1.34-1 4.115+0 0.917 8.16-1 1.37-1 1.042+0 1.997 -2.70-2 -7.77-5 7.397-1 1.486 5.22-1 1.86-2 1.395+0 1.525	4.263+0 1.997 6.08-2 -8.82-5 3.276+0 1.401 7.21-1 3.26-2 6.070+0 1.443 7.50-1 3.21-2 1.012+0 0.805 9.56-1 1.75-1 1.446+0 0.793 9.50-1 1.79-1 5.878-1 1.997 9.71-2 -8.36-5 3.582-1 1.392 7.45-1 3.22-2 6.664-1 1.433	2.704+0 1.995 2.07-1 -9.08-5 1.809+0 1.317 9.07-1 4.73-2 3.316+0 1.360 9.42-1 4.56-2 4.401-1 0.704 1.05+0 2.14-1 6.261-1 0.699 1.04+0 2.19-1 3.709-1 1.994 2.45-1 -8.56-5 1.982-1 1.307 9.24-1 4.72-2 3.649-1 1.350	1.844+0 1.991 3.62-1 -9.17-5 1.094+0 1.239 1.06+0 6.25-2 1.987+0 1.284 1.10+0 5.97-2 2.194-1 0.623 1.11+0 2.52-1 3.109-1 0.624 1.11+0 2.56-1 2.520-1 1.990 4.00-1 -8.66-5 1.201-1 1.229 1.07+0 6.27-2 2.191-1 1.274	1.323+0 1.987 5.17-1 -9.15-5 7.065-1 1.169 1.18+0 7.79-2 1.274+0 1.213 1.22+0 7.42-2 1.206-1 0.556 1.16+0 2.88-1 1.703-1 0.563 1.16+0 2.92-1 1.804-1 1.985 5.53-1 -8.62-5 7.767-2 1.159 1.19+0 7.83-2 1.407-1 1.203	9.875-1 1.981 6.68-1 -9.06-5 4.799-1 1.104 1.29+0 9.33-2 8.593-1 1.149 1.33+0 8.87-2 7.130-2 0.498 1.19+0 3.21-1 1.003-1 0.512 1.20+0 3.25-1 1.344-1 1.980 7.02-1 -8.52-5 5.283-2 1.094 1.29+0 9.39-2 9.504-2 1.140	7.594-1 1.974 8.13-1 -8.90-5 3.391-1 1.045 1.37+0 1.09-1 6.035-1 1.090 1.42+0 1.03-1 4.460-2 0.449 1.22+0 3.53-1 6.255-2 0.469 1.23+0 3.56-1 1.032-1 1.973 8.46-1 -8.31-5 3.737-2 1.035 1.38+0 1.09-1 6.683-2 1.080	5.983— 1.967 9.52—1 -8.67— 2.473— 0.990 1.45+0 1.24—1 4.378— 1.035 1.49+0 1.18—1 2.919— 0.405 1.24+0 3.83—1 4.081— 0.430 1.25+0 3.86—1 8.121— 1.966 9.83—1 -8.08= 2.729— 0.981 1.45+0 1.25—1 4.853—1 4.853—1
$3s_{1/2}$ $E_b = 393.6 \text{ eV}$ $3p_{1/2}$ $E_b = 312.4 \text{ eV}$ $3p_{3/2}$ $E_b = 300.3 \text{ eV}$ $3d_{3/2}$ $E_b = 159.6 \text{ eV}$ $4s_{1/2}$ $E_b = 45.4 \text{ eV}$	β γ δ σ σ β γ δ σ σ β γ δ σ σ β γ δ σ σ β γ δ σ σ β γ δ σ σ β γ δ σ σ β γ δ σ σ β γ δ σ σ β γ δ σ σ β γ δ σ σ β γ δ σ σ β γ δ σ σ β γ δ σ σ β γ δ σ σ β γ δ σ σ β γ δ σ σ σ β γ δ σ σ σ β γ δ σ σ σ σ σ σ σ σ σ σ σ σ σ σ σ σ σ σ	2.613+1 1.991 -1.84-2 -6.34-5 3.202+1 1.614 6.07-2 4.11-3 6.225+1 1.640 6.73-2 5.87-3 2.933+1 1.177 4.60-1 7.22-2 4.246+1 1.161 4.61-1 7.34-2 3.783+0 1.994 -6.29-2 -5.86-5 3.508+0 1.639 1.10-1 3.64-3 6.828+0 1.665 1.16-1	1.586+1 1.994 -8.14-2 -7.27-5 1.745+1 1.583 2.05-1 8.32-3 3.342+1 1.614 2.17-1 9.97-3 1.155+1 1.094 6.11-1 9.22-2 1.667+1 1.075 6.09-1 9.42-2 2.247+0 1.995 -8.58-2 -6.76-5 1.901+0 1.588 2.52-1 7.59-3 3.651+0 1.621 2.64-1	7.492+0 1.997 -5.44-2 -8.30-5 6.783+0 1.492 4.89-1 1.93-2 1.274+1 1.531 5.10-1 1.99-2 2.866+0 0.934 8.22-1 1.34-1 4.115+0 0.917 8.16-1 1.37-1 1.042+0 1.997 -2.70-2 -7.77-5 7.397-1 1.486 5.22-1 1.395+0 1.525 5.43-1	4.263+0 1.997 6.08-2 -8.82-5 3.276+0 1.401 7.21-1 3.26-2 6.070+0 1.443 7.50-1 3.21-2 1.012+0 0.805 9.56-1 1.75-1 1.446+0 0.793 9.50-1 1.79-1 5.878-1 1.997 9.71-2 -8.36-5 3.582-1 1.392 7.45-1 3.22-2 6.664-1 1.433 7.73-1	2.704+0 1.995 2.07-1 -9.08-5 1.809+0 1.317 9.07-1 4.73-2 3.316+0 1.360 9.42-1 4.56-2 4.401-1 0.704 1.05+0 2.14-1 6.261-1 0.699 1.04+0 2.19-1 3.709-1 1.994 2.45-1 -8.56-5 1.982-1 1.307 9.24-1 4.72-2 3.649-1 1.350 9.57-1	1.844+0 1.991 3.62-1 -9.17-5 1.094+0 1.239 1.06+0 6.25-2 1.987+0 1.284 1.10+0 5.97-2 2.194-1 0.623 1.11+0 2.52-1 3.109-1 0.624 1.11+0 2.56-1 2.520-1 1.990 4.00-1 -8.66-5 1.201-1 1.229 1.07+0 6.27-2 2.191-1 1.274 1.11+0	1.323+0 1.987 5.17-1 -9.15-5 7.065-1 1.169 1.18+0 7.79-2 1.274+0 1.213 1.22+0 7.42-2 1.206-1 0.556 1.16+0 2.88-1 1.703-1 0.563 1.16+0 2.92-1 1.804-1 1.985 5.53-1 -8.62-5 7.767-2 1.159 1.19+0 7.83-2 1.407-1 1.203 1.23+0	9.875-1 1.981 6.68-1 -9.06-5 4.799-1 1.104 1.29+0 9.33-2 8.593-1 1.149 1.33+0 8.87-2 7.130-2 0.498 1.19+0 3.21-1 1.003-1 0.512 1.20+0 3.25-1 1.344-1 1.980 7.02-1 -8.52-5 5.283-2 1.094 1.29+0 9.39-2 9.504-2 1.140 1.33+0	7.594-1 1.974 8.13-1 -8.90-5 3.391-1 1.045 1.37+0 1.09-1 6.035-1 1.090 1.42+0 1.03-1 4.460-2 0.449 1.22+0 3.53-1 6.255-2 0.469 1.23+0 3.56-1 1.032-1 1.973 8.46-1 -8.31-5 3.737-2 1.035 1.38+0 1.09-1 6.683-2 1.080 1.42+0	5.983— 1.967 9.52—1 -8.67— 2.473— 0.990 1.45+0 1.24—1 4.378— 1.035 1.49+0 1.18—1 2.919— 0.405 1.24+0 3.83—1 4.081— 0.430 1.25+0 3.86—1 8.121— 1.966 9.83—1 -8.08— 2.729— 0.981 1.45+0 1.25—1 4.853— 1.026 1.49+0
$3s_{1/2}$ $E_b = 393.6 \text{ eV}$ $3p_{1/2}$ $E_b = 312.4 \text{ eV}$ $3p_{3/2}$ $E_b = 300.3 \text{ eV}$ $3d_{3/2}$ $E_b = 159.6 \text{ eV}$ $3d_{5/2}$ $E_b = 45.4 \text{ eV}$ $4p_{1/2}$ $E_b = 25.1 \text{ eV}$ $4p_{3/2}$ $E_b = 22.8 \text{ eV}$	β γ δ σ β γ δ σ β γ δ σ β γ δ σ β γ δ σ β γ δ σ β γ δ γ	2.613+1 1.991 -1.84-2 -6.34-5 3.202+1 1.614 6.07-2 4.11-3 6.225+1 1.640 6.73-2 5.87-3 2.933+1 1.177 4.60-1 7.22-2 4.246+1 1.161 4.61-1 7.34-2 3.783+0 1.994 -6.29-2 -5.86-5 3.508+0 1.64-3 6.828+0 1.665 1.16-1 5.30-3	1.586+1 1.994 -8.14-2 -7.27-5 1.745+1 1.583 2.05-1 8.32-3 3.342+1 1.614 2.17-1 9.97-3 1.155+1 1.094 6.11-1 9.22-2 1.667+1 1.075 6.09-1 9.42-2 2.247+0 1.995 -8.58-2 -6.76-5 1.901+0 1.588 2.52-1 7.59-3 3.651+0 1.621 2.64-1 9.07-3	7.492+0 1.997 -5.44-2 -8.30-5 6.783+0 1.492 4.89-1 1.93-2 1.274+1 1.531 5.10-1 1.99-2 2.866+0 0.934 8.22-1 1.34-1 4.115+0 0.917 8.16-1 1.37-1 1.042+0 1.997 -2.70-2 -7.77-5 7.397-1 1.486 5.22-1 1.86-2 1.395+0 1.525 5.43-1 1.91-2	4.263+0 1.997 6.08-2 -8.82-5 3.276+0 1.401 7.21-1 3.26-2 6.070+0 1.443 7.50-1 3.21-2 1.012+0 0.805 9.56-1 1.75-1 1.446+0 0.793 9.50-1 1.79-1 5.878-1 1.997 9.71-2 -8.36-5 3.582-1 1.392 7.45-1 3.22-2 6.664-1 1.433 7.73-1 3.16-2	2.704+0 1.995 2.07-1 -9.08-5 1.809+0 1.317 9.07-1 4.73-2 3.316+0 1.360 9.42-1 4.56-2 4.401-1 0.704 1.05+0 2.14-1 6.261-1 0.699 1.04+0 2.19-1 3.709-1 1.994 2.45-1 -8.56-5 1.982-1 1.307 9.24-1 4.72-2 3.649-1 1.350 9.57-1 4.54-2	1.844+0 1.991 3.62-1 -9.17-5 1.094+0 1.239 1.06+0 6.25-2 1.987+0 1.284 1.10+0 5.97-2 2.194-1 0.623 1.11+0 2.52-1 3.109-1 0.624 1.11+0 2.56-1 2.520-1 1.990 4.00-1 -8.66-5 1.201-1 1.229 1.07+0 6.27-2 2.191-1 1.274 1.11+0 5.98-2	1.323+0 1.987 5.17-1 -9.15-5 7.065-1 1.169 1.18+0 7.79-2 1.274+0 1.213 1.22+0 7.42-2 1.206-1 0.556 1.16+0 2.88-1 1.703-1 0.563 1.16+0 2.92-1 1.804-1 1.985 5.53-1 -8.62-5 7.767-2 1.159 1.19+0 7.83-2 1.407-1 1.203 1.23+0 7.45-2	9.875-1 1.981 6.68-1 -9.06-5 4.799-1 1.104 1.29+0 9.33-2 8.593-1 1.149 1.33+0 8.87-2 7.130-2 0.498 1.19+0 3.21-1 1.003-1 0.512 1.20+0 3.25-1 1.344-1 1.980 7.02-1 -8.52-5 5.283-2 1.094 1.29+0 9.39-2 9.504-2 1.140 1.33+0 8.93-2	7.594-1 1.974 8.13-1 -8.90-5 3.391-1 1.045 1.37+0 1.09-1 6.035-1 1.090 1.42+0 1.03-1 4.460-2 0.449 1.22+0 3.53-1 6.255-2 0.469 1.23+0 3.56-1 1.032-1 1.973 8.46-1 -8.31-5 3.737-2 1.035 1.38+0 1.09-1 6.683-2 1.080 1.42+0 1.04-1	5.983— 1.967 9.52—1 —8.67— 2.473— 0.990 1.45+0 1.24—1 4.378— 1.035 1.49+0 1.18—1 2.919— 0.405 1.24+0 3.83—1 4.081— 0.430 1.25+0 3.86—1 8.121— 1.966 9.83—1 —8.08— 2.729— 0.981 1.45+0 1.25—1 4.853— 1.026 1.49+0 1.18—1
$3s_{1/2}$ $E_b = 393.6 \text{ eV}$ $3p_{1/2}$ $E_b = 312.4 \text{ eV}$ $3p_{3/2}$ $E_b = 300.3 \text{ eV}$ $3d_{3/2}$ $E_b = 159.6 \text{ eV}$ $4s_{1/2}$ $E_b = 45.4 \text{ eV}$ $4p_{1/2}$ $E_b = 25.1 \text{ eV}$	β γ δ σ σ β γ δ σ σ β γ δ σ σ β γ δ σ σ β γ δ σ σ β γ δ σ σ β γ δ σ σ β γ δ σ σ β γ δ σ σ β γ δ σ σ β γ δ σ σ β γ δ σ σ β γ δ σ σ β γ δ σ σ β γ δ σ σ β γ δ σ σ β γ δ σ σ σ β γ δ σ σ σ β γ δ σ σ σ σ σ σ σ σ σ σ σ σ σ σ σ σ σ σ	2.613+1 1.991 -1.84-2 -6.34-5 3.202+1 1.614 6.07-2 4.11-3 6.225+1 1.640 6.73-2 5.87-3 2.933+1 1.177 4.60-1 7.22-2 4.246+1 1.161 4.61-1 7.34-2 3.783+0 1.994 -6.29-2 -5.86-5 3.508+0 1.639 1.10-1 3.64-3 6.828+0 1.665 1.16-1	1.586+1 1.994 -8.14-2 -7.27-5 1.745+1 1.583 2.05-1 8.32-3 3.342+1 1.614 2.17-1 9.97-3 1.155+1 1.094 6.11-1 9.22-2 1.667+1 1.075 6.09-1 9.42-2 2.247+0 1.995 -8.58-2 -6.76-5 1.901+0 1.588 2.52-1 7.59-3 3.651+0 1.621 2.64-1	7.492+0 1.997 -5.44-2 -8.30-5 6.783+0 1.492 4.89-1 1.93-2 1.274+1 1.531 5.10-1 1.99-2 2.866+0 0.934 8.22-1 1.34-1 4.115+0 0.917 8.16-1 1.37-1 1.042+0 1.997 -2.70-2 -7.77-5 7.397-1 1.486 5.22-1 1.395+0 1.525 5.43-1	4.263+0 1.997 6.08-2 -8.82-5 3.276+0 1.401 7.21-1 3.26-2 6.070+0 1.443 7.50-1 3.21-2 1.012+0 0.805 9.56-1 1.75-1 1.446+0 0.793 9.50-1 1.79-1 5.878-1 1.997 9.71-2 -8.36-5 3.582-1 1.392 7.45-1 3.22-2 6.664-1 1.433 7.73-1	2.704+0 1.995 2.07-1 -9.08-5 1.809+0 1.317 9.07-1 4.73-2 3.316+0 1.360 9.42-1 4.56-2 4.401-1 0.704 1.05+0 2.14-1 6.261-1 0.699 1.04+0 2.19-1 3.709-1 1.994 2.45-1 -8.56-5 1.982-1 1.307 9.24-1 4.72-2 3.649-1 1.350 9.57-1	1.844+0 1.991 3.62-1 -9.17-5 1.094+0 1.239 1.06+0 6.25-2 1.987+0 1.284 1.10+0 5.97-2 2.194-1 0.623 1.11+0 2.52-1 3.109-1 0.624 1.11+0 2.56-1 2.520-1 1.990 4.00-1 -8.66-5 1.201-1 1.229 1.07+0 6.27-2 2.191-1 1.274 1.11+0	1.323+0 1.987 5.17-1 -9.15-5 7.065-1 1.169 1.18+0 7.79-2 1.274+0 1.213 1.22+0 7.42-2 1.206-1 0.556 1.16+0 2.88-1 1.703-1 0.563 1.16+0 2.92-1 1.804-1 1.985 5.53-1 -8.62-5 7.767-2 1.159 1.19+0 7.83-2 1.407-1 1.203 1.23+0	9.875-1 1.981 6.68-1 -9.06-5 4.799-1 1.104 1.29+0 9.33-2 8.593-1 1.149 1.33+0 8.87-2 7.130-2 0.498 1.19+0 3.21-1 1.003-1 0.512 1.20+0 3.25-1 1.344-1 1.980 7.02-1 -8.52-5 5.283-2 1.094 1.29+0 9.39-2 9.504-2 1.140 1.33+0	7.594-1 1.974 8.13-1 -8.90-5 3.391-1 1.045 1.37+0 1.09-1 6.035-1 1.090 1.42+0 1.03-1 4.460-2 0.449 1.22+0 3.53-1 6.255-2 0.469 1.23+0 3.56-1 1.032-1 1.973 8.46-1 -8.31-5 3.737-2 1.035 1.38+0 1.09-1 6.683-2 1.080 1.42+0	5.983— 1.967 9.52—1 -8.67— 2.473— 0.990 1.45+0 1.24—1 4.378— 1.035 1.49+0 1.18—1 2.919— 0.405 1.24+0 3.83—1 4.081— 0.430 1.25+0 3.86—1 8.121— 1.966 9.83—1 -8.08— 2.729— 0.981 1.45+0 1.25—1 4.853— 1.026 1.49+0

Table 1 (contin	ued)										
abic 1 (contin	δ	6.84-2	8.96-2	1.33-1	1.75-1	2.15-1	2.52-1	2.88-1	3.21-1	3.53-1	3.83-1
5s _{1/2}	σ	2.784-1	1.645-1	7.590-2	4.270-2	2.690-2	1.825-2	1.306-2	9.719-3	7.460-3	5.869-3
$E_b = 6.0 \text{ eV}$	β	1.994 -6.55-2	1.995 -8.64-2	1.997 -2.53-2	1.997 9.98-2	1.994 2.48-1	1.990 4.02-1	1.985 5.55-1	1.979 7.03-1	1.973 8.45-1	1.966 9.81-1
0.0 6	$_{\delta}^{\gamma}$	-5.78-5	-6.69-5	-2.33-2 -7.75-5	-8.27-5	-8.50-5	-8.62-5	-8.65-5	-8.50-5	-8.41-5	-7.98-5
Z= 40, Zr: [K	r]4d _{3/2} !	5s _{1/2}									
		k (eV)									
Shell		1500	2000	3000	4000	5000	6000	7000	8000	9000	10000
3s _{1/2}	σ	2.770+1	1.689+1	8.025+0	4.586+0	2.919+0	1.995+0	1.436+0	1.073+0	8.267-1	6.524-1
$E_b = 430.3 \text{ eV}$	β γ	1.990 7.92-4	1.993 -7.61-2	1.996 -6.85-2	1.997 3.38-2	1.995 1.71-1	1.992 3.21-1	1.988 4.72-1	1.982 6.20-1	1.976 7.63-1	1.969 9.01-1
450.5 CV	δ	-7.13-5	-8.21-5	-9.45 - 5	-1.00-4	-1.04-4	-1.05-4	-1.06-4	-1.05-4	-1.03-4	-1.01-4
$3p_{1/2}$	σ	3.462+1	1.907+1	7.518+0	3.665+0	2.037+0	1.238+0	8.029-1	5.472-1	3.878-1	2.836-1
$E_b = 344.2 \text{ eV}$	β	1.616 4.02-2	1.590 1.77-1	1.506 4.58-1	1.418 6.93-1	1.336 8.83-1	1.261 1.04+0	1.191 1.17+0	1.128 1.27+0	1.069 1.37+0	1.015 1.45+0
J44.2 CV	δ	3.44-3	7.32 - 3	1.76-2	3.02-2	4.42-2	5.87-2	7.36-2	8.86-2	1.04-1	1.18-1
3p _{3/2}	σ	6.746+1	3.656+1	1.412+1	6.784+0	3.728+0	2.245+0	1.444+0	9.775-1	6.883-1	5.005-1
$E_b = 330.5 \text{ eV}$	β	1.642 4.60-2	1.622 1.89-1	1.546 4.80-1	1.462 7.23-1	1.381 9.19-1	1.307 1.08+0	1.238 1.21+0	1.175 1.32+0	1.117 1.41+0	1.063 1.49+0
550,5 CV	$\delta \gamma$	5.32-3	9.19-3	1.86-2	2.99-2	4.27-2	5.61-2	6.99-2	8.40-2	9.81-2	1.12-1
3d _{3/2}	σ	3,458+1	1.377+1	3.465+0	1.235+0	5.400-1	2.705-1	1.492-1	8.847-2	5.549-2	3.641-2
$E_b = 182.4 \text{ eV}$	β	1.190 4.40-1	1.112 5.96-1	0.957 8.16-1	0.830 9.58-1	0.728 1.05+0	0.646 1.12+0	0.578 1.17+0	0.519 1.21+0	0.468 1.24+0	0.423 1.26+0
102.4 EV	$\delta \gamma$	6.99-2	8.92-2	1.29-1	9.58 – 1 1.70 – 1	2.08-1	2.45-1	2.81-1	3.14–1	3.45-1	3.75-1
3d _{5/2}	σ	4.996+1	1.983+1	4.961+0	1.759+0	7.660-1	3.821-1	2.100-1	1.241-1	7.758-2	5.074-2
$E_b = 180.0 \text{ eV}$	β	1.174 4.42-1	1.092 5.95-1	0.938 8.10-1	0.816 9.51-1	0.720 1.05+0	0.644 1.12+0	0.583 1.17+0	0.530 1.21+0	0.486 1.25+0	0.446 1.27+0
160.0 EV	$\gamma \\ \delta$	7.09-2	9.12-2	1.33-1	1.74-1	2.13-1	2.50-1	2.85-1	3.18-1	3.49-1	3.79-1
4s _{1/2}	σ	4.261+0	2.535+0	1.180+0	6.682-1	4.229-1	2.880-1	2.067-1	1.542-1	1.186-1	9.347-2
$E_b = 51.3 \text{ eV}$	β	1.993	1.995	1.997 -4.20-2	1.997	1.995 2.12-1	1.991	1.986	1.981 6.58-1	1.975 8.00-1	1.968 9.36-1
31.3 eV	$\gamma \\ \delta$	-5.68-2 $-6.62-5$	-8.70-2 $-7.67-5$	-4.20-2 $-8.80-5$	7.14-2 $-9.49-5$	-9.79-5	3.61-1 -9.94-5	5.11-1 -9.93-5	-9.88-5	-9.68-5	-9.49-5
4p _{1/2}	σ	4.054+0	2.215+0	8.732-1	4.268-1	2.377-1	1.448-1	9.405-2	6.419-2	4.555-2	3.335-2
$E_b = 29.3 \text{ eV}$	β	1.646 9.19-2	1.599 2.29-1	1.500 4.96-1	1.409 7.20-1	1.325 9.03-1	1.249 1.05+0	1.179 1.18+0	1.116 1.28+0	1.057 1.37+0	1.003 1.45+0
23.3 CV	δ	3.03-3	6.65 - 3	1.69-2	2.97-2	4.39-2	5.87-2	7.37-2	8.89-2	1.04-1	1.19-1
4p _{3/2}	σ	7.955+0	4.286+0	1.657+0	7.986-1	4.400-1	2.655-1	1.711-1	1.160-1	8.179-2	5.955-2
$E_b = 25.7 \text{ eV}$	β γ	1.672 9.84-2	1.632 2.41-1	1.540 5.17-1	1.452 7.49-1	1.370 9.37-1	1.295 1.09+0	1.226 1.22+0	1.163 1.33+0	1.104 1.42+0	1.050 1.49+0
23.7 CV	δ	4.82-3	8.32-3	1.77-2	2.93-2	4.23-2	5.61-2	7.01-2	8.43-2	9.85-2	1.13-1
4d _{3/2}	σ	1.739+0	7.130-1	1.848-1	6.673-2	2.938-2	1.477-2	8.171-3	4.855-3	3.050-3	2.004-3
$E_b = 3.0 \text{ eV}$	β γ	1.194 4.56-1	1.102 6.03-1	0.944 8.17-1	0.818 9.58-1	0.717 1.05+0	0.635 1.12+0	0.565 1.17+0	0.507 1.21+0	0.455 1.23+0	0.410 1.25+0
3.0 CV	δ	6.59-2	8.65-2	1.28-1	1.69-1	2.08-1	2.45-1	2.80-1	3.13-1	3.45-1	3.75-1
5s _{1/2}	σ	3.188-1	1.885-1	8.726-2	4.926-2	3.112-2	2.117-2	1.517-2	1.131-2	8.697-3	6.853-3
$E_b = 7.0 \text{ eV}$	β γ	1.993 -5.99-2	1.995 -8.77-2	1.997 -4.01-2	1.997 7.43-2	1.995 2.15-1	1.991 3.64-1	1.986 5.13-1	1.981 6.58-1	1.974 7.99-1	1.968 9.34-1
7.0 € ₹	δ	-6.51-5	-7.53-5	-8.78-5	-9.40-5	-9.72-5	-9.87-5	-9.95-5	-9.83-5	-9.70-5	-9.35-5
Z= 41, Nb: [K	(r]4d _{3/2}	5s _{1/2}									
		k (eV)									
Shell		1500	2000	3000	4000	5000	6000	7000	8000	9000	10000
$3s_{1/2}$	σ	2.931+1	1.795+1	8.573+0	4.919+0	3.141+0	2.153+0 1.993	1.553+0	1.163+0	8.973-1	7.091-1
$E_b = 468.4 \text{ eV}$	$eta \ \gamma$	1.989 2.34-2	1.992 -6.72-2	1.996 -7.95-2	1.997 8.47-3	1.996 1.36-1	1.993 2.80—1	1.989 4.28-1	1.984 5.74-1	1.978 7.16-1	1.971 8.54-1
	δ	-8.12 - 5	-9.27 - 5	-1.06-4	-1.13-4	-1.18 - 4	-1.19 - 4	-1.20-4	-1.20-4	-1.18 - 4	-1.16-4
$3p_{1/2}$	σ	3.738+1	2.080+1	8.307+0	4.086+0	2.286+0	1.396+0	9.090-1	6.215-1	4.417-1	3.238-1
$E_b = 378.4 \text{ eV}$	$eta \ \gamma$	1.617 2.16-2	1.597 1.49-1	1.520 4.24-1	1.438 6.63-1	1.358 8.59-1	1.284 1.02+0	1.215 1.15+0	1.151 1.26+0	1.092 1.36+0	1.038 1.44+0
	δ	2.84-3	6.48-3	1.61-2	2.82-2	4.17-2	5.59-2	7.03-2	8.46-2	9.90-2	1.13-1
3p _{3/2}	σ	7.302+1	3.994+1	1.560+1	7.557+0	4.178+0	2.527+0	1.632+0	1.107+0	7.817-1	5.697-1
$E_b = 363.0 \text{ eV}$	$eta \ \gamma$	1.643 2.63-2	1.630 1.60-1	1.561 4.46-1	1.483 6.93-1	1.406 8.96-1	1.332 1.06+0	1.264 1.20+0	1.200 1.31+0	1.142 1.41+0	1.088 1.49+0
_ 55.0 C V	δ	4.84-3	8.56-3	1.73-2	2.82-2	4.05-2	5.34-2	6.68-2	8.01-2	9.36-2	1.07-1
3d _{3/2}	σ	4.074+1	1.637+1	4.171+0	1.498+0	6.589-1	3.313-1	1.834-1	1.091-1	6.858-2	4.509-2
$E_b = 207.4 \text{ eV}$	β	1.201	1.130 5.81_1	0.982 8 10—1	0.855	0.752	0.666	0.596	0.536 1.23+0	0.485 1.26±0	0.439
201.4 EV	$\frac{\gamma}{\delta}$	4.21-1 $6.82-2$	5.81-1 $8.75-2$	8.10-1 1.27-1	9.59-1 1.65-1	1.06+0 2.03-1	1.13+0 2.39-1	1.19+0 2.73-1	1.23+0 3.06-1	1.26+0 3.37-1	1.28+0 3.67-1
	•		- -	-	<u> </u>	,	<u> </u>	· •	-		<u> </u>

$\begin{array}{c ccccccccccccccccccccccccccccccccccc$		tinued)									
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	5.866+1 1.185		2.349+1 1.110	5.951+0 0.962	2.127+0 0.840	9.310-1 0.742	4.662-1 0.663	2.570-1 0.599	1.523-1 0.545	9.545-2 0.500	6.257—2 0.460
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	4.24-1	•	5.81-1	8.04-1	9.52-1	1.05+0	1.13+0	1.18+0	1.23+0	1.26+0	1.29+0
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	5.92-2	δ	8.94-2	1.30-1	1.70-1	2.08-1	2.44-1	2.78-1	3.11-1	3.42-1	3.71-1
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	4.690+0		2.792+0	1.304+0	7.405-1	4.700-1	3.209-1	2.307-1	1.724-1	1.328-1	1.049-
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	1.992 -4.87-2	,	1.994 -8.56-2	1.996 -5.49-2	1.997 4.67-2	1.995 1.79-1	1.992 3.23-1	1.987 4.69-1	1.982 6.14-1	1.976 7.54–1	1.970 8.90-1
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	-7.45-5		-8.57-5	-9.88 - 5	-1.07-4	-1.11-4	-1.13-4	-1.13-4	-1.13-4	-1.11-4	-1.10-
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	4.529+0	σ	2.492+0	9.939-1	4.901-1	2.748-1	1.682-1	1.097-1	7.515-2	5.348-2	3.926-
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	1.653		1.609	1.516	1.428	1.347	1.272	1.204	1.140	1.081	1.027
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	7.44-2 2.50-3	,	2.05-1 5.85-3	4.67-1 1.53-2	6.93-1 2.75-2	8.81-1 4.12-2	1.04+0 5.56-2	1.16+0 7.03-2	1.27+0 8.50-2	1.37+0 9.95-2	1.44+0 1.14-1
$\begin{array}{cccccccccccccccccccccccccccccccccccc$			4.876+0	1.906+0	9.261-1	5.134-1	3.113-1			9.681-2	7.064-
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	8.995+0 1.680		1.643	1.557	1.473	1.394	3.113-1 1.321	2.014-1 1.253	1.369-1 1.189	1.131	1.077
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	8.07-2		2.16-1	4.88-1	7.23-1	9.17-1	1.08+0	1.21+0	1.32+0	1.41+0	1.49+0
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	4.42-3	δ	7.70-3	1.63-2	2.73-2	3.97-2	5.30-2	6.66-2	8.03-2	9.40-2	1.08-1
3.2 eV β δ 6.5 $5s_{1/2}$ σ 2.5 $E_b = \beta$ 1.9 7.0 eV γ -1.5 δ -1.5 Z= 42, Mo: [Kr] $4d_{3/2}^4$ $4d_{5/2}^1$ Shell $\frac{k(1)}{3s_{1/2}}$ σ 3.1 $E_b = \beta$ 1.9 504.6 eV γ 4.9 δ -1.9 δ δ -1.9 eV δ δ δ δ δ δ δ δ δ δ	2.070+0		8.595-1	2.268-1	8.279-2	3.672-2	1.857-2	1.031-2	6.147-3	3.874-3	2.551-
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	1.212 4.42-1		1.124 5.90-1	0.969 8.11-1	0.844 9.59-1	0.743 1.06+0	0.659 1.13+0	0.588 1.19+0	0.528 1.22+0	0.474 1.25+0	0.428 1.27+0
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	5.42-2		8.39-2	1.24-1	1.64-1	2.03-1	2.39-1	2.74-1	3.06-1	3.37-1	3.67-1
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	2.893-1	σ	1.711-1	7.943-2	4.500-2	2.852-2	1.944-2	1.396-2	1.043-2	8.027-3	6.333-
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	1.992	,	1.994	1.996	1.997	1.995	1.992	1.987	1.982	1.976	1.969
Z= 42, Mo: [Kr] $4d_{3/2}^4$ $4d_{5/2}^1$ Shell $\frac{k}{15}$ $3s_{1/2}$ σ 3.1 $E_b =$ β 1.5 504.6 eV γ 4.6 504.6 eV γ 4.7 $3p_{1/2}$ σ 4.1 409.7 eV γ 6.2 $3p_{3/2}$ σ 7.3 $E_b =$ β 1.1 392.3 eV γ 9.2 δ δ 4.2 $3d_{3/2}$ σ 4.2 $E_b =$ β 1.2 303.3 eV γ 4.3 δ δ 6.3 $3d_{5/2}$ σ 6.3 $4s_{1/2}$ σ 6.3 $4s_{1/2}$ σ 5.3 δ δ 6.3 $4p_{1/2}$ σ 5.3 δ δ 1.3 $4p_{3/2}$ σ 1.4 $4d_{3/2}$ σ 2.7 δ 6.3 δ 6.3 <td>-5.29-2 -7.35-5</td> <td></td> <td>-8.67-2 $-8.39-5$</td> <td>-5.30-2 $-9.82-5$</td> <td>5.01-2 $-1.06-4$</td> <td>1.84-1 -1.10-4</td> <td>3.28-1 -1.12-4</td> <td>4.74-1 -1.14-4</td> <td>6.16-1 $-1.13-4$</td> <td>7.55-1 $-1.12-4$</td> <td>8.88-1 -1.09-</td>	-5.29-2 -7.35-5		-8.67-2 $-8.39-5$	-5.30-2 $-9.82-5$	5.01-2 $-1.06-4$	1.84-1 -1.10-4	3.28-1 -1.12-4	4.74-1 -1.14-4	6.16-1 $-1.13-4$	7.55-1 $-1.12-4$	8.88-1 -1.09-
Shell $\frac{15}{15}$ $3s_{1/2}$ σ				-5.62-5	-1.00-4	-1.10-4	-1.12-4	-1,14-4	-1.13-4	-1.12-4	-1.03-
Shell 15 $3s_{1/2}$ σ 3.1 $E_b = \beta$ 1.9 504.6 eV γ 4.9 8 $3p_{1/2}$ σ 4.1 8 8 8 8 9 9 9 9	k (eV)										
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	1500		2000	3000	4000	5000	6000	7000	8000	9000	10000
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	3.087+1		1.898+1	9.121+0	5.255+0	3.367+0	2.314+0	1.673+0	1.255+0	9.702-1	7.679-
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	1.987		1.990	1.995	1.996	1.996	1.993	1.990	1.985	1.979	1.973
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	4.75-2	γ	-5.61-2	-8.82-2	-1.37 - 2	1.05-1	2.41-1	3.85-1	5.28-1	6.69-1	8.05-1
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	-8.86-5		-1.03-4	-1.19-4	-1.28-4	-1.33-4	-1.36-4	-1.37-4	-1.37-4	-1.36-4	-1.34-
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	4.000+1 1.616		2.248+1 1.602	9.103+0 1.532	4.519+0 1.453	2.545+0 1.376	1.562+0 1.304	1.022+0 1.236	7.010-1 1.173	4.996-1 1.115	3.673- 1.061
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	5.32-3		1.22-1	3.92-1	6.32-1	8.31-1	9.97-1	1.13+0	1.25+0	1.35+0	1.43+0
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	2.34-3		5.61 - 3	1.45 - 2	2.59-2	3.89-2	5.27 - 2	6.66 - 2	8.06 - 2	9.44 - 2	1.08 - 1
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	7.837+1		4.324+1	1.710+1	8.354+0	4.647+0	2.824+0	1.830+0	1.246+0	8.821-1	6.444—
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	1.642 9.79—3		1.636 1.33-1	1.574 4.14-1	1.499 6.63-1	1.426 8.70-1	1.355 1.04+0	1.288 1.18+0	1.225 1.30+0	1.167 1.40+0	1.113 1.49+0
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	4.41-3		7.88–3	1.60-2	2.62-2	3.78-2	5.04-2	6.32-2	7.61–2	8.90-2	1.49+0
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	4.716+1		1.913+1	4.944+0	1.792+0	7.928-1	4.005-1	2.225-1	1.327-1	8.367-2	5.515-
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	1.212		1.148	1.005	0.880	0.776	0.689	0.617	0.556	0.503	0.456
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	4.00-1		5.64-1	8.01-1	9.58-1	1.07+0	1.14+0	1.20+0	1.24+0	1.27+0	1.30+0
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	5.65-2		8.50-2	1.23-1	1.61-1	1.97-1	2.32-1	2.66-1	2.99-1	3.30-1	3.59-1
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	5.786+1 1.196		2.744+1 1.127	7.048+0 0.983	2.542+0 0.862	1.119+0 0.763	5.631-1 0.683	3.116-1 0.617	1.852-1 0.562	1.163-1 0.516	7.643—: 0.475
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	4.04—1	•	5.64-1	7.95-1	9.50–1	1.06+0	1.14+0	1.20+0	1.24+0	1.28+0	1.31+0
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	6.74-2		8.69 - 2	1.27 - 1	1.66 - 1	2.03 - 1	2.38 - 1	2.72 - 1	3.04 - 1	3.35 - 1	3.64 - 1
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	5.174+0		3.083+0	1.444+0	8.232-1	5.241-1	3.587-1	2.584-1	1.935-1	1.493-1	1.180-
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	1.991		1.993	1.996	1.996	1.995	1.992 2.87-1	1.988	1.983	1.978	1.971
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	-4.03-2 -8.22-5	,	-8.39-2 $-9.54-5$	-6.60-2 $-1.11-4$	2.50-2 $-1.20-4$	1.49-1 -1.26-4	-1.28-4	4.29-1 -1.29-4	5.71-1 -1.29-4	7.10-1 $-1.28-4$	8.44-1 -1.26-
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	5.134+0		2.845+0	1.148+0	5.712-1	3.225-1	1.984-1	1.300-1	8.934-2	6.377-2	4.693-
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	1.660	β	1.618	1.528	1.443	1.365	1.292	1.224	1.162	1.104	1.050
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	5.86-2	γ	1.82-1	4.39-1	6.66-1	8.57-1	1.02+0	1.15+0	1.26+0	1.36+0	1.44+0
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	1.99-3		4.98-3	1.37-2	2.51-2	3.82-2	5.22-2	6.64-2	8.07-2	9.49-2	1.09-1
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	1.013+1 1.686		5.527+0 1.652	2.183+0 1.571	1.070+0 1.490	5.967-1 1.414	3.635-1 1.342	2.361-1 1.276	1.611-1 1.213	1.142-1 1.155	8.352- 1.101
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	5.44–2		1.94-1	4.61-1	6.96-1	8.94-1	1.06+0	1.19+0	1.31+0	1.41+0	1.49+0
$E_b = \beta 1.5 = 0.9 \text{ eV}$ $A_b = 0.9 \text{ eV}$ A	4.02-3		7.02-3	1.49-2	2.51-2	3.70-2	4.98-2	6.29-2	7.61-2	8.93-2	1.02-1
1.9 eV γ 4 δ 6. $4d_{5/2}$ σ 3 $E_b = \beta$ 1	2.734+0		1.150+0	3.090-1	1.141-1	5.104-2	2.595-2	1.448-2	8.662-3	5.475-3	3.615-
$ \begin{array}{ccc} \delta & 6. \\ 4d_{5/2} & \sigma & 3. \\ E_b = & \beta & 1. \end{array} $	1.227 1.27_1		1.142 5.76—1	0.989 8.02—1	0.866 9.57—1	0.765 1.07+0	0.680 1.14+0	0.608 1.20+0	0.546 1.24+0	0.492 1.27+0	0.444 1.29+0
$\begin{array}{ccc} 4d_{5/2} & \sigma & 3.3 \\ E_b = & \beta & 1.3 \end{array}$	4.27-1 5.17-2		5.76-1 8.07-2	8.02-1 1.20-1	9.57-1 1.59-1	1.07+0 1.97-1	1.14+0 2.33-1	1.20+0 2.67-1	1.24+0 2.99-1	3.29-1	3.59-1
$E_b = \beta$ 1.3	3.842+0		1.609+0	4.292-1	1.576-1	7.012-2	3.549-2	1.972-2	1.175-2	7.401-3	4.871-
1.2 eV γ 4.3	1.207	β	1.119	0.966	0.848	0.753	0.675	0.610	0.553	0.506	0.463
	4.29-1	•	5.75-1	7.96-1	9.49-1	1.06+0	1.14+0	1.20+0	1.24+0	1.28+0	1.30+0
	5.27-2	δ	8.27-2	1.23-1	1.64-1 4.897-2	2.03-1 3.112-2	2.39-1 2.126-2	2.73-1	3.04-1	3.34-1 8.824-3	3.63-1
$5s_{1/2} \qquad \qquad \sigma \qquad 3.$ $E_b = \qquad \qquad \beta \qquad 1.$	3.130-1		1.852 - 1	8.617 - 2	A QU7 ')	2117 7	9 196 9	1.530 - 2	1.145 - 2	0 0 1/1 2	6.971 -

Table 1 (contin	iued)										
7.0 eV	γ δ	-4.54-2 -8.13-5	-8.55-2 $-9.36-5$	-6.41-2 $-1.10-4$	2.83-2 -1.19-4	1.54-1 -1.24-4	2.92-1 -1.27-4	4.34-1 $-1.29-4$	5.74-1 -1.29-4	7.10-1 -1.28-4	8.43-1 $-1.26-4$
Z= 43, Tc: [K	[r]4d ⁴ _{3/2}	4d _{5/2} 5s _{1/2}									
		k (eV)									
Shell		1500	2000	3000	4000	5000	6000	7000	8000	9000	10000
$3s_{1/2} E_b =$	$\frac{\sigma}{eta}$	3.241+1 1.986	2.003+1 1.989	9.683+0 1.994	5.602+0 1.996	3.601+0 1.996	2.482+0 1.994	1.797+0 1.990	1.351+0 1.986	1.046+0 1.981	8.290-1 1.975
544.0 eV	γ	7.35 - 2	-4.34-2	-9.47 - 2	-3.36-2	7.56 - 2	2.06 - 1	3.44 - 1	4.84 - 1	6.21 - 1	7.54 - 1
2	δ	-9.72-5	-1.15-4	-1.33-4	-1.43-4	-1.50-4	-1.54-4	-1.56-4	-1.57-4	-1.56-4	-1.55-4
$3p_{1/2}$ $E_b =$	$\frac{\sigma}{eta}$	4.262+1 1.614	2.420+1 1.606	9.933+0 1.542	4.975+0 1.466	2.820+0 1.391	1.740+0 1.321	1.143+0 1.254	7.867-1 1.193	5.624-1 1.137	4.145-1 1.085
444.9 eV	γ δ	-5.96-3 $1.93-3$	9.84-2 $4.86-3$	3.62-1 1.33-2	6.02 - 1 $2.41 - 2$	8.05-1 3.63-2	9.73 - 1 $4.92 - 2$	1.11+0 6.24-2	1.23+0 7.60-2	1.34+0 8.96-2	1.42+0 1.03-1
$3p_{3/2}$	σ	8.374+1	4.663+1	1.866+1	9.192+0	5.143+0	3.140+0	2.043+0	1.395+0	9.904-1	7.252-1
$E_b = 425.0 \text{ eV}$	β γ	1.640 -4.05-3	1.640 1.09-1	1.586 3.84-1	1.515 6.34-1	1.443 8.44-1	1.373 1.02+0	1.308 1.16+0	1.247 1.29+0	1.191 1.39+0	1.139 1.48+0
	δ	4.05 - 3	7.33-3	1.51-2	2.47 - 2	3.55-2	4.72 - 2	5.92-2	7.16-2	8.41-2	9.68 - 2
$3d_{3/2}$	σ	5.412+1	2.217+1	5.808+0	2.125+0	9.461-1	4.803-1	2.678-1	1.603-1	1.013-1	6.693-2
$E_b = 256.4 \text{ eV}$	β γ	1.220 3.78-1	1.161 5.46-1	1.023 7.90-1	0.900 9.54-1	0.796 1.07+0	0.711 1.15+0	0.639 1.21+0	0.578 1.26+0	0.524 1.29+0	0.476 1.32+0
	δ	6.43 - 2	8.25-2	1.19-1	1.56 - 1	1.92 - 1	2.26 - 1	2.60 - 1	2.92 - 1	3.23-1	3.52 - 1
3d _{5/2}	σ	7.779+1 1.204	3.175+1	8.267+0	3.008+0	1.333+0	6.740-1 0.702	3.743-1 0.637	2.231-1	1.406-1	9.255-2 0.492
$E_b = 252.9 \text{ eV}$	$eta \gamma$	1.204 3.83—1	1.140 5.47-1	1.000 7.85-1	0.880 9.45-1	0.782 1.06+0	0.702 1.14+0	0.637 1.21+0	0.581 1.26+0	0.534 1.30+0	0.492 1.33+0
	δ	6.52-2	8.44-2	1.23-1	1.61-1	1.97-1	2.32-1	2.66-1	2.98-1	3.28-1	3.57-1
$4s_{1/2}$	σ	5.741+0 1.990	3.424+0 1.992	1.609+0 1.995	9.197-1 1.996	5.871-1 1.995	4.027-1 1.993	2.907-1 1.989	2.180-1 1.984	1.685-1 1.979	1.333-1 1.973
$E_b = 68.8 \text{ eV}$	$eta \ \gamma$	-3.18-2	-8.12-2	-7.55-2	5.22-3	1.21-1	2.54-1	3.92-1	5.30-1	6.65-1	7.97–1
	δ	-9.23-5	-1.06-4	-1.24-4	-1.35-4	-1.42-4	-1.45-4	-1.47 - 4	-1.48 - 4	-1.47 - 4	-1.46-4
$4p_{1/2}$	$rac{\sigma}{eta}$	5.829+0 1.666	3.252+0 1.627	1.327+0 1.540	6.660-1 1.457	3.785-1 1.380	2.341-1 1.308	1.540-1 1.242	1.062-1 1.180	7.604-2 1.123	5.612-2 1.071
$E_b = 42.8 \text{ eV}$	γ	4.53-2	1.63-1	4.15-1	6.42-1	8.34-1	9.95-1	1.13+0	1.25+0	1.34+0	1.43+0
	δ	1.54-3	4.30-3	1.25-2	2.33-2	3.57-2	4.88-2	6.24-2	7.59-2	8.97-2	1.03-1
$4p_{3/2} E_b =$	$\frac{\sigma}{eta}$	1.149+1 1.692	6.307+0 1.661	2.516+0 1.584	1.243+0 1.506	6.974-1 1.431	4.268-1 1.361	2.783-1 1.295	1.904-1 1.234	1.354-1 1.177	9.926-2 1.125
36.9 eV	γ	5.03 - 2	1.74 - 1	4.37 - 1	6.72 - 1	8.72 - 1	1.04+0	1.18+0	1.30+0	1.40+0	1.49+0
	δ	3.69-3	6.53-3	1.40-2	2.36-2	3.47-2	4.66-2	5.90-2	7.16-2	8.41-2	9.69-2
$4d_{3/2}$ $E_b =$	$\frac{\sigma}{eta}$	3.811+0 1.241	1.623+0 1.158	4.441-1 1.009	1.660-1 0.885	7.486-2 0.783	3.830-2 0.697	2.146-2 0.625	1.289-2 0.563	8.174-3 0.509	5.413-3 0.462
2.0 eV	γ	4.13 - 1	5.64 - 1	7.94 - 1	9.54 - 1	1.07+0	1.15+0	1.21+0	1.25+0	1.29+0	1.31+0
4.1	δ	5.95-2	7.83-2	1.17-1	1.54-1	1.91-1	2.26-1	2.59-1	2.91-1	3.22-1	3.51-1
$4d_{5/2}$ $E_b =$	$\frac{\sigma}{eta}$	5.416+0 1.220	2.296+0 1.134	6.237-1 0.986	2.317-1 0.866	1.039-1 0.769	5.291-2 0.690	2.953-2 0.624	1.767-2 0.568	1.116-2 0.520	7.366-3 0.478
1.2 eV	γ	4.15 - 1	5.63 - 1	7.88 - 1	9.46 - 1	1.06+0	1.14+0	1.20+0	1.25+0	1.29+0	1.32+0
5s _{1/2}	$\frac{\delta}{\sigma}$	6.05-2 4.145-1	8.03-2 2.453-1	1.20-1 1.144-1	1.59-1 6.514-2	1.97-1 4.149-2	2.32-1 2.841-2	2.66-1 2.048-2	2.98-1 1.535-2	3.28-1 1.185-2	3.57-1 9.377-3
$E_b =$	β	1.990	1.992	1.144-1	1.996	1.995	1.993	1.989	1.984	1.183-2	1.973
7.0 eV	γ	-3.86-2	-8.42-2	-7.41-2	8.84-3	1.26-1	2.58-1	3.95-1	5.31-1	6.66-1	7.98-1
Z= 44, Ru: [I	$\frac{\delta}{\text{Cr]4d}_{3/2}^4}$	$\frac{-9.17-5}{4d_{5/2}^3 5s_{1/2}^1}$	-1.06-4	-1.24-4	-1.35-4	-1.40-4	-1.44-4	-1.47-4	-1.47-4	-1.46-4	-1.44-4
		k (eV)									
Shell		1500	2000	3000	4000	5000	6000	7000	8000	9000	10000
3s _{1/2}	σ	3.404+1	2.111+1	1.026+1	5.959+0	3.841+0	2.653+0	1.926+0	1.451+0	1.125+0	8.930-1
$E_b = 585.0 \text{ eV}$	$eta \ \gamma$	1.984 1.05-1	1.988 -2.62-2	1.993 -9.92-2	1.995 -5.20-2	1.996 4.70-2	1.994 1.69-1	1.991 3.02-1	1.987 4.38-1	1.982 5.74-1	1.976 7.07-1
	δ	-1.03-4	-1.25-4	-1.49-4	-1.61-4	-1.69-4	-1.74-4	-1.76-4	-1.77-4	-1.76-4	-1.75-4
3p _{1/2}	σ	4.545+1	2.605+1	1.082+1	5.466+0	3.118+0	1.934+0	1.275+0	8.808-1	6.314-1	4.664-1
$E_b = 482.8 \text{ eV}$	β γ	1.610 -1.61-2	1.610 7.32-2	1.552 3.29-1	1.480 5.68-1	1.409 7.73-1	1.342 9.46-1	1.278 1.09+0	1.217 1.22+0	1.160 1.32+0	1.106 1.42+0
	δ	1.61-3	4.08-3	1.17-2	2.16-2	3.32-2	4.61-2	5.95-2	7.29–2	8.61-2	9.92-2
3p _{3/2}	σ	8.966+1	5.031+1	2.036+1	1.010+1	5.684+0	3.486+0	2.277+0	1.560+0	1.110+0	8.142-1
$E_b = 460.6 \text{ eV}$	β γ	1.636 -1.63-2	1.644 8.29-2	1.597 3.51-1	1.530 6.00-1	1.462 8.13-1	1.397 9.94-1	1.334 1.15+0	1.274 1.27+0	1.217 1.38+0	1.164 1.48+0
	δ	3.70-3	6.71-3	1.38-2	2.25-2	3.27-2	4.43-2	5.64-2	6.86-2	8.07-2	9.28-2
$3d_{3/2}$	σ	6.228+1	2.570+1	6.808+0	2.511+0	1.125+0	5.732-1	3.206-1	1.924-1	1.219-1	8.069-2
$E_b = 283.6 \text{ eV}$	β	1.227 3.53-1	1.177 5.24-1	1.046 7.78-1	0.927 9.51-1	0.825 1.07+0	0.736 1.16+0	0.661 1.22+0	0.596 1.27+0	0.540 1.31+0	0.492 1.34+0
203.0 (7	$_{\delta}^{\gamma}$	6.27-2	7.98-2	1.15-1	1.52-1	1.87-1	2.21-1	2.53-1	2.84-1	3.14–1	3.43-1

Tab	nle 1	l (c	nnt	inı	ed)

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$3d_{5/2}$	σ	8.966+1	3.685+1	9.703+0	3.559+0	1.587+0	8.052 - 1	4.485 - 1	2.681 - 1	1.692 - 1	1.117-1
$E_b =$	β	1.213	1.155	1.021	0.905	0.807	0.725	0.656	0.597	0.548	0.505
279.4 eV	γ	3.60 - 1	5.27 - 1	7.73 - 1	9.42 - 1	1.06+0	1.15+0	1.22+0	1.27+0	1.31+0	1.34+0
	δ	6.34-2	8.15-2	1.19 - 1	1.57 - 1	1.93-1	2.28 - 1	2.60-1	2.91 - 1	3.21 - 1	3.49 - 1
4s _{1/2}	σ	6.187+0	3.692+0	1.738+0	9.963 - 1	6.375 - 1	4.383 - 1	3.170 - 1	2.382 - 1	1.843 - 1	1.461 - 1
$E_b =$	β	1.989	1.991	1.994	1.996	1.995	1.993	1.990	1.985	1.980	1.975
74.9 eV	γ	-2.10-2	-7.75 - 2	-8.41-2	-1.36-2	9.37 - 2	2.19 - 1	3.51 - 1	4.87 - 1	6.21 - 1	7.52 - 1
	δ	-1.00 - 4	-1.18 - 4	-1.39 - 4	-1.52 - 4	-1.60 - 4	-1.64 - 4	-1.66-4	-1.67 - 4	-1.66-4	-1.66-4
4p _{1/2}	σ	6.406+0	3.595+0	1.482+0	7.494-1	4.286-1	2.665-1	1.760-1	1.218-1	8.747-2	6.471-2
$E_b =$	β	1.671	1.635	1.552	1.471	1.397	1.329	1.264	1.204	1.147	1.093
47.0 eV	γ	3.10-2	1.42 - 1	3.88 - 1	6.12 - 1	8.06 - 1	9.72 - 1	1.11+0	1.23+0	1.33+0	1.42+0
	δ	1.09 - 3	3.49 - 3	1.08 - 2	2.08 - 2	3.26 - 2	4.56 - 2	5.91 - 2	7.27 - 2	8.61 - 2	9.93 - 2
4p _{3/2}	σ	1.255+1	6.920+0	2.786+0	1.386+0	7.822-1	4.811-1	3.149-1	2.161-1	1.540-1	1.132-1
$E_b =$	β	1.697	1.670	1.597	1.521	1.450	1.383	1.320	1.260	1.203	1.151
41.2 eV	γ	3.53 - 2	1.52 - 1	4.09 - 1	6.44 - 1	8.45 - 1	1.02+0	1.16+0	1.29+0	1.39+0	1.48+0
	δ	3.34 - 3	5.92 - 3	1.26 - 2	2.14 - 2	3.18 - 2	4.35 - 2	5.58 - 2	6.83 - 2	8.06 - 2	9.30 - 2
4d _{3/2}	σ	4.293+0	1.846+0	5.130-1	1.939-1	8.808-2	4.532-2	2.551-2	1.537-2	9.771-3	6.486-3
$E_b =$	β	1.256	1.175	1.028	0.907	0.808	0.723	0.650	0.585	0.529	0.479
2.4 eV	γ	3.95 - 1	5.48 - 1	7.83 - 1	9.49 - 1	1.07+0	1.16+0	1.22+0	1.27+0	1.31+0	1.33+0
	δ	5.69 - 2	7.49 - 2	1.12 - 1	1.49 - 1	1.86 - 1	2.21 - 1	2.54 - 1	2.85 - 1	3.15 - 1	3.43 - 1
4d _{5/2}	σ	6.075+0	2.600+0	7.170-1	2.693-1	1.217-1	6.231-2	3.492-2	2.096-2	1.327-2	8.780-3
$E_b =$	β	1.235	1.150	1.002	0.885	0.791	0.713	0.646	0.587	0.538	0.493
1.8 eV	γ	3.99-1	5.49-1	7.77-1	9.41-1	1.06+0	1.15+0	1.22+0	1.27+0	1.31+0	1.34+0
	δ	5.78 - 2	7.68-2	1.16-1	1.54-1	1.92 - 1	2.27 - 1	2.60 - 1	2.92 - 1	3.21 - 1	3.49 - 1
5s _{1/2}	σ	3.529-1	2.089-1	9.754-2	5.571-2	3.559-2	2.443-2	1.765-2	1.324-2	1.024-2	8.109-3
E _b =	β	1.989	1.991	1.994	1.996	1.995	1.993	1.990	1.985	1.980	1.974
$E_b = 7.0 \text{ eV}$	γ	-2.88-2	-8.06-2	-8.21-2	-9.93-3	9.86-2	2.25-1	3.59-1	4.93-1	6.24-1	7.53-1
	δ	-9.95-5	-1.16-4	-1.37 - 4	-1.49 - 4	-1.57 - 4	-1.62 - 4	-1.65-4	-1.67 - 4	-1.67 - 4	-1.66-4
Z= 45, Rh: [K	7-14-14										
Z= 45, KII: [N	17 J4u _{3/2}										
		k (eV)									
Shell		1500	2000	3000	4000	5000	6000	7000	8000	9000	10000
3s _{1/2}	σ	3.561+1	2.219+1	1.085+1	6.322+0	4.087+0	2.830+0	2.058+0	1.553+0	1.206+0	9.589-1
$E_b =$	β	1.983	1.986	1.991	1.994	1.995	1.994	1.992	1.988	1.983	1.978
627.1 eV	γ	1.38-1	-7.42 - 3	-1.01-1	-6.79-2	2.11-2	1.36-1	2.62-1	3.94-1	5.27-1	6.59-1
02/// 07	δ	-1.11-4	-1.38-4	-1.65-4	-1.81-4	-1.90-4	-1.96-4	-1.99-4	-2.01-4	-2.00-4	-2.00-4
3p _{1/2}	σ	4.816+1	2.788+1	1.173+1	5.975+0	3.430+0	2.138+0	1.415+0	9.809-1	7.052-1	5.223-1
$E_b =$	β	1.604	1.612	1.562	1.493	1.424	1.359	1.297	1.238	1.182	1.129
521.0 eV	γ	-2.18-2	5.17-2	2.98-1	5.37-1	7.43-1	9.19-1	1.07+0	1.20+0	1.31+0	1.40+0
											9.49-2
	δ	1.42 - 3	3.44 - 3	1.05 - 2	1.98 - 2	3.07 - 2	4.30 - 2	5.59-2	6.91-2	8.22-2	9.49-2
3n	δ	1.42-3	3.44-3 5.308+1	1.05-2	1.98-2	3.07-2 6.248+0	4.30-2 3.849+0	5.59-2 2.523+0	6.91-2	8.22-2	
$3p_{3/2}$	$\frac{\delta}{\sigma}$	9.540+1	5.398+1	2.209+1	1.104+1	6.248+0	3.849+0	2.523+0	1.734+0	1.237+0	9.094-1
$E_b =$	$\frac{\delta}{\sigma}$	9.540+1 1.630	5.398+1 1.647	2.209+1 1.607	1.104+1 1.544	6.248+0 1.479	3.849+0 1.416	2.523+0 1.355	1.734+0 1.297	1.237+0 1.242	9.094-1 1.188
	δ σ β γ	9.540+1 1.630 -2.46-2	5.398+1 1.647 6.04-2	2.209+1 1.607 3.20-1	1.104+1 1.544 5.70-1	6.248+0 1.479 7.84-1	3.849+0 1.416 9.68-1	2.523+0 1.355 1.12+0	1.734+0 1.297 1.26+0	1.237+0 1.242 1.37+0	9.094-1 1.188 1.47+0
$E_b = 496.2 \text{ eV}$	δ σ β γ δ	9.540+1 1.630 -2.46-2 3.46-3	5.398+1 1.647 6.04-2 6.24-3	2.209+1 1.607 3.20-1 1.30-2	1.104+1 1.544 5.70-1 2.10-2	6.248+0 1.479 7.84-1 3.06-2	3.849+0 1.416 9.68-1 4.14-2	2.523+0 1.355 1.12+0 5.30-2	1.734+0 1.297 1.26+0 6.50-2	1.237+0 1.242 1.37+0 7.69-2	9.094-1 1.188 1.47+0 8.85-2
$E_b = 496.2 \text{ eV}$	δ σ β γ δ	9.540+1 1.630 -2.46-2 3.46-3 7.094+1	5.398+1 1.647 6.04-2 6.24-3 2.950+1	2.209+1 1.607 3.20-1 1.30-2 7.907+0	1.104+1 1.544 5.70-1 2.10-2 2.940+0	6.248+0 1.479 7.84-1 3.06-2 1.325+0	3.849+0 1.416 9.68-1 4.14-2 6.786-1	2.523+0 1.355 1.12+0 5.30-2 3.809-1	1.734+0 1.297 1.26+0 6.50-2 2.292-1	1.237+0 1.242 1.37+0 7.69-2 1.456-1	9.094-1 1.188 1.47+0 8.85-2 9.657-2
$E_b = 496.2 \text{ eV}$ $3d_{3/2}$ $E_b = 600$	δ σ β γ δ	9.540+1 1.630 -2.46-2 3.46-3 7.094+1 1.232	5.398+1 1.647 6.04-2 6.24-3 2.950+1 1.189	2.209+1 1.607 3.20-1 1.30-2 7.907+0 1.064	1.104+1 1.544 5.70-1 2.10-2 2.940+0 0.948	6.248+0 1.479 7.84-1 3.06-2 1.325+0 0.847	3.849+0 1.416 9.68-1 4.14-2 6.786-1 0.760	2.523+0 1.355 1.12+0 5.30-2 3.809-1 0.684	1.734+0 1.297 1.26+0 6.50-2 2.292-1 0.617	1.237+0 1.242 1.37+0 7.69-2 1.456-1 0.560	9.094-1 1.188 1.47+0 8.85-2 9.657-2 0.510
$E_b = 496.2 \text{ eV}$	δ σ β γ δ σ β γ	9.540+1 1.630 -2.46-2 3.46-3 7.094+1	5.398+1 1.647 6.04-2 6.24-3 2.950+1 1.189 5.04-1	2.209+1 1.607 3.20-1 1.30-2 7.907+0 1.064 7.64-1	1.104+1 1.544 5.70-1 2.10-2 2.940+0	6.248+0 1.479 7.84-1 3.06-2 1.325+0 0.847 1.07+0	3.849+0 1.416 9.68-1 4.14-2 6.786-1 0.760 1.17+0	2.523+0 1.355 1.12+0 5.30-2 3.809-1 0.684 1.23+0	1.734+0 1.297 1.26+0 6.50-2 2.292-1 0.617 1.29+0	1.237+0 1.242 1.37+0 7.69-2 1.456-1	9.094-1 1.188 1.47+0 8.85-2 9.657-2 0.510 1.36+0
$E_b = 496.2 \text{ eV}$ $3d_{3/2}$ $E_b = 311.7 \text{ eV}$	δ σ β γ δ σ β γ δ	9.540+1 1.630 -2.46-2 3.46-3 7.094+1 1.232 3.28-1 6.09-2	5.398+1 1.647 6.04-2 6.24-3 2.950+1 1.189 5.04-1 7.76-2	2.209+1 1.607 3.20-1 1.30-2 7.907+0 1.064 7.64-1 1.12-1	1.104+1 1.544 5.70-1 2.10-2 2.940+0 0.948 9.44-1 1.47-1	6.248+0 1.479 7.84-1 3.06-2 1.325+0 0.847 1.07+0 1.82-1	3.849+0 1.416 9.68-1 4.14-2 6.786-1 0.760 1.17+0 2.16-1	2.523+0 1.355 1.12+0 5.30-2 3.809-1 0.684 1.23+0 2.48-1	1.734+0 1.297 1.26+0 6.50-2 2.292-1 0.617 1.29+0 2.78-1	1.237+0 1.242 1.37+0 7.69-2 1.456-1 0.560 1.33+0 3.07-1	9.094-1 1.188 1.47+0 8.85-2 9.657-2 0.510 1.36+0 3.35-1
$E_b = 496.2 \text{ eV}$ $3d_{3/2}$ $E_b = 311.7 \text{ eV}$	δ σ β γ δ σ β γ δ	9.540+1 1.630 -2.46-2 3.46-3 7.094+1 1.232 3.28-1 6.09-2 1.022+2	5.398+1 1.647 6.04-2 6.24-3 2.950+1 1.189 5.04-1 7.76-2 4.231+1	2.209+1 1.607 3.20-1 1.30-2 7.907+0 1.064 7.64-1 1.12-1 1.127+1	1.104+1 1.544 5.70-1 2.10-2 2.940+0 0.948 9.44-1 1.47-1 4.167+0	6.248+0 1.479 7.84-1 3.06-2 1.325+0 0.847 1.07+0 1.82-1 1.869+0	3.849+0 1.416 9.68-1 4.14-2 6.786-1 0.760 1.17+0 2.16-1 9.529-1	2.523+0 1.355 1.12+0 5.30-2 3.809-1 0.684 1.23+0 2.48-1 5.327-1	1.734+0 1.297 1.26+0 6.50-2 2.292-1 0.617 1.29+0 2.78-1 3.192-1	1.237+0 1.242 1.37+0 7.69-2 1.456-1 0.560 1.33+0 3.07-1 2.020-1	9.094-1 1.188 1.47+0 8.85-2 9.657-2 0.510 1.36+0 3.35-1
$E_b = 496.2 \text{ eV}$ $3d_{3/2}$ $E_b = 311.7 \text{ eV}$ $3d_{5/2}$ $E_b = 6$	δ σ β γ δ σ β γ δ	9.540+1 1.630 -2.46-2 3.46-3 7.094+1 1.232 3.28-1 6.09-2 1.022+2 1.219	5.398+1 1.647 6.04-2 6.24-3 2.950+1 1.189 5.04-1 7.76-2 4.231+1 1.167	2.209+1 1.607 3.20-1 1.30-2 7.907+0 1.064 7.64-1 1.12-1 1.127+1 1.038	1.104+1 1.544 5.70-1 2.10-2 2.940+0 0.948 9.44-1 1.47-1 4.167+0 0.923	6.248+0 1.479 7.84-1 3.06-2 1.325+0 0.847 1.07+0 1.82-1 1.869+0 0.828	3.849+0 1.416 9.68-1 4.14-2 6.786-1 0.760 1.17+0 2.16-1 9.529-1 0.746	2.523+0 1.355 1.12+0 5.30-2 3.809-1 0.684 1.23+0 2.48-1 5.327-1 0.676	1.734+0 1.297 1.26+0 6.50-2 2.292-1 0.617 1.29+0 2.78-1 3.192-1 0.616	1.237+0 1.242 1.37+0 7.69-2 1.456-1 0.560 1.33+0 3.07-1 2.020-1 0.564	9.094-1 1.188 1.47+0 8.85-2 9.657-2 0.510 1.36+0 3.35-1 1.335-1 0.520
$E_b = 496.2 \text{ eV}$ $3d_{3/2}$ $E_b = 311.7 \text{ eV}$	δ σ β γ δ σ β γ δ	9.540+1 1.630 -2.46-2 3.46-3 7.094+1 1.232 3.28-1 6.09-2 1.022+2 1.219 3.36-1	5.398+1 1.647 6.04-2 6.24-3 2.950+1 1.189 5.04-1 7.76-2 4.231+1 1.167 5.08-1	2.209+1 1.607 3.20-1 1.30-2 7.907+0 1.064 7.64-1 1.12-1 1.127+1 1.038 7.61-1	1.104+1 1.544 5.70-1 2.10-2 2.940+0 0.948 9.44-1 1.47-1 4.167+0 0.923 9.36-1	6.248+0 1.479 7.84-1 3.06-2 1.325+0 0.847 1.07+0 1.82-1 1.869+0 0.828 1.06+0	3.849+0 1.416 9.68-1 4.14-2 6.786-1 0.760 1.17+0 2.16-1 9.529-1 0.746 1.16+0	2.523+0 1.355 1.12+0 5.30-2 3.809-1 0.684 1.23+0 2.48-1 5.327-1 0.676 1.23+0	1.734+0 1.297 1.26+0 6.50-2 2.292-1 0.617 1.29+0 2.78-1 3.192-1 0.616 1.28+0	1.237+0 1.242 1.37+0 7.69-2 1.456-1 0.560 1.33+0 3.07-1 2.020-1 0.564 1.32+0	9.094-1 1.188 1.47+0 8.85-2 9.657-2 0.510 1.36+0 3.35-1 1.335-1 0.520 1.36+0
$E_b = 496.2 \text{ eV}$ $3d_{3/2}$ $E_b = 311.7 \text{ eV}$ $3d_{5/2}$ $E_b = 307.0 \text{ eV}$	δ σ β γ δ σ β γ δ σ β γ δ	9.540+1 1.630 -2.46-2 3.46-3 7.094+1 1.232 3.28-1 6.09-2 1.022+2 1.219 3.36-1 6.14-2	5.398+1 1.647 6.04-2 6.24-3 2.950+1 1.189 5.04-1 7.76-2 4.231+1 1.167 5.08-1 7.91-2	2.209+1 1.607 3.20-1 1.30-2 7.907+0 1.064 7.64-1 1.12-1 1.127+1 1.038 7.61-1 1.15-1	1.104+1 1.544 5.70-1 2.10-2 2.940+0 0.948 9.44-1 1.47-1 4.167+0 0.923 9.36-1 1.52-1	6.248+0 1.479 7.84-1 3.06-2 1.325+0 0.847 1.07+0 1.82-1 1.869+0 0.828 1.06+0 1.88-1	3.849+0 1.416 9.68-1 4.14-2 6.786-1 0.760 1.17+0 2.16-1 9.529-1 0.746 1.16+0 2.23-1	2.523+0 1.355 1.12+0 5.30-2 3.809-1 0.684 1.23+0 2.48-1 5.327-1 0.676 1.23+0 2.55-1	1.734+0 1.297 1.26+0 6.50-2 2.292-1 0.617 1.29+0 2.78-1 3.192-1 0.616 1.28+0 2.85-1	1.237+0 1.242 1.37+0 7.69-2 1.456-1 0.560 1.33+0 3.07-1 2.020-1 0.564 1.32+0 3.14-1	9.094-1 1.188 1.47+0 8.85-2 9.657-2 0.510 1.36+0 3.35-1 1.335-1 0.520 1.36+0 3.42-1
$E_b = 496.2 \text{ eV}$ $3d_{3/2}$ $E_b = 311.7 \text{ eV}$ $3d_{5/2}$ $E_b = 307.0 \text{ eV}$ $4s_{1/2}$	δ σ β γ δ σ β γ δ σ β γ δ	9.540+1 1.630 -2.46-2 3.46-3 7.094+1 1.232 3.28-1 6.09-2 1.022+2 1.219 3.36-1 6.14-2 6.709+0	5.398+1 1.647 6.04-2 6.24-3 2.950+1 1.189 5.04-1 7.76-2 4.231+1 1.167 5.08-1 7.91-2 4.007+0	2.209+1 1.607 3.20-1 1.30-2 7.907+0 1.064 7.64-1 1.12-1 1.127+1 1.038 7.61-1 1.15-1 1.891+0	1.104+1 1.544 5.70-1 2.10-2 2.940+0 0.948 9.44-1 1.47-1 4.167+0 0.923 9.36-1 1.52-1 1.086+0	6.248+0 1.479 7.84-1 3.06-2 1.325+0 0.847 1.07+0 1.82-1 1.869+0 0.828 1.06+0 1.88-1 6.966-1	3.849+0 1.416 9.68-1 4.14-2 6.786-1 0.760 1.17+0 2.16-1 9.529-1 0.746 1.16+0 2.23-1	2.523+0 1.355 1.12+0 5.30-2 3.809-1 0.684 1.23+0 2.48-1 5.327-1 0.676 1.23+0 2.55-1 3.477-1	1.734+0 1.297 1.26+0 6.50-2 2.292-1 0.617 1.29+0 2.78-1 3.192-1 0.616 1.28+0 2.85-1 2.617-1	1.237+0 1.242 1.37+0 7.69-2 1.456-1 0.560 1.33+0 3.07-1 2.020-1 0.564 1.32+0 3.14-1 2.028-1	9.094-1 1.188 1.47+0 8.85-2 9.657-2 0.510 1.36+0 3.35-1 1.335-1 0.520 1.36+0 3.42-1 1.610-1
$E_b = 496.2 \text{ eV}$ $3d_{3/2}$ $E_b = 311.7 \text{ eV}$ $3d_{5/2}$ $E_b = 307.0 \text{ eV}$ $4s_{1/2}$ $E_b = 60.2 \text{ eV}$	δ σ β γ δ σ β γ δ σ β γ δ σ β γ δ σ β γ δ σ β γ δ	9.540+1 1.630 -2.46-2 3.46-3 7.094+1 1.232 3.28-1 6.09-2 1.022+2 1.219 3.36-1 6.14-2 6.709+0 1.988	5.398+1 1.647 6.04-2 6.24-3 2.950+1 1.189 5.04-1 7.76-2 4.231+1 1.167 5.08-1 7.91-2 4.007+0 1.990	2.209+1 1.607 3.20-1 1.30-2 7.907+0 1.064 7.64-1 1.12-1 1.127+1 1.038 7.61-1 1.15-1 1.891+0 1.993	1.104+1 1.544 5.70-1 2.10-2 2.940+0 0.948 9.44-1 1.47-1 4.167+0 0.923 9.36-1 1.52-1 1.086+0 1.995	6.248+0 1.479 7.84-1 3.06-2 1.325+0 0.847 1.07+0 1.82-1 1.869+0 0.828 1.06+0 1.88-1 6.966-1 1.995	3.849+0 1.416 9.68-1 4.14-2 6.786-1 0.760 1.17+0 2.16-1 9.529-1 0.746 1.16+0 2.23-1 4.799-1 1.993	2.523+0 1.355 1.12+0 5.30-2 3.809-1 0.684 1.23+0 2.48-1 5.327-1 0.676 1.23+0 2.55-1 3.477-1 1.990	1.734+0 1.297 1.26+0 6.50-2 2.292-1 0.617 1.29+0 2.78-1 3.192-1 0.616 1.28+0 2.85-1 2.617-1 1.986	1.237+0 1.242 1.37+0 7.69-2 1.456-1 0.560 1.33+0 3.07-1 2.020-1 0.564 1.32+0 3.14-1 2.028-1 1.981	9.094-1 1.188 1.47+0 8.85-2 9.657-2 0.510 1.36+0 3.35-1 1.335-1 0.520 1.36+0 3.42-1 1.610-1 1.976
$E_b = 496.2 \text{ eV}$ $3d_{3/2}$ $E_b = 311.7 \text{ eV}$ $3d_{5/2}$ $E_b = 307.0 \text{ eV}$ $4s_{1/2}$	δ σ β γ δ σ β γ δ σ β γ δ σ β γ δ	9.540+1 1.630 -2.46-2 3.46-3 7.094+1 1.232 3.28-1 6.09-2 1.022+2 1.219 3.36-1 6.14-2 6.709+0 1.988 -1.03-2	5.398+1 1.647 6.04-2 6.24-3 2.950+1 1.189 5.04-1 7.76-2 4.231+1 1.167 5.08-1 7.91-2 4.007+0 1.990 -7.26-2	2.209+1 1.607 3.20-1 1.30-2 7.907+0 1.064 7.64-1 1.12-1 1.127+1 1.038 7.61-1 1.15-1 1.891+0 1.993 -9.09-2	1.104+1 1.544 5.70-1 2.10-2 2.940+0 0.948 9.44-1 1.47-1 4.167+0 0.923 9.36-1 1.52-1 1.086+0 1.995 -3.05-2	6.248+0 1.479 7.84-1 3.06-2 1.325+0 0.847 1.07+0 1.82-1 1.869+0 0.828 1.06+0 1.88-1 6.966-1 1.995 6.89-2	3.849+0 1.416 9.68-1 4.14-2 6.786-1 0.760 1.17+0 2.16-1 9.529-1 0.746 1.16+0 2.23-1 4.799-1 1.993 1.87-1	2.523+0 1.355 1.12+0 5.30-2 3.809-1 0.684 1.23+0 2.48-1 5.327-1 0.676 1.23+0 2.55-1 3.477-1 1.990 3.15-1	1.734+0 1.297 1.26+0 6.50-2 2.292-1 0.617 1.29+0 2.78-1 3.192-1 0.616 1.28+0 2.85-1 2.617-1 1.986 4.46-1	1.237+0 1.242 1.37+0 7.69-2 1.456-1 0.560 1.33+0 3.07-1 2.020-1 0.564 1.32+0 3.14-1 2.028-1 1.981 5.77-1	9.094-1 1.188 1.47+0 8.85-2 9.657-2 0.510 1.36+0 3.35-1 1.335-1 0.520 1.36+0 3.42-1 1.610-1 1.976 7.07-1
$E_b = 496.2 \text{ eV}$ $3d_{3/2}$ $E_b = 311.7 \text{ eV}$ $3d_{5/2}$ $E_b = 307.0 \text{ eV}$ $4s_{1/2}$ $E_b = 81.0 \text{ eV}$	δ σ β γ δ σ β γ δ σ β γ δ σ β γ δ σ β γ δ σ β γ δ σ β γ δ σ β γ δ	9.540+1 1.630 -2.46-2 3.46-3 7.094+1 1.232 3.28-1 6.09-2 1.022+2 1.219 3.36-1 6.14-2 6.709+0 1.988 -1.03-2 -1.10-4	5.398+1 1.647 6.04-2 6.24-3 2.950+1 1.189 5.04-1 7.76-2 4.231+1 1.167 5.08-1 7.91-2 4.007+0 1.990 -7.26-2 -1.30-4	2.209+1 1.607 3.20-1 1.30-2 7.907+0 1.064 7.64-1 1.12-1 1.127+1 1.038 7.61-1 1.15-1 1.891+0 1.993 -9.09-2 -1.55-4	1.104+1 1.544 5.70-1 2.10-2 2.940+0 0.948 9.44-1 1.47-1 4.167+0 0.923 9.36-1 1.52-1 1.086+0 1.995 -3.05-2 -1.69-4	6.248+0 1.479 7.84-1 3.06-2 1.325+0 0.847 1.07+0 1.82-1 1.869+0 0.828 1.06+0 1.88-1 6.966-1 1.995 6.89-2 -1.79-4	3.849+0 1.416 9.68-1 4.14-2 6.786-1 0.760 1.17+0 2.16-1 9.529-1 0.746 1.16+0 2.23-1 4.799-1 1.993 1.87-1 -1.85-4	2.523+0 1.355 1.12+0 5.30-2 3.809-1 0.684 1.23+0 2.48-1 5.327-1 0.676 1.23+0 2.55-1 3.477-1 1.990 3.15-1 -1.88-4	1.734+0 1.297 1.26+0 6.50-2 2.292-1 0.617 1.29+0 2.78-1 3.192-1 0.616 1.28+0 2.85-1 2.617-1 1.986 4.46-1 -1.89-4	1.237+0 1.242 1.37+0 7.69-2 1.456-1 0.560 1.33+0 3.07-1 2.020-1 0.564 1.32+0 3.14-1 2.028-1 1.981 5.77-1 -1.88-4	9.094-1 1.188 1.47+0 8.85-2 9.657-2 0.510 1.36+0 3.35-1 1.335-1 0.520 1.36+0 3.42-1 1.610-1 1.976 7.07-1 -1.88-4
$E_b = 496.2 \text{ eV}$ $3d_{3/2}$ $E_b = 311.7 \text{ eV}$ $3d_{5/2}$ $E_b = 307.0 \text{ eV}$ $4s_{1/2}$ $E_b = 81.0 \text{ eV}$	δ σ β γ δ σ β γ δ σ β γ δ σ β γ δ σ σ β γ δ σ σ σ σ σ σ σ σ σ σ σ σ	9.540+1 1.630 -2.46-2 3.46-3 7.094+1 1.232 3.28-1 6.09-2 1.022+2 1.219 3.36-1 6.14-2 6.709+0 1.988 -1.03-2 -1.10-4 7.069+0	5.398+1 1.647 6.04-2 6.24-3 2.950+1 1.189 5.04-1 7.76-2 4.231+1 1.167 5.08-1 7.91-2 4.007+0 1.990 -7.26-2 -1.30-4 3.991+0	2.209+1 1.607 3.20-1 1.30-2 7.907+0 1.064 7.64-1 1.12-1 1.127+1 1.038 7.61-1 1.15-1 1.891+0 1.993 -9.09-2 -1.55-4 1.661+0	1.104+1 1.544 5.70-1 2.10-2 2.940+0 0.948 9.44-1 1.47-1 4.167+0 0.923 9.36-1 1.52-1 1.086+0 1.995 -3.05-2 -1.69-4 8.464-1	6.248+0 1.479 7.84-1 3.06-2 1.325+0 0.847 1.07+0 1.82-1 1.869+0 0.828 1.06+0 1.88-1 6.966-1 1.995 6.89-2 -1.79-4 4.871-1	3.849+0 1.416 9.68-1 4.14-2 6.786-1 0.760 1.17+0 2.16-1 9.529-1 0.746 1.16+0 2.23-1 4.799-1 1.993 1.87-1 -1.85-4 3.043-1	2.523+0 1.355 1.12+0 5.30-2 3.809-1 0.684 1.23+0 2.48-1 5.327-1 0.676 1.23+0 2.55-1 3.477-1 1.990 3.15-1 -1.88-4 2.019-1	1.734+0 1.297 1.26+0 6.50-2 2.292-1 0.617 1.29+0 2.78-1 3.192-1 0.616 1.28+0 2.85-1 2.617-1 1.986 4.46-1 -1.89-4 1.402-1	1.237+0 1.242 1.37+0 7.69-2 1.456-1 0.560 1.33+0 3.07-1 2.020-1 0.564 1.32+0 3.14-1 2.028-1 1.981 5.77-1 -1.88-4 1.010-1	9.094-1 1.188 1.47+0 8.85-2 9.657-2 0.510 1.36+0 3.35-1 1.335-1 0.520 1.36+0 3.42-1 1.610-1 1.976 7.07-1 -1.88-4 7.489-2
$E_b = 496.2 \text{ eV}$ $3d_{3/2}$ $E_b = 311.7 \text{ eV}$ $3d_{5/2}$ $E_b = 307.0 \text{ eV}$ $4s_{1/2}$ $E_b = 81.0 \text{ eV}$	δ σ β γ δ σ β γ δ σ β γ δ σ β γ δ σ β γ δ σ β γ δ σ β γ δ σ β γ δ	9.540+1 1.630 -2.46-2 3.46-3 7.094+1 1.232 3.28-1 6.09-2 1.022+2 1.219 3.36-1 6.14-2 6.709+0 1.988 -1.03-2 -1.10-4 7.069+0 1.676	5.398+1 1.647 6.04-2 6.24-3 2.950+1 1.189 5.04-1 7.76-2 4.231+1 1.167 5.08-1 7.91-2 4.007+0 1.990 -7.26-2 -1.30-4 3.991+0 1.643	2.209+1 1.607 3.20-1 1.30-2 7.907+0 1.064 7.64-1 1.12-1 1.127+1 1.038 7.61-1 1.15-1 1.891+0 1.993 -9.09-2 -1.55-4 1.661+0 1.563	1.104+1 1.544 5.70-1 2.10-2 2.940+0 0.948 9.44-1 1.47-1 4.167+0 0.923 9.36-1 1.52-1 1.086+0 1.995 -3.05-2 -1.69-4 8.464-1 1.484	6.248+0 1.479 7.84-1 3.06-2 1.325+0 0.847 1.07+0 1.82-1 1.869+0 0.828 1.06+0 1.88-1 6.966-1 1.995 6.89-2 -1.79-4 4.871-1 1.412	3.849+0 1.416 9.68-1 4.14-2 6.786-1 0.760 1.17+0 2.16-1 9.529-1 0.746 1.16+0 2.23-1 4.799-1 1.993 1.87-1 -1.85-4 3.043-1 1.345	2.523+0 1.355 1.12+0 5.30-2 3.809-1 0.684 1.23+0 2.48-1 5.327-1 0.676 1.23+0 2.55-1 3.477-1 1.990 3.15-1 -1.88-4 2.019-1 1.283	1.734+0 1.297 1.26+0 6.50-2 2.292-1 0.617 1.29+0 2.78-1 3.192-1 0.616 1.28+0 2.85-1 1.986 4.46-1 -1.89-4 1.402-1 1.224	1.237+0 1.242 1.37+0 7.69-2 1.456-1 0.560 1.33+0 3.07-1 2.020-1 0.564 1.32+0 3.14-1 2.028-1 1.981 5.77-1 -1.88-4 1.010-1 1.168	9.094-1 1.188 1.47+0 8.85-2 9.657-2 0.510 1.36+0 3.35-1 0.520 1.36+0 3.42-1 1.610-1 1.976 7.07-1 -1.88-4 7.489-2 1.116
$E_b = 496.2 \text{ eV}$ $3d_{3/2}$ $E_b = 311.7 \text{ eV}$ $3d_{5/2}$ $E_b = 307.0 \text{ eV}$ $4s_{1/2}$ $E_b = 81.0 \text{ eV}$	δ σ β γ δ σ β γ δ σ β γ δ σ β γ δ σ β γ δ σ β γ δ σ β γ δ σ σ σ σ σ σ σ σ σ σ σ σ σ	9.540+1 1.630 -2.46-2 3.46-3 7.094+1 1.232 3.28-1 6.09-2 1.022+2 1.219 3.36-1 6.14-2 6.709+0 1.988 -1.03-2 -1.10-4 7.069+0 1.676 1.91-2	5.398+1 1.647 6.04-2 6.24-3 2.950+1 1.189 5.04-1 7.76-2 4.231+1 1.167 5.08-1 7.91-2 4.007+0 1.990 -7.26-2 -1.30-4 3.991+0 1.643 1.23-1	2.209+1 1.607 3.20-1 1.30-2 7.907+0 1.064 7.64-1 1.12-1 1.127+1 1.038 7.61-1 1.15-1 1.891+0 1.993 -9.09-2 -1.55-4 1.661+0 1.563 3.63-1	1.104+1 1.544 5.70-1 2.10-2 2.940+0 0.948 9.44-1 1.47-1 4.167+0 0.923 9.36-1 1.52-1 1.086+0 1.995 -3.05-2 -1.69-4 8.464-1 1.484 5.86-1	6.248+0 1.479 7.84-1 3.06-2 1.325+0 0.847 1.07+0 1.82-1 1.869+0 0.828 1.06+0 1.88-1 6.966-1 1.995 6.89-2 -1.79-4 4.871-1 1.412 7.80-1	3.849+0 1.416 9.68-1 4.14-2 6.786-1 0.760 1.17+0 2.16-1 9.529-1 0.746 1.16+0 2.23-1 4.799-1 1.993 1.87-1 -1.85-4 3.043-1 1.345 9.48-1	2.523+0 1.355 1.12+0 5.30-2 3.809-1 0.684 1.23+0 2.48-1 5.327-1 0.676 1.23+0 2.55-1 3.477-1 1.990 3.15-1 -1.88-4 2.019-1 1.283 1.09+0	1.734+0 1.297 1.26+0 6.50-2 2.292-1 0.617 1.29+0 2.78-1 3.192-1 0.616 1.28+0 2.85-1 2.617-1 1.986 4.46-1 -1.89-4 1.402-1 1.224 1.22+0	1.237+0 1.242 1.37+0 7.69-2 1.456-1 0.560 1.33+0 3.07-1 2.020-1 0.564 1.32+0 3.14-1 2.028-1 1.981 5.77-1 -1.88-4 1.010-1 1.168 1.32+0	9.094-1 1.188 1.47+0 8.85-2 9.657-2 0.510 1.36+0 3.35-1 0.520 1.36+0 3.42-1 1.610-1 1.976 7.07-1 -1.88-4 7.489-2 1.116 1.41+0
$E_b = 496.2 \text{ eV}$ $3d_{3/2}$ $E_b = 311.7 \text{ eV}$ $3d_{5/2}$ $E_b = 307.0 \text{ eV}$ $4s_{1/2}$ $E_b = 81.0 \text{ eV}$ $4p_{1/2}$ $E_b = 51.9 \text{ eV}$	δ σ β γ δ σ β γ δ σ β γ δ σ β γ δ σ β γ δ σ β γ δ σ β γ δ σ β γ δ σ β γ δ σ β γ δ σ β γ δ σ β γ δ σ β γ δ	9.540+1 1.630 -2.46-2 3.46-3 7.094+1 1.232 3.28-1 6.09-2 1.022+2 1.219 3.36-1 6.14-2 6.709+0 1.988 -1.03-2 -1.10-4 7.069+0 1.676 1.91-2 7.12-4	5.398+1 1.647 6.04-2 6.24-3 2.950+1 1.189 5.04-1 7.76-2 4.231+1 1.167 5.08-1 7.91-2 4.007+0 1.990 -7.26-2 -1.30-4 3.991+0 1.643 1.23-1 2.87-3	2.209+1 1.607 3.20-1 1.30-2 7.907+0 1.064 7.64-1 1.12-1 1.127+1 1.038 7.61-1 1.15-1 1.891+0 1.993 -9.09-2 -1.55-4 1.661+0 1.563 3.63-1 9.66-3	1.104+1 1.544 5.70-1 2.10-2 2.940+0 0.948 9.44-1 1.47-1 4.167+0 0.923 9.36-1 1.52-1 1.086+0 1.995 -3.05-2 -1.69-4 8.464-1 1.484 5.86-1 1.89-2	6.248+0 1.479 7.84-1 3.06-2 1.325+0 0.847 1.07+0 1.82-1 1.869+0 0.828 1.06+0 1.88-1 6.966-1 1.995 6.89-2 -1.79-4 4.871-1 1.412 7.80-1 3.00-2	3.849+0 1.416 9.68-1 4.14-2 6.786-1 0.760 1.17+0 2.16-1 9.529-1 0.746 1.16+0 2.23-1 4.799-1 1.993 1.87-1 -1.85-4 3.043-1 1.345 9.48-1 4.24-2	2.523+0 1.355 1.12+0 5.30-2 3.809-1 0.684 1.23+0 2.48-1 5.327-1 0.676 1.23+0 2.55-1 3.477-1 1.990 3.15-1 -1.88-4 2.019-1 1.283 1.09+0 5.55-2	1.734+0 1.297 1.26+0 6.50-2 2.292-1 0.617 1.29+0 2.78-1 3.192-1 0.616 1.28+0 2.85-1 2.617-1 1.986 4.46-1 -1.89-4 1.402-1 1.224 1.22+0 6.88-2	1.237+0 1.242 1.37+0 7.69-2 1.456-1 0.560 1.33+0 3.07-1 2.020-1 0.564 1.32+0 3.14-1 2.028-1 1.981 5.77-1 -1.88-4 1.010-1 1.168 1.32+0 8.20-2	9.094-1 1.188 1.47+0 8.85-2 9.657-2 0.510 1.36+0 3.35-1 0.520 1.36+0 3.42-1 1.610-1 1.976 7.07-1 -1.88-4 7.489-2 1.116 1.41+0 9.51-2
$E_b = 496.2 \text{ eV}$ $3d_{3/2}$ $E_b = 311.7 \text{ eV}$ $3d_{5/2}$ $E_b = 307.0 \text{ eV}$ $4s_{1/2}$ $E_b = 81.0 \text{ eV}$ $4p_{1/2}$ $E_b = 51.9 \text{ eV}$	δ σ β γ δ σ β γ δ σ β γ δ σ β γ δ σ β γ δ σ β γ δ σ σ β γ δ σ σ β γ δ σ σ σ σ σ σ σ σ σ σ σ σ σ σ σ σ σ σ	9.540+1 1.630 -2.46-2 3.46-3 7.094+1 1.232 3.28-1 6.09-2 1.022+2 1.219 3.36-1 6.14-2 6.709+0 1.988 -1.03-2 -1.10-4 7.069+0 1.676 1.91-2 7.12-4 1.382+1	5.398+1 1.647 6.04-2 6.24-3 2.950+1 1.189 5.04-1 7.76-2 4.231+1 1.167 5.08-1 7.91-2 4.007+0 1.990 -7.26-2 -1.30-4 3.991+0 1.643 1.23-1 2.87-3 7.664+0	2.209+1 1.607 3.20-1 1.30-2 7.907+0 1.064 7.64-1 1.12-1 1.127+1 1.038 7.61-1 1.15-1 1.891+0 1.993 -9.09-2 -1.55-4 1.661+0 1.563 3.63-1 9.66-3 3.111+0	1.104+1 1.544 5.70-1 2.10-2 2.940+0 0.948 9.44-1 1.47-1 4.167+0 0.923 9.36-1 1.52-1 1.086+0 1.995 -3.05-2 -1.69-4 8.464-1 1.484 5.86-1 1.89-2 1.558+0	6.248+0 1.479 7.84-1 3.06-2 1.325+0 0.847 1.07+0 1.82-1 1.869+0 0.828 1.06+0 1.88-1 6.966-1 1.995 6.89-2 -1.79-4 4.871-1 1.412 7.80-1 3.00-2 8.846-1	3.849+0 1.416 9.68-1 4.14-2 6.786-1 0.760 1.17+0 2.16-1 9.529-1 0.746 1.16+0 2.23-1 4.799-1 1.993 1.87-1 -1.85-4 3.043-1 1.345 9.48-1 4.24-2 5.465-1	2.523+0 1.355 1.12+0 5.30-2 3.809-1 0.684 1.23+0 2.48-1 5.327-1 0.676 1.23+0 2.55-1 3.477-1 1.990 3.15-1 -1.88-4 2.019-1 1.283 1.09+0 5.55-2 3.590-1	1.734+0 1.297 1.26+0 6.50-2 2.292-1 0.617 1.29+0 2.78-1 3.192-1 0.616 1.28+0 2.85-1 2.617-1 1.986 4.46-1 -1.89-4 1.402-1 1.224 1.22+0 6.88-2 2.472-1	1.237+0 1.242 1.37+0 7.69-2 1.456-1 0.560 1.33+0 3.07-1 2.020-1 0.564 1.32+0 3.14-1 2.028-1 1.981 5.77-1 -1.88-4 1.010-1 1.168 1.32+0 8.20-2 1.767-1	9.094-1 1.188 1.47+0 8.85-2 9.657-2 0.510 1.36+0 3.35-1 0.520 1.36+0 3.42-1 1.610-1 1.976 7.07-1 -1.88-4 7.489-2 1.116 1.41+0 9.51-2 1.301-1
$E_b = 496.2 \text{ eV}$ $3d_{3/2}$ $E_b = 311.7 \text{ eV}$ $3d_{5/2}$ $E_b = 307.0 \text{ eV}$ $4s_{1/2}$ $E_b = 81.0 \text{ eV}$ $4p_{1/2}$ $E_b = 51.9 \text{ eV}$	δ σ β γ δ σ β γ δ σ β γ δ σ β γ δ σ β γ δ σ β γ δ σ β γ δ σ β γ δ σ β γ δ σ β γ δ	9.540+1 1.630 -2.46-2 3.46-3 7.094+1 1.232 3.28-1 6.09-2 1.022+2 1.219 3.36-1 6.14-2 6.709+0 1.988 -1.03-2 -1.10-4 7.069+0 1.676 1.91-2 7.12-4 1.382+1 1.702	5.398+1 1.647 6.04-2 6.24-3 2.950+1 1.189 5.04-1 7.76-2 4.231+1 1.167 5.08-1 7.91-2 4.007+0 1.990 -7.26-2 -1.30-4 3.991+0 1.643 1.23-1 2.87-3 7.664+0 1.678	2.209+1 1.607 3.20-1 1.30-2 7.907+0 1.064 7.64-1 1.12-1 1.127+1 1.038 7.61-1 1.15-1 1.891+0 1.993 -9.09-2 -1.55-4 1.661+0 1.563 3.63-1 9.66-3 3.111+0 1.609	1.104+1 1.544 5.70-1 2.10-2 2.940+0 0.948 9.44-1 1.47-1 4.167+0 0.923 9.36-1 1.52-1 1.086+0 1.995 -3.05-2 -1.69-4 8.464-1 1.484 5.86-1 1.89-2 1.558+0 1.536	6.248+0 1.479 7.84-1 3.06-2 1.325+0 0.847 1.07+0 1.82-1 1.869+0 0.828 1.06+0 1.88-1 6.966-1 1.995 6.89-2 -1.79-4 4.871-1 1.412 7.80-1 3.00-2 8.846-1 1.467	3.849+0 1.416 9.68-1 4.14-2 6.786-1 0.760 1.17+0 2.16-1 9.529-1 0.746 1.16+0 2.23-1 4.799-1 1.993 1.87-1 -1.85-4 3.043-1 1.345 9.48-1 4.24-2 5.465-1 1.402	2.523+0 1.355 1.12+0 5.30-2 3.809-1 0.684 1.23+0 2.48-1 5.327-1 0.676 1.23+0 2.55-1 3.477-1 1.990 3.15-1 -1.88-4 2.019-1 1.283 1.09+0 5.55-2 3.590-1 1.341	1.734+0 1.297 1.26+0 6.50-2 2.292-1 0.617 1.29+0 2.78-1 3.192-1 0.616 1.28+0 2.85-1 2.617-1 1.986 4.46-1 -1.89-4 1.402-1 1.224 1.22+0 6.88-2 2.472-1 1.283	1.237+0 1.242 1.37+0 7.69-2 1.456-1 0.560 1.33+0 3.07-1 2.020-1 0.564 1.32+0 3.14-1 2.028-1 1.981 5.77-1 -1.88-4 1.010-1 1.168 1.32+0 8.20-2 1.767-1 1.228	9.094-1 1.188 1.47+0 8.85-2 9.657-2 0.510 1.36+0 3.35-1 1.335-1 0.520 1.36+0 3.42-1 1.610-1 1.976 7.07-1 -1.88-4 7.489-2 1.116 1.41+0 9.51-2 1.301-1 1.175
$E_b = 496.2 \text{ eV}$ $3d_{3/2}$ $E_b = 311.7 \text{ eV}$ $3d_{5/2}$ $E_b = 307.0 \text{ eV}$ $4s_{1/2}$ $E_b = 81.0 \text{ eV}$ $4p_{1/2}$ $E_b = 51.9 \text{ eV}$	δ σ β γ δ σ β γ δ σ β γ δ σ β γ δ σ β γ δ σ β γ δ σ β γ δ σ β γ δ σ β γ δ σ β γ δ σ β γ γ δ σ σ β γ γ δ σ β γ γ δ σ σ β γ γ δ σ σ β γ γ δ σ σ β γ γ δ σ σ β γ γ δ σ σ β γ γ δ σ σ β γ γ δ σ σ β γ γ δ σ σ β γ γ δ σ σ β γ γ δ σ σ β γ γ σ σ σ σ β γ γ σ σ σ σ σ σ σ σ	9.540+1 1.630 -2.46-2 3.46-3 7.094+1 1.232 3.28-1 6.09-2 1.022+2 1.219 3.36-1 6.14-2 6.709+0 1.988 -1.03-2 -1.10-4 7.069+0 1.676 1.91-2 7.12-4 1.382+1 1.702 2.25-2	5.398+1 1.647 6.04-2 6.24-3 2.950+1 1.189 5.04-1 7.76-2 4.231+1 1.167 5.08-1 7.91-2 4.007+0 1.990 -7.26-2 -1.30-4 3.991+0 1.643 1.23-1 2.87-3 7.664+0 1.678 1.33-1	2.209+1 1.607 3.20-1 1.30-2 7.907+0 1.064 7.64-1 1.12-1 1.127+1 1.038 7.61-1 1.15-1 1.891+0 1.993 -9.09-2 -1.55-4 1.661+0 1.563 3.63-1 9.66-3 3.111+0 1.609 3.84-1	1.104+1 1.544 5.70-1 2.10-2 2.940+0 0.948 9.44-1 1.47-1 4.167+0 0.923 9.36-1 1.52-1 1.086+0 1.995 -3.05-2 -1.69-4 8.464-1 1.484 5.86-1 1.89-2 1.558+0 1.536 6.17-1	6.248+0 1.479 7.84-1 3.06-2 1.325+0 0.847 1.07+0 1.82-1 1.869+0 0.828 1.06+0 1.88-1 6.966-1 1.995 6.89-2 -1.79-4 4.871-1 1.412 7.80-1 3.00-2 8.846-1 1.467 8.20-1	3.849+0 1.416 9.68-1 4.14-2 6.786-1 0.760 1.17+0 2.16-1 9.529-1 0.746 1.16+0 2.23-1 4.799-1 1.993 1.87-1 -1.85-4 3.043-1 1.345 9.48-1 4.24-2 5.465-1 1.402 9.95-1	2.523+0 1.355 1.12+0 5.30-2 3.809-1 0.684 1.23+0 2.48-1 5.327-1 0.676 1.23+0 2.55-1 3.477-1 1.990 3.15-1 -1.88-4 2.019-1 1.283 1.09+0 5.55-2 3.590-1 1.341 1.14+0	1.734+0 1.297 1.26+0 6.50-2 2.292-1 0.617 1.29+0 2.78-1 3.192-1 0.616 1.28+0 2.85-1 2.617-1 1.986 4.46-1 -1.89-4 1.402-1 1.224 1.22+0 6.88-2 2.472-1 1.283 1.27+0	1.237+0 1.242 1.37+0 7.69-2 1.456-1 0.560 1.33+0 3.07-1 2.020-1 0.564 1.32+0 3.14-1 2.028-1 1.981 5.77-1 -1.88-4 1.010-1 1.168 1.32+0 8.20-2 1.767-1 1.228 1.38+0	9.094-1 1.188 1.47+0 8.85-2 9.657-2 0.510 1.36+0 3.35-1 1.335-1 0.520 1.36+0 3.42-1 1.610-1 1.976 7.07-1 -1.88-4 7.489-2 1.116 1.41+0 9.51-2 1.301-1 1.175 1.48+0
$E_b = 496.2 \text{ eV}$ $3d_{3/2} E_b = 311.7 \text{ eV}$ $3d_{5/2} E_b = 307.0 \text{ eV}$ $4s_{1/2} E_b = 81.0 \text{ eV}$ $4p_{1/2} E_b = 51.9 \text{ eV}$ $4p_{3/2} E_b = 46.3 \text{ eV}$	δ σ β γ δ σ β γ δ σ β γ δ σ β γ δ σ β γ δ σ β γ δ σ β γ δ σ β γ δ σ β γ δ σ β γ δ	9.540+1 1.630 -2.46-2 3.46-3 7.094+1 1.232 3.28-1 6.09-2 1.022+2 1.219 3.36-1 6.14-2 6.709+0 1.988 -1.03-2 -1.10-4 7.069+0 1.676 1.91-2 7.12-4 1.382+1 1.702 2.25-2 3.06-3	5.398+1 1.647 6.04-2 6.24-3 2.950+1 1.189 5.04-1 7.76-2 4.231+1 1.167 5.08-1 7.91-2 4.007+0 1.990 -7.26-2 -1.30-4 3.991+0 1.643 1.23-1 2.87-3 7.664+0 1.678 1.33-1 5.49-3	2.209+1 1.607 3.20-1 1.30-2 7.907+0 1.064 7.64-1 1.12-1 1.127+1 1.038 7.61-1 1.15-1 1.891+0 1.993 -9.09-2 -1.55-4 1.661+0 1.563 3.63-1 9.66-3 3.111+0 1.609 3.84-1 1.17-2	1.104+1 1.544 5.70-1 2.10-2 2.940+0 0.948 9.44-1 1.47-1 4.167+0 0.923 9.36-1 1.52-1 1.086+0 1.995 -3.05-2 -1.69-4 8.464-1 1.484 5.86-1 1.89-2 1.558+0 1.536 6.17-1 1.98-2	6.248+0 1.479 7.84-1 3.06-2 1.325+0 0.847 1.07+0 1.82-1 1.869+0 0.828 1.06+0 1.88-1 6.966-1 1.995 6.89-2 -1.79-4 4.871-1 1.412 7.80-1 3.00-2 8.846-1 1.467 8.20-1 2.95-2	3.849+0 1.416 9.68-1 4.14-2 6.786-1 0.760 1.17+0 2.16-1 9.529-1 0.746 1.16+0 2.23-1 4.799-1 1.993 1.87-1 -1.85-4 3.043-1 1.345 9.48-1 4.24-2 5.465-1 1.402 9.95-1 4.06-2	2.523+0 1.355 1.12+0 5.30-2 3.809-1 0.684 1.23+0 2.48-1 5.327-1 0.676 1.23+0 2.55-1 3.477-1 1.990 3.15-1 -1.88-4 2.019-1 1.283 1.09+0 5.55-2 3.590-1 1.341 1.14+0 5.23-2	1.734+0 1.297 1.26+0 6.50-2 2.292-1 0.617 1.29+0 2.78-1 3.192-1 0.616 1.28+0 2.85-1 2.617-1 1.986 4.46-1 -1.89-4 1.402-1 1.224 1.22+0 6.88-2 2.472-1 1.283 1.27+0 6.45-2	1.237+0 1.242 1.37+0 7.69-2 1.456-1 0.560 1.33+0 3.07-1 2.020-1 0.564 1.32+0 3.14-1 2.028-1 1.981 5.77-1 -1.88-4 1.010-1 1.168 1.32+0 8.20-2 1.767-1 1.228 1.38+0 7.66-2	9.094-1 1.188 1.47+0 8.85-2 9.657-2 0.510 1.36+0 3.35-1 1.335-1 0.520 1.36+0 3.42-1 1.610-1 1.976 7.07-1 -1.88-4 7.489-2 1.116 1.41+0 9.51-2 1.301-1 1.175 1.48+0 8.86-2
$E_b = 496.2 \text{ eV}$ $3d_{3/2}$ $E_b = 311.7 \text{ eV}$ $3d_{5/2}$ $E_b = 307.0 \text{ eV}$ $4s_{1/2}$ $E_b = 81.0 \text{ eV}$ $4p_{1/2}$ $E_b = 51.9 \text{ eV}$ $4p_{3/2}$ $E_b = 46.3 \text{ eV}$	δ σ β γ δ σ β γ δ σ β γ δ σ β γ δ σ β γ δ σ β γ δ σ β γ δ σ β γ δ σ β γ δ σ σ β γ δ σ σ β γ δ σ σ σ σ σ σ σ σ σ σ σ σ σ σ σ σ σ σ	9.540+1 1.630 -2.46-2 3.46-3 7.094+1 1.232 3.28-1 6.09-2 1.022+2 1.219 3.36-1 6.14-2 6.709+0 1.988 -1.03-2 -1.10-4 7.069+0 1.676 1.91-2 7.12-4 1.382+1 1.702 2.25-2 3.06-3 5.196+0	5.398+1 1.647 6.04-2 6.24-3 2.950+1 1.189 5.04-1 7.76-2 4.231+1 1.167 5.08-1 7.91-2 4.007+0 1.990 -7.26-2 -1.30-4 3.991+0 1.643 1.23-1 2.87-3 7.664+0 1.678 1.33-1 5.49-3 2.257+0	2.209+1 1.607 3.20-1 1.30-2 7.907+0 1.064 7.64-1 1.12-1 1.127+1 1.038 7.61-1 1.15-1 1.891+0 1.993 -9.09-2 -1.55-4 1.661+0 1.563 3.63-1 9.66-3 3.111+0 1.609 3.84-1 1.17-2 6.368-1	1.104+1 1.544 5.70-1 2.10-2 2.940+0 0.948 9.44-1 1.47-1 4.167+0 0.923 9.36-1 1.52-1 1.086+0 1.995 -3.05-2 -1.69-4 8.464-1 1.484 5.86-1 1.89-2 1.558+0 1.536 6.17-1 1.98-2 2.433-1	6.248+0 1.479 7.84-1 3.06-2 1.325+0 0.847 1.07+0 1.82-1 1.869+0 0.828 1.06+0 1.88-1 6.966-1 1.995 6.89-2 -1.79-4 4.871-1 1.412 7.80-1 3.00-2 8.846-1 1.467 8.20-1 2.95-2 1.114-1	3.849+0 1.416 9.68-1 4.14-2 6.786-1 0.760 1.17+0 2.16-1 9.529-1 0.746 1.16+0 2.23-1 4.799-1 1.993 1.87-1 -1.85-4 3.043-1 1.345 9.48-1 4.24-2 5.465-1 1.402 9.95-1 4.06-2 5.767-2	2.523+0 1.355 1.12+0 5.30-2 3.809-1 0.684 1.23+0 2.48-1 5.327-1 0.676 1.23+0 2.55-1 3.477-1 1.990 3.15-1 -1.88-4 2.019-1 1.283 1.09+0 5.55-2 3.590-1 1.341 1.14+0 5.23-2 3.261-2	1.734+0 1.297 1.26+0 6.50-2 2.292-1 0.617 1.29+0 2.78-1 3.192-1 0.616 1.28+0 2.85-1 2.617-1 1.986 4.46-1 -1.89-4 1.402-1 1.224 1.22+0 6.88-2 2.472-1 1.283 1.27+0 6.45-2 1.972-2	1.237+0 1.242 1.37+0 7.69-2 1.456-1 0.560 1.33+0 3.07-1 2.020-1 0.564 1.32+0 3.14-1 2.028-1 1.981 5.77-1 -1.88-4 1.010-1 1.168 1.32+0 8.20-2 1.767-1 1.228 1.38+0 7.66-2 1.257-2	9.094-1 1.188 1.47+0 8.85-2 9.657-2 0.510 1.36+0 3.35-1 1.335-1 0.520 1.36+0 3.42-1 1.610-1 1.976 7.07-1 -1.88-4 7.489-2 1.116 1.41+0 9.51-2 1.301-1 1.175 1.48+0 8.86-2 8.367-3
$E_b = 496.2 \text{ eV}$ $3d_{3/2}$ $E_b = 311.7 \text{ eV}$ $3d_{5/2}$ $E_b = 307.0 \text{ eV}$ $4s_{1/2}$ $E_b = 81.0 \text{ eV}$ $4p_{1/2}$ $E_b = 51.9 \text{ eV}$ $4p_{3/2}$ $E_b = 46.3 \text{ eV}$	δ σ β γ δ δ σ β γ δ δ σ β γ δ δ σ β γ δ δ σ β γ δ δ σ β γ δ δ σ β γ δ δ σ β γ δ δ σ β γ δ δ σ β γ δ δ σ β γ δ δ σ β γ δ δ σ β γ δ δ σ β γ δ δ σ δ ρ γ δ δ σ δ ρ γ δ δ σ δ ρ γ δ δ σ δ ρ γ δ δ σ δ ρ γ δ δ σ δ ρ γ δ δ σ δ ρ γ δ δ σ δ ρ γ δ δ σ δ ρ γ δ δ σ δ ρ γ δ δ σ δ ρ γ δ δ σ δ ρ γ δ δ σ δ ρ γ δ δ σ δ σ δ ρ γ δ δ σ δ σ δ ρ γ δ δ σ δ σ δ ρ γ δ δ σ δ σ δ ρ γ δ δ σ δ σ δ σ δ σ δ σ δ σ δ σ δ σ δ σ	9.540+1 1.630 -2.46-2 3.46-3 7.094+1 1.232 3.28-1 6.09-2 1.022+2 1.219 3.36-1 6.14-2 6.709+0 1.988 -1.03-2 -1.10-4 7.069+0 1.676 1.91-2 7.12-4 1.382+1 1.702 2.25-2 3.06-3 5.196+0 1.269	5.398+1 1.647 6.04-2 6.24-3 2.950+1 1.189 5.04-1 7.76-2 4.231+1 1.167 5.08-1 7.91-2 4.007+0 1.990 -7.26-2 -1.30-4 3.991+0 1.643 1.23-1 2.87-3 7.664+0 1.678 1.33-1 5.49-3 2.257+0 1.192	2.209+1 1.607 3.20-1 1.30-2 7.907+0 1.064 7.64-1 1.12-1 1.127+1 1.038 7.61-1 1.15-1 1.891+0 1.993 -9.09-2 -1.55-4 1.661+0 1.563 3.63-1 9.66-3 3.111+0 1.609 3.84-1 1.17-2 6.368-1 1.047	1.104+1 1.544 5.70-1 2.10-2 2.940+0 0.948 9.44-1 1.47-1 4.167+0 0.923 9.36-1 1.52-1 1.086+0 1.995 -3.05-2 -1.69-4 8.464-1 1.484 5.86-1 1.89-2 1.558+0 1.536 6.17-1 1.98-2 2.433-1 0.927	6.248+0 1.479 7.84-1 3.06-2 1.325+0 0.847 1.07+0 1.82-1 1.869+0 0.828 1.06+0 1.88-1 6.966-1 1.995 6.89-2 -1.79-4 4.871-1 1.412 7.80-1 3.00-2 8.846-1 1.467 8.20-1 2.95-2 1.114-1 0.828	3.849+0 1.416 9.68-1 4.14-2 6.786-1 0.760 1.17+0 2.16-1 9.529-1 0.746 1.16+0 2.23-1 4.799-1 1.993 1.87-1 -1.85-4 3.043-1 1.345 9.48-1 4.24-2 5.465-1 1.402 9.95-1 4.06-2 5.767-2 0.744	2.523+0 1.355 1.12+0 5.30-2 3.809-1 0.684 1.23+0 2.48-1 5.327-1 0.676 1.23+0 2.55-1 3.477-1 1.990 3.15-1 -1.88-4 2.019-1 1.283 1.09+0 5.55-2 3.590-1 1.341 1.14+0 5.23-2 3.261-2 0.671	1.734+0 1.297 1.26+0 6.50-2 2.292-1 0.617 1.29+0 2.78-1 3.192-1 0.616 1.28+0 2.85-1 2.617-1 1.986 4.46-1 -1.89-4 1.402-1 1.224 1.22+0 6.88-2 2.472-1 1.283 1.27+0 6.45-2 1.972-2 0.606	1.237+0 1.242 1.37+0 7.69-2 1.456-1 0.560 1.33+0 3.07-1 2.020-1 0.564 1.32+0 3.14-1 2.028-1 1.981 5.77-1 -1.88-4 1.010-1 1.168 1.32+0 8.20-2 1.767-1 1.228 1.38+0 7.66-2 1.257-2 0.548	9.094-1 1.188 1.47+0 8.85-2 9.657-2 0.510 1.36+0 3.35-1 1.335-1 0.520 1.36+0 3.42-1 1.610-1 1.976 7.07-1 -1.88-4 7.489-2 1.116 1.41+0 9.51-2 1.301-1 1.175 1.48+0 8.86-2 8.367-3 0.497
$E_b = 496.2 \text{ eV}$ $3d_{3/2} E_b = 311.7 \text{ eV}$ $3d_{5/2} E_b = 307.0 \text{ eV}$ $4s_{1/2} E_b = 81.0 \text{ eV}$ $4p_{1/2} E_b = 51.9 \text{ eV}$ $4p_{3/2} E_b = 46.3 \text{ eV}$	δ σ β γ δ	9.540+1 1.630 -2.46-2 3.46-3 7.094+1 1.232 3.28-1 6.09-2 1.022+2 1.219 3.36-1 6.14-2 6.709+0 1.988 -1.03-2 -1.10-4 7.069+0 1.676 1.91-2 7.12-4 1.382+1 1.702 2.25-2 3.06-3 5.196+0 1.269 3.79-1	5.398+1 1.647 6.04-2 6.24-3 2.950+1 1.189 5.04-1 7.76-2 4.231+1 1.167 5.08-1 7.91-2 4.007+0 1.990 -7.26-2 -1.30-4 3.991+0 1.643 1.23-1 2.87-3 7.664+0 1.678 1.33-1 5.49-3 2.257+0 1.192 5.34-1	2.209+1 1.607 3.20-1 1.30-2 7.907+0 1.064 7.64-1 1.12-1 1.127+1 1.038 7.61-1 1.15-1 1.891+0 1.993 -9.09-2 -1.55-4 1.661+0 1.563 3.63-1 9.66-3 3.111+0 1.609 3.84-1 1.17-2 6.368-1 1.047 7.72-1	1.104+1 1.544 5.70-1 2.10-2 2.940+0 0.948 9.44-1 1.47-1 4.167+0 0.923 9.36-1 1.52-1 1.086+0 1.995 -3.05-2 -1.69-4 8.464-1 1.484 5.86-1 1.89-2 1.558+0 1.536 6.17-1 1.98-2 2.433-1 0.927 9.44-1	6.248+0 1.479 7.84-1 3.06-2 1.325+0 0.847 1.07+0 1.82-1 1.869+0 0.828 1.06+0 1.88-1 6.966-1 1.995 6.89-2 -1.79-4 4.871-1 1.412 7.80-1 3.00-2 8.846-1 1.467 8.20-1 2.95-2 1.114-1 0.828 1.07+0	3.849+0 1.416 9.68-1 4.14-2 6.786-1 0.760 1.17+0 2.16-1 9.529-1 0.746 1.16+0 2.23-1 4.799-1 1.993 1.87-1 -1.85-4 3.043-1 1.345 9.48-1 4.24-2 5.465-1 1.402 9.95-1 4.06-2 5.767-2 0.744 1.16+0	2.523+0 1.355 1.12+0 5.30-2 3.809-1 0.684 1.23+0 2.48-1 5.327-1 0.676 1.23+0 2.55-1 3.477-1 1.990 3.15-1 -1.88-4 2.019-1 1.283 1.09+0 5.55-2 3.590-1 1.341 1.14+0 5.23-2 3.261-2 0.671 1.23+0	1.734+0 1.297 1.26+0 6.50-2 2.292-1 0.617 1.29+0 2.78-1 3.192-1 0.616 1.28+0 2.85-1 2.617-1 1.986 4.46-1 -1.89-4 1.402-1 1.224 1.22+0 6.88-2 2.472-1 1.283 1.27+0 6.45-2 1.972-2 0.606 1.28+0	1.237+0 1.242 1.37+0 7.69-2 1.456-1 0.560 1.33+0 3.07-1 2.020-1 0.564 1.32+0 3.14-1 2.028-1 1.981 5.77-1 -1.88-4 1.010-1 1.168 1.32+0 8.20-2 1.767-1 1.228 1.38+0 7.66-2 1.257-2 0.548 1.32+0	9.094-1 1.188 1.47+0 8.85-2 9.657-2 0.510 1.36+0 3.35-1 1.335-1 0.520 1.36+0 3.42-1 1.610-1 1.976 7.07-1 -1.88-4 7.489-2 1.116 1.41+0 9.51-2 1.301-1 1.175 1.48+0 8.86-2 8.367-3 0.497 1.35+0
$E_b = 496.2 \text{ eV}$ $3d_{3/2}$ $E_b = 311.7 \text{ eV}$ $3d_{5/2}$ $E_b = 307.0 \text{ eV}$ $4s_{1/2}$ $E_b = 81.0 \text{ eV}$ $4p_{1/2}$ $E_b = 51.9 \text{ eV}$ $4p_{3/2}$ $E_b = 46.3 \text{ eV}$	δ σ β γ δ σ β γ δ σ β γ δ σ β γ δ σ β γ δ σ β γ δ σ β γ δ σ β γ δ σ β γ δ σ β γ δ σ β γ δ σ β γ δ	9.540+1 1.630 -2.46-2 3.46-3 7.094+1 1.232 3.28-1 6.09-2 1.022+2 1.219 3.36-1 6.14-2 6.709+0 1.988 -1.03-2 -1.10-4 7.069+0 1.676 1.91-2 7.12-4 1.382+1 1.702 2.25-2 3.06-3 5.196+0 1.269	5.398+1 1.647 6.04-2 6.24-3 2.950+1 1.189 5.04-1 7.76-2 4.231+1 1.167 5.08-1 7.91-2 4.007+0 1.990 -7.26-2 -1.30-4 3.991+0 1.643 1.23-1 2.87-3 7.664+0 1.678 1.33-1 5.49-3 2.257+0 1.192	2.209+1 1.607 3.20-1 1.30-2 7.907+0 1.064 7.64-1 1.12-1 1.127+1 1.038 7.61-1 1.15-1 1.891+0 1.993 -9.09-2 -1.55-4 1.661+0 1.563 3.63-1 9.66-3 3.111+0 1.609 3.84-1 1.17-2 6.368-1 1.047	1.104+1 1.544 5.70-1 2.10-2 2.940+0 0.948 9.44-1 1.47-1 4.167+0 0.923 9.36-1 1.52-1 1.086+0 1.995 -3.05-2 -1.69-4 8.464-1 1.484 5.86-1 1.89-2 1.558+0 1.536 6.17-1 1.98-2 2.433-1 0.927	6.248+0 1.479 7.84-1 3.06-2 1.325+0 0.847 1.07+0 1.82-1 1.869+0 0.828 1.06+0 1.88-1 6.966-1 1.995 6.89-2 -1.79-4 4.871-1 1.412 7.80-1 3.00-2 8.846-1 1.467 8.20-1 2.95-2 1.114-1 0.828	3.849+0 1.416 9.68-1 4.14-2 6.786-1 0.760 1.17+0 2.16-1 9.529-1 0.746 1.16+0 2.23-1 4.799-1 1.993 1.87-1 -1.85-4 3.043-1 1.345 9.48-1 4.24-2 5.465-1 1.402 9.95-1 4.06-2 5.767-2 0.744	2.523+0 1.355 1.12+0 5.30-2 3.809-1 0.684 1.23+0 2.48-1 5.327-1 0.676 1.23+0 2.55-1 3.477-1 1.990 3.15-1 -1.88-4 2.019-1 1.283 1.09+0 5.55-2 3.590-1 1.341 1.14+0 5.23-2 3.261-2 0.671	1.734+0 1.297 1.26+0 6.50-2 2.292-1 0.617 1.29+0 2.78-1 3.192-1 0.616 1.28+0 2.85-1 2.617-1 1.986 4.46-1 -1.89-4 1.402-1 1.224 1.22+0 6.88-2 2.472-1 1.283 1.27+0 6.45-2 1.972-2 0.606	1.237+0 1.242 1.37+0 7.69-2 1.456-1 0.560 1.33+0 3.07-1 2.020-1 0.564 1.32+0 3.14-1 2.028-1 1.981 5.77-1 -1.88-4 1.010-1 1.168 1.32+0 8.20-2 1.767-1 1.228 1.38+0 7.66-2 1.257-2 0.548	9.094-1 1.188 1.47+0 8.85-2 9.657-2 0.510 1.36+0 3.35-1 1.335-1 0.520 1.36+0 3.42-1 1.610-1 1.976 7.07-1 -1.88-4 7.489-2 1.116 1.41+0 9.51-2 1.301-1 1.175 1.48+0 8.86-2 8.367-3 0.497

Table 1 (contin	ued)										
$E_b =$	β	1.248	1.165	1.019	0.902	0.808	0.731	0.664	0.605	0.554	0.509
2.2 eV	$\gamma \over \delta$	3.84-1 5.56-2	5.35-1 7.42-2	7.67-1 1.12-1	9.35-1 1.50-1	1.06+0 1.86-1	1.15+0 2.22-1	1.22+0 2.55-1	1.28+0 2.85-1	1.32+0 3.14-1	1.35+0 3.42-1
	σ	3.702-1	2.192-1	1.025-1	5.865-2	3.755-2	2.583-2	1.870-2	1.405-2	1.088-2	8.628-3
$E_b =$	β	1.988	1.990	1.994	1.995	1.995	1.993	1.990	1.986	1.981	1.976
7.0 eV	$\gamma \delta$	-1.95-2 $-1.09-4$	-7.66-2 $-1.28-4$	-8.91-2 $-1.53-4$	-2.65-2 $-1.66-4$	7.36-2 $-1.75-4$	1.94 - 1 $-1.81 - 4$	3.23-1 -1.86-4	4.54 - 1 $-1.88 - 4$	5.83-1 -1.89-4	7.09-1 $-1.89-4$
Z= 46, Pd: [K	(r]4d _{3/2}										
	3,2	k (eV)									
Shell		1500	2000	3000	4000	5000	6000	7000	8000	9000	10000
3s _{1/2}	σ	3.721+1	2.331+1	1.144+1	6.696+0	4.343+0	3.014+0	2.195+0	1.659+0	1.290+0	1.027+0
$E_b = 669.9 \text{ eV}$	$eta \ \gamma$	1.981 1.74-1	1.984 1.51-2	1.990 -9.87-2	1.994 -8.11-2	1.995 -3.18-3	1.994 1.05-1	1.992 2.26-1	1.989 3.52-1	1.984 4.80-1	1.979 6.08-1
	δ	-1.13-4	-1.48-4	-1.80-4	-1.99-4	-2.12-4	-2.20-4	-2.25-4	-2.27-4	-2.28-4	-2.27-4
$\begin{array}{l} 3p_{1/2} \\ E_b = \end{array}$	$\frac{\sigma}{eta}$	5.090+1 1.596	2.978+1 1.613	1.269+1 1.571	6.515+0 1.506	3.762+0 1.438	2.355+0 1.372	1.565+0 1.312	1.088+0 1.256	7.848-1 1.204	5.827-1 1.153
559.1 eV	γ	-2.34-2	3.15-2	2.65-1	5.05-1	7.14-1	8.92-1	1.04+0	1.18+0	1.204	1.39+0
	δ	1.40-3	2.90-3	9.46-3	1.85-2	2.89-2	4.00-2	5.18-2	6.45-2	7.78-2	9.09-2
$3p_{3/2}$ $E_b =$	$\frac{\sigma}{eta}$	1.013+2 1.622	5.784+1 1.648	2.391+1 1.617	1.204+1 1.559	6.850+0 1.495	4.236+0 1.431	2.785+0 1.372	1.920+0 1.318	1.373+0 1.266	1.012+0 1.216
531.5 eV	γ	-2.96-2	3.88 - 2	2.87 - 1	5.38 - 1	7.57 - 1	9.43 - 1	1.10+0	1.24+0	1.36+0	1.46+0
	δ	3.30-3	5.81-3	1.22-2	2.02-2	2.92-2	3.88-2	4.92-2	6.06-2	7.26-2	8.45-2
$3d_{3/2} E_b =$	$\frac{\sigma}{eta}$	8.068+1 1.234	3.379+1 1.201	9.151+0 1.084	3.426+0 0.966	1.553+0 0.865	7.988-1 0.780	4.501-1 0.708	2.716-1 0.642	1.729-1 0.583	1.149-1 0.529
340.0 eV	γ	3.04-1	4.83-1	7.52 - 1	9.37-1	1.07+0	1.17+0	1.24+0	1.30+0	1.34+0	1.38+0
3d _{5/2}	$\frac{\delta}{\sigma}$	5.94-2 1.164+2	7.63-2 4.853+1	1.10-1 1.306+1	1.43-1 4.861+0	1.76-1 2.192+0	2.09-1 1.123+0	2.42-1 6.299-1	2.72-1 3.786-1	3.01-1 2.401-1	3.28-1 1.590-1
$E_b =$	β	1.223	1.180	1.057	0.940	0.843	0.764	0.299-1	0.638	0.585	0.537
334.7 eV	$_{\delta}^{\gamma}$	3.13-1 5.98-2	4.89-1 7.77-2	7.50-1 1.13-1	9.29 - 1 $1.48 - 1$	1.06+0 1.83-1	1.16+0 2.17-1	1.23+0 2.49-1	1.29+0 2.80-1	1.34+0 3.08-1	1.37+0 3.35-1
4s _{1/2}	σ	7.197+0	4.300+0	2.032+0	1.170+0	7.523-1	5.192-1	3.767-1	2.839-1	2.203-1	1.751-1
$E_b =$	β	1.987	1.989	1.993	1.994	1.995	1.993	1.991	1.987	1.983	1.977
86.4 eV	δ	2.16-3 $-1.18-4$	-6.53-2 $-1.40-4$	-9.52-2 $-1.69-4$	-4.58-2 $-1.87-4$	4.54-2 $-1.99-4$	1.58 - 1 $-2.07 - 4$	2.80-1 $-2.12-4$	4.06-1 $-2.15-4$	5.33-1 -2.14-4	6.59 - 1 $-2.14 - 4$
$-4p_{1/2}$	σ	7.691+0	4.365+0	1.833+0	9.414-1	5.448-1	3.418-1	2.277-1	1.587-1	1.146-1	8.523-2
$E_b = 54.4 \text{ eV}$	β	1.681 8.06-3	1.650 1.03-1	1.575 3.36-1	1.499 5.60-1	1.426 7.57-1	1.359 9.24-1	1.298 1.07+0	1.242 1.20+0	1.189 1.31+0	1.139 1.40+0
34.4 CV	$\frac{\gamma}{\delta}$	3.73-4	2.32-3	8.72-3	1.77-2	2.81-2	3.92-2	5.14-2	6.43-2	7.75-2	9.08-2
$4p_{3/2}$	σ	1.499+1	8.348+0	3.416+0	1.723+0	9.828-1	6.095-1	4.018-1	2.776-1	1.989-1	1.469-1
$E_b = 50.0 \text{ eV}$	β γ	1.706 1.04-2	1.686 1.12-1	1.622 3.58-1	1.552 5.92-1	1.483 7.97-1	1.418 9.73-1	1.358 1.12+0	1.303 1.25+0	1.251 1.37+0	1.201 1.47+0
	δ	2.80-3	5.10-3	1.11-2	1.90-2	2.80-2	3.78-2	4.85 - 2	6.00-2	7.21-2	8.43-2
4d _{3/2}	σ	5.747+0	2.519+0	7.208-1	2.781-1	1.283-1	6.676-2	3.792-2	2.302-2	1.472-2	9.821-3
$E_b = 1.7 \text{ eV}$	$eta \ \gamma$	1.282 3.63-1	1.210 5.20-1	1.070 7.63-1	0.948 9.39-1	0.845 1.07+0	0.760 1.16+0	0.690 1.24+0	0.627 1.30+0	0.571 1.34+0	0.519 1.37+0
	δ	5.31-2	7.03-2	1.06-1	1.41-1	1.75-1	2.08 - 1	2.41 - 1	2.72 - 1	3.01-1	3.29-1
$4d_{5/2} E_b =$	$\frac{\sigma}{eta}$	8.101+0 1.262	3.533+0 1.183	1.003+0 1.041	3.845-1 0.922	1.763-1 0.824	9.133-2 0.744	5.165-2 0.680	3.122-2 0.623	1.989-2 0.573	1.322-2 0.527
1.3 eV	γ	3.68-1	5.21 - 1	7.59-1	9.30-1	1.06+0	1.15+0	1.23+0	1.29+0	1.33+0	1.37+0
	δ	5.38-2	7.21-2	1.10-1	1.46-1	1.81-1	2.15-1	2.48-1	2.80-1	3.09-1	3.36-1
Z= 47, Ag: [K	(r]4d _{3/2}										
Chell		k (eV) 1500	2000	2000	4000	5000	6000	7000	9000	0000	10000
$\frac{\text{Shell}}{3s_{1/2}}$	σ	3.871+1	2.437+1	3000 1.204+1	4000 7.071+0	5000 4.598+0	3.198+0	7000 2.335+0	8000 1.768+0	9000 1.377+0	10000
$E_b =$	β	1.979	1.983	1.989	1.992	1.994	1.994	1.992	1.989	1.985	1.981
717.5 eV	$\gamma \over \delta$	2.13-1 $-1.18-4$	3.91-2 $-1.60-4$	-9.61-2 $-2.02-4$	-9.28-2 $-2.23-4$	-2.50-2 $-2.37-4$	7.46-2 $-2.45-4$	1.89-1 -2.51-4	3.11-1 -2.55-4	4.37 - 1 $-2.56 - 4$	5.62 - 1 -2.55 - 4
3p _{1/2}	σ	5.352+1	3.162+1	1.364+1	7.063+0	4.103+0	2.582+0	1.723+0	1.202+0	8.694-1	6.471-1
$E_b =$	β	1.586	1.613	1.578	1.517	1.452	1.389	1.331	1.276	1.223	1.172
602.4 eV	$\frac{\gamma}{\delta}$	-2.01-2 1.57-3	1.49-2 $2.41-3$	2.36-1 8.41-3	4.73 - 1 $1.67 - 2$	6.82 - 1 $2.65 - 2$	8.62-1 $3.72-2$	1.02+0 4.90-2	1.15+0 6.13-2	1.27+0 7.41-2	1.38+0 8.67-2
3p _{3/2}	σ	1.070+2	6.159+1	2.574+1	1.305+1	7.467+0	4.639+0	3.062+0	2.117+0	1.518+0	1.121+0
$E_b = 571.4 \text{ eV}$	β	1.613 -3.02-2	1.649 2.06-2	1.625 2.58-1	1.571 5.07-1	1.510 7.26-1	1.450 9.14-1	1.394 1.08+0	1.340 1.22+0	1.288 1.34+0	1.237 1.45+0
	$\delta ^{\gamma }$	3.27 - 3	5.45 - 3	1.15 - 2	1.88 - 2	2.71 - 2	3.63 - 2	4.66 - 2	5.77 - 2	6.90-2	8.04 - 2
Shell	-	1500 9.083+1	2000 3.831+1	3000	4000	5000 1.806+0	6000 9.337-1	7000 5.280 1	8000	9000	10000 1.358-1
$3d_{3/2}$ $E_b =$	$\frac{\sigma}{eta}$	9.083+1 1.235	3.831+1 1.210	1.049+1 1.100	3.961+0 0.987	0.888	9.337—1 0.804	5.280-1 0.729	3.195-1 0.662	2.039-1 0.601	0.548

Table 1 (contin	ued)										
372.8 eV	$_{\delta}^{\gamma}$	2.75-1 5.72-2	4.60-1 7.37-2	7.36-1 1.06-1	9.27-1 1.39-1	1.07+0 1.72-1	1.17+0 2.05-1	1.25+0 2.36-1	1.31+0 2.65-1	1.36+0 2.93-1	1.39+0 3.20-1
$3d_{5/2}$ $E_b =$	$\sigma \ eta$	1.309+2 1.225	5.497+1 1.189	1.495+1 1.071	5.613+0 0.959	2.547+0 0.864	1.310+0 0.785	7.377-1 0.716	4.446-1 0.655	2.827-1 0.600	1.876-1 0.553
366.7 eV	$\frac{\gamma}{\delta}$	2.85-1 5.74-2	4.67-1 7.49-2	7.34-1 1.10-1	9.20-1 1.44-1	1.06+0 1.78-1	1.16+0 2.12-1	1.24+0 2.44-1	1.30+0 2.74-1	1.35+0 3.02-1	1.39+0 3.29-1
$4s_{1/2} E_b =$	$\sigma \ eta$	7.791+0 1.985	4.663+0 1.988	2.207+0 1.991	1.273+0 1.994	8.202-1 1.994	5.672-1 1.993	4.124-1 1.991	3.113-1 1.988	2.419-1 1.983	1.925-1 1.979
95.2 eV	$\frac{\gamma}{\delta}$	1.39-2 $-1.30-4$	-5.90-2 $-1.56-4$	-9.96-2 $-1.88-4$	-5.95-2 $-2.08-4$	2.37-2 $-2.23-4$	1.29-1 -2.31-4	2.46-1 $-2.37-4$	3.68 - 1 $-2.40 - 4$	4.92 - 1 $-2.40 - 4$	6.17-1 -2.41-4
$\begin{array}{l} 4p_{1/2} \\ E_b = \end{array}$	$\sigma \ eta$	8.448+0 1.684	4.823+0 1.657	2.043+0 1.584	1.056+0 1.510	6.150-1 1.440	3.879-1 1.376	2.594-1 1.317	1.814-1 1.261	1.314-1 1.208	9.796-2 1.158
62.6 eV	$_{\delta}^{\gamma}$	-8.86-4 $4.86-5$	8.70-2 1.79-3	3.13-1 7.62-3	5.33-1 1.58-2	7.29-1 2.56-2	8.99-1 3.65-2	1.05+0 4.84-2	1.18+0 6.11-2	1.29+0 7.38-2	1.39+0 8.65-2
$\begin{array}{l} 4p_{3/2} \\ E_b = \end{array}$	$\sigma \ eta$	1.650+1 1.709	9.237+0 1.692	3.809+0 1.632	1.933+0 1.565	1.109+0 1.499	6.909-1 1.437	4.572-1 1.379	3.168-1 1.325	2.276-1 1.272	1.684-1 1.222
55.9 eV	$_{\delta}^{\gamma}$	6.98 - 4 $2.57 - 3$	9.60-2 $4.78-3$	3.35-1 1.03-2	5.66-1 1.74-2	7.70-1 2.58-2	9.48-1 3.53-2	1.10+0 4.58-2	1.24+0 5.71-2	1.36+0 6.86-2	1.46+0 8.01-2
$4d_{3/2} E_b =$	σ β	7.263+0 1.294	3.215+0 1.223	9.331-1 1.085	3.640-1 0.966	1.693-1 0.867	8.867-2 0.784	5.060-2 0.712	3.083-2 0.647	1.978-2 0.589	1.323-2 0.536
$E_b = 3.6 \text{ eV}$	$\gamma \over \delta$	3.46-1 5.09-2	5.06-1 6.79-2	7.51-1 1.02-1	9.31-1 1.36-1	1.07+0 1.69-1	1.17+0 2.03-1	1.25+0 2.35-1	1.31+0 2.65-1	1.35+0 2.94-1	1.39+0 3.21-1
$4d_{5/2}$ $E_b =$	σ β	1.031+1 1.273	4.538+0 1.196	1.307+0 1.055	5.063-1 0.938	2.342-1 0.843	1.220-1 0.765	6.932-2 0.699	4.205-2 0.640	2.687-2 0.588	1.791-2 0.541
3.1 eV	γ δ	3.53-1 5.15-2	5.08-1 6.96-2	7.47-1 1.06-1	9.22-1 1.41-1	1.05+0 1.76-1	1.16+0 2.10-1	1.24+0 2.43-1	1.30+0 2.74-1	1.35+0 3.02-1	1.38+0 3.29-1
$5s_{1/2}$ $E_b =$	σ β	4.011-1 1.986	2.377-1 1.988	1.114-1 1.992	6.394-2 1.994	4.109-2 1.994	2.838-2 1.993	2.061-2 1.991	1.554-2 1.987	1.207-2 1.983	9.593-3 1.978
8.0 eV	γ δ	1.35-3 -1.30-4	-6.55-2 $-1.54-4$	-9.93-2 $-1.87-4$	-5.55-2 $-2.06-4$	2.86-2 -2.18-4	1.35-1 -2.26-4	2.53-1 -2.33-4	3.77-1 -2.37-4	5.02 - 1 $-2.38 - 4$	6.25 - 1 $-2.41 - 4$
Z= 48, Cd: [K	(r]4d ⁴ _{3/2}										
Shell		k (eV) 1500	2000	3000	4000	5000	6000	7000	8000	9000	10000
$3s_{1/2} E_b =$	σ β	4.022+1 1.977	2.547+1 1.981	1.265+1 1.987	7.454+0 1.991	4.860+0 1.993	3.388+0 1.994	2.479+0 1.992	1.880+0 1.990	1.467+0 1.986	1.171+0 1.982
770.2 eV	γ δ	2.55-1 -1.22-4	6.69-2 -1.72-4	-9.00-2 -2.22-4	-1.02-1 $-2.47-4$	-4.49-2 $-2.62-4$	4.61-2 -2.72-4	1.55-1 -2.79-4	2.72-1 -2.84-4	3.94-1 -2.86-4	5.18-1 -2.87-4
$3p_{1/2}$ $E_b =$	$\frac{\sigma}{\beta}$	5.614+1 1.573	3.352+1 1.612	1.463+1 1.585	7.638+0 1.528	4.465+0 1.466	2.824+0 1.406	1.891+0 1.349	1.324+0 1.294	9.602-1 1.241	7.164-1 1.190
650.7 eV	γ δ	-1.17-2 $2.02-3$	2.92-4 2.02-3	2.05-1 7.29-3	4.38-1 1.50-2	6.48-1 2.43-2	8.32-1 3.49-2	9.92-1 4.64-2	1.13+0 5.84-2	1.25+0 7.05-2	1.36+0 8.24-2
$3p_{3/2}$ $E_b =$	$\frac{\sigma}{\beta}$	1.129+2 1.600	6.551+1 1.647	2.765+1 1.633	1.412+1 1.583	8.122+0 1.527	5.068+0 1.469	3.357+0 1.414	2.327+0 1.360	1.673+0 1.308	1.238+0 1.258
616.5 eV	γ δ	-2.69-2 $3.42-3$	3.65-3 5.09-3	2.27-1 1.07-2	4.72-1 1.74-2	6.92-1 2.53-2	8.85-1 3.44-2	1.05+0 4.43-2	1.20+0 5.50-2	1.32+0 6.56-2	1.43+0 7.63-2
3d _{3/2}	σ	1.022+2	4.339+1	1.200+1	4.565+0	2.093+0	1.086+0	6.164-1	3.741-1	2.393-1	1.598-1
$E_b = 410.5 \text{ eV}$	$eta \ \gamma \ \delta$	1.234 2.48-1 5.57-2	1.219 4.34-1 7.17-2	1.118 7.18-1 1.03-1	1.010 9.18-1 1.35-1	0.912 1.06+0 1.68-1	0.826 1.17+0 2.00-1	0.749 1.26+0 2.30-1	0.680 1.32+0 2.59-1	0.620 1.37+0 2.86-1	0.567 1.41+0 3.13-1
3d _{5/2}	σ	1.472+2	6.220+1	1.708+1	6.460+0	2.947+0	1.522+0	8.600-1	5.198-1	3.312-1	2.203-1
$E_b = 403.7 \text{ eV}$	β	1.225 2.60-1	1.199 4.43-1	1.089 7.18-1	0.980 9.11-1	0.886 1.05+0	0.804 1.16+0	0.733 1.24+0	0.671 1.31+0	0.616 1.36+0	0.568 1.40+0
4s _{1/2}	$\frac{\delta}{\sigma}$	5.57-2 8.440+0	7.28-2 5.055+0	1.06-1 2.396+0	1.41-1 1.385+0	1.75-1 8.938-1	2.07-1 6.193-1	2.38-1 4.511-1	2.67-1 3.410-1	2.95-1 2.654-1	3.22-1 2.114-1
$E_b = 107.6 \text{ eV}$	β γ	1.984 2.75-2	1.986 -5.06-2	1.990 -1.02-1	1.993 -7.13-2	1.994 3.28-3	1.993 1.02-1	1.991 2.13-1	1.988 3.32-1	1.984 4.53-1	1.980 5.75-1
4p _{1/2}	$\frac{\delta}{\sigma}$	-1.40-4 9.254+0	-1.70-4 5.311+0	-2.08-4 2.269+0	-2.30-4 1.182+0	-2.47-4 6.919-1	-2.56-4 4.386-1	-2.63-4 2.945-1	-2.68-4 2.066-1	-2.69-4 1.501-1	-2.70-4 1.122-1
$E_b = 70.8 \text{ eV}$	β γ	1.687 -8.44-3	1.663 7.05-2	1.594 2.88-1	1.523 5.05-1	1.455 7.00-1	1.393 8.73-1	1.334 1.02+0	1.279 1.16+0	1.226 1.27+0	1.175 1.37+0
4p _{3/2}	δ	-2.01-4 1.817+1	1.29-3 1.021+1	6.47-3 4.240+0	1.41-2 2.165+0	2.35-2 1.248+0	3.43-2 7.812-1	4.59-2 5.189-1	5.80-2 3.606-1	7.02-2 2.597-1	8.22-2 1.926-1
$E_b = 65.0 \text{ eV}$	β γ	1.712 -8.27-3	1.698 7.84–2	1.643 3.09-1	1.579 5.37—1	1.516 7.43-1	1.456 9.24-1	1.399 1.08+0	1.345 1.22+0	1.292 1.34+0	1.242 1.45+0
	δ	2.35-3	4.42-3	9.42-3	1.60-2	2.40-2	3.33-2	4.36-2	5.43-2	6.51-2	7.59-2
$4d_{3/2}$ $E_b =$	$\frac{\sigma}{eta}$	8.979+0 1.306	4.008+0 1.240	1.179+0 1.105	4.645-1 0.989	2.177-1 0.891	1.146-1 0.806	6.572-2 0.732	4.018-2 0.665	2.586—2 0.605	1.734-2 0.552
9.7 eV	$\delta \gamma$	3.28-1 4.89-2	4.88-1 6.50-2	7.39-1 9.80-2	9.24-1 1.32-1	1.06+0 1.65-1	1.17+0 1.98-1	1.25+0 2.29-1	1.31+0 2.58-1	1.36+0 2.86-1	1.40+0 3.13-1

Table	e 1 ((continued)	١
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abic i (contini	ucu)										
4d _{5/2}	σ	1.278+1	5.675+0	1.655+0	6.479-1	3.019-1	1.582-1	9.025-2	5.494-2	3.521-2	2.353-2
$E_b =$	β	1.285	1.211	1.072	0.958	0.864	0.785	0.716	0.656	0.602	0.555
9.0 eV	γ	3.35-1	4.92-1	7.35-1	9.15-1	1.05+0	1.16+0	1.24+0	1.30+0	1.35+0	1.39+0
	δ	4.94-2	6.66-2	1.02-1	1.37-1	1.72-1	2.06-1	2.37-1	2.67-1	2.95-1	3.22-1
$5s_{1/2}$	σ	5.374-1	3.188-1	1.496-1	8.608-2	5.543-2	3.835-2	2.790-2	2.107-2	1.638-2	1.304-2
$E_b = 2.2 \text{ eV}$	β	1.985 1.10-2	1.987 -5.86-2	1.991	1.993	1.994	1.993	1.991 2.23-1	1.988 3.42-1	1.984 4.62-1	1.979
2.2 EV	$_{\delta}^{\gamma}$	-1.40-4	-3.80-2 $-1.68-4$	-1.01-1 $-2.04-4$	-6.64-2 $-2.27-4$	9.65-3 -2.41-4	1.10-1 $-2.52-4$	-2.60-4	-2.66-4	-2.68-4	5.81-1 -2.71-4
7= 40 In [I/s		$\frac{1}{\text{Id}_{5/2}^6 5\text{s}_{1/2}^2 5\text{p}_{1/2}^1}$		2.01	2,2, 1	2,,,	2,02	2.00	2,00	2,00 1	21,7 1
Z= 49, III: [KI	rj4u _{3/2} 4		2								
Shell		k (eV) 1500	2000	3000	4000	5000	6000	7000	8000	9000	10000
		4.168+1	2.655+1	1.327+1	7.843+0	5.127+0	3.584+0	2.627+0	1.996+0		
$3s_{1/2}$ $E_b =$	$\frac{\sigma}{\beta}$	1.975	2.655+1 1.979	1.327+1	1.990	1.992	3.584+0 1.993	1.992	1.996+0	1.559+0 1.987	1.246+0 1.983
825.6 eV	γ	3.02-1	9.75-2	-8.04-2	-1.07 - 1	-6.23-2	1.99-2	1.22-1	2.36-1	3.54-1	4.75-1
	δ	-1.25-4	-1.87 - 4	-2.41-4	-2.70-4	-2.88 - 4	-3.01-4	-3.10-4	-3.16-4	-3.20 - 4	-3.22-4
$3p_{1/2}$	σ	5.867+1	3.543+1	1.566+1	8.239+0	4.845+0	3.078+0	2.069+0	1.453+0	1.057+0	7.903-1
$E_b =$	β	1.559	1.608	1.591	1.539	1.480	1.421	1.364	1.309	1.257	1.207
702.2 eV	$_{\delta}^{\gamma}$	2.90-3 2.83-3	-1.09-2 1.73-3	1.76-1 6.48-3	4.05-1 1.39-2	6.17 - 1 $2.29 - 2$	8.03-1 3.31-2	9.66-1 4.39-2	1.11+0 5.51-2	1.23+0 6.64-2	1.34+0 7.78-2
2n		1.187+2	6.950+1	2.964+1	1.524+1	8.810+0	5.519+0	3.668+0	2.550+0	1.837+0	1.363+0
$3p_{3/2}$ $E_b =$	$\frac{\sigma}{\beta}$	1.187+2	1.644	1.640	1.524+1	1.542	1.486	1.431	2.550+0 1.378	1.837+0	1.363+0
664.3 eV	γ	-1.84-2	-1.02-2	1.97-1	4.39-1	6.62-1	8.58-1	1.03+0	1.18+0	1.30+0	1.42+0
	δ	3.77-3	4.84-3	1.02-2	1.67-2	2.44-2	3.30-2	4.23-2	5.20-2	6.18-2	7.19-2
3d _{3/2}	σ	1.143+2	4.887+1	1.365+1	5.229+0	2.410+0	1.257+0	7.155-1	4.356-1	2.794-1	1.870-1
$E_b =$	β	1.230	1.226	1.135	1.029	0.930	0.843	0.766	0.699	0.640	0.588
450.8 eV	γ	2.19-1	4.11-1	7.03-1	9.09-1	1.06+0	1.17+0	1.26+0	1.33+0	1.38+0	1.42+0
	δ	5.37-2	7.03-2	1.01-1	1.33-1	1.64-1	1.94-1	2.23-1	2.52-1	2.80-1	3.07-1
$3d_{5/2}$	σ	1.646+2 1.224	6.999+1 1.207	1.940+1 1.105	7.391+0 0.998	3.389+0 0.902	1.758+0 0.819	9.968-1 0.748	6.042-1 0.686	3.861-1 0.633	2.574-1
$E_b = 443.1 \text{ eV}$	$eta \ \gamma$	2.31-1	4.21-1	7.04–1	9.03-1	1.05+0	1.16+0	1.25+0	1.31+0	1.37+0	0.586 1.41+0
	δ	5.35-2	7.12-2	1.05-1	1.38-1	1.70-1	2.02-1	2.32-1	2.61-1	2.89-1	3.16-1
4s _{1/2}	σ	9.111+0	5.464+0	2.594+0	1.501+0	9.708-1	6.739-1	4.917-1	3.722-1	2.900-1	2.313-1
$E_b =$	β	1.983	1.985	1.989	1.992	1.993	1.993	1.991	1.988	1.985	1.981
121.9 eV	γ	4.14 - 2	-4.10-2	-1.02 - 1	-8.13-2	-1.53-2	7.65 - 2	1.83 - 1	2.98 - 1	4.16 - 1	5.35 - 1
	δ	-1.53-4	-1.85-4	-2.27-4	-2.52-4	-2.71-4	-2.83-4	-2.92-4	-2.99-4	-3.01-4	-3.04-4
$4p_{1/2}$	σ	1.013+1	5.847+0	2.518+0 1.604	1.320+0	7.773-1	4.949-1	3.335-1	2.347-1	1.710-1	1.281-1
$E_b = 81.9 \text{ eV}$	β γ	1.690 -1.47-2	1.669 5.54-2	2.64-1	1.535 4.78-1	1.470 6.75-1	1.408 8.50-1	1.349 1.00+0	1.293 1.14+0	1.241 1.25+0	1.191 1.36+0
01.5 CV	δ	-4.56-4	8.90-4	5.72-3	1.30-2	2.21-2	3.24-2	4.33-2	5.45-2	6.60-2	7.75-2
$4p_{3/2}$	σ	1.994+1	1.126+1	4.707+0	2.417+0	1.401+0	8.802-1	5.865-1	4.088-1	2.951-1	2.193-1
$E_b =$	β	1.713	1.704	1.653	1.593	1.532	1.473	1.416	1.362	1.309	1.260
75.1 eV	γ	-1.57-2	6.25-2	2.84-1	5.11-1	7.18-1	9.02 - 1	1.06+0	1.20+0	1.32+0	1.43+0
	δ	2.16-3	4.17-3	8.96-3	1.53-2	2.31-2	3.19-2	4.13-2	5.12-2	6.12-2	7.15-2
$4d_{3/2}$	σ	1.087+1	4.895+0	1.458+0	5.799-1	2.738-1	1.450-1	8.350-2	5.125-2	3.309-2	2.225-2
$E_b = 16.8 \text{ eV}$	β γ	1.316 3.11-1	1.254 4.74-1	1.124 7.28-1	1.009 9.16-1	0.910 1.06+0	0.823 1.17+0	0.748 1.25+0	0.681 1.32+0	0.622 1.37+0	0.571 1.41+0
10.0 C V	δ	4.74-2	6.34-2	9.59-2	1.29-1	1.61-1	1.92-1	2.22-1	2.51-1	2.79-1	3.06-1
4d _{5/2}	σ	1.558+1	6.977+0	2.060+0	8.140-1	3.820-1	2.013-1	1.154-1	7.050-2	4.533-2	3.036-2
$E_b =$	β	1.296	1.226	1.091	0.977	0.881	0.800	0.730	0.669	0.616	0.569
15.8 eV	γ δ	3.20 - 1	4.79 - 1	7.25 - 1	9.08 - 1	1.05+0	1.16+0	1.24+0	1.31+0	1.36+0	1.41+0
	δ	4.78-2	6.50-2	9.96-2	1.34-1	1.68-1	2.00-1	2.31-1	2.60-1	2.88-1	3.16-1
$5s_{1/2}$	σ	7.283-1	4.328-1	2.035-1	1.172-1	7.558-2	5.237-2	3.815-2	2.886-2	2.247-2	1.791-2
$E_b = 0.1 \text{ eV}$	β	1.983	1.986 -5.28-2	1.989	1.992 -7.72-2	1.993	1.993	1.991 1.92-1	1.988 3.05-1	1.985 4.22-1	1.980
0.167	$\delta ^{\gamma }$	2.06-2 $-1.54-4$	-5.28-2 $-1.87-4$	-1.04-1 $-2.26-4$	-7.72-2 -2.52-4	-8.12-3 $-2.69-4$	8.53-2 $-2.81-4$	-2.90-4	-2.96-4	-2.99-4	5.40-1 -3.03-4
5n _{1/2}	σ	4.187-1	2.401-1	1.028-1	5.373-2	3.160-2	2.010-2	1.354-2	9.529-3	6.942-3	5.201-3
$5p_{1/2}$ $E_b =$	β	1.701	1.675	1.606	1.535	1.468	1.404	1.334-2	9.329-3 1.291	1.241	3.201-3 1.194
0.8 eV	γ	-1.19-2	6.26-2	2.73-1	4.88-1	6.83-1	8.55-1	1.01+0	1.14+0	1.26+0	1.36+0
	δ	-6.83 - 4	6.67 - 4	5.50-3	1.28-2	2.18 - 2	3.16-2	4.22 - 2	5.35 - 2	6.53 - 2	7.74-2
Z= 50, Sn: [K	r]4d _{3/2} 4	$4d_{5/2}^6 5s_{1/2}^2 5p_{1/2}^2$	2								
	· ·	k (eV)									
Shell		1500	2000	3000	4000	5000	6000	7000	8000	9000	10000
3s _{1/2}	σ	4.306+1	2.762+1	1.389+1	8.241+0	5.401+0	3.783+0	2.778+0	2.114+0	1.654+0	1.323+0
$E_b =$	β	1.973	1.976	1.983	1.988	1.991	1.992	1.992	1.990	1.987	1.984
883.8 eV	γ	3.52-1 -1.25-4	1.31-1 -1.99-4	-6.98-2 $-2.66-4$	-1.12-1 $-2.99-4$	-7.85-2	-4.48-3 $-3.36-4$	9.16-2	2.00-1	3.14-1	4.30-1
			- 1.99-4	-2.00-4	-2.99-4	-3.21 - 4	4—ەد.د—	-3.46 - 4	-3.54 - 4	-3.59 - 4	-3.62-4
3p _{1/2}	$\frac{\delta}{\sigma}$	6.115+1	3.732+1	1.671+1	8.859+0	5.240+0	3.344+0	2.257+0	1.590+0	1.159+0	8.692-1

$E_b =$	ued) β	1.539	1.604	1.596	1.548	1.491	1.434	1.378	1.324	1.274	1.226
756.4 eV	γ	2.38 - 2	-1.87 - 2	1.49 - 1	3.73 - 1	5.85 - 1	7.72 - 1	9.36 - 1	1.08+0	1.21+0	1.32+0
	δ	4.13-3	1.57-3	5.62-3	1.25-2	2.09-2	3.05-2	4.06-2	5.13-2	6.22-2	7.34-2
$ \begin{array}{l} 3p_{3/2} \\ E_b = \end{array} $	$\frac{\sigma}{eta}$	1.245+2 1.569	7.352+1 1.639	3.168+1 1.646	1.639+1 1.606	9.524+0 1.554	5.991+0 1.500	3.994+0 1.447	2.784+0 1.395	2.011+0 1.345	1.495+0 1.298
-₀ — 714.4 eV	γ	-4.84 - 3	-2.14-2	1.69-1	4.08-1	6.31-1	8.28-1	1.00+0	1.15+0	1.28+0	1.40+0
	δ	4.42 - 3	4.64-3	9.68-3	1.58-2	2.29-2	3.08-2	3.94-2	4.85-2	5.79-2	6.77-2
$3d_{3/2}$	σ	1.275+2	5.483+1	1.545+1	5.961+0	2.763+0	1.447+0	8.269-1	5.049-1	3.247-1	2.177-
$E_b = 493.3 \text{ eV}$	β γ	1.223 1.87-1	1.231 3.83-1	1.149 6.83-1	1.045 8.95-1	0.949 1.05+0	0.864 1.17+0	0.789 1.26+0	0.722 1.34+0	0.663 1.39+0	0.610 1.44+0
155.5 CV	δ	5.16-2	6.82-2	9.82-2	1.28-1	1.58-1	1.88-1	2.17-1	2.46-1	2.74-1	3.00-1
3d _{5/2}	σ	1.835+2	7.848+1	2.195+1	8.415+0	3.880+0	2.022+0	1.150+0	6.993-1	4.479-1	2.992-
$E_b = 484.8 \text{ eV}$	β	1.220 2.01-1	1.213 3.95-1	1.118 6.85-1	1.013 8.90-1	0.918 1.04+0	0.837 1.16+0	0.767 1.25+0	0.706 1.32+0	0.652 1.38+0	0.605 1.43+0
404.0 EV	$_{\delta}^{\gamma}$	5.13-2	6.89-2	1.01-1	1.33-1	1.65-1	1.16+0	2.26-1	2.56-1	2.84-1	3.10-1
4s _{1/2}	σ	9.808+0	5.892+0	2.802+0	1.624+0	1.052+0	7.314-1	5.344-1	4.051-1	3.160-1	2.523-
$E_b =$	β	1.981	1.984	1.988	1.991	1.992	1.992	1.991	1.989	1.985	1.981
136.5 eV	$\gamma \\ \delta$	5.59-2 -1.66-4	-3.13-2 $-2.04-4$	-1.03-1 $-2.51-4$	-9.11-2 $-2.80-4$	-3.26-2 $-3.01-4$	5.29-2 -3.15-4	1.54-1 -3.25-4	2.64-1 $-3.34-4$	3.78-1 -3.38-4	4.93-1 -3.41-
1n		1.106+1	6,419+0	2.786+0	1.470+0	8.698-1	5.563-1	3.763-1	2.657-1	1.941-1	1.458-
$\begin{array}{l} 4p_{1/2} \\ E_b = \end{array}$	$\frac{\sigma}{\beta}$	1.691	1.674	1.612	1.470+0	1.481	1.420	3.763—1 1.362	1.308	1.941 – 1	1.458-
93.9 eV	γ	-1.94-2	4.18 - 2	2.42 - 1	4.54 - 1	6.49 - 1	8.23 - 1	9.77 - 1	1.11+0	1.23+0	1.34+0
	δ	-6.80-4	4.72-4	4.84-3	1.16-2	2.01-2	2.97-2	3.99-2	5.07-2	6.18-2	7.31-2
$4p_{3/2}$ $E_b =$	$\frac{\sigma}{\beta}$	2.181+1 1.714	1.237+1 1.709	5.207+0 1.662	2.688+0 1.604	1.565+0 1.545	9.873-1 1.487	6.601-1 1.431	4.613-1 1.379	3.339-1 1.329	2.487 – 1.281
86.0 eV	γ	-2.19-2	4.81-2	2.63-1	4.87-1	6.93-1	8.76-1	1.431	1.18+0	1.30+0	1.42+0
	δ	1.98 - 3	3.92 - 3	8.42 - 3	1.43-2	2.14 - 2	2.96-2	3.83-2	4.76 - 2	5.72-2	6.71 - 2
$4d_{3/2}$	σ	1.293+1	5.871+0	1.769+0	7.104-1	3.378-1	1.800-1	1.041-1	6.418-2	4.156-2	2.803-
$E_b = 24.6 \text{ eV}$	β γ	1.325 2.93-1	1.267 4.57-1	1.139 7.15-1	1.025 9.06-1	0.926 1.05+0	0.841 1.17+0	0.767 1.26+0	0.702 1.33+0	0.645 1.38+0	0.593 1.43+0
24.0 C V	δ	4.53-2	6.09-2	9.22-2	1.24-1	1.55-1	1.86-1	2.16-1	2.45-1	2.73-1	3.00-1
$4d_{5/2}$	σ	1.863+1	8.409+0	2.512+0	1.001+0	4.734-1	2.509-1	1.445-1	8.862-2	5.715-2	3.839-
$E_b =$	β	1.305	1.238	1.104	0.990	0.895	0.815	0.746	0.687	0.634	0.588
23.4 eV	$\gamma \\ \delta$	3.02-1 4.57-2	4.63-1 6.23-2	7.13-1 9.59-2	8.98-1 1.29-1	1.04+0 1.62-1	1.15+0 1.94-1	1.24+0 2.25-1	1.31+0 2.55-1	1.37+0 2.83-1	1.42+0 3.10-1
5s _{1/2}	σ	9.174-1	5.457-1	2.567-1	1.481-1	9.561-2	6.636-2	4.842-2	3.668-2	2.860-2	2.282-
$E_b =$	β	1.982	1.984	1.988	1.991	1.992	1.992	1.991	1.989	1.985	1.981
0.9 eV	$\gamma \\ \delta$	3.13-2 -1.68-4	-4.45-2 $-2.03-4$	-1.03-1 $-2.47-4$	-8.56-2 $-2.76-4$	-2.46-2 $-2.96-4$	6.16-2 $-3.09-4$	1.63-1 -3.19-4	2.72 - 1 $-3.27 - 4$	3.86-1 -3.31-4	5.01-1 -3.36-
5 <i>p</i> _{1/2}	σ	6.047-1	3.484-1	1.502-1	7.902-2	4.672-2	2.986-2	2.020-2	1.426-2	1.042-2	7.825-
$E_b =$	β	1.705	1.681	1.615	1.546	1.481	1.420	1.364	1.311	1.260	1.212
1.1 eV	γ	-1.68-2	4.96-2	2.51-1	4.61-1	6.54-1	8.27-1	9.81-1	1.12+0	1.24+0	1.34+0
	δ	-9.05-4	2.16-4	4.45-3	1.11-2	1.94-2	2.91-2	3.97-2	5.09-2	6.26-2	7.42-2
Z= 51, Sb: [Ki	r]4d _{3/2}	$4d_{5/2}^6 5s_{1/2}^2 5p_{1/2}^2$	₂ 5p _{3/2}								
		k (eV)									
Shell		1500	2000	3000	4000	5000	6000	7000	8000	9000	10000
$3s_{1/2} E_b =$	$\frac{\sigma}{\beta}$	4.438+1 1.970	2.866+1 1.974	1.451+1 1.981	8.640+0 1.987	5.677+0 1.990	3.984+0 1.992	2.931+0 1.991	2.234+0 1.990	1.750+0 1.988	1.402+0 1.984
ь — 943.7 eV	γ	4.03-1	1.68-1	-5.59-2	-1.14-1	-9.19-2	-2.69-2	6.19-2	1.64-1	2.73-1	3.85-1
	δ	-1.20-4	-2.11-4	-2.91-4	-3.30 - 4	-3.54 - 4	-3.72 - 4	-3.85 - 4	-3.93 - 4	-4.00-4	-4.03-
$3p_{1/2}$	σ	6.348+1	3.920+1	1.777+1	9.494+0	5.648+0	3.621+0	2.453+0	1.734+0	1.268+0	9.530-
$E_b = 811.9 \text{ eV}$	β	1.516 5.14-2	1.597 -2.25-2	1.601 1.22-1	1.557 3.40-1	1.503 5.49-1	1.447	1.394 9.04-1	1.342 1.05+0	1.293 1.18+0	1.247 1.29+0
611.9 EV	$_{\delta}^{\gamma}$	6.08 - 3	-2.23-2 1.57-3	4.82-3	1.11-2	1.89-2	7.37-1 2.79-2	3.77-2	4.81-2	5.89-2	7.00-2
$3p_{3/2}$	σ	1.302+2	7.757+1	3.376+1	1.758+1	1.027+1	6.483+0	4.337+0	3.032+0	2.195+0	1.635+
$E_b =$	β	1.547	1.633	1.651	1.616	1.568	1.516	1.465	1.415	1.367	1.322
765.6 eV	$_{\delta}^{\gamma}$	1.39-2 5.47-3	-2.93-2 $4.51-3$	1.41-1 9.17-3	3.74-1 1.48-2	5.96-1 2.13-2	7.94-1 2.87-2	9.69-1 3.69-2	1.12+0 4.56-2	1.26+0 5.49-2	1.38+0 6.45-2
3d _{3/2}	σ	1.416+2	6.125+1	1.741+1	6.764+0	3.153+0	1.658+0	9.511-1	5.824-1	3.754-1	2.523-
$E_b =$	β	1.213	1.235	1.163	1.065	0.972	0.888	0.813	0.746	0.686	0.631
536.9 eV	γ	1.56 - 1	3.54 - 1	6.61 - 1	8.81 - 1	1.04+0	1.17+0	1.27+0	1.34+0	1.40+0	1.45+0
0.1	δ	4.95-2	6.62-2	9.53-2	1.24-1	1.54-1	1.84-1	2.13-1	2.41-1	2.68-1	2.94-1
3d _{5/2}	σ_{ρ}	2.036+2 1.214	8.760+1 1.218	2.471+1 1.132	9.537+0 1.031	4.421+0 0.939	2.314+0 0.858	1.321+0 0.788	8.054-1 0.726	5.170-1 0.672	3.461- 0.622
$E_b = 527.5 \text{ eV}$	$eta \ \gamma$	1.214	3.68–1	6.66—1	8.77—1	0.939 1.03+0	0.858 1.16+0	0.788 1.25+0	0.726 1.33+0	1.39+0	1.44+0
-	δ	4.90-2	6.67-2	9.82-2	1.30-1	1.61-1	1.92-1	2.22-1	2.51-1	2.78-1	3.05-1
4s _{1/2}	σ	1.053+1	6.338+0	3.019+0	1.752+0	1.137+0	7.913-1	5.790-1	4.395-1	3.433-1	2.744-
$E_b = 152.0 \text{ eV}$	β	1.979 7.12-2	1.982	1.986	1.990	1.991	1.992	1.991	1.989	1.986	1.982
	γ	/ 1/-7	-2.04-2	-1.02 - 1	-9.90 - 2	-4.83 - 2	3.03 - 2	1.25 - 1	2.30 - 1	3.39 - 1	4.50 - 1

	δ	-1.79-4	-2.22-4	-2.76-4	-3.10-4	-3.32 - 4	-3.48 - 4	-3.60 - 4	-3.71-4	-3.77 - 4	-3.80-4
$4p_{1/2}$	σ	1.199+1	7.000+0	3.062+0	1.625+0	9.666-1	6.209-1	4.216-1	2.987-1	2.189-1	1.648-1
$E_b =$	β	1.693	1.678	1.620	1.556	1.493	1.434	1.379	1.327	1.277	1.230
104.3 eV	$\delta ^{\gamma }$	-2.24-2 $-8.60-4$	2.94-2 1.09-4	2.20-1 3.99-3	4.27-1 1.01-2	6.20-1 1.80-2	7.95-1 2.71-2	9.50-1 3.70-2	1.09+0 4.76-2	1.21+0 5.85-2	1.32+0 6.97-2
$4p_{3/2}$	σ	2.378+1	1.355+1	5.739+0	2.978+0	1.741+0	1.103+0	7.399-1	5.186-1	3.764-1	2.810-1
$E_b =$	β	1.715	1.713	1.671	1.616	1.559	1.503	1.450	1.399	1.351	1.305
95.4 eV	$\frac{\gamma}{\delta}$	-2.65-2 $1.82-3$	3.46-2 3.69-3	2.40-1 7.86-3	4.60-1 1.32-2	6.65 - 1 $1.98 - 2$	8.48-1 2.73-2	1.01+0 3.57-2	1.16+0 4.47-2	1.29+0 5.41-2	1.40+0 6.39-2
4d _{3/2}	σ	1.520+1	6.961+0	2.122+0	8.598-1	4.119-1	2.207-1	1.283-1	7.937-2	5.156-2	3.486-2
$E_b =$	β	1.334	1.280	1.157	1.045	0.949	0.865	0.791	0.726	0.666	0.613
32.2 eV	δ	2.73-1 4.35-2	4.39 - 1 $5.86 - 2$	7.01-1 8.87-2	8.97-1 1.20-1	1.05+0 1.51-1	1.17+0 1.81-1	1.26+0 2.11-1	1.34+0 2.39-1	1.40+0 2.67-1	1.44+0 2.93-1
4d _{5/2}	σ	2.188+1	9.955+0	3.008+0	1.210+0	5.759-1	3.070-1	1.776-1	1.093-1	7.073-2	4.763-2
$E_b = 30.8 \text{ eV}$	β	1.315 2.83-1	1.251 4.46-1	1.120 7.00-1	1.008 8.89-1	0.915 1.04+0	0.835 1.15+0	0.766 1.25+0	0.707 1.32+0	0.653 1.38+0	0.605 1.43+0
30.8 EV	$\delta ^{\gamma }$	4.37-2	5.99-2	9.24-2	1.25-1	1.58-1	1.90-1	2.20-1	2.50-1	2.78-1	3.04-1
5s _{1/2}	σ	1.111+0	6.617-1	3.115-1	1.798-1	1.162-1	8.076-2	5.901-2	4.475-2	3.493-2	2.790-2
$E_b = 6.7 \text{ eV}$	β	1.980 4.34-2	1.983 -3.61-2	1.987 -1.03-1	1.990 -9.38-2	1.992 -4.02-2	1.992 3.97-2	1.991 1.36-1	1.989 2.41-1	1.986 3.51-1	1.982 4.64-1
0.7 CV	δ	-1.83-4	-2.20-4	-2.72-4	-3.03-4	-3.25-4	-3.40-4	-3.53-4	-3.63-4	-3.67-4	-3.74-4
$5p_{1/2}$	σ	8.142-1	4.715-1	2.047-1	1.083-1	6.435-2	4.131-2	2.804-2	1.986-2	1.455-2	1.095-2
$E_b = 2.2 \text{ eV}$	β γ	1.708 -2.06-2	1.687 3.70-2	1.624 2.29-1	1.558 4.36-1	1.495 6.29-1	1.435 8.03-1	1.379 9.58-1	1.326 1.10+0	1.275 1.22+0	1.226 1.33+0
2.2 C V	δ	-1.11-3	-1.32-4	3.73-3	1.00-2	1.81-2	2.75-2	3.77-2	4.84-2	5.93-2	7.02-2
5p _{3/2}	σ	1.555+0	8.797-1	3.701-1	1.916-1	1.119-1	7.082-2	4.750-2	3.329-2	2.415-2	1.803-2
$E_b = 2.0 \text{ eV}$	β	1.729 -2.37-2	1.722 4.21-2	1.675 2.48-1	1.618 4.68-1	1.561 6.72-1	1.505 8.56-1	1.451 1.02+0	1.399 1.17+0	1.349 1.29+0	1.302 1.41+0
2.0 EV	δ	1.65-3	3.44-3	7.49-3	1.30-2	1.97 - 2	2.76-2	3.63-2	4.55-2	5.49-2	6.46-2
Z= 52, Te: [K	r]4d _{3/2} 4	$4d_{5/2}^6 5s_{1/2}^2 5p_{1/2}^2$	2 5p _{3/2}								
		k (eV)	·								
Shell		1500	2000	3000	4000	5000	6000	7000	8000	9000	10000
		4 = 00 4								1 0 10 . 0	1 100.0
$3s_{1/2}$	σ	4.562+1	2.969+1	1.514+1	9.043+0	5.957+0	4.189+0	3.087+0	2.356+0	1.849+0	1.483+0
$3s_{1/2}$ $E_b =$ 1006.0 eV	β	1.968	1.972	1.979	1.985	1.989	1.991	1.991	1.990	1.988	1.985
$E_b =$											1.985 3.43-1
$E_b = 1006.0 \text{ eV}$	β γ δ	1.968 4.65-1 -1.10-4 6.567+1	1.972 2.09-1 -2.21-4 4.105+1	1.979 -3.91-2 -3.16-4 1.885+1	1.985 -1.13-1 -3.62-4 1.015+1	1.989 -1.03-1 -3.90-4 6.072+0	1.991 -4.72-2 -4.09-4 3.911+0	1.991 3.40-2 -4.23-4 2.660+0	1.990 1.30-1 -4.33-4 1.886+0	1.988 2.34-1 -4.41-4 1.383+0	1.985 3.43-1 -4.46-4 1.042+0
$E_b = 1006.0 \text{ eV}$ $3p_{1/2}$ $E_b = $	β γ δ σ β	1.968 4.65-1 -1.10-4 6.567+1 1.487	1.972 2.09-1 -2.21-4 4.105+1 1.588	1.979 -3.91-2 -3.16-4 1.885+1 1.604	1.985 -1.13-1 -3.62-4 1.015+1 1.565	1.989 -1.03-1 -3.90-4 6.072+0 1.514	1.991 -4.72-2 -4.09-4 3.911+0 1.461	1.991 3.40-2 -4.23-4 2.660+0 1.410	1.990 1.30-1 -4.33-4 1.886+0 1.360	1.988 2.34-1 -4.41-4 1.383+0 1.312	1.985 3.43-1 -4.46-4 1.042+0 1.265
$E_b = 1006.0 \text{ eV}$	β γ δ	1.968 4.65-1 -1.10-4 6.567+1	1.972 2.09-1 -2.21-4 4.105+1	1.979 -3.91-2 -3.16-4 1.885+1	1.985 -1.13-1 -3.62-4 1.015+1	1.989 -1.03-1 -3.90-4 6.072+0	1.991 -4.72-2 -4.09-4 3.911+0	1.991 3.40-2 -4.23-4 2.660+0	1.990 1.30-1 -4.33-4 1.886+0	1.988 2.34-1 -4.41-4 1.383+0	1.985 3.43-1 -4.46-4 1.042+0
$E_b = 1006.0 \text{ eV}$ $3p_{1/2}$ $E_b = 869.7 \text{ eV}$	β γ δ σ β γ δ	1.968 4.65-1 -1.10-4 6.567+1 1.487 8.63-2 8.96-3 1.358+2	1.972 2.09-1 -2.21-4 4.105+1 1.588 -2.17-2 1.75-3 8.167+1	1.979 -3.91-2 -3.16-4 1.885+1 1.604 9.64-2 4.12-3 3.590+1	1.985 -1.13-1 -3.62-4 1.015+1 1.565 3.07-1 9.88-3 1.882+1	1.989 -1.03-1 -3.90-4 6.072+0 1.514 5.14-1 1.73-2 1.104+1	1.991 -4.72-2 -4.09-4 3.911+0 1.461 7.04-1 2.59-2 6.999+0	1.991 3.40-2 -4.23-4 2.660+0 1.410 8.72-1 3.56-2 4.697+0	1.990 1.30-1 -4.33-4 1.886+0 1.360 1.02+0 4.58-2 3.293+0	1.988 2.34-1 -4.41-4 1.383+0 1.312 1.16+0 5.64-2 2.390+0	1.985 3.43-1 -4.46-4 1.042+0 1.265 1.27+0 6.71-2 1.784+0
$E_b = 1006.0 \text{ eV}$ $3p_{1/2}$ $E_b = 869.7 \text{ eV}$ $3p_{3/2}$ $E_b = 69.7 \text{ eV}$	$\begin{array}{c} \beta \\ \gamma \\ \delta \\ \\ \sigma \\ \beta \\ \\ \gamma \\ \delta \\ \\ \sigma \\ \beta \end{array}$	1.968 4.65-1 -1.10-4 6.567+1 1.487 8.63-2 8.96-3 1.358+2 1.521	1.972 2.09-1 -2.21-4 4.105+1 1.588 -2.17-2 1.75-3 8.167+1 1.625	1.979 -3.91-2 -3.16-4 1.885+1 1.604 9.64-2 4.12-3 3.590+1 1.655	1.985 -1.13-1 -3.62-4 1.015+1 1.565 3.07-1 9.88-3 1.882+1 1.625	1.989 -1.03-1 -3.90-4 6.072+0 1.514 5.14-1 1.73-2 1.104+1 1.581	1.991 -4.72-2 -4.09-4 3.911+0 1.461 7.04-1 2.59-2 6.999+0 1.532	1.991 3.40-2 -4.23-4 2.660+0 1.410 8.72-1 3.56-2 4.697+0 1.483	1.990 1.30-1 -4.33-4 1.886+0 1.360 1.02+0 4.58-2 3.293+0 1.435	1.988 2.34-1 -4.41-4 1.383+0 1.312 1.16+0 5.64-2 2.390+0 1.388	1.985 3.43-1 -4.46-4 1.042+0 1.265 1.27+0 6.71-2 1.784+0 1.343
$E_b = 1006.0 \text{ eV}$ $3p_{1/2} E_b = 869.7 \text{ eV}$ $3p_{3/2} E_b = 818.7 \text{ eV}$	β γ δ σ β γ δ	1.968 4.65-1 -1.10-4 6.567+1 1.487 8.63-2 8.96-3 1.358+2 1.521 3.85-2 7.07-3	1.972 2.09-1 -2.21-4 4.105+1 1.588 -2.17-2 1.75-3 8.167+1	1.979 -3.91-2 -3.16-4 1.885+1 1.604 9.64-2 4.12-3 3.590+1	1.985 -1.13-1 -3.62-4 1.015+1 1.565 3.07-1 9.88-3 1.882+1	1.989 -1.03-1 -3.90-4 6.072+0 1.514 5.14-1 1.73-2 1.104+1 1.581 5.61-1 2.01-2	1.991 -4.72-2 -4.09-4 3.911+0 1.461 7.04-1 2.59-2 6.999+0	1.991 3.40-2 -4.23-4 2.660+0 1.410 8.72-1 3.56-2 4.697+0	1.990 1.30-1 -4.33-4 1.886+0 1.360 1.02+0 4.58-2 3.293+0	1.988 2.34-1 -4.41-4 1.383+0 1.312 1.16+0 5.64-2 2.390+0	1.985 3.43-1 -4.46-4 1.042+0 1.265 1.27+0 6.71-2 1.784+0
$E_b = 1006.0 \text{ eV}$ $3p_{1/2} E_b = 869.7 \text{ eV}$ $3p_{3/2} E_b = 818.7 \text{ eV}$ $3d_{3/2}$	β γ δ σ β γ δ δ σ β γ γ δ δ σ σ β γ γ δ δ σ σ σ δ σ σ σ σ σ σ σ σ σ σ σ σ	1.968 4.65-1 -1.10-4 6.567+1 1.487 8.63-2 8.96-3 1.358+2 1.521 3.85-2 7.07-3 1.567+2	1.972 2.09-1 -2.21-4 4.105+1 1.588 -2.17-2 1.75-3 8.167+1 1.625 -3.36-2 4.48-3 6.820+1	1.979 -3.91-2 -3.16-4 1.885+1 1.604 9.64-2 4.12-3 3.590+1 1.655 1.14-1 8.74-3	1.985 -1.13-1 -3.62-4 1.015+1 1.565 3.07-1 9.88-3 1.882+1 1.625 3.41-1 1.40-2 7.646+0	1.989 -1.03-1 -3.90-4 6.072+0 1.514 5.14-1 1.73-2 1.104+1 1.581 5.61-1 2.01-2 3.583+0	1.991 -4.72-2 -4.09-4 3.911+0 1.461 7.04-1 2.59-2 6.999+0 1.532 7.61-1 2.72-2 1.892+0	1.991 3.40-2 -4.23-4 2.660+0 1.410 8.72-1 3.56-2 4.697+0 1.483 9.40-1 3.52-2 1.089+0	1.990 1.30-1 -4.33-4 1.886+0 1.360 1.02+0 4.58-2 3.293+0 1.435 1.10+0 4.37-2 6.688-1	1.988 2.34-1 -4.41-4 1.383+0 1.312 1.16+0 5.64-2 2.390+0 1.388 1.24+0 5.27-2	1.985 3.43-1 -4.46-4 1.042+0 1.265 1.27+0 6.71-2 1.784+0 1.343 1.36+0 6.19-2 2.910-1
$E_b = 1006.0 \text{ eV}$ $3p_{1/2}$ $E_b = 869.7 \text{ eV}$ $3p_{3/2}$ $E_b = 818.7 \text{ eV}$ $3d_{3/2}$ $E_b = 60.7 \text{ eV}$	β γ δ σ β γ δ δ σ β β γ δ δ σ β β γ δ δ σ β β γ δ δ σ β β γ δ δ σ β β γ δ δ σ β β γ δ δ σ β β γ δ δ σ β β γ δ δ σ β β γ δ δ σ β β γ δ δ σ β β γ δ δ σ β β γ δ δ σ β β γ δ δ σ β β γ δ δ σ β γ δ δ σ β γ δ δ σ β γ δ δ σ β γ δ δ σ δ β γ δ δ σ δ δ σ δ δ σ δ δ δ σ δ δ δ δ σ δ δ σ δ δ σ δ δ σ δ δ σ δ δ σ δ δ σ δ δ σ δ δ δ σ δ	1.968 4.65-1 -1.10-4 6.567+1 1.487 8.63-2 8.96-3 1.358+2 1.521 3.85-2 7.07-3 1.567+2 1.201	1.972 2.09-1 -2.21-4 4.105+1 1.588 -2.17-2 1.75-3 8.167+1 1.625 -3.36-2 4.48-3 6.820+1 1.237	1.979 -3.91-2 -3.16-4 1.885+1 1.604 9.64-2 4.12-3 3.590+1 1.655 1.14-1 8.74-3 1.956+1 1.176	1.985 -1.13-1 -3.62-4 1.015+1 1.565 3.07-1 9.88-3 1.882+1 1.625 3.41-1 1.40-2 7.646+0 1.083	1.989 -1.03-1 -3.90-4 6.072+0 1.514 5.14-1 1.73-2 1.104+1 1.581 5.61-1 2.01-2 3.583+0 0.993	1.991 -4.72-2 -4.09-4 3.911+0 1.461 7.04-1 2.59-2 6.999+0 1.532 7.61-1 2.72-2 1.892+0 0.909	1.991 3.40-2 -4.23-4 2.660+0 1.410 8.72-1 3.56-2 4.697+0 1.483 9.40-1 3.52-2 1.089+0 0.834	1.990 1.30-1 -4.33-4 1.886+0 1.360 1.02+0 4.58-2 3.293+0 1.435 1.10+0 4.37-2 6.688-1 0.766	1.988 2.34-1 -4.41-4 1.383+0 1.312 1.16+0 5.64-2 2.390+0 1.388 1.24+0 5.27-2 4.321-1 0.704	1.985 3.43-1 -4.46-4 1.042+0 1.265 1.27+0 6.71-2 1.784+0 1.343 1.36+0 6.19-2 2.910-1 0.648
$E_b = 1006.0 \text{ eV}$ $3p_{1/2} E_b = 869.7 \text{ eV}$ $3p_{3/2} E_b = 818.7 \text{ eV}$ $3d_{3/2}$	β γ δ σ β γ δ δ σ β γ γ δ δ σ σ β γ γ δ δ σ σ σ δ σ σ σ σ σ σ σ σ σ σ σ σ	1.968 4.65-1 -1.10-4 6.567+1 1.487 8.63-2 8.96-3 1.358+2 1.521 3.85-2 7.07-3 1.567+2	1.972 2.09-1 -2.21-4 4.105+1 1.588 -2.17-2 1.75-3 8.167+1 1.625 -3.36-2 4.48-3 6.820+1	1.979 -3.91-2 -3.16-4 1.885+1 1.604 9.64-2 4.12-3 3.590+1 1.655 1.14-1 8.74-3	1.985 -1.13-1 -3.62-4 1.015+1 1.565 3.07-1 9.88-3 1.882+1 1.625 3.41-1 1.40-2 7.646+0	1.989 -1.03-1 -3.90-4 6.072+0 1.514 5.14-1 1.73-2 1.104+1 1.581 5.61-1 2.01-2 3.583+0	1.991 -4.72-2 -4.09-4 3.911+0 1.461 7.04-1 2.59-2 6.999+0 1.532 7.61-1 2.72-2 1.892+0	1.991 3.40-2 -4.23-4 2.660+0 1.410 8.72-1 3.56-2 4.697+0 1.483 9.40-1 3.52-2 1.089+0	1.990 1.30-1 -4.33-4 1.886+0 1.360 1.02+0 4.58-2 3.293+0 1.435 1.10+0 4.37-2 6.688-1	1.988 2.34-1 -4.41-4 1.383+0 1.312 1.16+0 5.64-2 2.390+0 1.388 1.24+0 5.27-2	1.985 3.43-1 -4.46-4 1.042+0 1.265 1.27+0 6.71-2 1.784+0 1.343 1.36+0 6.19-2 2.910-1
$E_b = 1006.0 \text{ eV}$ $3p_{1/2}$ $E_b = 869.7 \text{ eV}$ $3p_{3/2}$ $E_b = 818.7 \text{ eV}$ $3d_{3/2}$ $E_b = 582.5 \text{ eV}$	β γ δ σ β γ δ δ σ β γ δ δ σ β γ δ δ σ β γ δ δ σ β γ δ δ σ β γ δ δ σ β γ δ δ σ β γ δ δ σ σ δ δ σ δ δ σ δ δ σ δ δ σ σ δ δ σ σ δ δ σ σ δ δ σ σ σ δ δ σ σ σ σ δ δ σ	1.968 4.65-1 -1.10-4 6.567+1 1.487 8.63-2 8.96-3 1.358+2 1.521 3.85-2 7.07-3 1.567+2 1.201 1.24-1 4.73-2 2.253+2	1.972 2.09-1 -2.21-4 4.105+1 1.588 -2.17-2 1.75-3 8.167+1 1.625 -3.36-2 4.48-3 6.820+1 1.237 3.24-1 6.44-2 9.747+1	1.979 -3.91-2 -3.16-4 1.885+1 1.604 9.64-2 4.12-3 3.590+1 1.655 1.14-1 8.74-3 1.956+1 1.176 6.40-1 9.29-2 2.771+1	1.985 -1.13-1 -3.62-4 1.015+1 1.565 3.07-1 9.88-3 1.882+1 1.625 3.41-1 1.40-2 7.646+0 1.083 8.66-1 1.21-1	1.989 -1.03-1 -3.90-4 6.072+0 1.514 5.14-1 1.73-2 1.104+1 1.581 5.61-1 2.01-2 3.583+0 0.993 1.04+0 1.51-1 5.016+0	1.991 -4.72-2 -4.09-4 3.911+0 1.461 7.04-1 2.59-2 6.999+0 1.532 7.61-1 2.72-2 1.892+0 0.909 1.17+0 1.80-1 2.636+0	1.991 3.40-2 -4.23-4 2.660+0 1.410 8.72-1 3.56-2 4.697+0 1.483 9.40-1 3.52-2 1.089+0 0.834 1.27+0 2.08-1	1.990 1.30-1 -4.33-4 1.886+0 1.360 1.02+0 4.58-2 3.293+0 1.435 1.10+0 4.37-2 6.688-1 0.766 1.35+0 2.35-1	1.988 2.34-1 -4.41-4 1.383+0 1.312 1.16+0 5.64-2 2.390+0 1.388 1.24+0 5.27-2 4.321-1 0.704 1.41+0 2.61-1 5.941-1	1.985 3.43-1 -4.46-4 1.042+0 1.265 1.27+0 6.71-2 1.784+0 1.364 6.19-2 2.910-1 0.648 1.46+0 2.87-1 3.984-1
$E_b = 1006.0 \text{ eV}$ $3p_{1/2}$ $E_b = 869.7 \text{ eV}$ $3p_{3/2}$ $E_b = 818.7 \text{ eV}$ $3d_{3/2}$ $E_b = 582.5 \text{ eV}$ $3d_{5/2}$ $E_b = 60.0 \text{ eV}$	β γ δ σ β γ δ δ σ β γ δ σ β γ δ σ β γ δ σ β γ δ σ β γ δ	1.968 4.65-1 -1.10-4 6.567+1 1.487 8.63-2 8.96-3 1.358+2 1.521 3.85-2 7.07-3 1.567+2 1.201 1.24-1 4.73-2 2.253+2 1.205	1.972 2.09-1 -2.21-4 4.105+1 1.588 -2.17-2 1.75-3 8.167+1 1.625 -3.36-2 4.48-3 6.820+1 1.237 3.24-1 6.44-2 9.747+1 1.222	1.979 -3.91-2 -3.16-4 1.885+1 1.604 9.64-2 4.12-3 3.590+1 1.655 1.14-1 8.74-3 1.956+1 1.176 6.40-1 9.29-2 2.771+1 1.145	1.985 -1.13-1 -3.62-4 1.015+1 1.565 3.07-1 9.88-3 1.882+1 1.625 3.41-1 1.40-2 7.646+0 1.083 8.66-1 1.21-1 1.077+1 1.048	1.989 -1.03-1 -3.90-4 6.072+0 1.514 5.14-1 1.73-2 1.104+1 1.581 5.61-1 2.01-2 3.583+0 0.993 1.04+0 1.51-1 5.016+0 0.958	1.991 -4.72-2 -4.09-4 3.911+0 1.461 7.04-1 2.59-2 6.999+0 1.532 7.61-1 2.72-2 1.892+0 0.909 1.17+0 1.80-1 2.636+0 0.878	1.991 3.40-2 -4.23-4 2.660+0 1.410 8.72-1 3.56-2 4.697+0 1.483 9.40-1 3.52-2 1.089+0 0.834 1.27+0 2.08-1 1.510+0 0.807	1.990 1.30-1 -4.33-4 1.886+0 1.360 1.02+0 4.58-2 3.293+0 1.435 1.10+0 4.37-2 6.688-1 0.766 1.35+0 2.35-1 9.232-1 0.743	1.988 2.34-1 -4.41-4 1.383+0 1.312 1.16+0 5.64-2 2.390+0 1.388 1.24+0 5.27-2 4.321-1 0.704 1.41+0 2.61-1 5.941-1 0.687	1.985 3.43-1 -4.46-4 1.042+0 1.265 1.27+0 6.71-2 1.784+0 1.343 1.36+0 6.19-2 2.910-1 0.648 1.46+0 2.87-1 3.984-1 0.637
$E_b = 1006.0 \text{ eV}$ $3p_{1/2}$ $E_b = 869.7 \text{ eV}$ $3p_{3/2}$ $E_b = 818.7 \text{ eV}$ $3d_{3/2}$ $E_b = 582.5 \text{ eV}$	β γ δ σ β γ δ δ σ β γ δ δ σ β γ δ δ σ β γ δ δ σ β γ δ δ σ β γ δ δ σ β γ δ δ σ β γ δ δ σ σ δ δ σ δ δ σ δ δ σ δ δ σ σ δ δ σ σ δ δ σ σ δ δ σ σ σ δ δ σ σ σ σ δ δ σ	1.968 4.65-1 -1.10-4 6.567+1 1.487 8.63-2 8.96-3 1.358+2 1.521 3.85-2 7.07-3 1.567+2 1.201 1.24-1 4.73-2 2.253+2	1.972 2.09-1 -2.21-4 4.105+1 1.588 -2.17-2 1.75-3 8.167+1 1.625 -3.36-2 4.48-3 6.820+1 1.237 3.24-1 6.44-2 9.747+1	1.979 -3.91-2 -3.16-4 1.885+1 1.604 9.64-2 4.12-3 3.590+1 1.655 1.14-1 8.74-3 1.956+1 1.176 6.40-1 9.29-2 2.771+1	1.985 -1.13-1 -3.62-4 1.015+1 1.565 3.07-1 9.88-3 1.882+1 1.625 3.41-1 1.40-2 7.646+0 1.083 8.66-1 1.21-1	1.989 -1.03-1 -3.90-4 6.072+0 1.514 5.14-1 1.73-2 1.104+1 1.581 5.61-1 2.01-2 3.583+0 0.993 1.04+0 1.51-1 5.016+0	1.991 -4.72-2 -4.09-4 3.911+0 1.461 7.04-1 2.59-2 6.999+0 1.532 7.61-1 2.72-2 1.892+0 0.909 1.17+0 1.80-1 2.636+0	1.991 3.40-2 -4.23-4 2.660+0 1.410 8.72-1 3.56-2 4.697+0 1.483 9.40-1 3.52-2 1.089+0 0.834 1.27+0 2.08-1	1.990 1.30-1 -4.33-4 1.886+0 1.360 1.02+0 4.58-2 3.293+0 1.435 1.10+0 4.37-2 6.688-1 0.766 1.35+0 2.35-1	1.988 2.34-1 -4.41-4 1.383+0 1.312 1.16+0 5.64-2 2.390+0 1.388 1.24+0 5.27-2 4.321-1 0.704 1.41+0 2.61-1 5.941-1	1.985 3.43-1 -4.46-4 1.042+0 1.265 1.27+0 6.71-2 1.784+0 1.364 6.19-2 2.910-1 0.648 1.46+0 2.87-1 3.984-1
$E_b = 1006.0 \text{ eV}$ $3p_{1/2}$ $E_b = 869.7 \text{ eV}$ $3p_{3/2}$ $E_b = 818.7 \text{ eV}$ $3d_{3/2}$ $E_b = 582.5 \text{ eV}$ $3d_{5/2}$ $E_b = 572.1 \text{ eV}$	β γ δ σ β γ δ δ σ β γ δ δ σ β γ δ σ β γ δ σ σ β γ δ σ σ β γ δ σ σ σ σ σ σ σ σ σ σ σ σ σ σ σ σ σ σ	1.968 4.65-1 -1.10-4 6.567+1 1.487 8.63-2 8.96-3 1.358+2 1.521 3.85-2 7.07-3 1.567+2 1.201 1.24-1 4.73-2 2.253+2 1.205 1.39-1 4.67-2 1.128+1	1.972 2.09-1 -2.21-4 4.105+1 1.588 -2.17-2 1.75-3 8.167+1 1.625 -3.36-2 4.48-3 6.820+1 1.237 3.24-1 6.44-2 9.747+1 1.222 3.39-1 6.47-2 6.800+0	1.979 -3.91-2 -3.16-4 1.885+1 1.604 9.64-2 4.12-3 3.590+1 1.655 1.14-1 8.74-3 1.956+1 1.176 6.40-1 9.29-2 2.771+1 1.145 6.46-1 9.57-2 3.245+0	1.985 -1.13-1 -3.62-4 1.015+1 1.565 3.07-1 9.88-3 1.882+1 1.625 3.41-1 1.40-2 7.646+0 1.083 8.66-1 1.21-1 1.077+1 1.048 8.63-1 1.26-1 1.886+0	1.989 -1.03-1 -3.90-4 6.072+0 1.514 5.14-1 1.73-2 1.104+1 1.581 5.61-1 2.01-2 3.583+0 0.993 1.04+0 1.51-1 5.016+0 0.958 1.03+0 1.58-1 1.225+0	1.991 -4.72-2 -4.09-4 3.911+0 1.461 7.04-1 2.59-2 6.999+0 1.532 7.61-1 2.72-2 1.892+0 0.909 1.17+0 1.80-1 2.636+0 0.878 1.15+0 1.88-1 8.539-1	1.991 3.40-2 -4.23-4 2.660+0 1.410 8.72-1 3.56-2 4.697+0 1.483 9.40-1 3.52-2 1.089+0 0.834 1.27+0 2.08-1 1.510+0 0.807 1.25+0 2.18-1 6.257-1	1.990 1.30-1 -4.33-4 1.886+0 1.360 1.02+0 4.58-2 3.293+0 1.435 1.10+0 4.37-2 6.688-1 0.766 1.35+0 2.35-1 9.232-1 0.743 1.33+0 2.46-1 4.756-1	1.988 2.34-1 -4.41-4 1.383+0 1.312 1.16+0 5.64-2 2.390+0 1.388 1.24+0 5.27-2 4.321-1 0.704 1.41+0 2.61-1 5.941-1 0.687 1.39+0 2.72-1 3.719-1	1.985 3.43-1 -4.46-4 1.042+0 1.265 1.27+0 6.71-2 1.784+0 1.343 1.36+0 6.19-2 2.910-1 0.648 1.46+0 2.87-1 3.984-1 0.637 1.45+0 2.98-1 2.976-1
$E_b = 1006.0 \text{ eV}$ $3p_{1/2}$ $E_b = 869.7 \text{ eV}$ $3p_{3/2}$ $E_b = 818.7 \text{ eV}$ $3d_{3/2}$ $E_b = 582.5 \text{ eV}$ $3d_{5/2}$ $E_b = 572.1 \text{ eV}$	β γ δ σ β γ δ δ σ β γ δ δ σ β γ δ δ σ β γ δ δ σ β γ δ δ σ β γ δ δ σ β γ δ δ σ β γ δ δ σ β γ δ δ σ β β γ δ δ σ δ β β γ δ δ σ δ β β γ δ δ σ δ β β γ δ δ σ δ δ δ δ δ δ δ δ δ δ δ δ δ δ δ δ	1.968 4.65-1 -1.10-4 6.567+1 1.487 8.63-2 8.96-3 1.358+2 1.521 3.85-2 7.07-3 1.567+2 1.201 1.24-1 4.73-2 2.253+2 1.205 1.39-1 4.67-2	1.972 2.09-1 -2.21-4 4.105+1 1.588 -2.17-2 1.75-3 8.167+1 1.625 -3.36-2 4.48-3 6.820+1 1.237 3.24-1 6.44-2 9.747+1 1.222 3.39-1 6.47-2	1.979 -3.91-2 -3.16-4 1.885+1 1.604 9.64-2 4.12-3 3.590+1 1.655 1.14-1 8.74-3 1.956+1 1.176 6.40-1 9.29-2 2.771+1 1.145 6.46-1 9.57-2	1.985 -1.13-1 -3.62-4 1.015+1 1.565 3.07-1 9.88-3 1.882+1 1.625 3.41-1 1.40-2 7.646+0 1.083 8.66-1 1.21-1 1.077+1 1.048 8.63-1 1.26-1	1.989 -1.03-1 -3.90-4 6.072+0 1.514 5.14-1 1.73-2 1.104+1 1.581 5.61-1 2.01-2 3.583+0 0.993 1.04+0 1.51-1 5.016+0 0.958 1.03+0 1.58-1	1.991 -4.72-2 -4.09-4 3.911+0 1.461 7.04-1 2.59-2 6.999+0 1.532 7.61-1 2.72-2 1.892+0 0.909 1.17+0 1.80-1 2.636+0 0.878 1.15+0 1.88-1	1.991 3.40-2 -4.23-4 2.660+0 1.410 8.72-1 3.56-2 4.697+0 1.483 9.40-1 3.52-2 1.089+0 0.834 1.27+0 2.08-1 1.510+0 0.807 1.25+0 2.18-1	1.990 1.30-1 -4.33-4 1.886+0 1.360 1.02+0 4.58-2 3.293+0 1.435 1.10+0 4.37-2 6.688-1 0.766 1.35+0 2.35-1 9.232-1 0.743 1.33+0 2.46-1	1.988 2.34-1 -4.41-4 1.383+0 1.312 1.16+0 5.64-2 2.390+0 1.388 1.24+0 5.27-2 4.321-1 0.704 1.41+0 2.61-1 5.941-1 0.687 1.39+0 2.72-1	1.985 3.43-1 -4.46-4 1.042+0 1.265 1.27+0 6.71-2 1.784+0 1.343 1.36+0 6.19-2 2.910-1 0.648 1.46+0 2.87-1 3.984-1 0.637 1.45+0
$E_b = 1006.0 \text{ eV}$ $3p_{1/2}$ $E_b = 869.7 \text{ eV}$ $3p_{3/2}$ $E_b = 818.7 \text{ eV}$ $3d_{3/2}$ $E_b = 582.5 \text{ eV}$ $3d_{5/2}$ $E_b = 572.1 \text{ eV}$	β γ δ σ β γ δ δ σ β γ δ δ σ β γ δ σ β γ δ σ σ β γ δ σ σ β γ δ σ σ σ σ σ σ σ σ σ σ σ σ σ σ σ σ σ σ	1.968 4.65-1 -1.10-4 6.567+1 1.487 8.63-2 8.96-3 1.358+2 1.521 3.85-2 7.07-3 1.567+2 1.201 1.24-1 4.73-2 2.253+2 1.205 1.39-1 4.67-2 1.128+1 1.978 8.71-2 -1.92-4	1.972 2.09-1 -2.21-4 4.105+1 1.588 -2.17-2 1.75-3 8.167+1 1.625 -3.36-2 4.48-3 6.820+1 1.237 3.24-1 6.44-2 9.747+1 1.222 3.39-1 6.47-2 6.800+0 1.980 -8.51-3 -2.41-4	1.979 -3.91-2 -3.16-4 1.885+1 1.604 9.64-2 4.12-3 3.590+1 1.655 1.14-1 8.74-3 1.956+1 1.176 6.40-1 9.29-2 2.771+1 1.145 6.46-1 9.57-2 3.245+0 1.985 -9.94-2 -3.02-4	1.985 -1.13-1 -3.62-4 1.015+1 1.565 3.07-1 9.88-3 1.882+1 1.625 3.41-1 1.40-2 7.646+0 1.083 8.66-1 1.21-1 1.077+1 1.048 8.63-1 1.26-1 1.886+0 1.988 -1.05-1 -3.39-4	1.989 -1.03-1 -3.90-4 6.072+0 1.514 5.14-1 1.73-2 1.104+1 1.581 5.61-1 2.01-2 3.583+0 0.993 1.04+0 1.51-1 5.016+0 0.958 1.03+0 1.58-1 1.225+0 1.990 -6.22-2 -3.64-4	1.991 -4.72-2 -4.09-4 3.911+0 1.461 7.04-1 2.59-2 6.999+0 1.532 7.61-1 2.72-2 1.892+0 0.909 1.17+0 1.80-1 2.636+0 0.878 1.15+0 1.88-1 8.539-1 1.991 9.20-3 -3.82-4	1.991 3.40-2 -4.23-4 2.660+0 1.410 8.72-1 3.56-2 4.697+0 1.483 9.40-1 3.52-2 1.089+0 0.834 1.27+0 2.08-1 1.510+0 0.807 1.25+0 2.18-1 6.257-1 1.990 9.80-2 -3.97-4	1.990 1.30-1 -4.33-4 1.886+0 1.360 1.02+0 4.58-2 3.293+0 1.435 1.10+0 4.37-2 6.688-1 0.766 1.35+0 2.35-1 9.232-1 0.743 1.33+0 2.46-1 4.756-1 1.989 1.97-1 -4.08-4	1.988 2.34-1 -4.41-4 1.383+0 1.312 1.16+0 5.64-2 2.390+0 1.388 1.24+0 5.27-2 4.321-1 0.704 1.41+0 2.61-1 5.941-1 0.687 1.39+0 2.72-1 3.719-1 1.986 3.03-1 -4.16-4	1.985 3.43-1 -4.46-4 1.265 1.27+0 6.71-2 1.784+0 1.343 1.36+0 6.19-2 2.910-1 0.648 1.46+0 2.87-1 0.637 1.45+0 2.98-1 2.976-1 1.983 4.11-1 -4.20-4
$E_b = 1006.0 \text{ eV}$ $3p_{1/2}$ $E_b = 869.7 \text{ eV}$ $3p_{3/2}$ $E_b = 818.7 \text{ eV}$ $3d_{3/2}$ $E_b = 582.5 \text{ eV}$ $3d_{5/2}$ $E_b = 572.1 \text{ eV}$ $4s_{1/2}$ $E_b = 168.3 \text{ eV}$	β γ δ σ β γ δ δ σ β γ δ σ β γ δ σ β γ δ σ β γ δ σ σ β γ δ σ σ β γ δ σ σ β γ δ σ σ σ σ σ σ σ σ σ σ σ σ σ σ σ σ σ σ	1.968 4.65-1 -1.10-4 6.567+1 1.487 8.63-2 8.96-3 1.358+2 1.521 3.85-2 7.07-3 1.567+2 1.201 1.24-1 4.73-2 2.253+2 1.205 1.39-1 4.67-2 1.128+1 1.978 8.71-2 -1.92-4 1.296+1	1.972 2.09-1 -2.21-4 4.105+1 1.588 -2.17-2 1.75-3 8.167+1 1.625 -3.36-2 4.48-3 6.820+1 1.237 3.24-1 6.44-2 9.747+1 1.222 3.39-1 6.47-2 6.800+0 1.980 -8.51-3 -2.41-4 7.607+0	1.979 -3.91-2 -3.16-4 1.885+1 1.604 9.64-2 4.12-3 3.590+1 1.655 1.14-1 8.74-3 1.956+1 1.176 6.40-1 9.29-2 2.771+1 1.145 6.46-1 9.57-2 3.245+0 1.985 -9.94-2 -3.02-4 3.353+0	1.985 -1.13-1 -3.62-4 1.015+1 1.565 3.07-1 9.88-3 1.882+1 1.625 3.41-1 1.40-2 7.646+0 1.083 8.66-1 1.21-1 1.077+1 1.048 8.63-1 1.26-1 1.886+0 1.988 -1.05-1 -3.39-4 1.789+0	1.989 -1.03-1 -3.90-4 6.072+0 1.514 5.14-1 1.73-2 1.104+1 1.581 5.61-1 2.01-2 3.583+0 0.993 1.04+0 1.51-1 5.016+0 0.958 1.03+0 1.58-1 1.225+0 1.990 -6.22-2 -3.64-4 1.070+0	1.991 -4.72-2 -4.09-4 3.911+0 1.461 7.04-1 2.59-2 6.999+0 1.532 7.61-1 2.72-2 1.892+0 0.909 1.17+0 1.80-1 2.636+0 0.878 1.15+0 1.88-1 8.539-1 1.991 9.20-3 -3.82-4 6.903-1	1.991 3.40-2 -4.23-4 2.660+0 1.410 8.72-1 3.56-2 4.697+0 1.483 9.40-1 3.52-2 1.089+0 0.834 1.27+0 2.08-1 1.510+0 0.807 1.25+0 2.18-1 6.257-1 1.990 9.80-2 -3.97-4 4.705-1	1.990 1.30-1 -4.33-4 1.886+0 1.360 1.02+0 4.58-2 3.293+0 1.435 1.10+0 4.37-2 6.688-1 0.766 1.35+0 2.35-1 9.232-1 0.743 1.33+0 2.46-1 4.756-1 1.989 1.97-1 -4.08-4 3.344-1	1.988 2.34-1 -4.41-4 1.383+0 1.312 1.16+0 5.64-2 2.390+0 1.388 1.24+0 5.27-2 4.321-1 0.704 1.41+0 2.61-1 5.941-1 0.687 1.39+0 2.72-1 3.719-1 1.986 3.03-1 -4.16-4 2.457-1	1.985 3.43-1 -4.46-4 1.265 1.27+0 6.71-2 1.784+0 1.343 1.36+0 6.19-2 2.910-1 0.648 1.46+0 2.87-1 3.984-1 0.637 1.45+0 2.976-1 1.983 4.11-1 -4.20-4 1.855-1
$E_b = 1006.0 \text{ eV}$ $3p_{1/2} = E_b = 869.7 \text{ eV}$ $3p_{3/2} = E_b = 818.7 \text{ eV}$ $3d_{3/2} = E_b = 582.5 \text{ eV}$ $3d_{5/2} = E_b = 572.1 \text{ eV}$ $4s_{1/2} = E_b = 168.3 \text{ eV}$	β γ δ σ β γ δ σ β γ δ σ β γ δ σ β γ δ σ β γ δ σ β γ δ σ β γ δ σ β γ δ σ β γ δ σ β γ δ σ β γ δ	1.968 4.65-1 -1.10-4 6.567+1 1.487 8.63-2 8.96-3 1.358+2 1.521 3.85-2 7.07-3 1.567+2 1.201 1.24-1 4.73-2 2.253+2 1.205 1.39-1 4.67-2 1.128+1 1.978 8.71-2 -1.92-4	1.972 2.09-1 -2.21-4 4.105+1 1.588 -2.17-2 1.75-3 8.167+1 1.625 -3.36-2 4.48-3 6.820+1 1.237 3.24-1 6.44-2 9.747+1 1.222 3.39-1 6.47-2 6.800+0 1.980 -8.51-3 -2.41-4	1.979 -3.91-2 -3.16-4 1.885+1 1.604 9.64-2 4.12-3 3.590+1 1.655 1.14-1 8.74-3 1.956+1 1.176 6.40-1 9.29-2 2.771+1 1.145 6.46-1 9.57-2 3.245+0 1.985 -9.94-2 -3.02-4	1.985 -1.13-1 -3.62-4 1.015+1 1.565 3.07-1 9.88-3 1.882+1 1.625 3.41-1 1.40-2 7.646+0 1.083 8.66-1 1.21-1 1.077+1 1.048 8.63-1 1.26-1 1.886+0 1.988 -1.05-1 -3.39-4	1.989 -1.03-1 -3.90-4 6.072+0 1.514 5.14-1 1.73-2 1.104+1 1.581 5.61-1 2.01-2 3.583+0 0.993 1.04+0 1.51-1 5.016+0 0.958 1.03+0 1.58-1 1.225+0 1.990 -6.22-2 -3.64-4	1.991 -4.72-2 -4.09-4 3.911+0 1.461 7.04-1 2.59-2 6.999+0 1.532 7.61-1 2.72-2 1.892+0 0.909 1.17+0 1.80-1 2.636+0 0.878 1.15+0 1.88-1 8.539-1 1.991 9.20-3 -3.82-4	1.991 3.40-2 -4.23-4 2.660+0 1.410 8.72-1 3.56-2 4.697+0 1.483 9.40-1 3.52-2 1.089+0 0.834 1.27+0 2.08-1 1.510+0 0.807 1.25+0 2.18-1 6.257-1 1.990 9.80-2 -3.97-4	1.990 1.30-1 -4.33-4 1.886+0 1.360 1.02+0 4.58-2 3.293+0 1.435 1.10+0 4.37-2 6.688-1 0.766 1.35+0 2.35-1 9.232-1 0.743 1.33+0 2.46-1 4.756-1 1.989 1.97-1 -4.08-4	1.988 2.34-1 -4.41-4 1.383+0 1.312 1.16+0 5.64-2 2.390+0 1.388 1.24+0 5.27-2 4.321-1 0.704 1.41+0 2.61-1 5.941-1 0.687 1.39+0 2.72-1 3.719-1 1.986 3.03-1 -4.16-4	1.985 3.43-1 -4.46-4 1.265 1.27+0 6.71-2 1.784+0 1.343 1.36+0 6.19-2 2.910-1 0.648 1.46+0 2.87-1 0.637 1.45+0 2.98-1 2.976-1 1.983 4.11-1 -4.20-4
$E_b = 1006.0 \text{ eV}$ $3p_{1/2}$ $E_b = 869.7 \text{ eV}$ $3p_{3/2}$ $E_b = 818.7 \text{ eV}$ $3d_{3/2}$ $E_b = 582.5 \text{ eV}$ $3d_{5/2}$ $E_b = 168.3 \text{ eV}$ $4p_{1/2}$ $E_b = 1068.3 \text{ eV}$	β γ δ σ β γ δ δ σ β γ δ σ β σ β γ δ σ β γ δ σ β γ δ σ β γ δ σ β γ δ σ β σ β γ δ σ β σ β σ β σ β σ β σ β σ β σ β σ β σ	1.968 4.65-1 -1.10-4 6.567+1 1.487 8.63-2 8.96-3 1.358+2 1.521 3.85-2 7.07-3 1.567+2 1.201 1.24-1 4.73-2 2.253+2 1.205 1.39-1 4.67-2 1.128+1 1.978 8.71-2 -1.92-4 1.296+1 1.693	1.972 2.09-1 -2.21-4 4.105+1 1.588 -2.17-2 1.75-3 8.167+1 1.625 -3.36-2 4.48-3 6.820+1 1.237 3.24-1 6.44-2 9.747+1 1.222 3.39-1 6.47-2 6.800+0 1.980 -8.51-3 -2.41-4 7.607+0 1.682	1.979 -3.91-2 -3.16-4 1.885+1 1.604 9.64-2 4.12-3 3.590+1 1.655 1.14-1 8.74-3 1.956+1 1.176 6.40-1 9.29-2 2.771+1 1.145 6.46-1 9.57-2 3.245+0 1.985 -9.94-2 -3.02-4 3.353+0 1.628	1.985 -1.13-1 -3.62-4 1.015+1 1.565 3.07-1 9.88-3 1.882+1 1.625 3.41-1 1.40-2 7.646+0 1.083 8.66-1 1.21-1 1.077+1 1.048 8.63-1 1.26-1 1.886+0 1.988 -1.05-1 -3.39-4 1.789+0 1.567	1.989 -1.03-1 -3.90-4 6.072+0 1.514 5.14-1 1.73-2 1.104+1 1.581 5.61-1 2.01-2 3.583+0 0.993 1.04+0 1.51-1 5.016+0 0.958 1.03+0 1.58-1 1.225+0 1.990 -6.22-2 -3.64-4 1.070+0 1.506	1.991 -4.72-2 -4.09-4 3.911+0 1.461 7.04-1 2.59-2 6.999+0 1.532 7.61-1 2.72-2 1.892+0 0.909 1.17+0 1.80-1 2.636+0 0.878 1.15+0 1.88-1 8.539-1 1.991 9.20-3 -3.82-4 6.903-1 1.449	1.991 3.40-2 -4.23-4 2.660+0 1.410 8.72-1 3.56-2 4.697+0 1.483 9.40-1 3.52-2 1.089+0 0.834 1.27+0 2.08-1 1.510+0 0.807 1.25+0 2.18-1 6.257-1 1.990 9.80-2 -3.97-4 4.705-1 1.395	1.990 1.30-1 -4.33-4 1.886+0 1.360 1.02+0 4.58-2 3.293+0 1.435 1.10+0 4.37-2 6.688-1 0.766 1.35+0 2.35-1 9.232-1 0.743 1.33+0 2.46-1 4.756-1 1.989 1.97-1 -4.08-4 3.344-1 1.344	1.988 2.34-1 -4.41-4 1.383+0 1.312 1.16+0 5.64-2 2.390+0 1.388 1.24+0 5.27-2 4.321-1 0.704 1.41+0 2.61-1 5.941-1 0.687 1.39+0 2.72-1 3.719-1 1.986 3.03-1 -4.16-4 2.457-1 1.295	1.985 3.43-1 -4.46-4 1.265 1.27+0 6.71-2 1.784+0 1.343 1.36+0 6.19-2 2.910-1 0.648 1.46+0 2.87-1 3.984-1 0.637 1.45+0 2.98-1 1.983 4.11-1 -4.20-4 1.855-1 1.249
$E_b = 1006.0 \text{ eV}$ $3p_{1/2}$ $E_b = 869.7 \text{ eV}$ $3p_{3/2}$ $E_b = 818.7 \text{ eV}$ $3d_{3/2}$ $E_b = 582.5 \text{ eV}$ $3d_{5/2}$ $E_b = 672.1 \text{ eV}$ $4s_{1/2}$ $E_b = 1168.3 \text{ eV}$ $4p_{3/2}$	β γ δ σ β γ δ δ σ β γ δ δ σ β γ δ δ σ β γ δ δ σ β γ δ δ σ β γ δ δ σ β γ δ δ σ β γ δ δ σ β γ δ δ σ β γ δ δ σ β γ δ δ σ β γ δ δ σ β γ δ δ σ β γ δ δ σ β γ δ δ σ β γ δ δ σ β γ δ δ σ β γ δ δ σ δ β γ δ δ σ σ β γ δ δ σ σ β γ δ δ σ σ β γ δ δ σ σ β γ δ δ σ σ δ δ γ δ δ σ σ δ δ γ δ δ σ σ δ δ γ δ δ σ σ δ δ γ δ δ σ σ σ δ δ γ δ δ σ σ δ δ γ δ δ σ σ σ δ δ γ δ δ σ σ σ δ δ δ γ δ δ σ σ σ δ δ δ δ	1.968 4.65-1 -1.10-4 6.567+1 1.487 8.63-2 8.96-3 1.358+2 1.521 3.85-2 7.07-3 1.567+2 1.201 1.24-1 4.73-2 2.253+2 1.205 1.39-1 4.67-2 1.128+1 1.978 8.71-2 -1.92-4 1.296+1 1.693 -2.39-2 -1.01-3 2.570+1	1.972 2.09-1 -2.21-4 4.105+1 1.588 -2.17-2 1.75-3 8.167+1 1.625 -3.36-2 4.48-3 6.820+1 1.237 3.24-1 6.44-2 9.747+1 1.222 3.39-1 6.47-2 6.800+0 1.980 -8.51-3 -2.41-4 7.607+0 1.682 1.80-2 -2.16-4 1.472+1	1.979 -3.91-2 -3.16-4 1.885+1 1.604 9.64-2 4.12-3 3.590+1 1.655 1.14-1 8.74-3 1.956+1 1.176 6.40-1 9.29-2 2.771+1 1.145 6.46-1 9.57-2 3.245+0 1.985 -9.94-2 -3.02-4 3.353+0 1.628 1.98-1 3.23-3 6.281+0	1.985 -1.13-1 -3.62-4 1.015+1 1.565 3.07-1 9.88-3 1.882+1 1.625 3.41-1 1.40-2 7.646+0 1.083 8.66-1 1.21-1 1.077+1 1.048 8.63-1 1.26-1 1.886+0 1.988 -1.05-1 -3.39-4 1.789+0 1.567 4.00-1 8.92-3 3.277+0	1.989 -1.03-1 -3.90-4 6.072+0 1.514 5.14-1 1.73-2 1.104+1 1.581 5.61-1 2.01-2 3.583+0 0.993 1.04+0 1.51-1 5.016+0 0.958 1.03+0 1.58-1 1.225+0 1.990 -6.22-2 -3.64-4 1.070+0 1.506 5.92-1 1.64-2 1.925+0	1.991 -4.72-2 -4.09-4 3.911+0 1.461 7.04-1 2.59-2 6.999+0 1.532 7.61-1 2.72-2 1.892+0 0.909 1.17+0 1.80-1 2.636+0 0.878 1.15+0 1.88-1 8.539-1 1.991 9.20-3 -3.82-4 6.903-1 1.449 7.67-1 2.52-2 1.224+0	1.991 3.40-2 -4.23-4 2.660+0 1.410 8.72-1 3.56-2 4.697+0 1.483 9.40-1 3.52-2 1.089+0 0.834 1.27+0 2.08-1 1.510+0 0.807 1.25+0 2.18-1 6.257-1 1.990 9.80-2 -3.97-4 4.705-1 1.395 9.24-1 3.48-2 8.243-1	1.990 1.30-1 -4.33-4 1.886+0 1.360 1.02+0 4.58-2 3.293+0 1.435 1.10+0 4.37-2 6.688-1 0.766 1.35+0 2.35-1 9.232-1 0.743 1.33+0 2.46-1 4.756-1 1.989 1.97-1 -4.08-4 3.344-1 1.344 1.06+0 4.52-2 5.796-1	1.988 2.34-1 -4.41-4 1.383+0 1.312 1.16+0 5.64-2 2.390+0 1.388 1.24+0 5.27-2 4.321-1 0.704 1.41+0 2.61-1 5.941-1 0.687 1.39+0 2.72-1 3.719-1 1.986 3.03-1 -4.16-4 2.457-1 1.295 1.19+0 5.59-2 4.218-1	1.985 3.43-1 -4.46-4 1.042+0 1.265 1.27+0 6.71-2 1.784+0 1.343 1.36+0 6.19-2 2.910-1 0.648 1.46+0 2.87-1 3.984-1 0.637 1.45+0 2.98-1 2.976-1 1.983 4.11-1 -4.20-4 1.855-1 1.249 1.30+0 6.68-2 3.156-1
$E_b = 1006.0 \text{ eV}$ $3p_{1/2} E_b = 869.7 \text{ eV}$ $3p_{3/2} E_b = 818.7 \text{ eV}$ $3d_{3/2} E_b = 582.5 \text{ eV}$ $3d_{5/2} E_b = 168.3 \text{ eV}$ $4p_{1/2} E_b = 116.8 \text{ eV}$	β γ δ σ β γ δ σ β γ δ σ β γ δ σ β γ δ σ β γ δ σ β γ δ σ β γ δ σ β γ δ σ β γ δ σ β γ	1.968 4.65-1 -1.10-4 6.567+1 1.487 8.63-2 8.96-3 1.358+2 1.521 3.85-2 7.07-3 1.567+2 1.201 1.24-1 4.73-2 2.253+2 1.205 1.39-1 4.67-2 1.128+1 1.978 8.71-2 -1.92-4 1.296+1 1.693 -2.39-2 -1.01-3 2.570+1 1.715	1.972 2.09-1 -2.21-4 4.105+1 1.588 -2.17-2 1.75-3 8.167+1 1.625 -3.36-2 4.48-3 6.820+1 1.237 3.24-1 6.44-2 9.747+1 1.222 3.39-1 6.47-2 6.800+0 1.980 -8.51-3 -2.41-4 7.607+0 1.682 1.80-2 -2.16-4 1.472+1 1.717	1.979 -3.91-2 -3.16-4 1.885+1 1.604 9.64-2 4.12-3 3.590+1 1.655 1.14-1 8.74-3 1.956+1 1.176 6.40-1 9.29-2 2.771+1 1.145 6.46-1 9.57-2 3.245+0 1.985 -9.94-2 -3.02-4 3.353+0 1.628 1.98-1 3.23-3 6.281+0 1.679	1.985 -1.13-1 -3.62-4 1.015+1 1.565 3.07-1 9.88-3 1.882+1 1.625 3.41-1 1.40-2 7.646+0 1.083 8.66-1 1.21-1 1.077+1 1.048 8.63-1 1.26-1 1.886+0 1.988 -1.05-1 -3.39-4 1.789+0 1.567 4.00-1 8.92-3 3.277+0 1.627	1.989 -1.03-1 -3.90-4 6.072+0 1.514 5.14-1 1.73-2 1.104+1 1.581 5.61-1 2.01-2 3.583+0 0.993 1.04+0 1.51-1 5.016+0 0.958 1.03+0 1.58-1 1.225+0 1.990 -6.22-2 -3.64-4 1.070+0 1.506 5.92-1 1.64-2 1.925+0 1.573	1.991 -4.72-2 -4.09-4 3.911+0 1.461 7.04-1 2.59-2 6.999+0 1.532 7.61-1 2.72-2 1.892+0 0.909 1.17+0 1.80-1 2.636+0 0.878 1.15+0 1.88-1 8.539-1 1.991 9.20-3 -3.82-4 6.903-1 1.449 7.67-1 2.52-2 1.224+0 1.520	1.991 3.40-2 -4.23-4 2.660+0 1.410 8.72-1 3.56-2 4.697+0 1.483 9.40-1 3.52-2 1.089+0 0.834 1.27+0 2.08-1 1.510+0 0.807 1.25+0 2.18-1 6.257-1 1.990 9.80-2 -3.97-4 4.705-1 1.395 9.24-1 3.48-2 8.243-1 1.468	1.990 1.30-1 -4.33-4 1.886+0 1.360 1.02+0 4.58-2 3.293+0 1.435 1.10+0 4.37-2 6.688-1 0.766 1.35+0 2.35-1 9.232-1 0.743 1.33+0 2.46-1 4.756-1 1.989 1.97-1 -4.08-4 3.344-1 1.344 1.06+0 4.52-2 5.796-1 1.419	1.988 2.34-1 -4.41-4 1.383+0 1.312 1.16+0 5.64-2 2.390+0 1.388 1.24+0 5.27-2 4.321-1 0.704 1.41+0 2.61-1 5.941-1 0.687 1.39+0 2.72-1 3.719-1 1.986 3.03-1 -4.16-4 2.457-1 1.295 1.19+0 5.59-2 4.218-1 1.371	1.985 3.43-1 -4.46-4 1.042+0 1.265 1.27+0 6.71-2 1.784+0 1.343 1.36+0 6.19-2 2.910-1 0.648 1.46+0 2.87-1 3.984-1 0.637 1.45+0 2.98-1 2.976-1 1.983 4.11-1 -4.20-4 1.855-1 1.249 1.30+0 6.68-2 3.156-1 1.326
$E_b = 1006.0 \text{ eV}$ $3p_{1/2}$ $E_b = 869.7 \text{ eV}$ $3p_{3/2}$ $E_b = 818.7 \text{ eV}$ $3d_{3/2}$ $E_b = 582.5 \text{ eV}$ $3d_{5/2}$ $E_b = 672.1 \text{ eV}$ $4s_{1/2}$ $E_b = 1168.3 \text{ eV}$ $4p_{3/2}$	β γ δ σ β γ δ δ σ β γ δ δ σ β γ δ δ σ β γ δ δ σ β γ δ δ σ β γ δ δ σ β γ δ δ σ β γ δ δ σ β γ δ δ σ β γ δ δ σ β γ δ δ σ β γ δ δ σ β γ δ δ σ β γ δ δ σ β γ δ δ σ β γ δ δ σ β γ δ δ σ β γ δ δ σ δ β γ δ δ σ σ β γ δ δ σ σ β γ δ δ σ σ β γ δ δ σ σ β γ δ δ σ σ δ δ γ δ δ σ σ δ δ γ δ δ σ σ δ δ γ δ δ σ σ δ δ γ δ δ σ σ σ δ δ γ δ δ σ σ δ δ γ δ δ σ σ σ δ δ γ δ δ σ σ σ δ δ δ γ δ δ σ σ σ δ δ δ δ	1.968 4.65-1 -1.10-4 6.567+1 1.487 8.63-2 8.96-3 1.358+2 1.521 3.85-2 7.07-3 1.567+2 1.201 1.24-1 4.73-2 2.253+2 1.205 1.39-1 4.67-2 1.128+1 1.978 8.71-2 -1.92-4 1.296+1 1.693 -2.39-2 -1.01-3 2.570+1	1.972 2.09-1 -2.21-4 4.105+1 1.588 -2.17-2 1.75-3 8.167+1 1.625 -3.36-2 4.48-3 6.820+1 1.237 3.24-1 6.44-2 9.747+1 1.222 3.39-1 6.47-2 6.800+0 1.980 -8.51-3 -2.41-4 7.607+0 1.682 1.80-2 -2.16-4 1.472+1	1.979 -3.91-2 -3.16-4 1.885+1 1.604 9.64-2 4.12-3 3.590+1 1.655 1.14-1 8.74-3 1.956+1 1.176 6.40-1 9.29-2 2.771+1 1.145 6.46-1 9.57-2 3.245+0 1.985 -9.94-2 -3.02-4 3.353+0 1.628 1.98-1 3.23-3 6.281+0	1.985 -1.13-1 -3.62-4 1.015+1 1.565 3.07-1 9.88-3 1.882+1 1.625 3.41-1 1.40-2 7.646+0 1.083 8.66-1 1.21-1 1.077+1 1.048 8.63-1 1.26-1 1.886+0 1.988 -1.05-1 -3.39-4 1.789+0 1.567 4.00-1 8.92-3 3.277+0	1.989 -1.03-1 -3.90-4 6.072+0 1.514 5.14-1 1.73-2 1.104+1 1.581 5.61-1 2.01-2 3.583+0 0.993 1.04+0 1.51-1 5.016+0 0.958 1.03+0 1.58-1 1.225+0 1.990 -6.22-2 -3.64-4 1.070+0 1.506 5.92-1 1.64-2 1.925+0	1.991 -4.72-2 -4.09-4 3.911+0 1.461 7.04-1 2.59-2 6.999+0 1.532 7.61-1 2.72-2 1.892+0 0.909 1.17+0 1.80-1 2.636+0 0.878 1.15+0 1.88-1 8.539-1 1.991 9.20-3 -3.82-4 6.903-1 1.449 7.67-1 2.52-2 1.224+0	1.991 3.40-2 -4.23-4 2.660+0 1.410 8.72-1 3.56-2 4.697+0 1.483 9.40-1 3.52-2 1.089+0 0.834 1.27+0 2.08-1 1.510+0 0.807 1.25+0 2.18-1 6.257-1 1.990 9.80-2 -3.97-4 4.705-1 1.395 9.24-1 3.48-2 8.243-1	1.990 1.30-1 -4.33-4 1.886+0 1.360 1.02+0 4.58-2 3.293+0 1.435 1.10+0 4.37-2 6.688-1 0.766 1.35+0 2.35-1 9.232-1 0.743 1.33+0 2.46-1 4.756-1 1.989 1.97-1 -4.08-4 3.344-1 1.344 1.06+0 4.52-2 5.796-1	1.988 2.34-1 -4.41-4 1.383+0 1.312 1.16+0 5.64-2 2.390+0 1.388 1.24+0 5.27-2 4.321-1 0.704 1.41+0 2.61-1 5.941-1 0.687 1.39+0 2.72-1 3.719-1 1.986 3.03-1 -4.16-4 2.457-1 1.295 1.19+0 5.59-2 4.218-1	1.985 3.43-1 -4.46-4 1.042+0 1.265 1.27+0 6.71-2 1.784+0 1.343 1.36+0 6.19-2 2.910-1 0.648 1.46+0 2.87-1 3.984-1 0.637 1.45+0 2.98-1 1.983 4.11-1 -4.20-4 1.855-1 1.249 1.30+0 6.68-2 3.156-1
$E_b = 1006.0 \text{ eV}$ $3p_{1/2}$ $E_b = 869.7 \text{ eV}$ $3p_{3/2}$ $E_b = 818.7 \text{ eV}$ $3d_{3/2}$ $E_b = 582.5 \text{ eV}$ $3d_{5/2}$ $E_b = 572.1 \text{ eV}$ $4s_{1/2}$ $E_b = 168.3 \text{ eV}$ $4p_{1/2}$ $E_b = 116.8 \text{ eV}$ $4p_{3/2}$ $E_b = 96.9 \text{ eV}$	β γ δ σ β γ δ σ β γ δ σ β γ δ σ β γ δ σ β γ δ σ β γ δ σ σ σ σ σ	1.968 4.65-1 -1.10-4 6.567+1 1.487 8.63-2 8.96-3 1.358+2 1.521 3.85-2 7.07-3 1.567+2 1.201 1.24-1 4.73-2 2.253+2 1.205 1.39-1 4.67-2 1.128+1 1.978 8.71-2 -1.92-4 1.296+1 1.693 -2.39-2 -1.01-3 2.570+1 1.715 -2.92-2 1.69-3 1.767+1	1.972 2.09-1 -2.21-4 4.105+1 1.588 -2.17-2 1.75-3 8.167+1 1.625 -3.36-2 4.48-3 6.820+1 1.237 3.24-1 6.44-2 9.747+1 1.222 3.39-1 6.47-2 6.800+0 1.980 -8.51-3 -2.41-4 7.607+0 1.682 1.80-2 -2.16-4 1.472+1 1.717 2.34-2 3.50-3 8.155+0	1.979 -3.91-2 -3.16-4 1.885+1 1.604 9.64-2 4.12-3 3.590+1 1.655 1.14-1 8.74-3 1.956+1 1.176 6.40-1 9.29-2 2.771+1 1.145 6.46-1 9.57-2 3.245+0 1.985 -9.94-2 -3.02-4 3.353+0 1.628 1.98-1 3.23-3 6.281+0 1.679 2.19-1 7.42-3 2.514+0	1.985 -1.13-1 -3.62-4 1.015+1 1.565 3.07-1 9.88-3 1.882+1 1.625 3.41-1 1.40-2 7.646+0 1.083 8.66-1 1.21-1 1.077+1 1.048 8.63-1 1.26-1 1.886+0 1.988 -1.05-1 -3.39-4 1.789+0 1.567 4.00-1 8.92-3 3.277+0 1.627 4.34-1 1.24-2 1.027+0	1.989 -1.03-1 -3.90-4 6.072+0 1.514 5.14-1 1.73-2 1.104+1 1.581 5.61-1 2.01-2 3.583+0 0.993 1.04+0 1.51-1 5.016+0 0.958 1.03+0 1.58-1 1.225+0 1.990 -6.22-2 -3.64-4 1.070+0 1.506 5.92-1 1.64-2 1.925+0 1.925+0 1.573 6.37-1 1.86-2 4.955-1	1.991 -4.72-2 -4.09-4 3.911+0 1.461 7.04-1 2.59-2 6.999+0 1.532 7.61-1 2.72-2 1.892+0 0.909 1.17+0 1.80-1 2.636+0 0.878 1.15+0 1.88-1 8.539-1 1.991 9.20-3 -3.82-4 6.903-1 1.449 7.67-1 2.52-2 1.224+0 1.520 8.22-1 2.59-2 2.670-1	1.991 3.40-2 -4.23-4 2.660+0 1.410 8.72-1 3.56-2 4.697+0 1.483 9.40-1 3.52-2 1.089+0 0.834 1.27+0 2.08-1 1.510+0 0.807 1.25+0 2.18-1 6.257-1 1.990 9.80-2 -3.97-4 4.705-1 1.395 9.24-1 3.48-2 8.243-1 1.468 9.88-1 3.40-2 1.559-1	1.990 1.30-1 -4.33-4 1.886+0 1.360 1.02+0 4.58-2 3.293+0 1.435 1.10+0 4.37-2 6.688-1 0.766 1.35+0 2.35-1 9.232-1 0.743 1.33+0 2.46-1 4.756-1 1.989 1.97-1 -4.08-4 3.344-1 1.344 1.06+0 4.52-2 5.796-1 1.419 1.14+0 4.27-2 9.682-2	1.988 2.34-1 -4.41-4 1.383+0 1.312 1.16+0 5.64-2 2.390+0 1.388 1.24+0 5.27-2 4.321-1 0.704 1.41+0 2.61-1 5.941-1 0.687 1.39+0 2.72-1 3.719-1 1.986 3.03-1 -4.16-4 2.457-1 1.295 1.19+0 5.59-2 4.218-1 1.371 1.27+0 5.19-2 6.309-2	1.985 3.43-1 -4.46-4 1.265 1.27+0 6.71-2 1.784+0 1.343 1.36+0 6.19-2 2.910-1 0.648 1.46+0 2.87-1 0.637 1.45+0 2.98-1 2.976-1 1.983 4.11-1 -4.20-4 1.855-1 1.249 1.30+0 6.68-2 3.156-1 1.326 1.38+0 6.13-2 4.277-2
$E_b = 1006.0 \text{ eV}$ $3p_{1/2} E_b = 869.7 \text{ eV}$ $3p_{3/2} E_b = 818.7 \text{ eV}$ $3d_{3/2} E_b = 582.5 \text{ eV}$ $3d_{5/2} E_b = 168.3 \text{ eV}$ $4s_{1/2} E_b = 168.3 \text{ eV}$ $4p_{1/2} E_b = 116.8 \text{ eV}$	β γ δ σ β γ δ σ β γ δ σ β γ δ σ β γ δ σ β γ δ γ	1.968 4.65-1 -1.10-4 6.567+1 1.487 8.63-2 8.96-3 1.358+2 1.521 3.85-2 7.07-3 1.567+2 1.201 1.24-1 4.73-2 2.253+2 1.205 1.39-1 4.67-2 1.128+1 1.978 8.71-2 -1.92-4 1.296+1 1.693 -2.39-2 -1.01-3 2.570+1 1.715 -2.92-2 1.69-3	1.972 2.09-1 -2.21-4 4.105+1 1.588 -2.17-2 1.75-3 8.167+1 1.625 -3.36-2 4.48-3 6.820+1 1.237 3.24-1 6.44-2 9.747+1 1.222 3.39-1 6.47-2 6.800+0 1.980 -8.51-3 -2.41-4 7.607+0 1.682 1.80-2 -2.16-4 1.472+1 1.717 2.34-2 3.50-3	1.979 -3.91-2 -3.16-4 1.885+1 1.604 9.64-2 4.12-3 3.590+1 1.655 1.14-1 8.74-3 1.956+1 1.176 6.40-1 9.29-2 2.771+1 1.145 6.46-1 9.57-2 3.245+0 1.985 -9.94-2 -3.02-4 3.353+0 1.628 1.98-1 3.23-3 6.281+0 1.679 2.19-1 7.42-3	1.985 -1.13-1 -3.62-4 1.015+1 1.565 3.07-1 9.88-3 1.882+1 1.625 3.41-1 1.40-2 7.646+0 1.083 8.66-1 1.21-1 1.077+1 1.048 8.63-1 1.26-1 1.886+0 1.988 -1.05-1 -3.39-4 1.789+0 1.567 4.00-1 8.92-3 3.277+0 1.627 4.34-1 1.24-2	1.989 -1.03-1 -3.90-4 6.072+0 1.514 5.14-1 1.73-2 1.104+1 1.581 5.61-1 2.01-2 3.583+0 0.993 1.04+0 1.51-1 5.016+0 0.958 1.03+0 1.58-1 1.225+0 1.990 -6.22-2 -3.64-4 1.070+0 1.506 5.92-1 1.64-2 1.925+0 1.573 6.37-1 1.86-2	1.991 -4.72-2 -4.09-4 3.911+0 1.461 7.04-1 2.59-2 6.999+0 1.532 7.61-1 2.72-2 1.892+0 0.909 1.17+0 1.80-1 2.636+0 0.878 1.15+0 1.88-1 8.539-1 1.991 9.20-3 -3.82-4 6.903-1 1.449 7.67-1 2.52-2 1.224+0 1.520 8.22-1 2.59-2	1.991 3.40-2 -4.23-4 2.660+0 1.410 8.72-1 3.56-2 4.697+0 1.483 9.40-1 3.52-2 1.089+0 0.834 1.27+0 2.08-1 1.510+0 0.807 1.25+0 2.18-1 6.257-1 1.990 9.80-2 -3.97-4 4.705-1 1.395 9.24-1 3.48-2 8.243-1 1.468 9.88-1 3.40-2	1.990 1.30-1 -4.33-4 1.886+0 1.360 1.02+0 4.58-2 3.293+0 1.435 1.10+0 4.37-2 6.688-1 0.766 1.35+0 2.35-1 9.232-1 0.743 1.33+0 2.46-1 4.756-1 1.989 1.97-1 -4.08-4 3.344-1 1.344 1.06+0 4.52-2 5.796-1 1.419 1.14+0 4.27-2	1.988 2.34-1 -4.41-4 1.383+0 1.312 1.16+0 5.64-2 2.390+0 1.388 1.24+0 5.27-2 4.321-1 0.704 1.41+0 2.61-1 5.941-1 0.687 1.39+0 2.72-1 3.719-1 1.986 3.03-1 -4.16-4 2.457-1 1.295 1.19+0 5.59-2 4.218-1 1.371 1.27+0 5.19-2	1.985 3.43-1 -4.46-4 1.042+0 1.265 1.27+0 6.71-2 1.784+0 1.343 1.36+0 6.19-2 2.910-1 0.648 1.46+0 2.87-1 3.984-1 0.637 1.45+0 2.98-1 2.976-1 1.983 4.11-1 -4.20-4 1.855-1 1.249 1.30+0 6.68-2 3.156-1 1.326 1.38+0

able 1 (contin 4d _{5/2}	σ	2.539+1	1.165+1	3.557+0	1.443+0	6.915-1	3.706-1	2.154-1	1.331-1	8.635-2	5.829-2
$E_b =$	β	1.323	1.263	1.135	1.026	0.934	0.854	0.784	0.723	0.668	0.619
39.2 eV	δ	2.65-1 4.18-2	4.30-1 5.77-2	6.87-1 8.94-2	8.80-1 1.22-1	1.03+0 1.54-1	1.15+0 1.86-1	1.25+0 2.16-1	1.32+0 2.44-1	1.39+0 2.71-1	1.44+0 2.97-1
5s _{1/2}	σ	1.308+0	7.804-1	3.678-1	2.124-1	1.375-1	9.562-2	6.995-2	5.311-2	4.150-2	3.318-2
$E_b =$	β	1.979	1.981	1.986	1.989	1.990	1.991	1.990	1.988	1.986	1.982
11.6 eV	δ	5.56-2 -1.97-4	-2.72-2 $-2.41-4$	-1.03-1 $-2.99-4$	-1.01-1 $-3.34-4$	-5.48-2 $-3.60-4$	1.91-2 -3.77-4	1.10-1 $-3.92-4$	2.10-1 $-4.03-4$	3.16-1 $-4.10-4$	4.25 - 1 $-4.18 - 4$
$5p_{1/2}$	σ	1.033+0	6.012-1	2.629-1	1.398-1	8.346-2	5.380-2	3.665-2	2.604-2	1.913-2	1.443-2
$E_b = 2.6 \text{ eV}$	β	1.710 -2.33-2	1.692 2.61-2	1.632 2.10-1	1.568 4.13-1	1.506 6.05-1	1.447 7.79-1	1.391 9.34-1	1.339 1.07+0	1.289 1.20+0	1.242 1.30+0
2.0 CV	δ	-1.30-3	-4.71-4	3.04-3	8.95-3	1.66-2	2.54-2	3.49-2	4.49-2	5.53-2	6.58-2
5p _{3/2}	σ	1.973+0	1.121+0	4.744-1	2.466-1	1.446-1	9.188-2	6.182-2	4.344-2	3.160-2	2.364-2
$E_b = 2.0 \text{ eV}$	β γ	1.731 -2.77-2	1.726 3.01-2	1.684 2.28-1	1.630 4.45-1	1.573 6.49-1	1.518 8.33-1	1.465 9.97-1	1.414 1.14+0	1.365 1.27+0	1.319 1.39+0
2.0 C V	δ	1.48-3	3.24-3	7.13-3	1.23-2	1.87-2	2.60-2	3.39-2	4.24-2	5.12-2	6.05-2
Z= 53, I : [Kr]4d _{3/2} 4	$d_{5/2}^6 5s_{1/2}^2 5p_{1/2}^2$	5p _{3/2}								
		k (eV)									
Shell		1500	2000	3000	4000	5000	6000	7000	8000	9000	10000
$3s_{1/2}$	σ_{ρ}	4.677+1	3.070+1 1.969	1.577+1	9.455+0	6.243+0	4.399+0 1.990	3.248+0 1.990	2.483+0 1.990	1.951+0	1.567+0
$E_b = 1072.1 \text{ eV}$	β γ	1.965 5.31-1	2.53-1	1.977 -1.90-2	1.983 -1.10-1	1.987 -1.12-1	-6.55-2	8.04-3	9.80-2	1.988 1.98-1	1.985 3.03-1
	δ	-9.31-5	-2.31-4	-3.41-4	-3.95 - 4	-4.27 - 4	-4.49-4	-4.65-4	-4.78-4	-4.86-4	-4.93-4
$3p_{1/2}$	σ_{ρ}	6.771+1 1.457	4.287+1 1.578	1.995+1	1.082+1 1.572	6.512+0 1.525	4.213+0 1.474	2.876+0 1.424	2.046+0 1.375	1.504+0 1.327	1.136+0 1.281
$E_b = 930.5 \text{ eV}$	β γ	1.457	-1.59-2	1.606 7.25-2	2.75-1	4.80-1	6.70-1	8.41-1	9.94—1	1.13+0	1.25+0
	δ	1.30-2	2.19-3	3.49-3	8.79-3	1.58-2	2.41-2	3.34-2	4.34-2	5.36-2	6.40-2
$3p_{3/2}$ $E_b =$	σ_{ρ}	1.414+2 1.489	8.581+1 1.614	3.811+1 1.657	2.010+1 1.634	1.185+1 1.593	7.539+0 1.547	5.076+0 1.500	3.568+0 1.453	2.596+0 1.407	1.942+0 1.362
$E_b = 874.6 \text{ eV}$	β γ	6.95-2	-3.39-2	8.84-2	3.08-1	5.27-1	7.28-1	9.10-1	1.433	1.407	1.302
	δ	9.50-3	4.57-3	8.37-3	1.34-2	1.91-2	2.59-2	3.36-2	4.18-2	5.04-2	5.92-2
$3d_{3/2}$ $E_b =$	$\frac{\sigma}{\beta}$	1.732+2 1.184	7.579+1 1.236	2.190+1 1.188	8.616+0 1.100	4.057+0 1.012	2.151+0 0.929	1.242+0 0.853	7.650-1 0.784	4.955-1 0.722	3.343-1 0.665
631.3 eV	γ	9.02-2	2.93-1	6.17-1	8.50-1	1.03+0	1.16+0	1.27+0	1.35+0	1.42+0	1.47+0
	δ	4.48-2	6.25-2	9.07-2	1.18-1	1.47-1	1.75-1	2.03-1	2.29-1	2.55-1	2.79-1
$3d_{5/2}$ $E_b =$	$\frac{\sigma}{eta}$	2.488+2 1.193	1.082+2 1.224	3.100+1 1.157	1.211+1 1.063	5.671+0 0.975	2.992+0 0.895	1.719+0 0.823	1.054+0 0.759	6.799-1 0.702	4.569-1 0.651
619.4 eV	γ	1.07-1	3.09 - 1	6.24 - 1	8.49 - 1	1.02+0	1.15+0	1.25+0	1.33+0	1.40+0	1.45+0
	δ	4.41-2	6.25-2	9.32-2	1.23-1	1.54-1	1.84-1	2.13-1	2.40-1	2.66-1	2.91-1
$4s_{1/2}$ $E_b =$	$\frac{\sigma}{\beta}$	1.204+1 1.976	7.280+0 1.978	3.480+0 1.983	2.025+0 1.987	1.317+0 1.989	9.193-1 1.990	6.745-1 1.990	5.134-1 1.989	4.020-1 1.986	3.220-1 1.983
186.4 eV	γ	1.04 - 1	4.53 - 3	-9.58 - 2	-1.10 - 1	-7.49 - 2	-1.03-2	7.26-2	1.67 - 1	2.69 - 1	3.74 - 1
	δ	-2.06-4	-2.60-4	-3.30-4	-3.71-4	-3.98-4	-4.19-4	-4.36-4	-4.49-4	-4.58-4	-4.64-4
$4p_{1/2}$ $E_b =$	$\frac{\sigma}{\beta}$	1.395+1 1.693	8.235+0 1.686	3.658+0 1.636	1.963+0 1.577	1.179+0 1.519	7.640-1 1.463	5.226-1 1.410	3.726-1 1.359	2.746-1 1.310	2.078-1 1.264
130.1 eV	γ	-2.37 - 2	7.84 - 3	1.77 - 1	3.75 - 1	5.65 - 1	7.40 - 1	8.98 - 1	1.04+0	1.17+0	1.28+0
	δ	-1.13-3	-5.01-4	2.56-3	7.82-3	1.50-2	2.35-2	3.28-2	4.28-2	5.31-2	6.36-2
$\begin{array}{l} 4p_{3/2} \\ E_b = \end{array}$	$\frac{\sigma}{\beta}$	2.800+1 1.713	1.610+1 1.720	6.905+0 1.688	3.617+0 1.639	2.133+0 1.587	1.361+0 1.536	9.188-1 1.485	6.477-1 1.436	4.724-1 1.390	3.542-1 1.344
119.0 eV	γ	-3.17 - 2	1.04 - 2	1.96 - 1	4.07 - 1	6.10 - 1	7.96 - 1	9.64 - 1	1.11+0	1.25+0	1.37+0
4.4	δ	1.53-3	3.30-3	7.02-3	1.16-2	1.76-2	2.46-2	3.23-2	4.07-2	4.94-2	5.84-2
$4d_{3/2}$ $E_b =$	$\frac{\sigma}{\beta}$	2.032+1 1.349	9.458+0 1.305	2.947+0 1.190	1.214+0 1.084	5.894-1 0.989	3.193-1 0.905	1.873-1 0.829	1.167—1 0.762	7.629-2 0.701	5.185-2 0.645
50.7 eV	γ	2.34-1	4.03-1	6.72-1	8.77-1	1.04+0	1.16+0	1.26+0	1.34+0	1.41+0	1.46+0
4.1	δ	4.00-2 2.919+1	5.46-2	8.30-2	1.13-1	1.43-1	1.72-1	2.00-1	2.27-1 1.601-1	2.53-1	2.78-1
$4d_{5/2}$ $E_b =$	$\frac{\sigma}{\beta}$	1.331	1.350+1 1.275	4.164+0 1.151	1.702+0 1.043	8.212-1 0.950	4.424-1 0.870	2.582-1 0.799	0.737	1.042-1 0.681	7.053-2 0.632
48.9 eV	γ	2.46-1	4.12-1	6.74-1	8.71-1	1.02+0	1.15+0	1.25+0	1.33+0	1.39+0	1.44+0
56	δ	4.00-2 1.508+0	5.56-2 9.015-1	8.65-2 4.255-1	1.19-1 2.460-1	1.51-1 1.593-1	1.81-1 1.110-1	2.10-1 8.126-2	2.38-1 6.176-2	2.65-1 4.831-2	2.90-1 3.867-2
$5s_{1/2}$ $E_b =$	$\frac{\sigma}{\beta}$	1.977	1.980	1.984	1.987	1.989	1.990	1.990	1.988	1.986	1.983
13.6 eV	γ	6.73-2 $-2.12-4$	-1.77-2	-1.01-1	-1.07 - 1	-6.75-2 $-3.95-4$	8.08-6 $-4.16-4$	8.48-2 -4.33-4	1.80-1	2.81-1	3.87-1
5p _{1/2}	$\frac{\delta}{\sigma}$	1.260+0	-2.60-4 7.377-1	-3.27-4 3.248-1	-3.67-4 1.736-1	1.041-1	6.737-2	4.606-2	-4.45-4 3.283-2	-4.53-4 2.418-2	-4.63-4 1.829-2
$E_b =$	β	1.712	1.697	1.640	1.578	1.517	1.459	1.405	1.354	1.306	1.260
3.8 eV	γ	-2.47-2	1.60-2	1.90-1	3.90-1	5.79-1	7.52-1	9.07-1	1.05+0	1.17+0	1.28+0
5n _{2 /2}	$\frac{\delta}{\sigma}$	-1.48-3 2.412+0	-7.83-4 1.376+0	2.33-3 5.858-1	7.72-3 3.058-1	1.47-2 1.800-1	2.29-2 1.148-1	3.20-2 7.744-2	4.16-2 5.457-2	5.17-2 3.979-2	6.21-2 2.983-2
$5p_{3/2}$ $E_b =$	β	1.732	1.731	1.692	1.640	1.586	1.148-1	7.744-2 1.481	1.432	3.979-2 1.384	2.983—2 1.339
	•										

Table 1 (contin	ued)										
2.9 eV	γ δ	-3.06-2 1.33-3	1.90-2 3.05-3	2.09-1 6.74-3	4.22-1 1.15-2	6.24-1 1.73-2	8.07-1 2.41-2	9.72-1 3.14-2	1.12+0 3.94-2	1.25+0 4.79-2	1.37+0 5.68-2
Z= 54, Xe: [K	(r]4d _{3/2}	4d _{5/2} 5s _{1/2} 5p _{1/2}	2 5p _{3/2}								
Cl II		k (eV)	2000	2000	4000	5000	C000	7000	0000	0000	10000
Shell 3s _{1/2}	σ	1500 4.787+1	2000 3.175+1	3000 1.643+1	9.886+0	5000 6.542+0	6000 4.619+0	7000 3.415+0	8000 2.615+0	9000 2.057+0	10000
$E_b =$	β	1.962	1.966	1.974	1.981	1.985	1.988	1.989	1.989	1.988	1.986
1148.4 eV	δ	6.13-1 -6.17-5	3.07 - 1 $-2.35 - 4$	5.43-3 -3.68-4	-1.04-1 $-4.32-4$	-1.19-1 $-4.68-4$	-8.24-2 $-4.92-4$	-1.66-2 $-5.12-4$	6.73-2 $-5.26-4$	1.62-1 -5.37-4	2.64-1 -5.46-4
$3p_{1/2}$	σ	6.968+1	4.473+1	2.110+1	1.153+1	6.976+0	4.533+0	3.106+0	2.216+0	1.634+0	1.237+0
$E_b = 999.0 \text{ eV}$	$eta \ \gamma$	1.409 1.83-1	1.563 -3.72-3	1.608 4.97-2	1.579 2.43-1	1.535 4.45-1	1.486 6.35-1	1.438 8.09-1	1.389 9.64-1	1.342 1.10+0	1.297 1.22+0
333.0 CV	δ	1.97-2	3.01-3	2.93-3	7.77-3	1.43-2	2.23-2	3.13-2	4.08-2	5.06-2	6.05-2
$3p_{3/2}$	σ	1.470+2 1.454	9.012+1 1.601	4.044+1 1.659	2.145+1 1.641	1.270+1 1.604	8.111+0 1.561	5.478+0 1.515	3.861+0 1.469	2.815+0 1.424	2.110+0 1.379
$E_b = 937.0 \text{ eV}$	β γ	1.454	-2.96-2	6.34-2	2.75-1	4.92-1	6.95-1	8.79–1	1.469	1.424	1.32+0
	δ	1.31-2	4.85-3	8.01-3	1.28-2	1.82-2	2.46-2	3.19-2	3.98-2	4.78-2	5.61-2
$3d_{3/2}$ $E_b =$	$\frac{\sigma}{eta}$	1.927+2 1.161	8.467+1 1.233	2.461+1 1.200	9.722+0 1.117	4.596+0 1.031	2.446+0 0.949	1.416+0 0.872	8.741-1 0.803	5.674-1 0.741	3.835-1 0.685
690.6 eV	γ	5.31-2	2.56 - 1	5.91 - 1	8.32 - 1	1.02+0	1.16+0	1.27+0	1.35+0	1.42+0	1.48+0
24	δ	4.18-2	6.03-2	8.88-2	1.15-1	1.43-1	1.71-1	1.97-1	2.23-1	2.48-1	2.72-1
$3d_{5/2}$ $E_b =$	$\frac{\sigma}{eta}$	2.760+2 1.176	1.205+2 1.224	3.472+1 1.169	1.363+1 1.079	6.407+0 0.993	3.392+0 0.913	1.955+0 0.840	1.201+0 0.775	7.765-1 0.718	5.228-1 0.667
674.7 eV	γ δ	7.12-2 4.11-2	2.75 - 1 $6.01 - 2$	6.02-1 9.11-2	8.33-1 1.20-1	1.01+0	1.14+0 1.80-1	1.25+0 2.08-1	1.33+0	1.40+0 2.60-1	1.46+0 2.85-1
4s _{1/2}	σ	1.291+1	7.811+0	3.738+0	2.176+0	1.50-1 1.416+0	9.893-1	7.266-1	2.34-1 5.535-1	4.339-1	3.479-1
$E_b =$	β	1.974	1.976	1.981	1.985	1.988	1.989	1.989	1.988	1.986	1.984
217.7 eV	δ	1.25 - 1 $-2.18 - 4$	2.07-2 $-2.79-4$	-9.06-2 $-3.59-4$	-1.14-1 $-4.06-4$	-8.70-2 $-4.36-4$	-2.94-2 $-4.60-4$	4.78-2 $-4.79-4$	1.38-1 -4.94-4	2.35-1 -5.07-4	3.38-1 -5.15-4
4p _{1/2}	σ	1.510+1	8.959+0	4.004+0	2.158+0	1.301+0	8.460-1	5.805-1	4.150-1	3.065-1	2.324-1
$E_b = 163.9 \text{ eV}$	β	1.692	1.689 -2.99-3	1.644	1.587	1.531 5.36-1	1.476	1.424 8.72-1	1.373 1.02+0	1.325 1.14+0	1.279 1.26+0
105.9 ev	$\gamma \\ \delta$	-2.13-2 $-1.24-3$	-2.99-3 $-7.89-4$	1.54-1 1.88-3	3.48-1 6.70-3	1.34-2	7.12-1 2.16-2	3.06-2	4.01-2	4.99-2	5.99-2
4p _{3/2}	σ	3.064+1	1.768+1	7.608+0	3.996+0	2.363+0	1.512+0	1.023+0	7.228-1	5.282-1	3.967-1
$E_b = 156.5 \text{ eV}$	β γ	1.710 -3.22-2	1.722 -3.02-3	1.696 1.71-1	1.651 3.79-1	1.601 5.81-1	1.551 7.68-1	1.502 9.38-1	1.454 1.09+0	1.407 1.23+0	1.362 1.35+0
	δ	1.34-3	3.08-3	6.65-3	1.10-2	1.65-2	2.32-2	3.05-2	3.84-2	4.66-2	5.50-2
$4d_{3/2}$ $E_b =$	$\frac{\sigma}{eta}$	2.336+1 1.355	1.095+1 1.317	3.441+0 1.207	1.427+0 1.102	6.967-1 1.009	3.793-1 0.924	2.233-1 0.848	1.396-1 0.779	9.154-2 0.719	6.238-2 0.664
69.5 eV	γ	2.11 - 1	3.82 - 1	6.57 - 1	8.65-1	1.03+0	1.16+0	1.26+0	1.35+0	1.41+0	1.47+0
	δ	3.82-2	5.27-2	8.03-2	1.09-1	1.39-1	1.67-1	1.94-1	2.20-1	2.46-1	2.71-1
$4d_{5/2}$ $E_b =$	$\frac{\sigma}{eta}$	3.354+1 1.339	1.561+1 1.288	4.857+0 1.166	1.998+0 1.059	9.693-1 0.967	5.246-1 0.886	3.073-1 0.815	1.912-1 0.752	1.248-1 0.696	8.467-2 0.647
67.6 eV	γ	2.24 - 1	3.93 - 1	6.60 - 1	8.60 - 1	1.02+0	1.14+0	1.24+0	1.33+0	1.39+0	1.45+0
5s _{1/2}	$\frac{\delta}{\sigma}$	3.81-2 1.719+0	5.35-2 1.029+0	8.37-2 4.863-1	1.15-1 2.812-1	1.46-1 1.822-1	1.76-1 1.270-1	2.05-1 9.310-2	2.32-1 7.084-2	2.59-1 5.547-2	2.84-1 4.444-2
$E_b =$	β	1.975	1.978	1.982	1.986	1.988	1.989	1.989	1.988	1.986	1.983
23.4 eV	$\gamma \\ \delta$	8.12-2 $-2.26-4$	-6.68-3 $-2.82-4$	-9.81-2 $-3.56-4$	-1.12-1 $-4.01-4$	-7.94-2 $-4.33-4$	-1.83-2 $-4.55-4$	6.06-2 $-4.74-4$	1.51-1 -4.87-4	2.48 - 1 $-4.99 - 4$	3.50-1 $-5.08-4$
5p _{1/2}	σ	1.503+0	8.842-1	3.918-1	2.104-1	1.266-1	8.223-2	5.640-2	4.032-2	2.978-2	2.258-2
$E_b =$	β	1.714	1.702	1.649	1.588	1.529	1.473	1.420	1.371	1.324	1.279
13.4 eV	$_{\delta}^{\gamma}$	-2.51-2 $-1.65-3$	6.15 - 3 $-1.08 - 3$	1.70-1 1.64-3	3.65-1 6.55-3	5.52-1 1.31-2	7.24-1 $2.08-2$	8.80-1 $2.96-2$	1.02+0 3.90-2	1.15+0 4.89-2	1.26+0 5.92-2
5p _{3/2}	σ	2.885+0	1.653+0	7.066-1	3.702-1	2.186-1	1.398-1	9.458-2	6.682-2	4.884-2	3.668-2
$E_b = 12.1 \text{ eV}$	β	1.733 -3.28-2	1.735 7.79-3	1.701 1.88-1	1.651 3.97-1	1.599 5.97—1	1.548 7.80-1	1.498 9.46-1	1.450 1.10+0	1.405 1.23+0	1.361 1.35+0
12.1 CV	δ	1.16-3	2.86-3	6.36-3	1.08-2	1.61-2	2.24-2	2.94-2	3.71-2	4.54-2	5.41-2
Z= 55, Cs: [X	e]6s _{1/2}										
al .:		k (eV)			40						45
Shell		1500	2000	3000	4000	5000	6000	7000	8000	9000	10000
$3s_{1/2} E_b =$	$\frac{\sigma}{eta}$	4.865+1 1.959	3.263+1 1.963	1.702+1 1.972	1.029+1 1.979	6.830+0 1.984	4.833+0 1.987	3.580+0 1.988	2.744+0 1.988	2.161+0 1.987	1.740+0 1.985
1217.1 eV	γ	6.87-1	3.55-1	3.00-2	-9.48 - 2	-1.23-1	-9.69-2	-3.85-2	3.96-2	1.30-1	2.27-1
3p _{1/2}	$\frac{\delta}{\sigma}$	-2.11-5 7.121+1	-2.38-4 4.636+1	-3.95-4 2.217+1	-4.65-4 1.222+1	-5.10-4 7.439+0	-5.41-4 4.855+0	-5.65-4 3.338+0	-5.83-4 2.389+0	-5.95-4 1.765+0	-6.06-4 1.340+0
$E_b =$	β	1.363	1.549	1.608	1.585	1.544	1.497	1.448	1.401	1.356	1.312
1065.0 eV	$\gamma \\ \delta$	2.35-1 2.77-2	1.33-2 4.14-3	3.07-2 2.47-3	2.12-1 $6.92-3$	4.13-1 1.33-2	6.05 - 1 $2.08 - 2$	7.77 - 1 $2.89 - 2$	9.32-1 3.76-2	1.07+0 4.67-2	1.19+0 5.62-2
	U	2.11-2	J	2.41-3	0.32-3	1.33-2	2.00-2	2.03-2	5.70-2	4.07-2	3.02-2

Tabl	e 1	(contin	ued)

abic i (contin	ucu)										
$3p_{3/2}$	σ	1.519+2	9.404+1	4.265+1	2.278+1	1.355+1	8.688+0	5.884+0	4.157+0	3.038+0	2.281+0
$E_b =$	β	1.409	1.587	1.660	1.648	1.614	1.573	1.528	1.483	1.439	1.397
997.6 eV	γ	1.49-1	-2.10-2	4.14-2 7.70-3	2.43-1 1.24-2	4.61-1	6.65-1	8.48-1 3.01-2	1.01+0	1.16+0	1.29+0
0.1	δ	1.81-2	5.31-3			1.78-2	2.37-2		3.71-2	4.44-2	5.22-2
$3d_{3/2}$	σ	2.094+2	9.267+1	2.720+1	1.082+1	5.142+0	2.748+0	1.597+0	9.890-1	6.438-1	4.362-1
$E_b = 739.5 \text{ eV}$	β	1.139 2.24-2	1.229 2.24-1	1.210 5.65-1	1.132 8.16-1	1.045 1.00+0	0.964	0.890 1.26+0	0.824 1.35+0	0.764 1.43+0	0.709 1.49+0
739.3 EV	$\gamma \\ \delta$	3.88-2	5.81-2	8.68-2	1.13-1	1.40-1	1.15+0 1.65-1	1.91-1	2.17-1	2.42-1	2.67-1
24	σ	3.011+2	1.322+2	3.843+1	1.518+1	7.170+0	3.810+0	2.204+0	1.358+0	8.804-1	5.941-1
$3d_{5/2}$ $E_b =$	β	1.158	1.322+2	3.843+1 1.180	1.518+1	1.005	0.925	0.855	0.793	0.737	0.687
725.5 eV	γ	3.95-2	2.44-1	5.78-1	8.18-1	9.96-1	1.13+0	1.24+0	1.33+0	1.41+0	1.47+0
	δ	3.80-2	5.77-2	8.89-2	1.18-1	1.47 - 1	1.74 - 1	2.02 - 1	2.29 - 1	2.55 - 1	2.80 - 1
4s _{1/2}	σ	1.364+1	8.282+0	3.977+0	2.321+0	1.513+0	1.058+0	7.783-1	5.937-1	4.658-1	3.738-1
$E_b =$	β	1.972	1.975	1.980	1.984	1.987	1.988	1.988	1.988	1.986	1.984
230.8 eV	γ	1.40 - 1	3.32 - 2	-8.39 - 2	-1.16-1	-9.70 - 2	-4.56-2	2.64 - 2	1.11 - 1	2.05 - 1	3.03 - 1
	δ	-2.33-4	-3.00-4	-3.86-4	-4.40-4	-4.78-4	-5.08-4	-5.30-4	-5.46-4	-5.62-4	-5.72-4
$4p_{1/2}$	σ	1.604+1	9.579+0	4.319+0	2.343+0	1.420+0	9.265 - 1	6.379 - 1	4.574 - 1	3.388 - 1	2.575 - 1
$E_b =$	β	1.690	1.691	1.650	1.596	1.540	1.486	1.434	1.385	1.339	1.294
172.3 eV	γ	-1.83-2	-8.97-3	1.35-1	3.25-1	5.13-1	6.87-1	8.45-1	9.88-1	1.12+0	1.23+0
	δ	-1.33-3	-9.84-4	1.40-3	6.02-3	1.23-2	1.97-2	2.79-2	3.67-2	4.60-2	5.56-2
$4p_{3/2}$	σ	3.269+1	1.896+1	8.223+0	4.343+0	2.579+0	1.656+0	1.124+0	7.962-1	5.832-1	4.390-1
$E_b = 161.6 \text{ eV}$	β	1.708	1.724	1.703	1.660	1.612	1.563	1.514	1.467	1.422	1.379
161.6 eV	$\gamma \\ \delta$	-3.13-2 1.25-3	-1.03-2 $2.95-3$	1.52-1 6.41-3	3.57-1 1.07-2	5.58-1 1.59-2	7.44-1 2.18-2	9.13-1 2.84-2	1.06+0 3.55-2	1.20+0 4.32-2	1.33+0 5.11-2
1.1		2.621+1	1.241+1	3.948+0	1.650+0	8.107-1	4.437-1	2.625-1	1.648-1	1.084-1	7.410-2
$\begin{array}{l} 4d_{3/2} \\ E_b = \end{array}$	$\frac{\sigma}{eta}$	2.621+1 1.359	1.241+1	3.948+0 1.223	1.650+0	8.107—1 1.022	4.437—1 0.939	2.625—1 0.866	0.801	0.741	7.410-2 0.687
78.8 eV	γ	1.92-1	3.62-1	6.43-1	8.55-1	1.022	1.15+0	1.26+0	1.35+0	1.42+0	1.48+0
	δ	3.66-2	5.08-2	7.86-2	1.06-1	1.34-1	1.61-1	1.88-1	2.15-1	2.40-1	2.66-1
4d _{5/2}	σ	3.765+1	1.769+1	5.571+0	2.310+0	1.127+0	6.133-1	3.609-1	2.255-1	1.477-1	1.005-1
$E_b =$	β	1.344	1.298	1.181	1.073	0.979	0.898	0.830	0.769	0.715	0.666
76.5 eV	γ	2.06 - 1	3.74 - 1	6.47 - 1	8.50 - 1	1.01+0	1.14+0	1.24+0	1.33+0	1.40+0	1.46+0
	δ	3.63 - 2	5.15 - 2	8.18 - 2	1.12 - 1	1.42 - 1	1.71 - 1	1.99 - 1	2.27 - 1	2.54 - 1	2.79 - 1
5s _{1/2}	σ	2.026+0	1.216+0	5.760-1	3.336-1	2.165-1	1.511-1	1.109-1	8.448-2	6.622-2	5.311-2
$E_b =$	β	1.974	1.976	1.981	1.985	1.987	1.988	1.988	1.988	1.986	1.983
22.7 eV	γ	9.14-2	2.53-3	-9.35-2	-1.14-1	-8.87-2	-3.41-2	3.95-2	1.25-1	2.19-1	3.18-1
	δ	-2.43-4	-3.04-4	-3.84 - 4	-4.33-4	-4.70 - 4	-4.96-4	-5.18 - 4	-5.34 - 4	-5.47 - 4	-5.59 - 4
$5p_{1/2}$	σ	1.888+0	1.116+0	4.982-1	2.690-1	1.627-1	1.061-1	7.302-2	5.235-2	3.877-2	2.947-2
$E_b = 13.1 \text{ eV}$	β	1.715	1.705	1.656	1.598	1.541	1.486	1.434 8.57-1	1.384 9.99-1	1.337	1.292
	$\gamma \\ \delta$	-2.42-2 $-1.79-3$	-8.06-4 $-1.32-3$	1.52-1 1.02-3	3.40-1 5.61-3	5.26-1 1.20-2	6.99-1 1.97-2	2.82-2	3.73-2	1.13+0 4.68-2	1.24+0 5.64-2
F		3.690+0	2.122+0	9.129-1	4.805-1	2.849-1			8.789-2		4.847-2
$5p_{3/2}$ $E_b =$	$\frac{\sigma}{eta}$	1.733	1.738	9.129—1 1.708	4.805 – 1 1.662	1.613	1.828-1 1.563	1.241-1 1.515	8.789-2 1.467	6.439-2 1.422	4.847—2 1.378
11.4 eV	γ	-3.36-2	-3.88-4	1.69-1	3.72-1	5.70-1	7.56-1	9.24-1	1.08+0	1.21+0	1.33+0
	δ	1.04 - 3	2.72 - 3	5.98 - 3	1.01 - 2	1.54 - 2	2.16-2	2.86 - 2	3.60-2	4.39 - 2	5.20 - 2
6s _{1/2}	σ	1.083-1	6.478-2	3.059-2	1.769-2	1.146-2	7.993-3	5.862-3	4.463-3	3.497-3	2.804-3
$E_b =$	β	1.973	1.976	1.981	1.984	1.987	1.988	1.988	1.988	1.986	1.983
4.0 eV	γ	9.06 - 2	1.20 - 3	-9.43 - 2	-1.15 - 1	-8.94 - 2	-3.41-2	3.98 - 2	1.26 - 1	2.19 - 1	3.17 - 1
	δ	-2.44-4	-3.08 - 4	-3.85 - 4	-4.35 - 4	-4.73 - 4	-5.01-4	-5.19 - 4	-5.37 - 4	-5.48 - 4	-5.62 - 4
Z= 56, Ba: [X	e]6s _{1/2}										
	-,-	k (eV)									
Shell		1500	2000	3000	4000	5000	6000	7000	8000	9000	10000
$3s_{1/2}$	σ	4.926+1	3.348+1	1.762+1	1.070+1	7.122+0	5.049+0	3.746+0	2.876+0	2.268+0	1.828+0
$E_b = 1292.8 \text{ eV}$	$eta \ \gamma$	1.956 7.75-1	1.960 4.08-1	1.969 5.82-2	1.976 -8.46-2	1.981 -1.25-1	1.985 1.09 1	1.987 -5.83-2	1.988 1.28-2	1.987 9.68-2	1.986 1.89-1
1232.0 CV	δ	3.85-5	-2.35-4	-4.22-4	-5.40-2 $-5.08-4$	-5.59-4	-5.92-4	-6.17-4	-6.37 - 4	-6.51-4	-6.64-4
3p _{1/2}		7.254+1	4.800+1	2.327+1	1.293+1	7.915+0	5.188+0	3.580+0	2.571+0	1.905+0	1.449+0
$E_b =$	$\frac{\sigma}{eta}$	1.300	1.528	1.607	1.590	1.552	1.508	1.462	1.417	1.373	1.330
1136.7 eV	γ	2.93-1	3.72-2	1.40-2	1.82-1	3.78-1	5.67-1	7.40-1	8.97-1	1.04+0	1.17+0
	δ	4.03 - 2	5.90-3	2.09-3	5.93-3	1.17-2	1.87 - 2	2.66-2	3.52-2	4.44 - 2	5.40-2
3p _{3/2}	σ	1.566+2	9.808+1	4.493+1	2.415+1	1.443+1	9.284+0	6.307+0	4,468+0	3.273+0	2.463+0
$E_b =$	β	1.360	1.568	1.659	1.654	1.624	1.585	1.544	1.501	1.459	1.418
1062.2 eV	γ	1.94 - 1	-7.83 - 3	2.16-2	2.13 - 1	4.25 - 1	6.27 - 1	8.12 - 1	9.80 - 1	1.13+0	1.27+0
	δ	2.48 - 2	6.10 - 3	7.44 - 3	1.18-2	1.67 - 2	2.22-2	2.85 - 2	3.53-2	4.26 - 2	5.04-2
3d _{3/2}	σ	2.284+2	1.017+2	3.009+1	1.204+1	5.751+0	3.086+0	1.800+0	1.118+0	7.292-1	4.951-1
$E_b =$	β	1.111	1.221	1.218	1.146	1.065	0.987	0.914	0.847	0.785	0.728
796.1 eV	γ	-1.05-2	1.89-1	5.34-1	7.92-1	9.87-1	1.14+0	1.26+0	1.36+0	1.43+0	1.50+0
	δ	3.50-2	5.58-2	8.39-2	1.10-1	1.36-1	1.62-1	1.88-1	2.13-1	2.38-1	2.61-1
3d _{5/2}	σ	3.284+2	1.450+2	4.246+1	1.687+1	8.006+0	4.272+0	2.479+0	1.533+0	9.955-1	6.731-1

able 1 (contin	ued)										
$E_b =$	β	1.135	1.218	1.189	1.107	1.023	0.946	0.876	0.812	0.755	0.703
780.7 eV	$_{\delta}^{\gamma}$	6.39-3 3.42-2	2.10-1 5.52-2	5.50-1 8.56-2	7.97-1 1.14-1	9.82-1 1.43-1	1.13+0 1.71-1	1.24+0 1.99-1	1.33+0 2.25-1	1.41+0 2.51-1	1.47+0 2.75-1
4s _{1/2}	σ	1.443+1	8.789+0	4.234+0	2.474+0	1.614+0	1.131+0	8.323-1	6.356-1	4.992-1	4.011-1
$E_b =$	β	1.970	1.973	1.978	1.982	1.985	1.987	1.988	1.987	1.986	1.984
253.0 eV	$_{\delta}^{\gamma}$	1.57-1 -2.46-4	4.79-2 $-3.23-4$	-7.77-2 $-4.22-4$	-1.18-1 $-4.82-4$	-1.05-1 $-5.23-4$	-6.05-2 $-5.55-4$	5.24-3 -5.78-4	8.45-2 $-5.96-4$	1.73-1 -6.13-4	2.67-1 $-6.25-4$
4p _{1/2}	σ	1.707+1	1.025+1	4.660+0	2.541+0	1.546+0	1.013+0	6.999-1	5.035-1	3.739-1	2.849-1
$E_b =$	β	1.689	1.693	1.656	1.605	1.551	1.499	1.449	1.402	1.357	1.313
191.8 eV	$_{\delta}^{\gamma}$	-1.29-2 $-1.34-3$	-1.45-2 $-1.18-3$	1.17 - 1 $8.08 - 4$	3.00-1 4.88-3	4.84 - 1 $1.06 - 2$	6.56-1 1.77-2	8.15 - 1 $2.58 - 2$	9.60-1 $3.46-2$	1.09+0 4.38-2	1.21+0 5.35-2
4p _{3/2}	σ	3.500+1	2.039+1	8.900+0	4.721+0	2.813+0	1.811+0	1.233+0	8.760-1	6.432-1	4.852-1
$E_b =$	β	1.705	1.725	1.709	1.670	1.624	1.578	1.532	1.487	1.443	1.401
179.7 eV	$_{\delta}^{\gamma}$	-2.85-2 $1.16-3$	-1.78-2 $2.81-3$	1.33-1 6.10-3	3.31-1 9.95-3	5.29-1 1.47-2	7.14-1 $2.03-2$	8.84-1 2.67-2	1.04+0 3.38-2	1.18+0 4.14-2	1.31+0 4.93-2
4d _{3/2}	σ	2.934+1	1.400+1	4.505+0	1.898+0	9.384-1	5.164-1	3.069-1	1.934-1	1.276-1	8.744-2
$E_b =$	β	1.362	1.335	1.237	1.136	1.044	0.963	0.889	0.822	0.761	0.706
92.5 eV	$_{\delta}^{\gamma}$	1.72-1 3.48-2	3.39-1 4.85-2	6.23-1 7.51-2	8.40-1 $1.02-1$	1.01+0 1.30-1	1.15+0 1.57-1	1.26+0 1.84-1	1.35+0 2.10-1	1.43+0 2.35-1	1.49+0 2.59-1
4d _{5/2}	σ	4.216+1	1.997+1	6.357+0	2.655+0	1.304+0	7.132-1	4.216-1	2.643-1	1.736-1	1.184-1
$E_b =$	β	1.349	1.307	1.195	1.089	0.998	0.919	0.849	0.787	0.731	0.681
89.9 eV	δ	1.86-1 3.45-2	3.53-1 4.90-2	6.29-1 7.82-2	8.37 - 1 $1.08 - 1$	1.00+0 1.38-1	1.13+0 1.67-1	1.24+0 1.96-1	1.33+0 2.23-1	1.40+0 2.49-1	1.46+0 2.74-1
5s _{1/2}	σ	2.359+0	1.419+0	6.739-1	3.907-1	2.537-1	1.772-1	1.302-1	9.925-2	7.787-2	6.250-2
$E_b =$	β	1.972	1.974	1.979	1.983	1.985	1.987	1.987	1.987	1.985	1.983
29.1 eV	$\delta \gamma$	1.03-1 $-2.60-4$	1.29-2 $-3.30-4$	-9.02-2 $-4.22-4$	-1.18-1 $-4.76-4$	-9.84-2 $-5.17-4$	-4.94-2 $-5.46-4$	1.89-2 -5.71-4	9.97-2 $-5.88-4$	1.89 - 1 $-6.04 - 4$	2.83-1 $-6.18-4$
5p _{1/2}	σ	2.283+0	1.358+0	6.104-1	3.312-1	2.011-1	1.316-1	9.085-2	6.533-2	4.850-2	3.696-2
$E_b =$	β	1.717	1.709	1.663	1.606	1.550	1.497	1.445	1.397	1.351	1.307
16.6 eV	$\delta ^{\gamma }$	-2.22-2 $-1.90-3$	-7.10-3 $-1.56-3$	1.36-1 4.35-4	3.20-1 4.57-3	5.03-1 1.04-2	6.73-1 1.74-2	8.29-1 2.53-2	9.71-1 3.39-2	1.10+0 4.30-2	1.22+0 5.23-2
5p _{3/2}	σ	4.518+0	2.611+0	1.130+0	5.969-1	3.550-1	2.285-1	1.555-1	1.104-1	8.107-2	6.115-2
$E_b =$	β	1.733	1.741	1.715	1.671	1.623	1.575	1.528	1.481	1.437	1.395
14.6 eV	δ	-3.33-2 $9.14-4$	-8.10-3 $2.59-3$	1.52-1 5.73-3	3.51-1 9.56-3	5.47-1 1.43-2	7.30-1 $2.00-2$	8.97-1 2.62-2	1.05+0 3.31-2	1.19+0 4.05-2	1.31+0 4.81-2
6s _{1/2}	σ	1.865-1	1.118-1	5.288-2	3.058-2	1.983-2	1.384-2	1.016-2	7.744-3	6.074-3	4.875-3
$E_b = 5.0 \text{ eV}$	β γ	1.972 1.01-1	1.974 1.09-2	1.979 -9.13-2	1.983 -1.18-1	1.986 -9.76-2	1.987 -4.86-2	1.988 1.94-2	1.987 1.00-1	1.986 1.90-1	1.983 2.85-1
3.0 C V	δ	-2.62-4	-3.31-4	-4.22-4	-4.78 - 4	-5.15-4	-5.40-4	-5.60-4	-5.85-4	-6.02-4	-6.14-4
Z= 57, La: [X	e]5d _{3/2}	6s _{1/2}									
		k (eV)									
Shell		1500	2000	3000	4000	5000	6000	7000	8000	9000	10000
3s _{1/2}	σ_{ρ}	4.952+1 1.952	3.424+1 1.957	1.819+1 1.966	1.109+1 1.973	7.407+0 1.979	5.262+0 1.983	3.911+0 1.986	3.008+0 1.987	2.376+0 1.986	1.917+0 1.985
$E_b = 1361.3 \text{ eV}$	β γ	8.71–1	4.63-1	8.75-2	-7.12-2	-1.24-1	-1.18-1	-7.56-2	-1.14-2	6.71-2	1.55-1
	δ	1.25-4	-2.31-4	-4.50 - 4	-5.47 - 4	-6.04 - 4	-6.44 - 4	-6.72 - 4	-6.95 - 4	-7.12 - 4	-7.28-4
$\begin{array}{l} 3p_{1/2} \\ E_b = \end{array}$	$\frac{\sigma}{\beta}$	7.350+1 1.221	4.948+1 1.505	2.435+1 1.605	1.364+1 1.595	8.396+0 1.560	5.529+0 1.518	3.830+0 1.474	2.758+0 1.430	2.050+0 1.387	1.563+0 1.345
1204.4 eV	γ	3.40-1	6.67-2	7.07-4	1.54-1	3.44-1	5.32-1	7.06-1	8.66-1	1.01+0	1.14+0
	δ	5.69-2	8.26-3	1.83-3	5.15-3	1.05-2	1.72-2	2.49-2	3.34-2	4.23-2	5.14-2
$3p_{3/2}$ $E_b =$	$\frac{\sigma}{eta}$	1.609+2 1.297	1.019+2 1.547	4.720+1 1.657	2.553+1 1.659	1.533+1 1.633	9.897+0 1.597	6.745+0 1.558	4.791+0 1.517	3.517+0 1.476	2.652+0 1.435
1123.4 eV	γ	2.38-1	9.98 - 3	4.46 - 3	1.83-1	3.91-1	5.93 - 1	7.79 - 1	9.50 - 1	1.10+0	1.24+0
	δ	3.45-2	7.21-3	7.24-3	1.14-2	1.61-2	2.14-2	2.74-2	3.41-2	4.11-2	4.84-2
$3d_{3/2}$ $E_b =$	$\frac{\sigma}{\beta}$	2.475+2 1.079	1.110+2 1.212	3.311+1 1.225	1.334+1 1.161	6.401+0 1.082	3.448+0 1.005	2.018+0 0.932	1.257+0 0.864	8.221-1 0.802	5.593-1 0.745
848.5 eV	γ	-4.03-2	1.53-1	5.05-1	7.71-1	9.72-1	1.13+0	1.25+0	1.35+0	1.43+0	1.50+0
	δ	3.12-2	5.32-2	8.18-2	1.07-1	1.33-1	1.59-1	1.84-1	2.08-1	2.32-1	2.54-1
$3d_{5/2}$ $E_b =$	$\frac{\sigma}{\beta}$	3.558+2 1.110	1.581+2 1.212	4.668+1 1.197	1.866+1 1.121	8.897+0 1.039	4.767+0 0.962	2.775+0 0.891	1.720+0 0.827	1.120+0 0.769	7.589-1 0.717
831.7 eV	γ	-2.39-2	1.76 - 1	5.23 - 1	7.78 - 1	9.69 - 1	1.12+0	1.24+0	1.33+0	1.41+0	1.48+0
	δ	3.06-2	5.25-2	8.33-2	1.12-1	1.40-1	1.68-1	1.94-1	2.20-1	2.45-1	2.69-1
$4s_{1/2} E_b =$	$\frac{\sigma}{\beta}$	1.521+1 1.968	9.289+0 1.970	4.490+0 1.976	2.628+0 1.980	1.717+0 1.983	1.204+0 1.986	8.875-1 1.987	6.785-1 1.986	5.335-1 1.985	4.291-1 1.984
$E_b = 270.4 \text{ eV}$	γ	1.73-1	6.25-2	-6.96-2	-1.17-1	-1.12-1	-7.39-2	-1.41-2	6.02-2	1.44-1	2.35-1
	δ	-2.62-4	-3.47 - 4	-4.55-4	-5.22-4	-5.68-4	-6.03-4	-6.31-4	-6.50-4	-6.70-4	-6.85-4
$4p_{1/2}$	σ_{ρ}	1.807+1	1.092+1	5.005+0 1.662	2.744+0	1.678+0	1.103+0	7.649-1	5.519-1	4.109-1	3.139-1
$E_b = 205.8 \text{ eV}$	β γ	1.686 -6.60-3	1.694 1.84-2	1.662 1.00-1	1.613 2.76-1	1.561 4.57-1	1.511 6.29-1	1.462 7.89-1	1.415 9.35-1	1.370 1.07+0	1.327 1.19+0
	-										

	δ	-1.35-3	-1.34 - 3	3.55-4	4.08-3	9.53-3	1.64-2	2.42-2	3.27-2	4.16-2	5.08-2
$4p_{3/2}$	σ	3.727+1	2.182+1	9.585+0	5.107+0	3.055+0	1.974+0	1.348+0	9.597-1	7.062-1	5.338-
$E_b = 191.4 \text{ eV}$	β	1.702 -2.51-2	1.725 -2.36-2	1.714 1.15-1	1.679 3.07-1	1.636 5.02-1	1.591 6.87-1	1.546 8.59-1	1.502 1.02+0	1.459 1.16+0	1.417 1.29+0
191.4 ev	$\frac{\gamma}{\delta}$	1.09-3	2.70-3	5.90-3	9.54-3	1.40-2	1.95-2	2.57-2	3.25-2	3.97-2	4.71-2
4d _{3/2}	σ	3.256+1	1.569+1	5.107+0	2.168+0	1.079+0	5.966-1	3.561-1	2.252-1	1.491-1	1.024-
$E_b =$	β	1.365	1.343	1.251	1.153	1.062	0.981	0.906	0.838	0.777	0.721
100.7 eV	γ	1.53-1	3.19-1	6.06-1	8.28-1	1.00+0	1.14+0	1.26+0	1.35+0	1.43+0	1.49+0
	δ	3.32-2	4.68-2	7.29-2	9.96-2	1.27-1	1.53-1	1.79-1	2.04-1	2.29-1	2.52-1
$4d_{5/2}$ $E_b =$	$\frac{\sigma}{\beta}$	4.673+1 1.353	2.234+1 1.315	7.192+0 1.208	3.028+0 1.104	1.496+0 1.014	8.222-1 0.934	4.880-1 0.864	3.071-1 0.801	2.023-1 0.744	1.384- 0.693
97.7 eV	γ	1.68-1	3.34–1	6.14-1	8.26-1	9.92-1	1.13+0	1.24+0	1.33+0	1.40+0	1.47+0
	δ	3.27 - 2	4.71 - 2	7.58-2	1.05 - 1	1.35-1	1.63-1	1.91-1	2.17 - 1	2.43 - 1	2.67 - 1
5s _{1/2}	σ	2.653+0	1.599+0	7.613-1	4.419-1	2.872-1	2.008-1	1.476-1	1.127-1	8.847-2	7.108-
$E_b =$	β	1.970	1.972	1.977	1.981	1.984	1.986	1.987	1.986	1.985	1.983
32.3 eV	$\gamma \\ \delta$	1.15-1 -2.78-4	2.38-2 -3.55-4	-8.46-2 $-4.56-4$	-1.19-1 $-5.16-4$	-1.06-1 $-5.61-4$	-6.30-2 $-5.94-4$	-4.11-4 $-6.21-4$	7.53-2 $-6.40-4$	1.60-1 $-6.59-4$	2.50-1 -6.74-
5p _{1/2}	σ	2.599+0	1.554+0	7.036-1	3.837-1	2.339-1	1.536-1	1.064-1	7.674-2	5.713-2	4.363-
$E_b =$	β	1.717	1.712	1.669	1.615	1.561	1.509	1.459	1.413	1.368	1.325
16.6 eV	γ	-1.94-2	-1.23-2	1.19 - 1	2.97 - 1	4.76 - 1	6.45 - 1	8.02 - 1	9.45 - 1	1.08+0	1.20+0
	δ	-2.01-3	-1.76 - 3	-5.84 - 5	3.65-3	9.07-3	1.58-2	2.34-2	3.18-2	4.08-2	4.99-2
$5p_{3/2}$	σ	5.251+0	3.047+0	1.326+0	7.037-1	4.200-1	2.711-1	1.850-1	1.317-1	9.692-2	7.326-
$E_b = 13.3 \text{ eV}$	β γ	1.732 -3.24-2	1.743 -1.47-2	1.722 1.34-1	1.681 3.27-1	1.635 5.21-1	1.589 7.03-1	1.544 8.71-1	1.499 1.02+0	1.456 1.16+0	1.415 1.29+0
15.5 CV	δ	-3.24-2 $7.96-4$	2.47-3	5.48-3	9.02-3	1.35-2	1.87-2	2.48-2	3.14-2	3.85-2	4.60-2
5d _{3/2}	σ	2.041+0	9.857-1	3.215-1	1.366-1	6.805-2	3.768-2	2.251-2	1.425-2	9.443-3	6.492-
$E_b =$	β	1.385	1.354	1.253	1.150	1.057	0.975	0.902	0.836	0.777	0.722
6.0 eV	γ	1.67 - 1	3.34-1	6.19-1	8.36-1	1.01+0	1.14+0	1.26+0	1.35+0	1.43+0	1.49+0
	δ	3.21-2	4.56-2	7.19-2	9.84-2	1.25-1	1.51-1	1.77-1	2.03-1	2.28-1	2.52-1
$6s_{1/2} E_b =$	σ_{ρ}	2.261-1 1.970	1.358-1 1.972	6.434-2 1.977	3.725-2 1.981	2.418-2 1.984	1.689-2 1.986	1.241-2 1.987	9.466-3 1.986	7.431-3 1.985	5.968- 1.983
5.0 eV	β	1.12-1	2.15-2	-8.58-2	-1.19-1	-1.05-1	-6.25-2	2.99-4	7.68-2	1.62-1	2.54-1
.).U e v											
	$\frac{\gamma}{\delta}$	-2.80 - 4	-3.56-4	-4.55 - 4	-5.17 - 4	-5.59 - 4	-5.90 - 4	-6.14 - 4	-6.42 - 4	-6.62 - 4	-6.76-
Z= 58, Ce: [X	δ	-2.80 - 4			-5.17-4	-5.59-4	-5.90-4	-6.14-4	-6.42-4	-6.62-4	-6.76-
	δ	$-2.80-4$ $6s_{1/2}^2$ $k \text{ (eV)}$			-5.17-4	-5.59-4	-5.90-4	-6.14-4	-6.42-4	-6.62-4	-6.76-
	δ	$-2.80-4$ $6s_{1/2}^2$			-5.17-4 4000	-5.59-4 5000	-5.90-4 6000	7000	-6.42-4 8000	9000	10000
Z= 58, Ce: [X	$\frac{\delta}{\text{ce}]4f_{5/2}^2}$		-3.56-4 2000 3.515+1	-4.55-4 3000 1.885+1	4000 1.155+1	5000 7.728+0	6000 5.500+0	7000 4.094+0	8000 3.152+0	9000	10000
Z= 58, Ce: [X Shell $3s_{1/2}$ $E_b =$	$\frac{\delta}{\delta}$ (e)4 $f_{5/2}^2$ (2000 3.515+1 1.953	3000 1.885+1 1.962	4000 1.155+1 1.970	5000 7.728+0 1.976	6000 5.500+0 1.981	7000 4.094+0 1.984	8000 3.152+0 1.985	9000 2.492+0 1.985	10000 2.012+0 1.985
Z= 58, Ce: [X Shell $3s_{1/2}$	$\frac{\delta}{\text{fe]4f}_{5/2}^2}$ $\frac{\sigma}{\beta}$	-2.80-4 6s ² _{1/2} k (eV) 1500 4.933+1 1.947 1.01+0	2000 3.515+1 1.953 5.38-1	3000 1.885+1 1.962 1.25-1	4000 1.155+1 1.970 -5.46-2	5000 7.728+0 1.976 -1.22-1	6000 5.500+0 1.981 -1.27-1	7000 4.094+0 1.984 -9.32-2	8000 3.152+0 1.985 -3.54-2	9000 2.492+0 1.985 3.76-2	10000 2.012+0 1.985 1.20-1
Z= 58, Ce: [X Shell 3s _{1/2} E _b = 1434.6 eV	$\frac{\delta}{\text{ce}]\mathbf{4f}_{5/2}^2}$	-2.80-4 65s _{1/2} k (eV) 1500 4.933+1 1.947 1.01+0 3.81-4	2000 3.515+1 1.953 5.38-1 -2.14-4	3000 1.885+1 1.962 1.25-1 -4.79-4	4000 1.155+1 1.970 -5.46-2 -5.95-4	5000 7.728+0 1.976 -1.22-1 -6.62-4	6000 5.500+0 1.981 -1.27-1 -7.08-4	7000 4.094+0 1.984 -9.32-2 -7.40-4	8000 3.152+0 1.985 -3.54-2 -7.66-4	9000 2.492+0 1.985 3.76-2 -7.85-4	10000 2.012+0 1.985 1.20-1 -8.02-
Z= 58, Ce: [X Shell $3s_{1/2}$ $E_b =$	$\frac{\delta}{\text{fe]4f}_{5/2}^2}$ $\frac{\sigma}{\beta}$	-2.80-4 6s ² _{1/2} k (eV) 1500 4.933+1 1.947 1.01+0	2000 3.515+1 1.953 5.38-1	3000 1.885+1 1.962 1.25-1	4000 1.155+1 1.970 -5.46-2	5000 7.728+0 1.976 -1.22-1	6000 5.500+0 1.981 -1.27-1	7000 4.094+0 1.984 -9.32-2	8000 3.152+0 1.985 -3.54-2	9000 2.492+0 1.985 3.76-2	10000 2.012+(1.985 1.20-1 -8.02-
Z= 58, Ce: [X Shell $3s_{1/2}$ $E_b = 1434.6$ eV $3p_{1/2}$	δ $e 4f_{5/2}^2$ δ	$ \begin{array}{r} -2.80-4 \\ \hline 65s_{1/2}^2 \\ \underline{k \text{ (eV)}} \\ 1500 \\ 4.933+1 \\ 1.947 \\ 1.01+0 \\ 3.81-4 \\ 7.425+1 \\ 1.105 \\ 3.75-1 \end{array} $	2000 3.515+1 1.953 5.38-1 -2.14-4 5.111+1 1.477 1.10-1	3000 1.885+1 1.962 1.25-1 -4.79-4 2.555+1 1.601 -1.06-2	4000 1.155+1 1.970 -5.46-2 -5.95-4 1.443+1 1.598 1.26-1	5000 7.728+0 1.976 -1.22-1 -6.62-4 8.929+0 1.567 3.12-1	6000 5.500+0 1.981 -1.27-1 -7.08-4 5.903+0 1.527 4.98-1	7000 4.094+0 1.984 -9.32-2 -7.40-4 4.102+0 1.485 6.71-1	8000 3.152+0 1.985 -3.54-2 -7.66-4 2.962+0 1.442 8.30-1	9000 2.492+0 1.985 3.76-2 -7.85-4 2.207+0 1.400 9.75-1	10000 2.012+0 1.985 1.20-1 -8.02- 1.686+0 1.360 1.11+0
Z= 58, Ce: [X Shell $3s_{1/2}$ $E_b = 1434.6 \text{ eV}$ $3p_{1/2}$ $E_b = 1272.8 \text{ eV}$	δ (e)4f _{5/2} (σ β γ δ δ β γ δ δ β γ δ δ	-2.80-4 6s ² _{1/2} k (eV) 1500 4.933+1 1.947 1.01+0 3.81-4 7.425+1 1.105 3.75-1 8.54-2	2000 3.515+1 1.953 5.38-1 -2.14-4 5.111+1 1.477 1.10-1 1.20-2	3000 1.885+1 1.962 1.25-1 -4.79-4 2.555+1 1.601 -1.06-2 1.62-3	4000 1.155+1 1.970 -5.46-2 -5.95-4 1.443+1 1.598 1.26-1 4.36-3	5000 7.728+0 1.976 -1.22-1 -6.62-4 8.929+0 1.567 3.12-1 9.36-3	5.500+0 1.981 -1.27-1 -7.08-4 5.903+0 1.527 4.98-1 1.56-2	7000 4.094+0 1.984 -9.32-2 -7.40-4 4.102+0 1.485 6.71-1 2.27-2	8000 3.152+0 1.985 -3.54-2 -7.66-4 2.962+0 1.442 8.30-1 3.05-2	9000 2.492+0 1.985 3.76-2 -7.85-4 2.207+0 1.400 9.75-1 3.89-2	10000 2.012+0 1.985 1.20-1 -8.02- 1.686+0 1.360 1.11+0 4.77-2
Z= 58, Ce: [X Shell $3s_{1/2}$ $E_b = 1434.6 \text{ eV}$ $3p_{1/2}$ $E_b = 1272.8 \text{ eV}$ $3p_{3/2}$	$ \begin{array}{c} \delta \\ \mathbf{e} \mathbf{4f_{5/2}^2} 0 \\ \sigma \\ \beta \\ \gamma \\ \delta \\ \sigma \\ \beta \\ \gamma \\ \delta \\ \sigma \end{array} $	$\begin{array}{c} -2.80-4 \\ \hline 68_{1/2}^2 \\ \hline k (eV) \\ \hline 1500 \\ \hline 4.933+1 \\ 1.947 \\ 1.01+0 \\ 3.81-4 \\ \hline 7.425+1 \\ 1.105 \\ 3.75-1 \\ 8.54-2 \\ \hline 1.658+2 \\ \end{array}$	2000 3.515+1 1.953 5.38-1 -2.14-4 5.111+1 1.477 1.10-1 1.20-2 1.065+2	3000 1.885+1 1.962 1.25-1 -4.79-4 2.555+1 1.601 -1.06-2 1.62-3 4.983+1	4000 1.155+1 1.970 -5.46-2 -5.95-4 1.443+1 1.598 1.26-1 4.36-3 2.711+1	5000 7.728+0 1.976 -1.22-1 -6.62-4 8.929+0 1.567 3.12-1 9.36-3 1.634+1	5.500+0 1.981 -1.27-1 -7.08-4 5.903+0 1.527 4.98-1 1.56-2 1.058+1	7000 4.094+0 1.984 -9.32-2 -7.40-4 4.102+0 1.485 6.71-1 2.27-2 7.228+0	8000 3.152+0 1.985 -3.54-2 -7.66-4 2.962+0 1.442 8.30-1 3.05-2 5.145+0	9000 2.492+0 1.985 3.76-2 -7.85-4 2.207+0 1.400 9.75-1 3.89-2 3.784+0	10000 2.012+0 1.985 1.20-1 -8.02- 1.686+0 1.360 1.11+0 4.77-2 2.859+0
Z= 58, Ce: [X Shell $3s_{1/2}$ $E_b = 1434.6$ eV $3p_{1/2}$ $E_b = 1272.8$ eV $3p_{3/2}$ $E_b = 1272.8$ eV	$ \begin{array}{c} \delta \\ \mathbf{e} \mathbf{4f}_{5/2}^2 0 \\ & \sigma \\ \beta \\ \gamma \\ \delta \\ & \sigma \\ \beta \\ \gamma \\ \delta \\ & \sigma \\ \beta \\ \beta \\ \sigma \\ \beta \\ \beta \\ \sigma \\ \rho \\ \sigma \\ \sigma \\ \rho \\ \sigma \\ \sigma \\ \rho \\ \sigma \\ \sigma \\ \sigma \\ \rho \\ \sigma \\ \sigma$	$\begin{array}{c} -2.80-4 \\ \hline 68_{1/2}^2 \\ \hline k (eV) \\ \hline 1500 \\ \hline 4.933+1 \\ 1.947 \\ 1.01+0 \\ 3.81-4 \\ \hline 7.425+1 \\ 1.105 \\ 3.75-1 \\ 8.54-2 \\ \hline 1.658+2 \\ 1.213 \\ \end{array}$	2000 3.515+1 1.953 5.38-1 -2.14-4 5.111+1 1.477 1.10-1 1.20-2 1.065+2 1.520	3000 1.885+1 1.962 1.25-1 -4.79-4 2.555+1 1.601 -1.06-2 1.62-3 4.983+1 1.653	4000 1.155+1 1.970 -5.46-2 -5.95-4 1.443+1 1.598 1.26-1 4.36-3 2.711+1 1.663	5000 7.728+0 1.976 -1.22-1 -6.62-4 8.929+0 1.567 3.12-1 9.36-3 1.634+1 1.641	5.500+0 1.981 -1.27-1 -7.08-4 5.903+0 1.527 4.98-1 1.56-2 1.058+1 1.608	7000 4.094+0 1.984 -9.32-2 -7.40-4 4.102+0 1.485 6.71-1 2.27-2 7.228+0 1.570	8000 3.152+0 1.985 -3.54-2 -7.66-4 2.962+0 1.442 8.30-1 3.05-2 5.145+0 1.531	9000 2.492+0 1.985 3.76-2 -7.85-4 2.207+0 1.400 9.75-1 3.89-2 3.784+0 1.491	10000 2.012+0 1.985 1.20-1 -8.02- 1.686+0 1.360 4.77-2 2.859+0 1.452
Z= 58, Ce: [X Shell $3s_{1/2}$ $E_b = 1434.6 \text{ eV}$ $3p_{1/2}$ $E_b = 1272.8 \text{ eV}$ $3p_{3/2}$	$ \begin{array}{c} \delta \\ \mathbf{e} \mathbf{4f_{5/2}^2} 0 \\ \sigma \\ \beta \\ \gamma \\ \delta \\ \sigma \\ \beta \\ \gamma \\ \delta \\ \sigma \end{array} $	$\begin{array}{c} -2.80-4 \\ \hline 68_{1/2}^2 \\ \hline k (eV) \\ \hline 1500 \\ \hline 4.933+1 \\ 1.947 \\ 1.01+0 \\ 3.81-4 \\ \hline 7.425+1 \\ 1.105 \\ 3.75-1 \\ 8.54-2 \\ \hline 1.658+2 \\ \end{array}$	2000 3.515+1 1.953 5.38-1 -2.14-4 5.111+1 1.477 1.10-1 1.20-2 1.065+2	3000 1.885+1 1.962 1.25-1 -4.79-4 2.555+1 1.601 -1.06-2 1.62-3 4.983+1	4000 1.155+1 1.970 -5.46-2 -5.95-4 1.443+1 1.598 1.26-1 4.36-3 2.711+1	5000 7.728+0 1.976 -1.22-1 -6.62-4 8.929+0 1.567 3.12-1 9.36-3 1.634+1	5.500+0 1.981 -1.27-1 -7.08-4 5.903+0 1.527 4.98-1 1.56-2 1.058+1	7000 4.094+0 1.984 -9.32-2 -7.40-4 4.102+0 1.485 6.71-1 2.27-2 7.228+0	8000 3.152+0 1.985 -3.54-2 -7.66-4 2.962+0 1.442 8.30-1 3.05-2 5.145+0	9000 2.492+0 1.985 3.76-2 -7.85-4 2.207+0 1.400 9.75-1 3.89-2 3.784+0	10000 2.012+(1.985 1.20-1 -8.02- 1.686+(1.360 1.11+0 4.77-2 2.859+(
Z= 58, Ce: [X Shell $3s_{1/2}$ $E_b = 1434.6$ eV $3p_{1/2}$ $E_b = 1272.8$ eV $3p_{3/2}$ $E_b = 1272.8$ eV	$ \begin{array}{c} \delta \\ \mathbf{e} \mathbf{4f_{5/2}^2} 0 \\ \\ \sigma \\ \beta \\ \gamma \\ \delta \\ \\ \sigma \\ \beta \\ \gamma \\ \delta \\ \\ \sigma \\ \beta \\ \gamma \\ \delta \end{array} $	$\begin{array}{c} -2.80-4 \\ \hline 68_{1/2}^2 \\ \hline k (eV) \\ \hline 1500 \\ \hline 4.933+1 \\ 1.947 \\ 1.01+0 \\ 3.81-4 \\ \hline 7.425+1 \\ 1.105 \\ 3.75-1 \\ 8.54-2 \\ \hline 1.658+2 \\ 1.213 \\ 2.91-1 \\ \end{array}$	2000 3.515+1 1.953 5.38-1 -2.14-4 5.111+1 1.477 1.10-1 1.20-2 1.065+2 1.520 3.79-2	3000 1.885+1 1.962 1.25-1 -4.79-4 2.555+1 1.601 -1.06-2 1.62-3 4.983+1 1.653 -1.21-2	4000 1.155+1 1.970 -5.46-2 -5.95-4 1.443+1 1.598 1.26-1 4.36-3 2.711+1 1.663 1.53-1	5000 7.728+0 1.976 -1.22-1 -6.62-4 8.929+0 1.567 3.12-1 9.36-3 1.634+1 1.641 3.58-1	5.500+0 1.981 -1.27-1 -7.08-4 5.903+0 1.527 4.98-1 1.56-2 1.058+1 1.608 5.59-1	7000 4.094+0 1.984 -9.32-2 -7.40-4 4.102+0 1.485 6.71-1 2.27-2 7.228+0 1.570 7.45-1	8000 3.152+0 1.985 -3.54-2 -7.66-4 2.962+0 1.442 8.30-1 3.05-2 5.145+0 1.531 9.15-1	9000 2.492+0 1.985 3.76-2 -7.85-4 2.207+0 1.400 9.75-1 3.89-2 3.784+0 1.491 1.07+0	10000 2.012+0 1.985 1.20-1 -8.02- 1.686+0 1.360 4.77-2 2.859+0 1.452 1.21+0 4.53-2
Z= 58, Ce: [X Shell $3s_{1/2}$ $E_b = 1434.6$ eV $3p_{1/2}$ $E_b = 1272.8$ eV $3p_{3/2}$ $E_b = 1185.4$ eV $3d_{3/2}$ $E_b = 160.4$ eV	$ \begin{array}{c} \delta \\ \mathbf{e} \mathbf{4f_{5/2}^2} \\ \sigma \\ \beta \\ \gamma \\ \delta \\ \sigma \\ \beta \\ \gamma \\ \delta \\ \sigma \\ \beta \\ \beta \\ \rho \\ \delta \\ \sigma \\ \beta \\ \beta \\ \rho \\ \delta \\ \sigma \\ \beta \\ \beta \\ \rho \\ \delta \\ \sigma \\ \beta \\ \rho \\ \delta \\ \sigma \\ \beta \\ \rho \\ \delta \\ \sigma \\ \beta \\ \rho \\ \rho \\ \delta \\ \sigma \\ \beta \\ \rho \\ \rho \\ \delta \\ \sigma \\ \beta \\ \rho \\ \rho \\ \delta \\ \sigma \\ \beta \\ \rho \\ \rho \\ \delta \\ \sigma \\ \beta \\ \rho \\ \rho \\ \delta \\ \sigma \\ \beta \\ \rho \\ \rho \\ \delta \\ \sigma \\ \rho \\ \rho \\ \rho \\ \delta \\ \sigma \\ \rho \\ \rho$	$\begin{array}{c} -2.80-4 \\ \hline 68^2_{1/2} \\ \hline k (\mathrm{eV}) \\ \hline 1500 \\ \hline 4.933+1 \\ 1.947 \\ 1.01+0 \\ 3.81-4 \\ \hline 7.425+1 \\ 1.105 \\ 3.75-1 \\ 8.54-2 \\ \hline 1.658+2 \\ 1.213 \\ 2.91-1 \\ 5.05-2 \\ \hline 2.719+2 \\ 1.036 \\ \end{array}$	2000 3.515+1 1.953 5.38-1 -2.14-4 5.111+1 1.477 1.10-1 1.20-2 1.065+2 1.520 3.79-2 9.07-3 1.226+2 1.198	3000 1.885+1 1.962 1.25-1 -4.79-4 2.555+1 1.601 -1.06-2 1.62-3 4.983+1 1.653 -1.21-2 7.04-3 3.678+1 1.231	4000 1.155+1 1.970 -5.46-2 -5.95-4 1.443+1 1.598 1.26-1 4.36-3 2.711+1 1.663 1.53-1 1.11-2 1.487+1 1.172	5000 7.728+0 1.976 -1.22-1 -6.62-4 8.929+0 1.567 3.12-1 9.36-3 1.634+1 1.641 3.58-1 1.56-2 7.160+0 1.097	6000 5.500+0 1.981 -1.27-1 -7.08-4 5.903+0 1.527 4.98-1 1.56-2 1.058+1 1.608 5.59-1 2.05-2 3.869+0 1.022	7000 4.094+0 1.984 -9.32-2 -7.40-4 4.102+0 1.485 6.71-1 2.27-2 7.228+0 1.570 7.45-1 2.59-2 2.270+0 0.951	8000 3.152+0 1.985 -3.54-2 -7.66-4 2.962+0 1.442 8.30-1 3.05-2 5.145+0 1.531 9.15-1 3.18-2 1.417+0 0.886	9000 2.492+0 1.985 3.76-2 -7.85-4 2.207+0 1.400 9.75-1 3.89-2 3.784+0 1.491 1.07+0 3.83-2 9.288-1 0.825	10000 2.012+(1.985 1.20-1 -8.02- 1.686+(1.360 1.11+0 4.77-2 2.859+(1.452 1.21+0 4.53-2 0.769
Z= 58, Ce: [X Shell $3s_{1/2}$ $E_b = 1434.6$ eV $3p_{1/2}$ $E_b = 1272.8$ eV $3p_{3/2}$ $E_b = 1185.4$ eV $3d_{3/2}$	$ \begin{array}{c} \delta \\ \mathbf{fe} \mathbf{4f_{5/2}^2} \\ \sigma \\ \beta \\ \gamma \\ \delta \\ \sigma \\ \sigma \\ \beta \\ \gamma \\ \delta \\ \sigma \\ \sigma \\ \beta \\ \gamma \\ \delta \\ \sigma \\ \sigma \\ \beta \\ \gamma \\ \delta \\ \sigma \\ \sigma \\ \rho \\ \gamma \\ \delta \\ \sigma \\ \sigma \\ \rho \\ \gamma \\ \delta \\ \sigma \\ \sigma \\ \rho \\ \gamma \\ \delta \\ \sigma \\ \sigma \\ \rho \\ \gamma \\ \delta \\ \sigma \\ \sigma \\ \rho \\ \gamma \\ \delta \\ \sigma \\ \sigma \\ \rho \\ \gamma \\ \delta \\ \sigma \\ \sigma \\ \rho \\ \gamma \\ \delta \\ \sigma \\ \sigma \\ \rho \\ \gamma \\ \delta \\ \sigma \\ \sigma \\ \rho \\ \gamma \\ \delta \\ \sigma \\ \sigma \\ \rho \\ \rho \\ \sigma \\ \sigma \\ \rho \\ \sigma \\ \sigma \\ \sigma \\ \rho \\ \sigma \\ \sigma$	$\begin{array}{c} -2.80-4 \\ \hline 65s_{1/2}^2 \\ \hline k (\mathrm{eV}) \\ \hline 1500 \\ \hline 4.933+1 \\ 1.947 \\ 1.01+0 \\ 3.81-4 \\ \hline 7.425+1 \\ 1.105 \\ 3.75-1 \\ 8.54-2 \\ 1.658+2 \\ 1.213 \\ 2.91-1 \\ 5.05-2 \\ \hline 2.719+2 \\ 1.036 \\ -7.18-2 \\ \end{array}$	2000 3.515+1 1.953 5.38-1 -2.14-4 5.111+1 1.477 1.10-1 1.20-2 1.065+2 1.520 3.79-2 9.07-3 1.226+2 1.198 1.14-1	3000 1.885+1 1.962 1.25-1 -4.79-4 2.555+1 1.601 -1.06-2 1.62-3 4.983+1 1.653 -1.21-2 7.04-3 3.678+1 1.231 4.73-1	4000 1.155+1 1.970 -5.46-2 -5.95-4 1.443+1 1.598 1.26-1 4.36-3 2.711+1 1.663 1.53-1 1.11-2 1.487+1 1.172 7.47-1	5000 7.728+0 1.976 -1.22-1 -6.62-4 8.929+0 1.567 3.12-1 9.36-3 1.634+1 1.641 3.58-1 1.56-2 7.160+0 1.097 9.54-1	6000 5.500+0 1.981 -1.27-1 -7.08-4 5.903+0 1.527 4.98-1 1.56-2 1.058+1 1.608 5.59-1 2.05-2 3.869+0 1.022 1.12+0	7000 4.094+0 1.984 -9.32-2 -7.40-4 4.102+0 1.485 6.71-1 2.27-2 7.228+0 1.570 7.45-1 2.59-2 2.270+0 0.951 1.25+0	8000 3.152+0 1.985 -3.54-2 -7.66-4 2.962+0 1.442 8.30-1 3.05-2 5.145+0 1.531 9.15-1 3.18-2 1.417+0 0.886 1.35+0	9000 2.492+0 1.985 3.76-2 -7.85-4 2.207+0 1.400 9.75-1 3.89-2 3.784+0 1.491 1.07+0 3.83-2 9.288-1 0.825 1.44+0	10000 2.012+(1.985 1.20-1 -8.02- 1.686+(1.360 1.11+0 4.77-2 2.859+(1.452 1.21+0 4.53-2 0.769 1.51+0
Z= 58, Ce: [X Shell $3s_{1/2}$ $E_b = 1434.6$ eV $3p_{1/2}$ $E_b = 1272.8$ eV $3p_{3/2}$ $E_b = 1185.4$ eV $3d_{3/2}$ $E_b = 901.3$ eV	$ \begin{array}{c} \delta \\ \mathbf{e} \mathbf{4f_{5/2}^2} \\ \sigma \\ \beta \\ \gamma \\ \delta \\ \sigma \\ \rho \\ \gamma \\ \delta \\ \sigma \\ \sigma \\ \rho \\ \rho \\ \sigma \\ \sigma \\ \rho \\ \sigma \\ \sigma \\ \rho \\ \sigma \\ \rho \\ \sigma \\ \sigma \\ \rho \\ \sigma \\ \sigma \\ \rho \\ \sigma \\ \rho \\ \sigma \\ \sigma \\ \rho \\ \sigma \\ \sigma \\ \sigma \\ \sigma \\ \rho \\ \sigma \\ \sigma$	$\begin{array}{c} -2.80-4 \\ \hline 68^2_{1/2} \\ \hline k (\mathrm{eV}) \\ \hline 1500 \\ \hline 4.933+1 \\ 1.947 \\ 1.01+0 \\ 3.81-4 \\ \hline 7.425+1 \\ 1.105 \\ 3.75-1 \\ 8.54-2 \\ \hline 1.658+2 \\ 1.213 \\ 2.91-1 \\ 5.05-2 \\ \hline 2.719+2 \\ 1.036 \\ -7.18-2 \\ 2.65-2 \\ \end{array}$	2000 3.515+1 1.953 5.38-1 -2.14-4 5.111+1 1.477 1.10-1 1.20-2 1.065+2 1.520 3.79-2 9.07-3 1.226+2 1.198 1.14-1 5.05-2	3000 1.885+1 1.962 1.25-1 -4.79-4 2.555+1 1.601 -1.06-2 1.62-3 4.983+1 1.653 -1.21-2 7.04-3 3.678+1 1.231 4.73-1 7.96-2	4000 1.155+1 1.970 -5.46-2 -5.95-4 1.443+1 1.598 1.26-1 4.36-3 2.711+1 1.663 1.53-1 1.11-2 1.487+1 1.172 7.47-1 1.04-1	5000 7.728+0 1.976 -1.22-1 -6.62-4 8.929+0 1.567 3.12-1 9.36-3 1.634+1 1.641 3.58-1 1.56-2 7.160+0 1.097 9.54-1 1.29-1	6000 5.500+0 1.981 -1.27-1 -7.08-4 5.903+0 1.527 4.98-1 1.56-2 1.058+1 1.608 5.59-1 2.05-2 3.869+0 1.022 1.12+0 1.53-1	7000 4.094+0 1.984 -9.32-2 -7.40-4 4.102+0 1.485 6.71-1 2.27-2 7.228+0 1.570 7.45-1 2.59-2 2.270+0 0.951 1.25+0 1.78-1	8000 3.152+0 1.985 -3.54-2 -7.66-4 2.962+0 1.442 8.30-1 3.05-2 5.145+0 1.531 9.15-1 3.18-2 1.417+0 0.886 1.35+0 2.03-1	9000 2.492+0 1.985 3.76-2 -7.85-4 2.207+0 1.400 9.75-1 3.89-2 3.784+0 1.491 1.07+0 3.83-2 9.288-1 0.825 1.44+0 2.26-1	10000 2.012+(1.985 1.20-1 -8.02- 1.686+(1.360 1.11+0 4.77-2 2.859+(1.452 4.53-2 0.769 1.51+0 2.49-1
Z= 58, Ce: [X Shell $3s_{1/2}$ $E_b = 1434.6 \text{ eV}$ $3p_{1/2}$ $E_b = 1272.8 \text{ eV}$ $3p_{3/2}$ $E_b = 1185.4 \text{ eV}$ $3d_{3/2}$ $E_b = 901.3 \text{ eV}$	δ (e)4f ² _{5/2} (σ	$\begin{array}{c} -2.80-4 \\ \hline 65s_{1/2}^2 \\ \hline k (\mathrm{eV}) \\ \hline 1500 \\ \hline 4.933+1 \\ 1.947 \\ 1.01+0 \\ 3.81-4 \\ \hline 7.425+1 \\ 1.105 \\ 3.75-1 \\ 8.54-2 \\ \hline 1.658+2 \\ 1.213 \\ 2.91-1 \\ 5.05-2 \\ \hline 2.719+2 \\ 1.036 \\ -7.18-2 \\ 2.65-2 \\ \hline 3.926+2 \\ \hline \end{array}$	2000 3.515+1 1.953 5.38-1 -2.14-4 5.111+1 1.477 1.10-1 1.20-2 1.065+2 1.520 3.79-2 9.07-3 1.226+2 1.198 1.14-1 5.05-2 1.751+2	3000 1.885+1 1.962 1.25-1 -4.79-4 2.555+1 1.601 -1.06-2 1.62-3 4.983+1 1.653 -1.21-2 7.04-3 3.678+1 1.231 4.73-1 7.96-2 5.191+1	4000 1.155+1 1.970 -5.46-2 -5.95-4 1.443+1 1.598 1.26-1 4.36-3 2.711+1 1.663 1.53-1 1.11-2 1.487+1 1.172 7.47-1 1.04-1 2.082+1	5000 7.728+0 1.976 -1.22-1 -6.62-4 8.929+0 1.567 3.12-1 9.36-3 1.634+1 1.641 3.58-1 1.56-2 7.160+0 1.097 9.54-1 1.29-1 9.958+0	6000 5.500+0 1.981 -1.27-1 -7.08-4 5.903+0 1.527 4.98-1 1.56-2 1.058+1 1.608 5.59-1 2.05-2 3.869+0 1.022 1.12+0 1.53-1 5.349+0	7000 4.094+0 1.984 -9.32-2 -7.40-4 4.102+0 1.485 6.71-1 2.27-2 7.228+0 1.570 7.45-1 2.59-2 2.270+0 0.951 1.25+0 1.78-1 3.122+0	8000 3.152+0 1.985 -3.54-2 -7.66-4 2.962+0 1.442 8.30-1 3.05-2 5.145+0 1.531 9.15-1 3.18-2 1.417+0 0.886 1.35+0 2.03-1 1.939+0	9000 2.492+0 1.985 3.76-2 -7.85-4 2.207+0 1.400 9.75-1 3.89-2 3.784+0 1.491 1.07+0 3.83-2 9.288-1 0.825 1.44+0 2.26-1 1.265+0	10000 2.012+(1.985 1.20-1 -8.02- 1.686+(1.360 1.11+0 4.77-2 2.859+(1.452 1.21+0 4.53-2 0.769 1.51+0 2.49-1 8.589-
Z= 58, Ce: [X Shell $3s_{1/2}$ $E_b = 1434.6$ eV $3p_{1/2}$ $E_b = 1272.8$ eV $3p_{3/2}$ $E_b = 1185.4$ eV $3d_{3/2}$ $E_b = 901.3$ eV	$ \begin{array}{c} \delta \\ \mathbf{fe} \mathbf{4f_{5/2}^2} \\ \sigma \\ \beta \\ \gamma \\ \delta \\ \delta \\ \sigma \\ \beta \\ \gamma \\ \delta \\ \delta \\ \sigma \\ \beta \\ \gamma \\ \delta \\ \delta \\ \sigma \\ \beta \\ \gamma \\ \delta \\ \delta \\ \sigma \\ \beta \\ \gamma \\ \delta \\ \delta \\ \sigma \\ \beta \\ \gamma \\ \delta \\ \delta \\ \sigma \\ \beta \\ \gamma \\ \delta \\ \delta \\ \sigma \\ \beta \\ \gamma \\ \delta \\ \delta \\ \sigma \\ \beta \\ \gamma \\ \delta \\ \gamma \\ \delta \\ \delta$	$\begin{array}{c} -2.80-4 \\ \hline 68_{1/2}^2 \\ \hline k (\mathrm{eV}) \\ \hline 1500 \\ \hline 4.933+1 \\ 1.947 \\ 1.01+0 \\ 3.81-4 \\ \hline 7.425+1 \\ 1.105 \\ 3.75-1 \\ 8.54-2 \\ \hline 1.658+2 \\ 1.213 \\ 2.91-1 \\ 5.05-2 \\ \hline 2.719+2 \\ 1.036 \\ -7.18-2 \\ 2.65-2 \\ \hline 3.926+2 \\ 1.075 \\ -5.77-2 \\ \end{array}$	-3.56-4 2000 3.515+1 1.953 5.38-1 -2.14-4 5.111+1 1.477 1.10-1 1.20-2 1.065+2 1.520 3.79-2 9.07-3 1.226+2 1.198 1.14-1 5.05-2 1.751+2 1.203 1.38-1	3000 1.885+1 1.962 1.25-1 -4.79-4 2.555+1 1.601 -1.06-2 1.62-3 4.983+1 1.653 -1.21-2 7.04-3 3.678+1 1.231 4.73-1 7.96-2 5.191+1 1.204 4.93-1	4000 1.155+1 1.970 -5.46-2 -5.95-4 1.443+1 1.598 1.26-1 4.36-3 2.711+1 1.663 1.53-1 1.11-2 1.487+1 1.172 7.47-1 1.04-1 2.082+1 1.132 7.56-1	5000 7.728+0 1.976 -1.22-1 -6.62-4 8.929+0 1.567 3.12-1 9.36-3 1.634+1 1.641 3.58-1 1.56-2 7.160+0 1.097 9.54-1 1.29-1 9.958+0 1.052 9.53-1	6000 5.500+0 1.981 -1.27-1 -7.08-4 5.903+0 1.527 4.98-1 1.56-2 1.058+1 1.608 5.59-1 2.05-2 3.869+0 1.022 1.12+0 1.53-1 5.349+0 0.977 1.11+0	7000 4.094+0 1.984 -9.32-2 -7.40-4 4.102+0 1.485 6.71-1 2.27-2 7.228+0 1.570 7.45-1 2.59-2 2.270+0 0.951 1.25+0 1.78-1 3.122+0 0.908 1.23+0	8000 3.152+0 1.985 -3.54-2 -7.66-4 2.962+0 1.442 8.30-1 3.05-2 5.145+0 1.531 9.15-1 3.18-2 1.417+0 0.886 1.35+0 2.03-1 1.939+0 0.846 1.33+0	9000 2.492+0 1.985 3.76-2 -7.85-4 2.207+0 1.400 9.75-1 3.89-2 3.784+0 1.491 1.07+0 3.83-2 9.288-1 0.825 1.44+0 2.26-1 1.265+0 0.789 1.41+0	10000 2.012+(1.985 1.20-1 -8.02- 1.686+(1.360 1.11+0 4.77-2 2.859+(1.452 1.21+0 4.53-2 0.769 1.51+0 2.49-1 8.589- 0.737 1.48+0
Z= 58, Ce: [X Shell $3s_{1/2}$ $E_b = 1434.6 \text{ eV}$ $3p_{1/2}$ $E_b = 1272.8 \text{ eV}$ $3p_{3/2}$ $E_b = 1185.4 \text{ eV}$ $3d_{3/2}$ $E_b = 901.3 \text{ eV}$	$ \begin{array}{c} \delta \\ \mathbf{fe} \mathbf{4f_{5/2}^2} \\ \sigma \\ \beta \\ \gamma \\ \delta \\ \sigma \\ \beta \\ \beta \\ \gamma \\ \delta \\ \sigma \\ \beta \\ \beta \\ \gamma \\ \delta \\ \sigma \\ \beta \\ \beta$	$\begin{array}{c} -2.80-4 \\ \hline 68_{1/2}^2 \\ \hline k (eV) \\ \hline 1500 \\ \hline 4.933+1 \\ 1.947 \\ 1.01+0 \\ 3.81-4 \\ \hline 7.425+1 \\ 1.105 \\ 3.75-1 \\ 8.54-2 \\ \hline 1.658+2 \\ 1.213 \\ 2.91-1 \\ 5.05-2 \\ \hline 2.719+2 \\ 1.036 \\ -7.18-2 \\ 2.65-2 \\ \hline 3.926+2 \\ 1.075 \\ \end{array}$	-3.56-4 2000 3.515+1 1.953 5.38-1 -2.14-4 5.111+1 1.477 1.10-1 1.20-2 1.065+2 1.520 3.79-2 9.07-3 1.226+2 1.198 1.14-1 5.05-2 1.751+2 1.203	3000 1.885+1 1.962 1.25-1 -4.79-4 2.555+1 1.601 -1.06-2 1.62-3 4.983+1 1.653 -1.21-2 7.04-3 3.678+1 1.231 4.73-1 7.96-2 5.191+1 1.204	4000 1.155+1 1.970 -5.46-2 -5.95-4 1.443+1 1.598 1.26-1 4.36-3 2.711+1 1.663 1.53-1 1.11-2 1.487+1 1.172 7.47-1 1.04-1 2.082+1 1.132	5000 7.728+0 1.976 -1.22-1 -6.62-4 8.929+0 1.567 3.12-1 9.36-3 1.634+1 1.641 3.58-1 1.56-2 7.160+0 1.097 9.54-1 1.29-1 9.958+0 1.052	6000 5.500+0 1.981 -1.27-1 -7.08-4 5.903+0 1.527 4.98-1 1.56-2 1.058+1 1.608 5.59-1 2.05-2 3.869+0 1.022 1.12+0 1.53-1 5.349+0 0.977	7000 4.094+0 1.984 -9.32-2 -7.40-4 4.102+0 1.485 6.71-1 2.27-2 7.228+0 1.570 7.45-1 2.59-2 2.270+0 0.951 1.25+0 1.78-1 3.122+0 0.908	8000 3.152+0 1.985 -3.54-2 -7.66-4 2.962+0 1.442 8.30-1 3.05-2 5.145+0 1.531 9.15-1 3.18-2 1.417+0 0.886 1.35+0 2.03-1 1.939+0 0.846	9000 2.492+0 1.985 3.76-2 -7.85-4 2.207+0 1.400 9.75-1 3.89-2 3.784+0 1.491 1.07+0 3.83-2 9.288-1 0.825 1.44+0 2.26-1 1.265+0 0.789	10000 2.012+(1.985 1.20-1 -8.02- 1.686+(1.360 1.11+0 4.77-2 2.859+(1.21+0 4.53-2 6.332- 0.769 1.51+0 2.49-1 8.589- 0.737
Z= 58, Ce: [X] Shell $3s_{1/2}$ $E_b = 1434.6 \text{ eV}$ $3p_{1/2}$ $E_b = 1272.8 \text{ eV}$ $3p_{3/2}$ $E_b = 1185.4 \text{ eV}$ $3d_{3/2}$ $E_b = 901.3 \text{ eV}$ $3d_{5/2}$ $E_b = 883.3 \text{ eV}$	$\begin{array}{c} \delta \\ \mathbf{e} \mathbf{4f_{5/2}^2} \\ \mathbf{e} \\ \\ \sigma \\ \beta \\ \gamma \\ \delta \\ \\ \sigma \\ \beta \\ \gamma \\ \delta \\ \\ \sigma \\ \beta \\ \gamma \\ \delta \\ \\ \sigma \\ \beta \\ \gamma \\ \delta \\ \\ \sigma \\ \beta \\ \gamma \\ \delta \\ \\ \sigma \\ \\ \sigma \\ \beta \\ \gamma \\ \delta \\ \\ \sigma \\ \\ \sigma \\ \\ \sigma \\ \\ \beta \\ \\ \gamma \\ \delta \\ \\ \sigma \\ \\ \sigma \\ \\ \beta \\ \\ \gamma \\ \delta \\ \\ \sigma \\ \\ \sigma \\ \\ \beta \\ \\ \gamma \\ \delta \\ \\ \sigma \\ \\ \sigma \\ \sigma \\ \\ \sigma \\ \sigma \\ \sigma \\ \sigma \\ \\ \sigma \\ \sigma \\ \sigma \\ \sigma \\ \\ \sigma \\ \sigma \\ \sigma \\ \sigma$	$\begin{array}{c} -2.80-4 \\ \hline 68_{1/2}^2 \\ \hline k (\mathrm{eV}) \\ \hline 1500 \\ \hline 4.933+1 \\ 1.947 \\ 1.01+0 \\ 3.81-4 \\ \hline 7.425+1 \\ 1.105 \\ 3.75-1 \\ 8.54-2 \\ \hline 1.658+2 \\ 1.213 \\ 2.91-1 \\ 5.05-2 \\ \hline 2.719+2 \\ 1.036 \\ -7.18-2 \\ 2.65-2 \\ \hline 3.926+2 \\ 1.075 \\ -5.77-2 \\ 2.58-2 \\ \hline 1.585+1 \\ \hline \end{array}$	2000 3.515+1 1.953 5.38-1 -2.14-4 5.111+1 1.477 1.10-1 1.20-2 1.065+2 1.520 3.79-2 9.07-3 1.226+2 1.198 1.14-1 5.05-2 1.751+2 1.203 1.38-1 4.96-2 9.712+0	3000 1.885+1 1.962 1.25-1 -4.79-4 2.555+1 1.601 -1.06-2 1.62-3 4.983+1 1.653 -1.21-2 7.04-3 3.678+1 1.231 4.73-1 7.96-2 5.191+1 1.204 4.93-1 8.07-2 4.707+0	4000 1.155+1 1.970 -5.46-2 -5.95-4 1.443+1 1.598 1.26-1 4.36-3 2.711+1 1.663 1.53-1 1.11-2 1.487+1 1.172 7.47-1 1.04-1 2.082+1 1.132 7.56-1 1.08-1 2.758+0	5000 7.728+0 1.976 -1.22-1 -6.62-4 8.929+0 1.567 3.12-1 9.36-3 1.634+1 1.641 3.58-1 1.56-2 7.160+0 1.097 9.54-1 1.29-1 9.958+0 1.052 9.53-1 1.35-1 1.804+0	6000 5.500+0 1.981 -1.27-1 -7.08-4 5.903+0 1.527 4.98-1 1.56-2 1.058+1 1.608 5.59-1 2.05-2 3.869+0 1.022 1.12+0 1.53-1 5.349+0 0.977 1.11+0 1.62-1 1.266+0	7000 4.094+0 1.984 -9.32-2 -7.40-4 4.102+0 1.485 6.71-1 2.27-2 7.228+0 1.570 7.45-1 2.59-2 2.270+0 0.951 1.25+0 1.78-1 3.122+0 0.908 1.23+0 1.89-1 9.335-1	8000 3.152+0 1.985 -3.54-2 -7.66-4 2.962+0 1.442 8.30-1 3.05-2 5.145+0 1.531 9.15-1 3.18-2 1.417+0 0.886 1.35+0 2.03-1 1.939+0 0.846 1.33+0 2.15-1 7.141-1	9000 2.492+0 1.985 3.76-2 -7.85-4 2.207+0 1.400 9.75-1 3.89-2 3.784+0 1.491 1.07+0 3.83-2 9.288-1 0.825 1.44+0 2.26-1 1.265+0 0.789 1.41+0 2.40-1 5.620-1	10000 2.012+(1.985 1.20-1 -8.02- 1.686+(1.360 1.11+0 4.77-2 2.859+(1.452 1.21+0 4.53-2 0.769 1.51+0 2.49-1 8.589- 0.737 1.48+0 2.64-1
Z= 58, Ce: [X] Shell $3s_{1/2}$ $E_b = 1434.6 \text{ eV}$ $3p_{1/2}$ $E_b = 1272.8 \text{ eV}$ $3p_{3/2}$ $E_b = 1185.4 \text{ eV}$ $3d_{3/2}$ $E_b = 901.3 \text{ eV}$ $3d_{5/2}$ $E_b = 883.3 \text{ eV}$	$ \begin{array}{c} \delta \\ \mathbf{fe} \mathbf{4f_{5/2}^2} \\ \sigma \\ \beta \\ \gamma \\ \delta \\ \sigma \\ \beta \\ \beta \\ \gamma \\ \delta \\ \sigma \\ \beta \\ \beta \\ \gamma \\ \delta \\ \sigma \\ \beta \\ \beta \\ \gamma \\ \delta \\ \sigma \\ \beta \\ \beta \\ \gamma \\ \delta \\ \sigma \\ \beta \\ \beta \\ \gamma \\ \delta \\ \sigma \\ \beta \\ \beta \\ \gamma \\ \delta \\ \sigma \\ \beta \\ \beta \\ \gamma \\ \delta \\ \sigma \\ \beta \\ \beta \\ \gamma \\ \delta \\ \sigma \\ \sigma \\ \beta \\ \gamma \\ \delta \\ \sigma \\ \sigma \\ \beta \\ \gamma \\ \delta \\ \sigma \\ \sigma \\ \beta \\ \gamma \\ \delta \\ \sigma \\ \sigma \\ \rho \\ \rho \\ \sigma \\ \sigma \\ \rho \\ \rho \\ \sigma \\ \sigma \\ \rho \\ \rho \\ \rho \\ \sigma \\ \sigma \\ \rho \\ \rho \\ \sigma \\ \rho \\ \sigma \\ \rho \\ \sigma \\ \rho \\ \rho \\ \sigma \\ \rho \\ \sigma \\ \rho \\ \sigma \\ \rho \\ \rho \\ \sigma \\ \rho \\ \sigma \\ \rho \\ \rho \\ \sigma \\ \rho \\ \sigma \\ \rho \\ \rho \\ \sigma \\ \rho \\ \rho \\ \sigma \\ \rho \\ \rho$	$\begin{array}{c} -2.80-4 \\ \hline 65s_{1/2}^2 \\ \hline k (eV) \\ \hline 1500 \\ \hline 4.933+1 \\ 1.947 \\ 1.01+0 \\ 3.81-4 \\ \hline 7.425+1 \\ 1.105 \\ 3.75-1 \\ 8.54-2 \\ \hline 1.658+2 \\ 1.213 \\ 2.91-1 \\ 5.05-2 \\ \hline 2.719+2 \\ 1.036 \\ -7.18-2 \\ 2.65-2 \\ \hline 3.926+2 \\ 1.075 \\ -5.77-2 \\ 2.58-2 \\ \hline 1.585+1 \\ 1.965 \\ \hline \end{array}$	2000 3.515+1 1.953 5.38-1 -2.14-4 5.111+1 1.477 1.10-1 1.20-2 1.065+2 1.520 3.79-2 9.07-3 1.226+2 1.198 1.14-1 5.05-2 1.751+2 1.203 1.38-1 4.96-2 9.712+0 1.968	3000 1.885+1 1.962 1.25-1 -4.79-4 2.555+1 1.601 -1.06-2 1.62-3 4.983+1 1.653 -1.21-2 7.04-3 3.678+1 1.231 4.73-1 7.96-2 5.191+1 1.204 4.93-1 8.07-2 4.707+0 1.973	4000 1.155+1 1.970 -5.46-2 -5.95-4 1.443+1 1.598 1.26-1 4.36-3 2.711+1 1.663 1.53-1 1.11-2 1.487+1 1.172 7.47-1 1.04-1 2.082+1 1.132 7.56-1 1.08-1 2.758+0 1.978	5000 7.728+0 1.976 -1.22-1 -6.62-4 8.929+0 1.567 3.12-1 9.36-3 1.634+1 1.641 3.58-1 1.56-2 7.160+0 1.097 9.54-1 1.29-1 9.958+0 1.052 9.53-1 1.35-1 1.804+0 1.981	6000 5.500+0 1.981 -1.27-1 -7.08-4 5.903+0 1.527 4.98-1 1.56-2 1.058+1 1.608 5.59-1 2.05-2 3.869+0 1.022 1.12+0 1.53-1 5.349+0 0.977 1.11+0 1.62-1 1.266+0 1.984	7000 4.094+0 1.984 -9.32-2 -7.40-4 4.102+0 1.485 6.71-1 2.27-2 7.228+0 1.570 7.45-1 2.59-2 2.270+0 0.951 1.25+0 1.78-1 3.122+0 0.908 1.23+0 1.89-1 9.335-1 1.985	8000 3.152+0 1.985 -3.54-2 -7.66-4 2.962+0 1.442 8.30-1 3.05-2 5.145+0 1.531 9.15-1 3.18-2 1.417+0 0.886 1.35+0 2.03-1 1.939+0 0.846 1.33+0 2.15-1 7.141-1 1.985	9000 2.492+0 1.985 3.76-2 -7.85-4 2.207+0 1.400 9.75-1 3.89-2 3.784+0 1.491 1.07+0 3.83-2 9.288-1 0.825 1.44+0 2.26-1 1.265+0 0.789 1.41+0 2.40-1 5.620-1 1.985	10000 2.012+0 1.985 1.20-1 -8.02- 1.686+0 1.360 1.11+0 4.77-2 2.859+0 1.452 1.21+0 4.53-2 0.769 1.51+0 2.49-1 8.589-0 0.737 1.48+0 2.64-1 4.522-1.983
Z= 58, Ce: [X] Shell $3s_{1/2}$ $E_b = 1434.6 \text{ eV}$ $3p_{1/2}$ $E_b = 1272.8 \text{ eV}$ $3p_{3/2}$ $E_b = 1185.4 \text{ eV}$ $3d_{3/2}$ $E_b = 901.3 \text{ eV}$ $3d_{5/2}$ $E_b = 883.3 \text{ eV}$	$\begin{array}{c} \delta \\ \mathbf{e} \mathbf{4f_{5/2}^2} \\ \mathbf{e} \\ \\ \sigma \\ \beta \\ \gamma \\ \delta \\ \\ \sigma \\ \beta \\ \gamma \\ \delta \\ \\ \sigma \\ \beta \\ \gamma \\ \delta \\ \\ \sigma \\ \beta \\ \gamma \\ \delta \\ \\ \sigma \\ \beta \\ \gamma \\ \delta \\ \\ \sigma \\ \beta \\ \gamma \\ \delta \\ \\ \sigma \\ \beta \\ \gamma \\ \delta \\ \\ \sigma \\ \beta \\ \gamma \\ \delta \\ \\ \sigma \\ \beta \\ \gamma \\ \delta \\ \\ \sigma \\ \beta \\ \gamma \\ \delta \\ \\ \sigma \\ \beta \\ \gamma \\ \delta \\ \\ \sigma \\ \beta \\ \gamma \\ \delta \\ \\ \sigma \\ \beta \\ \gamma \\ \delta \\ \\ \sigma \\ \beta \\ \gamma \\ \delta \\ \\ \sigma \\ \sigma \\ \beta \\ \gamma \\ \delta \\ \\ \sigma \\ \sigma \\ \beta \\ \gamma \\ \delta \\ \\ \sigma \\ \sigma \\ \beta \\ \gamma \\ \delta \\ \\ \sigma \\ \sigma \\ \beta \\ \gamma \\ \delta \\ \\ \sigma \\ \sigma \\ \delta \\ \sigma \\ \sigma \\ \delta \\ \sigma \\ \sigma \\$	$\begin{array}{c} -2.80-4 \\ \hline 6s_{1/2}^2 \\ \hline k (eV) \\ \hline 1500 \\ \hline 4.933+1 \\ 1.947 \\ 1.01+0 \\ 3.81-4 \\ \hline 7.425+1 \\ 1.105 \\ 3.75-1 \\ 8.54-2 \\ \hline 1.658+2 \\ 1.213 \\ 2.91-1 \\ 5.05-2 \\ \hline 2.719+2 \\ 1.036 \\ -7.18-2 \\ 2.65-2 \\ \hline 3.926+2 \\ 1.075 \\ -5.77-2 \\ 2.58-2 \\ \hline 1.585+1 \\ 1.965 \\ 1.96-1 \\ \hline \end{array}$	2000 3.515+1 1.953 5.38-1 -2.14-4 5.111+1 1.477 1.10-1 1.20-2 1.065+2 1.520 3.79-2 9.07-3 1.226+2 1.198 1.14-1 5.05-2 1.751+2 1.203 1.38-1 4.96-2 9.712+0 1.968 8.17-2	3000 1.885+1 1.962 1.25-1 -4.79-4 2.555+1 1.601 -1.06-2 1.62-3 4.983+1 1.653 -1.21-2 7.04-3 3.678+1 1.231 4.73-1 7.96-2 5.191+1 1.204 4.93-1 8.07-2 4.707+0 1.973 -6.05-2	4000 1.155+1 1.970 -5.46-2 -5.95-4 1.443+1 1.598 1.26-1 4.36-3 2.711+1 1.663 1.53-1 1.11-2 1.487+1 1.172 7.47-1 1.04-1 2.082+1 1.132 7.56-1 1.08-1 2.758+0 1.978 -1.17-1	5000 7.728+0 1.976 -1.22-1 -6.62-4 8.929+0 1.567 3.12-1 9.36-3 1.634+1 1.56-2 7.160+0 1.097 9.54-1 1.29-1 9.958+0 1.052 9.53-1 1.35-1 1.804+0 1.981 -1.20-1	6000 5.500+0 1.981 -1.27-1 -7.08-4 5.903+0 1.527 4.98-1 1.56-2 1.058+1 1.608 5.59-1 2.05-2 3.869+0 1.022 1.12+0 1.53-1 5.349+0 0.977 1.11+0 1.62-1 1.266+0 1.984 -8.81-2	7000 4.094+0 1.984 -9.32-2 -7.40-4 4.102+0 1.485 6.71-1 2.27-2 7.228+0 1.570 7.45-1 2.59-2 2.270+0 0.951 1.25+0 1.78-1 3.122+0 0.908 1.23+0 1.89-1 9.335-1 1.985 -3.37-2	8000 3.152+0 1.985 -3.54-2 -7.66-4 2.962+0 1.442 8.30-1 3.05-2 5.145+0 1.531 9.15-1 3.18-2 1.417+0 0.886 1.35+0 2.03-1 1.939+0 0.846 1.33+0 2.15-1 7.141-1 1.985 3.57-2	9000 2.492+0 1.985 3.76-2 -7.85-4 2.207+0 1.400 9.75-1 3.89-2 3.784+0 1.491 1.07+0 3.83-2 9.288-1 0.825 1.44+0 2.26-1 1.265+0 0.789 1.41+0 2.40-1 5.620-1 1.985 1.15-1	10000 2.012+(1.985 1.20-1 -8.02- 1.686+(1.360 1.11+0 4.77-2 2.859+(1.452 1.21+0 4.53-2 0.769 1.51+0 2.49-1 8.589- 0.73 1.48+0 2.64-1 4.522- 1.983 2.01-1
Z= 58, Ce: [X Shell $3s_{1/2}$ $E_b = 1434.6 \text{ eV}$ $3p_{1/2}$ $E_b = 1272.8 \text{ eV}$ $3p_{3/2}$ $E_b = 1185.4 \text{ eV}$ $3d_{3/2}$ $E_b = 901.3 \text{ eV}$ $3d_{5/2}$ $E_b = 883.3 \text{ eV}$ $4s_{1/2}$ $E_b = 289.6 \text{ eV}$	$\begin{array}{c} \delta \\ \mathbf{e} \mathbf{4f_{5/2}^2} \\ \mathbf{e} \\ \\ \sigma \\ \beta \\ \gamma \\ \delta \\ \\ \sigma \\ \beta \\ \gamma \\ \delta \\ \\ \sigma \\ \beta \\ \gamma \\ \delta \\ \\ \sigma \\ \beta \\ \gamma \\ \delta \\ \\ \sigma \\ \beta \\ \gamma \\ \delta \\ \\ \sigma \\ \beta \\ \gamma \\ \delta \\ \\ \sigma \\ \beta \\ \gamma \\ \delta \\ \\ \sigma \\ \beta \\ \gamma \\ \delta \\ \\ \sigma \\ \beta \\ \gamma \\ \delta \\ \\ \sigma \\ \beta \\ \gamma \\ \delta \\ \\ \sigma \\ \beta \\ \gamma \\ \delta \\ \\ \sigma \\ \beta \\ \gamma \\ \delta \\ \\ \sigma \\ \beta \\ \gamma \\ \delta \\ \\ \sigma \\ \beta \\ \gamma \\ \delta \\ \\ \sigma \\ \beta \\ \gamma \\ \delta \\ \\ \sigma \\ \beta \\ \gamma \\ \delta \\ \\ \sigma \\ \sigma \\ \beta \\ \gamma \\ \delta \\ \\ \sigma \\ \sigma \\ \beta \\ \gamma \\ \delta \\ \\ \sigma \\ \sigma \\ \delta \\ \phi \\ \gamma \\ \delta \\ \\ \sigma \\ \sigma \\ \phi \\ \delta \\ \sigma \\ \phi \\ \delta \\ \sigma \\ \phi \\ \phi \\ \phi \\ \delta \\ \sigma \\ \phi \\ \phi \\ \delta \\ \phi \\ \phi \\ \phi \\ \phi \\ \delta \\ \phi \\ \phi$	$\begin{array}{c} -2.80-4 \\ \hline 68^2_{1/2} \\ \hline k (\mathrm{eV}) \\ \hline 1500 \\ \hline 4.933+1 \\ 1.947 \\ 1.01+0 \\ 3.81-4 \\ \hline 7.425+1 \\ 1.105 \\ 3.75-1 \\ 8.54-2 \\ \hline 1.658+2 \\ 1.213 \\ 2.91-1 \\ 5.05-2 \\ \hline 2.719+2 \\ 1.036 \\ -7.18-2 \\ 2.65-2 \\ \hline 3.926+2 \\ 1.075 \\ -5.77-2 \\ 2.58-2 \\ \hline 1.585+1 \\ 1.965 \\ 1.96-1 \\ -2.79-4 \\ \hline \end{array}$	2000 3.515+1 1.953 5.38-1 -2.14-4 5.111+1 1.477 1.10-1 1.20-2 1.065+2 1.520 3.79-2 9.07-3 1.226+2 1.198 1.14-1 5.05-2 1.751+2 1.203 1.38-1 4.96-2 9.712+0 1.968 8.17-2 -3.74-4	3000 1.885+1 1.962 1.25-1 -4.79-4 2.555+1 1.601 -1.06-2 1.62-3 4.983+1 1.653 -1.21-2 7.04-3 3.678+1 1.231 4.73-1 7.96-2 5.191+1 1.204 4.93-1 8.07-2 4.707+0 1.973 -6.05-2 -4.96-4	4000 1.155+1 1.970 -5.46-2 -5.95-4 1.443+1 1.598 1.26-1 4.36-3 2.711+1 1.663 1.53-1 1.11-2 1.487+1 1.172 7.47-1 1.04-1 2.082+1 1.132 7.56-1 1.08-1 2.758+0 1.978 -1.17-1 -5.71-4	5000 7.728+0 1.976 -1.22-1 -6.62-4 8.929+0 1.567 3.12-1 9.36-3 1.634+1 1.56-2 7.160+0 1.097 9.54-1 1.29-1 9.958+0 1.052 9.53-1 1.35-1 1.804+0 1.981 -1.20-1 -6.24-4	5.500+0 1.981 -1.27-1 -7.08-4 5.903+0 1.527 4.98-1 1.56-2 1.058+1 1.608 5.59-1 2.05-2 3.869+0 1.022 1.12+0 1.53-1 5.349+0 0.977 1.11+0 1.62-1 1.266+0 1.984 -8.81-2 -6.62-4	7000 4.094+0 1.984 -9.32-2 -7.40-4 4.102+0 1.485 6.71-1 2.27-2 7.228+0 1.570 7.45-1 2.59-2 2.270+0 0.951 1.25+0 1.78-1 3.122+0 0.908 1.23+0 1.89-1 9.335-1 1.985 -3.37-2 -6.93-4	8000 3.152+0 1.985 -3.54-2 -7.66-4 2.962+0 1.442 8.30-1 3.05-2 5.145+0 1.531 9.15-1 3.18-2 1.417+0 0.886 1.35+0 2.03-1 1.939+0 0.846 1.33+0 2.15-1 7.141-1 1.985 3.57-2 -7.15-4	9000 2.492+0 1.985 3.76-2 -7.85-4 2.207+0 1.400 9.75-1 3.89-2 3.784+0 1.491 1.07+0 3.83-2 9.288-1 0.825 1.44+0 2.26-1 1.265+0 0.789 1.41+0 2.40-1 5.620-1 1.985 1.15-1 -7.37-4	10000 2.012+(1.985 1.20-1 -8.02- 1.686+(1.360 1.11+0 4.77-2 2.859+(1.452 1.21+0 4.53-2 0.769 1.51+0 2.49-1 8.589- 0.737 1.48+0 2.64-1 4.522- 1.983 2.01-1 -7.54-
Z= 58, Ce: [X] Shell $3s_{1/2}$ $E_b = 1434.6 \text{ eV}$ $3p_{1/2}$ $E_b = 1272.8 \text{ eV}$ $3p_{3/2}$ $E_b = 1185.4 \text{ eV}$ $3d_{3/2}$ $E_b = 901.3 \text{ eV}$ $3d_{5/2}$ $E_b = 883.3 \text{ eV}$	$\begin{array}{c} \delta \\ \mathbf{e} \mathbf{4f_{5/2}^2} \\ \\ \sigma \\ \beta \\ \gamma \\ \delta \\ \\ \sigma \\ \beta \\ \gamma \\ \delta \\ \\ \sigma \\ \beta \\ \gamma \\ \delta \\ \\ \sigma \\ \beta \\ \gamma \\ \delta \\ \\ \sigma \\ \beta \\ \gamma \\ \delta \\ \\ \sigma \\ \beta \\ \gamma \\ \delta \\ \\ \sigma \\ \beta \\ \gamma \\ \delta \\ \\ \sigma \\ \\ \sigma \\ \beta \\ \gamma \\ \delta \\ \\ \sigma \\ \\ \sigma \\ \\ \beta \\ \gamma \\ \delta \\ \\ \sigma \\ \\ \sigma \\ \\ \beta \\ \\ \gamma \\ \delta \\ \\ \sigma \\ \\ \sigma \\ \\ \beta \\ \\ \gamma \\ \delta \\ \\ \sigma \\ \\ \sigma \\ \\ \beta \\ \\ \gamma \\ \delta \\ \\ \sigma \\ \sigma \\ \sigma \\ \sigma \\ \sigma \\ \\ \sigma \\ \\ \sigma \\ \sigma \\ \sigma \\ \\ \sigma \\ \sigma \\ \sigma \\ \sigma \\ \\ \sigma \\ \sigma \\ \sigma \\ \sigma \\ $	$\begin{array}{c} -2.80-4 \\ \hline 6s_{1/2}^2 \\ \hline k (eV) \\ \hline 1500 \\ \hline 4.933+1 \\ 1.947 \\ 1.01+0 \\ 3.81-4 \\ \hline 7.425+1 \\ 1.105 \\ 3.75-1 \\ 8.54-2 \\ \hline 1.658+2 \\ 1.213 \\ 2.91-1 \\ 5.05-2 \\ \hline 2.719+2 \\ 1.036 \\ -7.18-2 \\ 2.65-2 \\ \hline 3.926+2 \\ 1.075 \\ -5.77-2 \\ 2.58-2 \\ \hline 1.585+1 \\ 1.965 \\ 1.96-1 \\ \hline \end{array}$	2000 3.515+1 1.953 5.38-1 -2.14-4 5.111+1 1.477 1.10-1 1.20-2 1.065+2 1.520 3.79-2 9.07-3 1.226+2 1.198 1.14-1 5.05-2 1.751+2 1.203 1.38-1 4.96-2 9.712+0 1.968 8.17-2	3000 1.885+1 1.962 1.25-1 -4.79-4 2.555+1 1.601 -1.06-2 1.62-3 4.983+1 1.653 -1.21-2 7.04-3 3.678+1 1.231 4.73-1 7.96-2 5.191+1 1.204 4.93-1 8.07-2 4.707+0 1.973 -6.05-2	4000 1.155+1 1.970 -5.46-2 -5.95-4 1.443+1 1.598 1.26-1 4.36-3 2.711+1 1.663 1.53-1 1.11-2 1.487+1 1.172 7.47-1 1.04-1 2.082+1 1.132 7.56-1 1.08-1 2.758+0 1.978 -1.17-1	5000 7.728+0 1.976 -1.22-1 -6.62-4 8.929+0 1.567 3.12-1 9.36-3 1.634+1 1.56-2 7.160+0 1.097 9.54-1 1.29-1 9.958+0 1.052 9.53-1 1.35-1 1.804+0 1.981 -1.20-1	6000 5.500+0 1.981 -1.27-1 -7.08-4 5.903+0 1.527 4.98-1 1.56-2 1.058+1 1.608 5.59-1 2.05-2 3.869+0 1.022 1.12+0 1.53-1 5.349+0 0.977 1.11+0 1.62-1 1.266+0 1.984 -8.81-2	7000 4.094+0 1.984 -9.32-2 -7.40-4 4.102+0 1.485 6.71-1 2.27-2 7.228+0 1.570 7.45-1 2.59-2 2.270+0 0.951 1.25+0 1.78-1 3.122+0 0.908 1.23+0 1.89-1 9.335-1 1.985 -3.37-2	8000 3.152+0 1.985 -3.54-2 -7.66-4 2.962+0 1.442 8.30-1 3.05-2 5.145+0 1.531 9.15-1 3.18-2 1.417+0 0.886 1.35+0 2.03-1 1.939+0 0.846 1.33+0 2.15-1 7.141-1 1.985 3.57-2	9000 2.492+0 1.985 3.76-2 -7.85-4 2.207+0 1.400 9.75-1 3.89-2 3.784+0 1.491 1.07+0 3.83-2 9.288-1 0.825 1.44+0 2.26-1 1.265+0 0.789 1.41+0 2.40-1 5.620-1 1.985 1.15-1	10000 2.012+(1.985 1.20-1 -8.02- 1.686+(1.360 1.11+0 4.77-2 2.859+(1.452 1.21+0 4.53-2 0.769 1.51+0 2.49-1 8.589- 0.737 1.48+0 2.64-1 4.522- 1.983 2.01-1 -7.54-
Z= 58, Ce: [X] Shell $3s_{1/2}$ $E_b = 1434.6 \text{ eV}$ $3p_{1/2}$ $E_b = 1272.8 \text{ eV}$ $3p_{3/2}$ $E_b = 1185.4 \text{ eV}$ $3d_{3/2}$ $E_b = 901.3 \text{ eV}$ $3d_{5/2}$ $E_b = 883.3 \text{ eV}$ $4s_{1/2}$ $E_b = 289.6 \text{ eV}$	δ (e) 4f _{5/2} (σ	$\begin{array}{c} -2.80-4 \\ \hline 65s_{1/2}^2 \\ \hline k (eV) \\ \hline 1500 \\ \hline 4.933+1 \\ 1.947 \\ 1.01+0 \\ 3.81-4 \\ \hline 7.425+1 \\ 1.105 \\ 3.75-1 \\ 8.54-2 \\ \hline 1.658+2 \\ 1.213 \\ 2.91-1 \\ 5.05-2 \\ \hline 2.719+2 \\ 1.036 \\ -7.18-2 \\ 2.65-2 \\ \hline 3.926+2 \\ 1.075 \\ -5.77-2 \\ 2.58-2 \\ \hline 1.585+1 \\ 1.965 \\ 1.96-1 \\ -2.79-4 \\ \hline 1.885+1 \\ 1.682 \\ 3.66-3 \\ \hline \end{array}$	-3.56-4 2000 3.515+1 1.953 5.38-1 -2.14-4 5.111+1 1.477 1.10-1 1.20-2 1.065+2 1.520 3.79-2 9.07-3 1.226+2 1.198 1.14-1 5.05-2 1.751+2 1.203 1.38-1 4.96-2 9.712+0 1.968 8.17-2 -3.74-4 1.147+1 1.695 -2.18-2	3000 1.885+1 1.962 1.25-1 -4.79-4 2.555+1 1.601 -1.06-2 1.62-3 4.983+1 1.653 -1.21-2 7.04-3 3.678+1 1.231 4.73-1 7.96-2 5.191+1 1.204 4.93-1 8.07-2 4.707+0 1.973 -6.05-2 -4.96-4 5.296+0 1.667 8.23-2	4000 1.155+1 1.970 -5.46-2 -5.95-4 1.443+1 1.598 1.26-1 4.36-3 2.711+1 1.663 1.53-1 1.11-2 1.487+1 1.172 7.47-1 1.04-1 2.082+1 1.132 7.56-1 1.08-1 2.758+0 1.978 -1.17-1 -5.71-4 2.918+0 1.621 2.53-1	5000 7.728+0 1.976 -1.22-1 -6.62-4 8.929+0 1.567 3.12-1 9.36-3 1.634+1 1.641 3.58-1 1.56-2 7.160+0 1.097 9.54-1 1.29-1 9.958+0 1.052 9.53-1 1.35-1 1.804+0 1.981 -1.20-1 -6.24-4 1.790+0 1.571 4.31-1	6000 5.500+0 1.981 -1.27-1 -7.08-4 5.903+0 1.527 4.98-1 1.56-2 1.058+1 1.608 5.59-1 2.05-2 3.869+0 1.022 1.12+0 1.53-1 5.349+0 0.977 1.11+0 1.62-1 1.266+0 1.984 -8.81-2 -6.62-4 1.181+0 1.521 6.01-1	7000 4.094+0 1.984 -9.32-2 -7.40-4 4.102+0 1.485 6.71-1 2.27-2 7.228+0 1.570 7.45-1 2.59-2 2.270+0 0.951 1.25+0 1.78-1 3.122+0 0.908 1.23+0 1.89-1 9.335-1 1.985 -3.37-2 -6.93-4 8.210-1 1.474 7.59-1	8000 3.152+0 1.985 -3.54-2 -7.66-4 2.962+0 1.442 8.30-1 3.05-2 5.145+0 1.531 9.15-1 3.18-2 1.417+0 0.886 1.35+0 2.03-1 1.939+0 0.846 1.33+0 2.15-1 7.141-1 1.985 3.57-2 -7.15-4 5.938-1 1.428 9.05-1	9000 2.492+0 1.985 3.76-2 -7.85-4 2.207+0 1.400 9.75-1 3.89-2 3.784+0 1.491 1.07+0 3.83-2 9.288-1 0.825 1.44+0 2.26-1 1.265+0 0.789 1.41+0 2.40-1 5.620-1 1.985 1.15-1 -7.37-4 4.431-1 1.385 1.04+0	10000 2.012+(1.985 1.20-1 -8.02- 1.686+(1.360 1.11+0 4.77-2 2.859+(1.452 -0.769 1.51+0 2.49-1 8.589- 0.737 1.48+0 2.64-1 4.522- 1.983 2.01-1 -7.54- 3.392- 1.343 1.16+0
Z= 58, Ce: [X Shell $3s_{1/2}$ $E_b = 1434.6 \text{ eV}$ $3p_{1/2}$ $E_b = 1272.8 \text{ eV}$ $3p_{3/2}$ $E_b = 1185.4 \text{ eV}$ $3d_{3/2}$ $E_b = 901.3 \text{ eV}$ $3d_{5/2}$ $E_b = 883.3 \text{ eV}$ $4s_{1/2}$ $E_b = 289.6 \text{ eV}$	$\begin{array}{c} \delta \\ \text{fe} \text{Aff}_{5/2}^{2} \text{c} \end{array}$ $\begin{array}{c} \sigma \\ \beta \\ \gamma \\ \delta \\ \sigma \\ \sigma \\ \beta \\ \gamma \\ \delta \\ \sigma \\ \sigma \\ \beta \\ \gamma \\ \delta \\ \sigma \\ \sigma \\ \beta \\ \gamma \\ \delta \\ \sigma \\ \sigma \\ \beta \\ \gamma \\ \delta \\ \sigma \\ \sigma$	$\begin{array}{c} -2.80-4 \\ \hline 6s_{1/2}^2 \\ \hline k (eV) \\ \hline 1500 \\ \hline 4.933+1 \\ 1.947 \\ 1.01+0 \\ 3.81-4 \\ \hline 7.425+1 \\ 1.105 \\ 3.75-1 \\ 8.54-2 \\ \hline 1.658+2 \\ 1.213 \\ 2.91-1 \\ 5.05-2 \\ \hline 2.719+2 \\ 1.036 \\ -7.18-2 \\ 2.65-2 \\ \hline 3.926+2 \\ 1.075 \\ -5.77-2 \\ 2.58-2 \\ \hline 1.585+1 \\ 1.965 \\ 1.96-1 \\ -2.79-4 \\ \hline 1.885+1 \\ 1.682 \\ \hline \end{array}$	2000 3.515+1 1.953 5.38-1 -2.14-4 5.111+1 1.477 1.10-1 1.20-2 1.065+2 1.520 3.79-2 9.07-3 1.226+2 1.198 1.14-1 5.05-2 1.751+2 1.203 1.38-1 4.96-2 9.712+0 1.968 8.17-2 -3.74-4 1.147+1 1.695	3000 1.885+1 1.962 1.25-1 -4.79-4 2.555+1 1.601 -1.06-2 1.62-3 4.983+1 1.653 -1.21-2 7.04-3 3.678+1 1.231 4.73-1 7.96-2 5.191+1 1.204 4.93-1 8.07-2 4.707+0 1.973 -6.05-2 -4.96-4 5.296+0 1.667	4000 1.155+1 1.970 -5.46-2 -5.95-4 1.443+1 1.598 1.26-1 4.36-3 2.711+1 1.663 1.53-1 1.11-2 1.487+1 1.172 7.47-1 1.04-1 2.082+1 1.132 7.56-1 1.08-1 2.758+0 1.978 -1.17-1 -5.71-4 2.918+0 1.621	5000 7.728+0 1.976 -1.22-1 -6.62-4 8.929+0 1.567 3.12-1 9.36-3 1.634+1 1.56-2 7.160+0 1.097 9.54-1 1.29-1 9.958+0 1.052 9.53-1 1.35-1 1.804+0 1.981 -1.20-1 -6.24-4 1.790+0 1.571	6000 5.500+0 1.981 -1.27-1 -7.08-4 5.903+0 1.527 4.98-1 1.56-2 1.058+1 1.608 5.59-1 2.05-2 3.869+0 1.022 1.12+0 1.53-1 5.349+0 0.977 1.11+0 1.62-1 1.266+0 1.984 -8.81-2 -6.62-4 1.181+0 1.521	7000 4.094+0 1.984 -9.32-2 -7.40-4 4.102+0 1.485 6.71-1 2.27-2 7.228+0 1.570 7.45-1 2.59-2 2.270+0 0.951 1.25+0 1.78-1 3.122+0 0.908 1.23+0 1.89-1 9.335-1 1.985 -3.37-2 -6.93-4 8.210-1 1.474	8000 3.152+0 1.985 -3.54-2 -7.66-4 2.962+0 1.442 8.30-1 3.05-2 5.145+0 1.531 9.15-1 3.18-2 1.417+0 0.886 1.35+0 2.03-1 1.939+0 0.846 1.33+0 2.15-1 7.141-1 1.985 3.57-2 -7.15-4 5.938-1 1.428	9000 2.492+0 1.985 3.76-2 -7.85-4 2.207+0 1.400 9.75-1 3.89-2 3.784+0 1.491 1.07+0 3.83-2 9.288-1 0.825 1.44+0 2.26-1 1.265+0 0.789 1.41+0 2.40-1 1.985 1.15-1 -7.37-4 4.431-1 1.385	10000 2.012+(1.985 1.20-1 -8.02- 1.686+(1.360 1.11+0 4.77-2 2.859+(1.452 -0.769 1.51+0 2.49-1 8.589- 0.737 1.48+0 2.64-1 4.522- 1.983 2.01-1 -7.54- 3.392- 1.343 1.16+0
Z= 58, Ce: [X] Shell $3s_{1/2}$ $E_b = 1434.6 \text{ eV}$ $3p_{1/2}$ $E_b = 1185.4 \text{ eV}$ $3d_{3/2}$ $E_b = 901.3 \text{ eV}$ $3d_{5/2}$ $E_b = 883.3 \text{ eV}$ $4s_{1/2}$ $E_b = 289.6 \text{ eV}$ $4p_{1/2}$ $E_b = 223.3 \text{ eV}$	$\begin{array}{c} \delta \\ \epsilon \mathbf{4f_{5/2}^2} \\ \hline \\ \sigma \\ \beta \\ \gamma \\ \delta \\ \hline \\ \sigma \\ \beta \\ \gamma \\ \delta \\ \hline \\ \sigma \\ \beta \\ \gamma \\ \delta \\ \hline \\ \sigma \\ \beta \\ \gamma \\ \delta \\ \hline \\ \sigma \\ \beta \\ \gamma \\ \delta \\ \hline \\ \sigma \\ \beta \\ \gamma \\ \delta \\ \hline \\ \sigma \\ \beta \\ \gamma \\ \delta \\ \hline \\ \sigma \\ \beta \\ \gamma \\ \delta \\ \hline \\ \sigma \\ \beta \\ \gamma \\ \delta \\ \hline \\ \sigma \\ \beta \\ \gamma \\ \delta \\ \hline \\ \sigma \\ \beta \\ \gamma \\ \delta \\ \hline \\ \sigma \\ \beta \\ \gamma \\ \delta \\ \hline \\ \sigma \\ \beta \\ \gamma \\ \delta \\ \hline \\ \sigma \\ \beta \\ \gamma \\ \delta \\ \hline \\ \sigma \\ \beta \\ \gamma \\ \delta \\ \hline \\ \sigma \\ \beta \\ \gamma \\ \delta \\ \hline \\ \sigma \\ \sigma \\ \beta \\ \gamma \\ \delta \\ \hline \\ \sigma \\ \sigma \\ \beta \\ \gamma \\ \delta \\ \hline \\ \sigma \\ \sigma \\ \beta \\ \gamma \\ \delta \\ \hline \\ \sigma \\ \sigma \\ \beta \\ \gamma \\ \delta \\ \hline \\ \sigma \\ \sigma \\ \beta \\ \gamma \\ \delta \\ \hline \\ \sigma \\ \sigma \\ \beta \\ \gamma \\ \delta \\ \hline \\ \sigma \\ \sigma \\ \beta \\ \gamma \\ \delta \\ \hline \\ \sigma \\ \sigma \\ \beta \\ \gamma \\ \delta \\ \hline \\ \sigma \\ \sigma \\ \beta \\ \gamma \\ \delta \\ \hline \\ \sigma \\ \sigma \\ \delta \\ \sigma \\ \sigma \\ \rho \\ \gamma \\ \delta \\ \sigma \\ \sigma$	$\begin{array}{c} -2.80-4 \\ \hline 65s_{1/2}^2 \\ \hline k (eV) \\ \hline 1500 \\ \hline 4.933+1 \\ 1.947 \\ 1.01+0 \\ 3.81-4 \\ \hline 7.425+1 \\ 1.105 \\ 3.75-1 \\ 8.54-2 \\ \hline 1.658+2 \\ 1.213 \\ 2.91-1 \\ 5.05-2 \\ \hline 2.719+2 \\ 1.036 \\ -7.18-2 \\ 2.65-2 \\ \hline 3.926+2 \\ 1.075 \\ -5.77-2 \\ 2.58-2 \\ \hline 1.585+1 \\ 1.965 \\ 1.96-1 \\ -2.79-4 \\ \hline 1.885+1 \\ 1.682 \\ 3.66-3 \\ -1.38-3 \\ \hline 3.915+1 \\ \hline \end{array}$	-3.56-4 2000 3.515+1 1.953 5.38-1 -2.14-4 5.111+1 1.477 1.10-1 1.20-2 1.065+2 1.520 3.79-2 9.07-3 1.226+2 1.198 1.14-1 5.05-2 1.751+2 1.203 1.38-1 4.96-2 9.712+0 1.968 8.17-2 -3.74-4 1.147+1 1.695 -2.18-2 -1.56-3 2.303+1	3000 1.885+1 1.962 1.25-1 -4.79-4 2.555+1 1.601 -1.06-2 1.62-3 4.983+1 1.653 -1.21-2 7.04-3 3.678+1 1.231 4.73-1 7.96-2 5.191+1 1.204 4.93-1 8.07-2 4.707+0 1.973 -6.05-2 -4.96-4 5.296+0 1.667 8.23-2 -1.63-4 1.017+1	4000 1.155+1 1.970 -5.46-2 -5.95-4 1.443+1 1.598 1.26-1 4.36-3 2.711+1 1.663 1.53-1 1.11-2 1.487+1 1.172 7.47-1 1.04-1 2.082+1 1.132 7.56-1 1.08-1 2.758+0 1.978 -1.17-1 -5.71-4 2.918+0 1.621 2.53-1 3.22-3 5.437+0	5000 7.728+0 1.976 -1.22-1 -6.62-4 8.929+0 1.567 3.12-1 9.36-3 1.634+1 1.641 3.58-1 1.56-2 7.160+0 1.097 9.54-1 1.29-1 9.958+0 1.052 9.53-1 1.35-1 1.804+0 1.981 -1.20-1 -6.24-4 1.790+0 1.571 4.31-1 8.23-3 3.261+0	6000 5.500+0 1.981 -1.27-1 -7.08-4 5.903+0 1.527 4.98-1 1.56-2 1.058+1 1.608 5.59-1 2.05-2 3.869+0 1.022 1.12+0 1.53-1 5.349+0 0.977 1.11+0 1.62-1 1.266+0 1.984 -8.81-2 -6.62-4 1.181+0 1.521 6.01-1 1.45-2 2.112+0	7000 4.094+0 1.984 -9.32-2 -7.40-4 4.102+0 1.485 6.71-1 2.27-2 7.228+0 1.570 7.45-1 2.59-2 2.270+0 0.951 1.25+0 1.78-1 3.122+0 0.908 1.23+0 1.89-1 9.335-1 1.985 -3.37-2 -6.93-4 8.210-1 1.474 7.59-1 2.17-2 1.445+0	8000 3.152+0 1.985 -3.54-2 -7.66-4 2.962+0 1.442 8.30-1 3.05-2 5.145+0 1.531 9.15-1 3.18-2 1.417+0 0.886 1.35+0 2.03-1 1.939+0 0.846 1.33+0 2.15-1 7.141-1 1.985 3.57-2 -7.15-4 5.938-1 1.428 9.05-1 2.97-2 1.031+0	9000 2.492+0 1.985 3.76-2 -7.85-4 2.207+0 1.400 9.75-1 3.89-2 3.784+0 1.491 1.07+0 3.83-2 9.288-1 0.825 1.44+0 2.26-1 1.265+0 0.789 1.41+0 2.40-1 5.620-1 1.985 1.15-1 -7.37-4 4.431-1 1.385 1.04+0 3.82-2 7.601-1	10000 2.012+(1.985 1.20-1 -8.02- 1.686+(1.360 1.11+0 4.77-2 2.859+(1.452 1.21+0 4.53-2 0.769 1.51+0 2.49-1 8.589- 0.737 1.48+0 2.64-1 4.522- 1.983 2.01-1 -7.54- 3.392- 1.343 1.16+0 4.71-2 5.755-
Z= 58, Ce: [X] Shell $3s_{1/2}$ $E_b = 1434.6 \text{ eV}$ $3p_{1/2}$ $E_b = 1272.8 \text{ eV}$ $3d_{3/2}$ $E_b = 901.3 \text{ eV}$ $3d_{5/2}$ $E_b = 883.3 \text{ eV}$ $4s_{1/2}$ $E_b = 289.6 \text{ eV}$ $4p_{1/2}$ $E_b = 223.3 \text{ eV}$	δ (e) 4f ² _{5/2} (c) σ σ β γ γ δ σ σ β γ γ δ σ σ γ δ σ σ γ δ σ σ γ δ σ σ γ δ σ σ γ δ σ σ γ δ σ σ γ δ σ σ γ δ σ σ σ γ δ σ σ σ γ δ σ σ σ γ δ σ σ σ σ	$\begin{array}{c} -2.80-4 \\ \hline 65s_{1/2}^2 \\ \hline k (eV) \\ \hline 1500 \\ \hline 4.933+1 \\ 1.947 \\ 1.01+0 \\ 3.81-4 \\ \hline 7.425+1 \\ 1.105 \\ 3.75-1 \\ 8.54-2 \\ \hline 1.658+2 \\ 1.213 \\ 2.91-1 \\ 5.05-2 \\ \hline 2.719+2 \\ 1.036 \\ -7.18-2 \\ 2.65-2 \\ \hline 3.926+2 \\ 1.075 \\ -5.77-2 \\ 2.58-2 \\ \hline 1.585+1 \\ 1.965 \\ 1.96-1 \\ -2.79-4 \\ \hline 1.885+1 \\ 1.682 \\ 3.66-3 \\ -1.38-3 \\ \hline \end{array}$	2000 3.515+1 1.953 5.38-1 -2.14-4 5.111+1 1.477 1.10-1 1.20-2 1.065+2 1.520 3.79-2 9.07-3 1.226+2 1.198 1.14-1 5.05-2 1.751+2 1.203 1.38-1 4.96-2 9.712+0 1.98 8.17-2 -3.74-4 1.147+1 1.695 -2.18-2 -1.56-3	3000 1.885+1 1.962 1.25-1 -4.79-4 2.555+1 1.601 -1.06-2 1.62-3 4.983+1 1.653 -1.21-2 7.04-3 3.678+1 1.231 4.73-1 7.96-2 5.191+1 1.204 4.93-1 8.07-2 4.707+0 1.973 -6.05-2 -4.96-4 5.296+0 1.667 8.23-2 -1.63-4	4000 1.155+1 1.970 -5.46-2 -5.95-4 1.443+1 1.598 1.26-1 4.36-3 2.711+1 1.663 1.53-1 1.11-2 1.487+1 1.172 7.47-1 1.04-1 2.082+1 1.132 7.56-1 1.08-1 2.758+0 1.978 -1.17-1 -5.71-4 2.918+0 1.621 2.53-1 3.22-3	5000 7.728+0 1.976 -1.22-1 -6.62-4 8.929+0 1.567 3.12-1 9.36-3 1.634+1 1.56-2 7.160+0 1.097 9.54-1 1.29-1 9.958+0 1.052 9.53-1 1.35-1 1.804+0 1.981 -1.20-1 -6.24-4 1.790+0 1.571 4.31-1 8.23-3	6000 5.500+0 1.981 -1.27-1 -7.08-4 5.903+0 1.527 4.98-1 1.56-2 1.058+1 1.608 5.59-1 2.05-2 3.869+0 1.022 1.12+0 1.53-1 5.349+0 0.977 1.11+0 1.62-1 1.266+0 1.984 -8.81-2 -6.62-4 1.181+0 1.521 6.01-1 1.45-2	7000 4.094+0 1.984 -9.32-2 -7.40-4 4.102+0 1.485 6.71-1 2.27-2 7.228+0 1.570 7.45-1 2.59-2 2.270+0 0.951 1.25+0 1.78-1 3.122+0 0.908 1.23+0 1.89-1 9.335-1 1.985 -3.37-2 -6.93-4 8.210-1 1.474 7.59-1 2.17-2	8000 3.152+0 1.985 -3.54-2 -7.66-4 2.962+0 1.442 8.30-1 3.05-2 5.145+0 1.531 9.15-1 3.18-2 1.417+0 0.886 1.35+0 2.03-1 1.939+0 0.846 1.33+0 2.15-1 7.141-1 1.985 3.57-2 -7.15-4 5.938-1 1.428 9.05-1 2.97-2	9000 2.492+0 1.985 3.76-2 -7.85-4 2.207+0 1.400 9.75-1 3.89-2 3.784+0 1.491 1.07+0 3.83-2 9.288-1 0.825 1.44+0 2.26-1 1.265+0 0.789 1.41+0 2.40-1 1.985 1.15-1 -7.37-4 4.431-1 1.385 1.04+0 3.82-2	10000 2.012+(1.985 1.20-1 -8.02- 1.686+(1.360 1.11+0 4.77-2 2.859+(1.452 1.21+0 4.53-2 0.769 1.51+0 2.49-1 8.589- 0.737 1.48+0 2.64-1 4.522- 1.983 2.01-1 -7.54- 3.392- 1.343

Table 1 (contin	ued)										
$4d_{3/2}$ $E_b = 113.6 \text{ eV}$	σ β γ δ	3.530+1 1.365 1.30-1 3.15-2	1.713+1 1.350 2.95-1 4.49-2	5.623+0 1.264 5.87-1 7.04-2	2.400+0 1.168 8.12-1 9.59-2	1.199+0 1.078 9.90-1 1.22-1	6.659-1 0.999 1.13+0 1.48-1	3.988-1 0.927 1.25+0 1.74-1	2.530-1 0.861 1.35+0 1.99-1	1.680-1 0.800 1.43+0 2.23-1	1.157-1 0.745 1.50+0 2.47-1
$4d_{5/2}$ $E_b =$ 107.6 eV	σ β γ δ	5.060+1 1.356 1.45-1 3.09-2	2.436+1 1.323 3.12-1 4.50-2	7.905+0 1.220 5.96-1 7.31-2	3.345+0 1.117 8.12-1 1.01-1	1.660+0 1.027 9.81-1 1.30-1	9.158-1 0.949 1.12+0 1.58-1	5.454-1 0.880 1.23+0 1.86-1	3.443-1 0.819 1.33+0 2.12-1	2.274-1 0.764 1.41+0 2.38-1	1.559-1 0.713 1.47+0 2.62-1
$4f_{5/2}$ $E_b = 0.1 \text{ eV}$	σ β γ δ	4.446+0 1.013 5.22-1 1.20-1	1.504+0 0.925 6.44-1 1.50-1	3.078-1 0.780 8.04-1 2.08-1	9.568-2 0.678 9.15-1 2.62-1	3.752-2 0.600 1.00+0 3.13-1	1.708-2 0.534 1.07+0 3.59-1	8.634-3 0.476 1.13+0 4.01-1	4.724-3 0.423 1.17+0 4.40-1	2.750-3 0.375 1.20+0 4.76-1	1.684-3 0.330 1.23+0 5.09-1
$5s_{1/2}$ $E_b =$ 37.8 eV	σ β γ δ	2.611+0 1.967 1.32-1 -2.99-4	1.578+0 1.969 3.80-2 -3.84-4	7.536-1 1.974 -7.82-2 -4.96-4	4.379-1 1.979 -1.20-1 -5.63-4	2.848-1 1.982 -1.15-1 -6.14-4	1.993-1 1.984 -7.76-2 -6.52-4	1.466-1 1.985 -2.01-2 -6.83-4	1.120-1 1.985 5.13-2 -7.04-4	8.800-2 1.984 1.32-1 -7.26-4	7.075-2 1.983 2.19-1 -7.42-4
$ \begin{array}{c} 5p_{1/2} \\ E_b = \\ 21.8 \text{ eV} \end{array} $	σ β γ δ	2.558+0 1.716 -1.43-2 -2.17-3	1.538+0 1.714 -1.79-2 -2.02-3	7.020-1 1.675 1.01-1 -5.48-4	3.847-1 1.624 2.74-1 2.90-3	2.354-1 1.571 4.52-1 8.02-3	1.551-1 1.520 6.21-1 1.43-2	1.077-1 1.471 7.77-1 2.15-2	7.786-2 1.424 9.20-1 2.93-2	5.809-2 1.379 1.05+0 3.77-2	4.446-2 1.337 1.17+0 4.64-2
$5p_{3/2}$ $E_b =$ 18.8 eV	$\sigma \ eta \ eta \ \gamma \ \delta$	5.008+0 1.729 -3.00-2 5.90-4	2.919+0 1.744 -2.25-2 2.29-3	1.278+0 1.727 1.15-1 5.31-3	6.803-1 1.690 3.04-1 8.75-3	4.072-1 1.647 4.96-1 1.30-2	2.635-1 1.601 6.78-1 1.80-2	1.802-1 1.557 8.47-1 2.36-2	1.286-1 1.513 1.00+0 2.97-2	9.478-2 1.470 1.14+0 3.63-2	7.176-2 1.429 1.27+0 4.32-2
$6s_{1/2}$ $E_b = 6.0 \text{ eV}$	$\sigma \ eta \ eta \ \gamma \ \delta$	1.946-1 1.967 1.28-1 -3.02-4	1.173-1 1.969 3.50-2 -3.85-4	5.578-2 1.975 -7.99-2 -4.96-4	3.234-2 1.979 -1.21-1 -5.67-4	2.101-2 1.982 -1.14-1 -6.14-4	1.468-2 1.984 -7.64-2 -6.46-4	1.080-2 1.985 -1.90-2 -6.71-4	8.244-3 1.985 5.21-2 -7.00-4	6.477-3 1.985 1.33-1 -7.22-4	5.207-3 1.983 2.20-1 -7.37-4
Z= 59, Pr: [X	e]4f _{5/2} 6	*									
Shell		k (eV) 1500	2000	3000	4000	5000	6000	7000	8000	9000	10000
$3p_{1/2}$ $E_b =$ 1337.4 eV	σ β γ δ	7.420+1 0.959 3.48-1 1.21-1	5.243+1 1.446 1.55-1 1.67-2	2.663+1 1.596 -1.72-2 1.58-3	1.517+1 1.601 1.00-1 3.69-3	9.441+0 1.574 2.80-1 8.34-3	6.269+0 1.537 4.64-1 1.42-2	4.371+0 1.496 6.37-1 2.10-2	3.167+0 1.454 7.97-1 2.84-2	2.365+0 1.413 9.42-1 3.63-2	1.811+0 1.373 1.07+0 4.47-2
$3p_{3/2}$ $E_b = 1242.2 \text{ eV}$	σ β γ δ	1.695+2 1.121 3.18-1 6.93-2	1.104+2 1.492 6.77-2 1.14-2	5.223+1 1.649 -2.43-2 6.91-3	2.860+1 1.666 1.25-1 1.08-2	1.731+1 1.649 3.25-1 1.51-2	1.125+1 1.618 5.25-1 1.98-2	7.706+0 1.582 7.12-1 2.49-2	5.498+0 1.545 8.83-1 3.04-2	4.053+0 1.506 1.04+0 3.65-2	3.067+0 1.468 1.18+0 4.29-2
$3d_{3/2}$ $E_b = 951.1 \text{ eV}$	σ β γ δ	2.939+2 0.990 -9.71-2 2.17-2	1.336+2 1.182 7.83-2 4.77-2	4.040+1 1.235 4.40-1 7.76-2	1.642+1 1.184 7.22-1 1.02-1	7.941+0 1.112 9.36-1 1.26-1	4.305+0 1.038 1.10+0 1.49-1	2.533+0 0.969 1.24+0 1.73-1	1.586+0 0.904 1.35+0 1.97-1	1.042+0 0.844 1.44+0 2.21-1	7.117-1 0.788 1.51+0 2.44-1
$3d_{5/2}$ $E_b =$ 931.0 eV	σ β γ δ	4.254+2 1.038 -8.49-2 2.11-2	1.910+2 1.192 1.02-1 4.65-2	5.700+1 1.210 4.63-1 7.85-2	2.298+1 1.144 7.34-1 1.06-1	1.104+1 1.066 9.37-1 1.32-1	5.947+0 0.991 1.09+0 1.58-1	3.481+0 0.923 1.22+0 1.84-1	2.168+0 0.861 1.33+0 2.10-1	1.418+0 0.804 1.41+0 2.35-1	9.643-1 0.753 1.48+0 2.59-1
$4s_{1/2}$ $E_b =$ 304.5 eV	$\sigma \ eta \ eta \ \gamma \ \delta$	1.651+1 1.962 2.16-1 -2.96-4	1.015+1 1.965 9.91-2 -4.01-4	4.936+0 1.971 -5.02-2 -5.36-4	2.898+0 1.976 -1.15-1 -6.19-4	1.897+0 1.979 -1.25-1 -6.78-4	1.333+0 1.982 -9.98-2 -7.22-4	9.841-1 1.984 -5.11-2 -7.56-4	7.535-1 1.984 1.33-2 -7.82-4	5.935-1 1.984 8.84-2 -8.06-4	4.780-1 1.983 1.71-1 -8.26-4
$4p_{1/2}$ $E_b =$ 236.3 eV	$\sigma \ eta \ eta \ \gamma \ \delta$	1.967+1 1.678 1.43-2 -1.35-3	1.205+1 1.694 -2.28-2 -1.72-3	5.611+0 1.672 6.64-2 -5.84-4	3.108+0 1.628 2.30-1 2.50-3	1.915+0 1.580 4.05-1 7.19-3	1.267+0 1.532 5.74-1 1.30-2	8.836-1 1.485 7.32-1 1.98-2	6.408-1 1.440 8.77-1 2.74-2	4.793-1 1.397 1.01+0 3.55-2	3.677-1 1.357 1.13+0 4.41-2
$4p_{3/2}$ $E_b =$ 217.6 eV	σ β γ δ	4.110+1 1.690 -1.18-2 8.50-4	2.430+1 1.723 -3.35-2 2.35-3	1.080+1 1.724 7.79-2 5.51-3	5.797+0 1.695 2.59-1 8.86-3	3.488+0 1.656 4.50-1 1.28-2	2.265+0 1.615 6.33-1 1.74-2	1.554+0 1.573 8.03-1 2.26-2	1.111+0 1.531 9.60-1 2.84-2	8.207-1 1.491 1.10+0 3.47-2	6.225-1 1.452 1.24+0 4.15-2
$ \begin{array}{c} 4d_{3/2} \\ E_b = \\ 117.9 \text{ eV} \end{array} $	σ β γ δ	3.817+1 1.364 1.11-1 2.99-2	1.870+1 1.356 2.74-1 4.33-2	6.206+0 1.276 5.68-1 6.83-2	2.668+0 1.183 7.97-1 9.32-2	1.340+0 1.095 9.78-1 1.18-1	7.476-1 1.015 1.13+0 1.43-1	4.495-1 0.944 1.25+0 1.69-1	2.862-1 0.879 1.35+0 1.93-1	1.905-1 0.819 1.43+0 2.17-1	1.316-1 0.764 1.50+0 2.41-1
$4d_{5/2}$ $E_b = 110.1 \text{ eV}$	σ β γ δ	5.460+1 1.357 1.27-1 2.92-2	2.652+1 1.330 2.92-1 4.32-2	8.700+0 1.231 5.79-1 7.08-2	3.707+0 1.130 7.99-1 9.86-2	1.849+0 1.041 9.71-1 1.26-1	1.025+0 0.963 1.11+0 1.54-1	6.127-1 0.895 1.23+0 1.81-1	3.880-1 0.834 1.32+0 2.07-1	2.571-1 0.778 1.41+0 2.33-1	1.767-1 0.728 1.48+0 2.57-1
$\begin{array}{c} 4f_{5/2} \\ E_b = \end{array}$	σ β	5.602+0 1.022	1.908+0 0.938	3.933-1 0.793	1.229-1 0.689	4.845-2 0.611	2.217-2 0.545	1.126-2 0.487	6.187-3 0.434	3.615-3 0.386	2.220-3 0.341

able 1 (continu	ued)										
2.0 eV	γ	5.12-1 1.18-1	6.39-1 1.47-1	8.05-1 2.04-1	9.19-1 2.57-1	1.01+0 3.08-1	1.08+0 3.53-1	1.14+0 3.96-1	1.18+0 4.34-1	1.22+0 4.70-1	1.24+0 5.04-1
$5s_{1/2}$	σ	2.712+0	1.644+0	7.877-1	4.585-1	2.986-1	2.091-1	1.540-1	1.177-1	9.257-2	7.449-2
$E_b = 37.4 \text{ eV}$	β γ	1.965 1.46-1	1.967 5.07-2	1.972 -7.10-2	1.977 -1.20-1	1.980 -1.21-1	1.983 -8.97-2	1.984 -3.76-2	1.984 2.90-2	1.984 1.06-1	1.982 1.89-1
37.16	δ	-3.21-4	-4.13-4	-5.36-4	-6.11-4	-6.67 - 4	-7.09-4	-7.44-4	-7.68-4	-7.93-4	-8.12-4
$5p_{1/2}$	σ	2.672+0	1.616+0	7.431-1	4.092-1	2.513-1	1.661-1	1.157-1	8.387-2	6.272-2	4.811-2
$E_b =$	β	1.715	1.715	1.681	1.632	1.581	1.531	1.483	1.437	1.393	1.351
24.6 eV	γ	-8.29 - 3	-2.15-2	8.50-2	2.51 - 1	4.26 - 1	5.94 - 1	7.50 - 1	8.94 - 1	1.03+0	1.15+0
	δ	-2.30-3	-2.23-3	-9.90-4	2.15-3	6.92-3	1.30-2	1.98-2	2.74-2	3.54-2	4.37-2
$5p_{3/2}$	σ	5.206+0	3.048+0	1.342+0	7.171-1	4.305-1	2.793-1	1.915-1	1.369-1	1.011-1	7.670-2
$E_b = 21.2 \text{ eV}$	β γ	1.725 -2.67-2	1.744 -2.81-2	1.733 9.74–2	1.699 2.80-1	1.658 4.70-1	1.614 6.52-1	1.571 8.21-1	1.528 9.76-1	1.486 1.12+0	1.446 1.25+0
21.2 CV	δ	4.18-4	2.13-3	5.13-3	8.41-3	1.24-2	1.71-2	2.24-2	2.83-2	3.45-2	4.11-2
6s _{1/2}	σ	1.972-1	1.192-1	5.686-2	3.302-2	2.147-2	1.502-2	1.105-2	8.444-3	6.640-3	5.342-3
$E_b =$	β	1.965	1.967	1.972	1.977	1.980	1.983	1.984	1.984	1.984	1.982
6.0 eV	γ	1.43-1	4.78-2	-7.26-2	-1.21-1	-1.20-1	-8.88-2	-3.65-2	2.98-2	1.06-1	1.89-1
	δ	-3.23-4	-4.14-4	-5.36-4	-6.15-4	-6.69-4	-7.05-4	-7.33-4	-7.64-4	-7.89-4	-8.06-4
Z= 60, Nd: [X	e]4f _{5/2}	-/-									
		k (eV)									
Shell		1500	2000	3000	4000	5000	6000	7000	8000	9000	10000
$3p_{1/2}$	σ	7.314+1	5.361+1	2.769+1	1.591+1	9.960+0	6.643+0	4.649+0	3.377+0	2.529+0	1.941+0
$E_b = 1402.8 \text{ eV}$	β	0.738 2.03-1	1.408	1.589 -1.97-2	1.603 7.68-2	1.580	1.545 4.29-1	1.506	1.466	1.425 9.09-1	1.386
1402.8 eV	$_{\delta}^{\gamma}$	2.03 – 1 1.69 – 1	2.05-1 $2.29-2$	1.69-3	3.08-3	2.48-1 7.35-3	4.29—1 1.29—2	6.03-1 1.94-2	7.63-1 2.65-2	3.41–2	1.04+0 4.21-2
3p _{3/2}	σ	1.723+2	1.141+2	5.460+1	3.009+1	1.829+1	1.193+1	8.195+0	5.862+0	4.329+0	3.282+0
$E_b =$	β	1.004	1.462	1.642	1.669	1.656	1.628	1.594	1.558	1.521	1.484
1297.4 eV	γ	3.17 - 1	1.01 - 1	-3.34-2	9.93-2	2.92 - 1	4.90 - 1	6.78 - 1	8.50 - 1	1.01+0	1.15+0
	δ	9.46-2	1.45-2	6.83-3	1.05-2	1.47-2	1.92-2	2.41-2	2.93-2	3.49-2	4.10-2
$3d_{3/2}$	σ	3.158+2	1.450+2	4.420+1	1.807+1	8.774+0	4.774+0	2.818+0	1.768+0	1.164+0	7.971 - 1
$E_b =$	β	0.938	1.164	1.237	1.194	1.126	1.055	0.986	0.922	0.862	0.807
999.9 eV	$_{\delta}^{\gamma}$	-1.18-1 1.65-2	4.32-2 4.46-2	4.07-1 7.57-2	6.96-1 1.00-1	9.17-1 1.23-1	1.09+0 1.46-1	1.23+0 1.69-1	1.34+0 1.92-1	1.44+0 2.15-1	1.51+0 2.37-1
24		4,587+2	2.074+2	6.236+1	2.527+1	1.219+1	6.590+0	3.868+0	2.415+0	1.583+0	1.079+0
$3d_{5/2}$ $E_b =$	$\frac{\sigma}{\beta}$	0.996	2.074+2 1.179	1.214	1.154	1.219+1	1.005	0.937	0.876	0.819	0.768
977.7 eV	γ	-1.08-1	6.74-2	4.33-1	7.11-1	9.20-1	1.08+0	1.21+0	1.32+0	1.41+0	1.48+0
	δ	1.61 - 2	4.34 - 2	7.62 - 2	1.03 - 1	1.29 - 1	1.55 - 1	1.80 - 1	2.05 - 1	2.30 - 1	2.53 - 1
4s _{1/2}	σ	1.711+1	1.056+1	5.159+0	3.036+0	1.990+0	1.400+0	1.035+0	7.929-1	6.250-1	5.039-1
$E_b =$	β	1.959	1.962	1.968	1.973	1.977	1.980	1.982	1.983	1.983	1.982
315.2 eV	$_{\delta}^{\gamma}$	2.34-1 -3.14-4	1.16-1 -4.29-4	-3.93-2 $-5.77-4$	-1.11-1 $-6.70-4$	-1.29-1 $-7.36-4$	-1.10-1 $-7.85-4$	-6.70-2 $-8.24-4$	-7.59-3 -8.53-4	6.31-2 $-8.80-4$	1.41-1 -9.02-4
4n	σ	2.041+1	1.259+1	5.914+0	3.295+0	2.039+0	1.354+0	9.471-1	6.886-1	5.164-1	3.970-1
$\begin{array}{l} 4p_{1/2} \\ E_b = \end{array}$	β	1.674	1.694	1.676	1.635	1.589	1.534+0	1.496	1.452	1.410	1.370
243.3 eV	γ	2.54-2	-2.22-2	5.23-2	2.08-1	3.80-1	5.47-1	7.04-1	8.50-1	9.84-1	1.11+0
	δ	-1.30 - 3	-1.86 - 3	-9.61 - 4	1.83-3	6.20 - 3	1.18 - 2	1.82-2	2.53-2	3.31-2	4.12 - 2
4p _{3/2}	σ	4.296+1	2.553+1	1.142+1	6.157+0	3.717+0	2.420+0	1.664+0	1.193+0	8.828-1	6.708-1
$E_b =$	β	1.684	1.721	1.728	1.702	1.666	1.627	1.586	1.545	1.506	1.467
224.6 eV	δ	-4.03 - 3 $7.79 - 4$	-3.57-2 $2.21-3$	6.18-2 5.36-3	2.36-1 8.59-3	4.24-1 1.24-2	6.06 - 1 $1.67 - 2$	7.76-1 2.16-2	9.33-1 2.70-2	1.08+0 3.29-2	1.21+0 3.92-2
14		4.114+1	2.034+1	6.824+0	2.954+0	1.492+0	8.357-1	5.044-1	3.222-1	2.151-1	1.490-1
$4d_{3/2}$ $E_b =$	$\frac{\sigma}{\beta}$	1.363	1.361	1.288	1.198	1.492+0	1.033	0.961	0.897	0.837	0.783
123.4 eV	γ	9.28-2	2.53-1	5.48-1	7.82-1	9.66-1	1.12+0	1.24+0	1.35+0	1.43+0	1.51+0
	δ	2.84 - 2	4.18-2	6.63-2	9.06-2	1.15-1	1.39-1	1.64 - 1	1.88 - 1	2.12 - 1	2.35 - 1
4d _{5/2}	σ	5.870+1	2.877+1	9.536+0	4.091+0	2.051+0	1.141+0	6.849-1	4.352-1	2.891-1	1.993-1
$E_b =$	β	1.358	1.336	1.243	1.144	1.055	0.977	0.909	0.848	0.793	0.743
113.5 eV	$_{\delta}^{\gamma}$	1.09-1 2.76-2	2.72-1 4.15-2	5.61-1 6.86-2	7.85-1 9.59-2	9.60-1 1.23-1	1.10+0 1.50-1	1.22+0 1.76-1	1.32+0 2.02-1	1.41+0 2.27-1	1.48+0 2.51-1
1f		6.861+0	2.356+0				2.803-2	1.430-2	7.891-3	4.628-3	
$4f_{5/2}$ $E_b =$	$\frac{\sigma}{\beta}$	6.861+0 1.030	2.356+0 0.949	4.895-1 0.805	1.538-1 0.701	6.095-2 0.621	2.803-2 0.556	1.430-2 0.498	7.891-3 0.446	4.628-3 0.397	2.851-3 0.352
1.5 eV	γ	5.00-1	6.32-1	8.06-1	9.22-1	1.01+0	1.09+0	1.14+0	1.19+0	1.23+0	1.25+0
	δ	1.16-1	1.44-1	2.00-1	2.53-1	3.02-1	3.48-1	3.90-1	4.29-1	4.65-1	4.98-1
5s _{1/2}	σ	2.806+0	1.706+0	8.203-1	4.784-1	3.119-1	2.186-1	1.611-1	1.232-1	9.702-2	7.813-2
$E_b =$	β	1.962	1.964	1.970	1.975	1.978	1.981	1.982	1.983	1.983	1.982
37.5 eV	γ	1.60-1	6.40-2	-6.28 - 2	-1.18 - 1	-1.25 - 1	-1.01-1	-5.40-2	7.75-3	8.01-2	1.60-1
	δ	-3.44-4	-4.44-4	-5.79-4	-6.60-4	-7.24-4	-7.71-4	-8.10-4	-8.37-4	-8.65-4	-8.86-4
$5p_{1/2}$	σ	2.771+0	1.686+0	7.816-1	4.326-1	2.668-1	1.769-1	1.236-1	8.982-2	6.733-2	5.175-2
$E_b = 23.6 \text{ eV}$	β	1.713 -1.45-3	1.717 -2.35-2	1.686 7.01-2	1.639 2.29-1	1.590 4.01-1	1.542 5.67-1	1.495 7.23-1	1.450 8.67-1	1.406 1.00+0	1.365 1.12+0
23.0 EV	γ	-1.43-3	-2.55-2	7.01-2	2.25-1	4.01-1	J.07 — I	1.23-1	0.07-1	1.00⊤0	1.12+0

Table 1 (contin	ued)										
Table 1 (contin	δ	-2.43 - 3	-2.42 - 3	-1.39-3	1.43-3	5.90-3	1.16-2	1.82-2	2.54-2	3.31-2	4.11-2
5p _{3/2}	σ	5.376+0	3.162+0	1.401+0	7.516-1	4.527-1	2.944-1	2.024-1	1.450-1	1.073-1	8.153-2
$E_b =$	β	1.722	1.744	1.737	1.707	1.668	1.627	1.585	1.543	1.502	1.463
19.8 eV	δ	-2.25-2 $2.59-4$	-3.23-2 $1.98-3$	8.10-2 4.97-3	2.57-1 8.11-3	4.44-1 1.19-2	6.25-1 1.64-2	7.94-1 2.15-2	9.50-1 2.70-2	1.09+0 3.29-2	1.22+0 3.91-2
6s _{1/2}	σ	1.993-1	1.208-1	5.783-2	3.365-2	2.190-2	1.533-2	1.129-2	8.634-3	6.795-3	5.471-3
$E_b =$	β	1.962	1.965	1.970	1.975	1.978	1.981	1.983	1.983	1.983	1.982
5.0 eV	γ	1.57-1	6.09-2	-6.45 - 2	-1.19-1	-1.26-1	-1.00-1	-5.29-2	8.72-3	8.05-2	1.60-1
7= C1 Des. [7	δ	$\frac{-3.46-4}{c^2}$	-4.45-4	-5.78-4	-6.67-4	-7.27-4	-7.69-4	-8.00-4	-8.34-4	-8.61-4	-8.80-4
Z= 61, Pm: [X	xe j41 _{5/2}	k (eV)									
Shell		1500	2000	3000	4000	5000	6000	7000	8000	9000	10000
${3p_{1/2}}$	σ	6.997+1	5.468+1	2.874+1	1.666+1	1.049+1	7.027+0	4.935+0	3.596+0	2.700+0	2.077+0
$E_b =$	β	0.267	1.359	1.581	1.603	1.585	1.553	1.516	1.477	1.438	1.399
1471.4 eV	$\gamma \\ \delta$	-2.38-1 1.65-1	2.61-1 $3.19-2$	-1.79-2 1.99-3	5.49-2 2.53-3	2.16-1 6.41-3	3.94-1 1.17-2	5.67-1 1.79-2	7.28-1 2.47-2	8.76-1 3.19-2	1.01+0 3.96-2
		1.738+2	1.178+2	5.704+1	3.163+1				6.242+0		
$3p_{3/2} E_b =$	$\frac{\sigma}{eta}$	0.832	1.178+2	1.635	1.670	1.931+1 1.662	1.264+1 1.637	8.706+0 1.606	1.571	4.619+0 1.535	3.509+0 1.499
1356.9 eV	γ	2.57 - 1	1.41 - 1	-3.95 - 2	7.42 - 2	2.59 - 1	4.55 - 1	6.43 - 1	8.17 - 1	9.76 - 1	1.12+0
	δ	1.31-1	1.88-2	6.81-3	1.03-2	1.43-2	1.87-2	2.33-2	2.83-2	3.36-2	3.92-2
$3d_{3/2}$ $E_b =$	$\frac{\sigma}{eta}$	3.385+2 0.882	1.571+2 1.142	4.829+1 1.238	1.985+1 1.204	9.677+0 1.140	5.283+0 1.071	3.127+0 1.003	1.967+0 0.939	1.298+0 0.880	8.905-1 0.825
1051.5 eV	γ	-1.35-1	8.39 - 3	3.73 - 1	6.69 - 1	8.96 - 1	1.07+0	1.22+0	1.33+0	1.43+0	1.51+0
	δ	1.06-2	4.13-2	7.37-2	9.81-2	1.21-1	1.43-1	1.65-1	1.87-1	2.09-1	2.32 - 1
$3d_{5/2}$	σ	4.941+2	2.251+2	6.815+1	2.775+1	1.343+1	7.287+0	4.289+0	2.685+0	1.763+0	1.204+0
$E_b = 1026.9 \text{ eV}$	$eta \ \gamma$	0.946 -1.29-1	1.163 3.23-2	1.217 4.01-1	1.165 6.87-1	1.093 9.02-1	1.020 1.07+0	0.952 1.20+0	0.890 1.31+0	0.834 1.41+0	0.783 1.48+0
	δ	1.04-2	3.99-2	7.39-2	1.01-1	1.27-1	1.52-1	1.76-1	2.00-1	2.24-1	2.48-1
4s _{1/2}	σ	1.772+1	1.098+1	5.387+0	3.176+0	2.085+0	1.468+0	1.086+0	8.332-1	6.574-1	5.303-1
$E_b = 331.4 \text{ eV}$	β γ	1.956 2.55-1	1.959 1.35-1	1.965 -2.68-2	1.971 1.06 1	1.975 -1.31-1	1.978 -1.19-1	1.980 -8.19-2	1.981 -2.76-2	1.982 3.86-2	1.981 1.13-1
331.167	δ	-3.32-4	-4.59-4	-6.21-4	-7.23-4	-7.96-4	-8.51-4	-8.95 - 4	-9.29-4	-9.59-4	-9.84-4
$4p_{1/2}$	σ	2.115+1	1.314+1	6.226+0	3.488+0	2.167+0	1.445+0	1.013+0	7.386-1	5.551-1	4.277-1
$E_b = 254.7 \text{ eV}$	β γ	1.668 3.88-2	1.692 -2.01-2	1.680 3.87-2	1.642 1.86-1	1.597 3.54-1	1.552 5.20-1	1.507 6.76-1	1.464 8.22-1	1.423 9.57-1	1.383 1.08+0
20 117 01	δ	-1.21-3	-1.99-3	-1.32-3	1.18-3	5.27-3	1.05-2	1.66-2	2.35-2	3.08-2	3.86-2
$-4p_{3/2}$	σ	4.487+1	2.680+1	1.206+1	6.531+0	3.955+0	2.582+0	1.780+0	1.278+0	9.477-1	7.214-1
$E_b = 236.2 \text{ eV}$	β	1.676 5.67-3	1.718 -3.67-2	1.731 4.60-2	1.709 2.12-1	1.676 3.97-1	1.638 5.78-1	1.599 7.48-1	1.559 9.07-1	1.521 1.05+0	1.483 1.19+0
230.2 60	$\delta \gamma$	7.27 - 4	2.05-3	5.20-3	8.34-3	1.20-2	1.61-2	2.07-2	2.58-2	3.12-2	3.72-2
4d _{3/2}	σ	4.411+1	2.201+1	7.468+0	3.255+0	1.653+0	9.298-1	5.633-1	3.609-1	2.417-1	1.678-1
$E_b = 127.6 \text{ eV}$	β	1.360	1.365	1.299	1.213	1.128	1.049	0.979	0.914	0.855	0.801
127.0 ev	$\frac{\gamma}{\delta}$	7.57-2 2.69-2	2.32-1 $4.03-2$	5.28 - 1 $6.45 - 2$	7.65-1 8.81-2	9.54-1 1.12-1	1.11+0 1.35-1	1.23+0 1.59-1	1.34+0 1.82-1	1.43+0 2.06-1	1.51+0 2.28-1
4d _{5/2}	σ	6.277+1	3.104+1	1.040+1	4.492+0	2.264+0	1.265+0	7.618-1	4.855-1	3.235-1	2.235-1
$E_b = 115.6 \text{ eV}$	β γ	1.358 9.22-2	1.341 2.52-1	1.253 5.43-1	1.157 7.70—1	1.069 9.49-1	0.991 1.09+0	0.923 1.21+0	0.862 1.32+0	0.807 1.40+0	0.757 1.48+0
113.0 CV	δ	2.61-2	3.98-2	6.65-2	9.32-2	1.20-1	1.46-1	1.72-1	1.97 – 1	2.22-1	2.46-1
4f _{5/2}	σ	8.293+0	2.869+0	6.005-1	1.896-1	7.547-2	3.486-2	1.786-2	9.893-3	5.822-3	3.597-3
$E_b = 3.5 \text{ eV}$	β	1.037 4.88-1	0.960 6.25-1	0.819 8.06-1	0.713 9.25-1	0.632 1.02+0	0.566 1.09+0	0.508 1.15+0	0.456 1.20+0	0.408 1.24+0	0.363 1.26+0
3.3 ev	$\frac{\gamma}{\delta}$	1.14-1	1.42-1	1.97 – 1	2.49-1	2.97-1	3.43-1	3.85-1	4.24-1	4.59-1	4.92-1
5s _{1/2}	σ	2.891+0	1.764+0	8.514-1	4.975-1	3.248-1	2.278-1	1.681-1	1.287-1	1.014-1	8.171-2
$E_b = 36.0 \text{ eV}$	β	1.959 1.74-1	1.962 7.75-2	1.967 -5.39-2	1.972 -1.15-1	1.976 1.29 1	1.979 -1.10-1	1.981 -6.91-2	1.982 -1.22-2	1.982 5.58-2	1.981 1.31-1
30.0 6	$\delta ^{\gamma }$	-3.68-4	-4.76-4	-6.23-4	-7.14-4	-7.84-4	-8.35-4	-8.79-4	-9.10-4	-9.41-4	-9.65-4
5 <i>p</i> _{1/2}	σ	2.865+0	1.754+0	8.194-1	4.559-1	2.822-1	1.878-1	1.315-1	9.584-2	7.200-2	5.546-2
$E_b =$	β	1.711	1.717	1.690	1.646	1.599	1.552	1.506	1.462	1.420	1.379
24.5 eV	$\frac{\gamma}{\delta}$	6.81-3 $-2.55-3$	-2.43-2 $-2.61-3$	5.59-2 -1.76-3	2.08 - 1 $7.54 - 4$	3.75-1 4.89-3	5.40-1 1.03-2	6.96 - 1 $1.66 - 2$	8.40-1 $2.35-2$	9.73-1 3.10-2	1.10+0 3.87-2
5p _{3/2}	σ	5.537+0	3.272+0	1.458+0	7.855-1	4.745-1	3.094-1	2.131-1	1.530-1	1.135-1	8.636-2
$E_b =$	β	1.717	1.743	1.742	1.714	1.678	1.638	1.598	1.558	1.518	1.479
20.1 eV	$\gamma \over \delta$	-1.72-2 $8.84-5$	-3.55-2 $1.82-3$	6.52-2 4.82-3	2.34-1 7.83-3	4.18-1 1.14-2	5.98-1 1.57-2	7.67-1 2.05-2	9.24-1 2.58-2	1.07+0 3.14-2	1.20+0 3.73-2
	σ	2.012-1	1.223-1	5.876-2	3.426-2	2.232-2	1.564-2	1.153-2	8.821-3	6.947-3	5.597-3
$E_b =$	β	1.959	1.962	1.967	1.972	1.976	1.979	1.981	1.982	1.982	1.981
5.0 eV	γ	1.71-1	7.47-2	-5.56-2	-1.17 - 1	-1.30-1	-1.10-1	-6.83-2	-1.13-2	5.62-2	1.31-1
	δ	-3.70-4	-4.77-4	-6.23-4	-7.20-4	-7.89-4	-8.37-4	-8.73-4	-9.09-4	-9.39-4	-9.60-4

Table 1 (continued)

Z= 62, Sm: [Xe]4f⁶_{5/2} 6s²_{1/2}

	· 3/2	1/2									
		k (eV)									
Shell		1500	2000	3000	4000	5000	6000	7000	8000	9000	10000
$3p_{3/2}$	σ	1.728+2	1.215+2	5.953+1	3.321+1	2.037+1	1.337+1	9.237+0	6.637+0	4.922+0	3.745+0
$E_b = 1419.8 \text{ eV}$	β	0.561 6.60-2	1.381 1.86-1	1.625 -4.22-2	1.670 5.03-2	1.667 2.26-1	1.646 4.19-1	1.617 6.07-1	1.584 7.82-1	1.549 9.44-1	1.514 1.09+0
1419.0 EV	$\gamma \\ \delta$	1.77-1	2.48-2	6.88-3	1.00-2	1.39-2	1.81-2	2.26-2	2.74-2	3.24-2	3.77-2
3d _{3/2}	σ	3.617+2	1.701+2	5.271+1	2.177+1	1.066+1	5.836+0	3.464+0	2.184+0	1.444+0	9.926-1
$E_b =$	β	0.812	1.115	1.238	1.213	1.154	1.087	1.020	0.957	0.898	0.843
1106.0 eV	γ	-1.46-1	-2.60-2	3.37 - 1	6.40 - 1	8.74 - 1	1.06+0	1.21+0	1.33+0	1.43+0	1.51+0
	δ	4.15 - 3	3.76-2	7.18 - 2	9.61 - 2	1.18 - 1	1.40 - 1	1.61 - 1	1.83 - 1	2.04 - 1	2.26 - 1
3d _{5/2}	σ	5.318+2	2.444+2	7.445+1	3.045+1	1.479+1	8.048+0	4.749+0	2.979+0	1.960+0	1.341+0
$E_b =$	β	0.890	1.144	1.220	1.174	1.106	1.035	0.967	0.905	0.849	0.797
1080.2 eV	$_{\delta}^{\gamma}$	-1.43-1 $4.17-3$	-3.43-3 $3.61-2$	3.67-1 7.15-2	6.60-1 $9.88-2$	8.83-1 1.24-1	1.06+0 1.49-1	1.19+0 1.73-1	1.31+0 1.96-1	1.40+0 2.19-1	1.48+0 2.42-1
10			1.139+1	5.611+0	3.316+0	2.180+0					5.571-1
$4s_{1/2} E_b =$	$\frac{\sigma}{\beta}$	1.830+1 1.953	1.139+1	1.962	1.968	2.180+0 1.973	1.537+0 1.976	1.138+0 1.978	8.737-1 1.980	6.899-1 1.980	1.980
345.7 eV	γ	2.75-1	1.54-1	-1.36-2	-9.99-2	-1.32-1	-1.26-1	-9.52-2	-4.63-2	1.53-2	8.58-2
	δ	-3.51 - 4	-4.88 - 4	-6.66 - 4	-7.78 - 4	-8.60 - 4	-9.21 - 4	-9.71 - 4	-1.01 - 3	-1.04 - 3	-1.07 - 3
4p _{1/2}	σ	2.185+1	1.368+1	6.536+0	3.682+0	2.297+0	1.537+0	1.081+0	7.901-1	5.952-1	4.595-1
$E_b =$	β	1.662	1.690	1.683	1.648	1.606	1.562	1.518	1.476	1.435	1.396
265.6 eV	γ	5.35-2	-1.62-2	2.65-2	1.65-1	3.28-1	4.92-1	6.48-1	7.94-1	9.29-1	1.05+0
	δ	-1.09-3	-2.09-3	-1.65-3	5.76-4	4.35-3	9.36-3	1.52-2	2.17-2	2.87-2	3.62-2
$4p_{3/2}$	σ_{ρ}	4.675+1 1.667	2.807+1 1.715	1.271+1 1.734	6.911+0 1.716	4.198+0 1.685	2.748+0 1.649	1.898+0 1.611	1.366+0 1.573	1.015+0 1.535	7.736-1 1.498
$E_b = 247.4 \text{ eV}$	β γ	1.66-2	-3.62-2	3.14-2	1.89-1	3.70-1	5.50-1	7.21-1	8.79-1	1.03+0	1.16+0
2	δ	6.99-4	1.89-3	5.06-3	8.13-3	1.16-2	1.55-2	1.99-2	2.47-2	2.99-2	3.54-2
4d _{3/2}	σ	4.735+1	2.384+1	8.172+0	3.585+0	1.829+0	1.033+0	6.278-1	4.035-1	2.709-1	1.885-1
$E_b =$	β	1.356	1.368	1.310	1.227	1.144	1.067	0.996	0.932	0.872	0.819
137.5 eV	γ	5.81-2	2.09-1	5.06-1	7.47 - 1	9.40-1	1.10+0	1.23+0	1.34+0	1.43+0	1.51+0
	δ	2.54-2	3.88-2	6.26-2	8.59-2	1.09-1	1.32-1	1.55-1	1.77-1	2.00-1	2.22-1
$4d_{5/2}$	σ	6.720+1	3.351+1 1.346	1.134+1 1.264	4.928+0	2.495+0	1.399+0	8.455-1 0.937	5.404-1	3.610-1	2.500-1
$E_b = 123.3 \text{ eV}$	$eta \ \gamma$	1.358 7.46-2	2.30-1	5.23-1	1.171 7.55-1	1.084 9.38-1	1.006 1.09+0	0.937 1.21+0	0.876 1.31+0	0.821 1.40+0	0.771 1.48+0
123.3 CV	δ	2.45-2	3.81-2	6.44-2	9.08-2	1.17-1	1.42-1	1.67-1	1.92-1	2.16-1	2.40-1
$4f_{5/2}$	σ	9.888+0	3.447+0	7.269-1	2.306-1	9.216-2	4.274-2	2.199-2	1.222-2	7.217-3	4.473-3
$E_b =$	β	1.044	0.970	0.832	0.725	0.643	0.576	0.518	0.466	0.419	0.374
5.5 eV	γ	4.75-1	6.16-1	8.05-1	9.28-1	1.02+0	1.10+0	1.16+0	1.21+0	1.25+0	1.28+0
	δ	1.12-1	1.40-1	1.94-1	2.45-1	2.93-1	3.37-1	3.79-1	4.18-1	4.54-1	4.87-1
$5s_{1/2} E_b =$	σ_{ρ}	2.975+0 1.956	1.821+0 1.959	8.822-1 1.965	5.166-1 1.970	3.376-1 1.974	2.370-1 1.977	1.750-1 1.979	1.341-1 1.980	1.057 – 1 1.980	8.527-2 1.980
37.4 eV	β γ	1.89-1	9.20-2	-4.39-2	-1.12-1	-1.31-1	-1.19-1	-8.30-2	-3.12-2	3.23-2	1.04-1
	δ	-3.93 - 4	-5.10-4	-6.70 - 4	-7.70 - 4	-8.47 - 4	-9.05 - 4	-9.53 - 4	-9.87 - 4	-1.02 - 3	-1.05 - 3
5p _{1/2}	σ	2.950+0	1.817+0	8.558-1	4.787-1	2.975-1	1.986-1	1.395-1	1.019-1	7.673-2	5.922-2
$E_b =$	β	1.708	1.718	1.694	1.653	1.608	1.562	1.518	1.475	1.433	1.393
23.6 eV	γ	1.60-2	-2.38-2	4.29-2	1.87-1	3.50-1	5.13-1	6.68-1	8.12-1	9.46-1	1.07+0
	δ	-2.66-3	-2.78-3	-2.11-3	1.18-4	3.93-3	9.01-3	1.50-2	2.17-2	2.89-2	3.64-2
$5p_{3/2}$	σ_{ρ}	5.683+0 1.712	3.374+0 1.742	1.513+0 1.745	8.183-1 1.721	4.958-1 1.687	3.241-1 1.650	2.238-1 1.611	1.610-1 1.572	1.196-1 1.534	9.118-2 1.496
$E_b = 18.9 \text{ eV}$	$eta \ \gamma$	-1.11-2	-3.74-2	5.05-2	2.12-1	3.92-1	5.70–1	7.39–1	8.97—1	1.04+0	1.490
10.0 01	δ	-7.66-5	1.66-3	4.69-3	7.59-3	1.10-2	1.50-2	1.96-2	2.46-2	3.00-2	3.57-2
6s _{1/2}	σ	2.028-1	1.236-1	5.964-2	3.484-2	2.273-2	1.594-2	1.176-2	9.005-3	7.096-3	5.721-3
$E_b =$	β	1.956	1.959	1.965	1.970	1.974	1.977	1.979	1.980	1.980	1.980
5.0 eV	γ	1.86-1	8.89-2	-4.57-2	-1.13-1	-1.33-1	-1.19-1	-8.26-2	-3.03-2	3.30-2	1.04-1
	δ	-3.95-4	-5.11-4	-6.69-4	-7.77-4	-8.54-4	-9.09-4	-9.50-4	-9.90-4	-1.02-3	-1.05-3
Z= 63, Eu: [X	[e]4f _{5/2}	4f _{7/2} 6s _{1/2}									
		k (eV)									
Shell		1500	2000	3000	4000	5000	6000	7000	8000	9000	10000
$3p_{3/2}$	σ	1.679+2	1.243+2	6.165+1	3.462+1	2.134+1	1.406+1	9.741+0	7.018+0	5.216+0	3.977+0
$E_b = 1480.6 \text{ eV}$	β	0.123	1.337	1.616	1.669	1.671	1.653	1.627	1.597	1.564	1.531
1480.6 eV	$_{\delta}^{\gamma}$	-2.67-1 $1.26-1$	2.23-1 3.16-2	-4.11-2 $7.02-3$	3.05-2 9.79-3	1.98-1 1.37-2	3.86-1 1.77-2	5.71-1 2.20-2	7.46-1 $2.66-2$	9.09-1 3.16-2	1.06+0 3.69-2
3d		3.788+2	1.811+2	5.676+1	2.359+1	1.161+1	6.386+0	3.804+0	2.406+0	1.595+0	1.098+0
$3d_{3/2}$ $E_b =$	$\frac{\sigma}{\beta}$	3.788+2 0.747	1.811+2	1.236	2.359+1 1.220	1.161+1	6.386+0 1.102	3.804+0 1.038	2.406+0 0.976	0.917	0.861
1160.6 eV	γ	-1.50-1	-5.40-2	3.03-1	6.06-1	8.49-1	1.04+0	1.19+0	1.32+0	1.42+0	1.51+0
	δ	-1.76 - 3	3.41-2	6.98 - 2	9.31-2	1.15-1	1.37 - 1	1.59 - 1	1.80 - 1	2.01 - 1	2.22 - 1
3d _{5/2}	σ	5.594+2	2.601+2	8.008+1	3.295+1	1.609+1	8.792+0	5.206+0	3.275+0	2.161+0	1.481+0
$E_b =$	β	0.838	1.124	1.220	1.182	1.117	1.049	0.983	0.922	0.865	0.812

(continued on next page)

able 1 (contin	ued)										
1130.9 eV	γ	-1.50-1	-3.17-2	3.36 - 1	6.30 - 1	8.61 - 1	1.04+0	1.18+0	1.30+0	1.40+0	1.48+0
	δ	-1.12-3	3.27-2	6.93-2	9.53-2	1.21-1	1.46-1	1.70-1	1.94 - 1	2.17 - 1	2.39-1
$4s_{1/2}$	σ	1.885+1	1.179+1	5.836+0	3.461+0	2.280+0	1.609+0	1.193+0	9.168 - 1	7.247 - 1	5.857 - 1
$E_b =$	β	1.949	1.953	1.960	1.965	1.970	1.974	1.977	1.978	1.979	1.979
360.2 eV	γ	2.91-1	1.70-1	-1.15-3	-9.40-2	-1.31-1	-1.31-1	-1.06-1	-6.21-2	-5.61-3	6.03-2
	δ	-3.69-4	-5.19-4	-7.11-4	-8.42-4	-9.26-4	-9.90-4	-1.04-3	-1.09-3	-1.12-3	-1.16-3
$4p_{1/2}$	σ	2.261+1	1.424+1	6.866+0	3.892+0	2.439+0	1.637+0	1.155+0	8.467 - 1	6.394 - 1	4.947 - 1
$E_b =$	β	1.654	1.688	1.685	1.653	1.613	1.571	1.530	1.489	1.449	1.411
283.9 eV	γ	6.77-2	-1.12-2	1.65-2	1.46-1	3.03-1	4.64-1	6.18-1	7.64-1	9.01-1	1.03+0
	δ	-9.52-4	-2.15-3	-1.92-3	-1.19-5	3.51-3	8.24-3	1.39-2	2.03-2	2.73-2	3.47-2
$4p_{3/2}$	σ	4.856+1	2.931+1	1.337+1	7.306+0	4.453+0	2.923+0	2.025+0	1.460+0	1.087+0	8.306 - 1
$E_b =$	β	1.659	1.711	1.735	1.721	1.693	1.660	1.624	1.588	1.552	1.516
256.6 eV	$\gamma \\ \delta$	2.50-2	-3.46-2	1.99-2	1.70-1	3.45-1	5.21-1	6.91-1	8.51-1	9.99-1	1.14+0
		7.22-4	1.80-3	4.94-3	7.96-3	1.13-2	1.50-2	1.92-2	2.40-2	2.92-2	3.47-2
$4d_{3/2}$	σ	5.033+1	2.561+1	8.892+0	3.934+0	2.020+0	1.147+0	6.998-1	4.514-1	3.040-1	2.121-1
$E_b =$	β	1.354	1.370	1.319 4.82-1	1.240 7.29-1	1.160	1.085	1.015	0.950	0.890	0.835
141.4 eV	$\gamma \\ \delta$	4.61-2 2.42-2	1.92-1 3.75-2	6.02 - 2	8.30-2	9.26-1 1.06-1	1.09+0 1.29-1	1.22+0 1.52-1	1.33+0 1.74-1	1.43+0 1.96-1	1.51+0 2.17-1
$4d_{5/2}$	σ	7.130+1	3.592+1	1.230+1	5.391+0	2.745+0	1.548+0	9.388-1	6.021-1	4.034-1	2.801-1
$E_b =$	β	1.357 6.20-2	1.350	1.273	1.182	1.098	1.023	0.954	0.892	0.836	0.784 1.48+0
127.7 eV	$\gamma \\ \delta$	6.20—2 2.32—2	2.13-1 3.67-2	5.01-1 6.17-2	7.38-1 8.79-2	9.25-1 1.14-1	1.08+0 1.40-1	1.20+0 1.65-1	1.31+0 1.89-1	1.40+0 2.13-1	1.48+0 2.36-1
A.C.											
$4f_{5/2}$	σ_{ρ}	1.229+1 1.048	4.352+0 0.979	9.326-1 0.846	2.985-1 0.736	1.201-1 0.653	5.604-2 0.585	2.898-2 0.526	1.618-2 0.473	9.591-3 0.425	5.966-3 0.380
$E_b = 1.5 \text{ eV}$	β γ	1.048 4.62-1	0.979 6.07-1	0.846 8.03-1	0.736 9.29—1	0.653 1.02+0	0.585 1.10+0	0.526 1.16+0	0.473 1.21+0	0.425 1.25+0	0.380 1.28+0
1.5 ()	δ	1.10-1	1.38-1	1.91-1	2.41-1	2.88-1	3.32-1	3.73-1	4.11-1	4.46-1	4.79-1
4f _{7/2}	σ	7.493-3	2.600-3	5.443-4	1.718-4	6.852-5	3.171–5	1.630-5	9.053-6	5.349-6	3.316-6
$E_b =$	β	1.040	0.973	0.841	0.740	0.659	0.594	0.537	0.491	0.442	0.402
1.2 eV	γ	4.67-1	6.13-1	8.10-1	9.40-1	1.03+0	1.10+0	1.16+0	1.21+0	1.25+0	1.28+0
1.2 CV	δ	1.12-1	1.39-1	1.94-1	2.44-1	2.93-1	3.38-1	3.79-1	4.15-1	4.50-1	4.88-1
5s _{1/2}	σ	3.246+0	1.994+0	9.709-1	5.703-1	3.733-1	2.624-1	1.939-1	1.488-1	1.174-1	9.475-2
55 _{1/2} F _b =	β	1.954	1.956	1.962	1.967	1.972	1.975	1.977	1.979	1.979	1.979
$E_b = 31.8 \text{ eV}$	γ	1.96-1	1.02-1	-3.57-2	-1.08-1	-1.32-1	-1.25-1	-9.40-2	-4.71-2	1.15-2	7.87-2
	δ	-4.18 - 4	-5.44 - 4	-7.22 - 4	-8.33 - 4	-9.13 - 4	-9.75 - 4	-1.03 - 3	-1.07 - 3	-1.10 - 3	-1.14 - 3
5p _{1/2}	σ	3.297+0	2.042+0	9.698-1	5.456-1	3.404-1	2.279-1	1.606-1	1.176-1	8.875-2	6.865-2
$E_b =$	β	1.707	1.718	1.698	1.659	1.616	1.572	1.529	1.487	1.447	1.408
25.2 eV	γ	2.41-2	-2.21-2	3.27-2	1.69-1	3.27-1	4.86-1	6.38-1	7.82-1	9.16-1	1.04+0
	δ	-2.72 - 3	-2.90 - 3	-2.44 - 3	-4.60 - 4	3.02 - 3	7.67 - 3	1.33 - 2	1.97 - 2	2.65 - 2	3.39 - 2
5p _{3/2}	σ	6.482+0	3.865+0	1.744+0	9.477-1	5.759-1	3.774-1	2.612-1	1.883-1	1.401-1	1.070-1
$E_b =$	β	1.709	1.741	1.748	1.727	1.696	1.660	1.623	1.586	1.549	1.513
20.4 eV	γ	-5.47 - 3	-3.79 - 2	3.85 - 2	1.94 - 1	3.68 - 1	5.42 - 1	7.10 - 1	8.66 - 1	1.01+0	1.15+0
	δ	-1.84 - 4	1.54 - 3	4.59 - 3	7.43 - 3	1.06 - 2	1.42 - 2	1.84 - 2	2.30-2	2.80 - 2	3.35 - 2
6s _{1/2}	σ	3.573-1	2.182-1	1.056-1	6.183-2	4.039-2	2.836-2	2.094-2	1.604-2	1.265-2	1.021-2
$E_b =$	β	1.953	1.956	1.962	1.967	1.971	1.975	1.977	1.978	1.979	1.979
6.0 eV	γ	1.96 - 1	1.01 - 1	-3.71-2	-1.10-1	-1.34-1	-1.26-1	-9.48 - 2	-4.73 - 2	1.20 - 2	8.00 - 2
	δ	-4.20-4	-5.49 - 4	-7.22 - 4	-8.39 - 4	-9.20 - 4	-9.82 - 4	-1.03 - 3	-1.07 - 3	-1.11-3	-1.14 - 3
Z= 64, Gd: [X	e 4f _{5/2}	$4f_{7/2}^1 \ 5d_{3/2}^1 \ 6s_{1/2}^2$									
	-/-	k (eV)									
Shell		1500	2000	3000	4000	5000	6000	7000	8000	9000	10000
$3d_{3/2}$	σ_{ρ}	4.036+2 0.652	1.965+2 1.053	6.200+1 1.231	2.588+1 1.227	1.277+1 1.178	7.043+0 1.117	4.205+0 1.054	2.665+0 0.993	1.770+0 0.935	1.221+0 0.881
$E_b = 1217.2 \text{ eV}$	β	-1.45-1	-8.77-2	2.62-1	5.76-1	8.23-1	1.02+0	1.034	1.31+0	1.42+0	1.51+0
1217.2 CV	$\gamma \\ \delta$	-8.74-3	2.91-2	6.73-2	9.16-2	1.13-1	1.34-1	1.54-1	1.75-1	1.95-1	2.16-1
2.4											
3d _{5/2}	σ_{β}	5.990+2 0.754	2.822+2 1.098	8.734+1 1.220	3.608+1 1.190	1.767+1 1.129	9.674+0 1.061	5.740+0 0.996	3.618+0 0.935	2.391+0 0.880	1.642+0 0.828
$E_b = 1185.2 \text{ eV}$	β	0.754 -1.51-1	-6.66-2	1.220 2.97—1	6.03-1	8.38-1	1.061	0.996 1.17+0	0.935 1.29+0	0.880 1.39+0	0.828 1.48+0
. 103.2 CV	$\gamma \\ \delta$	-7.63-3	2.79-2	6.65-2	9.35-2	1.18-1	1.42-1	1.65-1	1.88-1	2.11-1	2.33-1
1c	σ	1.944+1	1.221+1	6.072+0	3.607+0	2.380+0	1.682+0	1.248+0	9.596-1	7.590-1	6.138-1
$4s_{1/2} E_b =$	β	1.944+1	1.221+1	1.956	1.962	2.380+0 1.967	1.082+0	1.248+0	9.596—1 1.976	7.590—1 1.977	1.977
375.8 eV	γ	3.13-1	1.92-1	1.45-2	-8.52-2	-1.30-1	-1.37 - 1	-1.18-1	-7.91-2	-2.68-2	3.52-2
= = •	δ	-3.77-4	-5.46-4	-7.65-4	-9.04-4	-1.00-3	-1.08 - 3	-1.14-3	-1.19-3	-1.23-3	-1.26 - 3
4p _{1/2}	σ	2.325+1	1.476+1	7.182+0	4.093+0	2.576+0	1.735+0	1.227+0	9.017-1	6.824-1	5.291-1
$E_b =$	β	1.648	1.685	1.687	1.658	1.620	1.580	1.539	1.498	1.460	1.422
288.5 eV	γ	8.49-2	-4.18-3	6.97-3	1.26-1	2.79-1	4.38-1	5.91-1	7.36-1	8.71-1	9.97-1
· · · · · · ·	δ	-7.33-4	-2.22 - 3	-2.23-3	-5.30-4	2.62-3	6.96-3	1.22-2	1.81-2	2.46-2	3.15-2
4p _{3/2}	σ	5.061+1	3.070+1	1.409+1	7.725+0	4.722+0	3.107+0	2.156+0	1.557+0	1.161+0	8.883-1
$E_b =$	β	1.649	1.706	1.409+1	7.725+0 1.726	4.722+0 1.701	1.669	1.635	1.557+0	1.161+0	8.883—1 1.529
270.9 eV	γ	4.01-2	-3.11-2	6.77-3	1.48-1	3.19-1	4.94-1	6.63-1	8.22-1	9.70-1	1.11+0
	δ	7.60-4	1.62-3	4.82-3	7.79-3	1.09-2	1.44-2	1.83-2	2.26-2	2.72-2	3.22-2
			-	-							=

Tab	nle 1	l (c	nnt	inı	ed)

	,										
4d _{3/2}	σ	5.391+1	2.766+1	9.699+0	4.315+0	2.224+0	1.267+0	7.756-1	5.016-1	3.387-1	2.368-1
$E_b =$	β	1.347	1.371	1.329	1.254	1.175	1.100	1.032	0.969	0.910	0.856
149.5 eV	γ	2.93-2	1.68 - 1	4.61 - 1	7.09 - 1	9.09 - 1	1.07+0	1.21+0	1.33+0	1.43+0	1.51+0
	δ	2.26-2	3.58-2	5.88-2	8.08-2	1.03-1	1.25-1	1.46-1	1.68-1	1.90-1	2.11-1
$4d_{5/2}$	σ	7.630+1	3.874+1	1.340+1	5.901+0	3.017+0	1.706+0	1.038+0	6.675 - 1	4.483 - 1	3.119 - 1
$E_b =$	β	1.355	1.353	1.283	1.195	1.111	1.035	0.967	0.906	0.851	0.801
134.5 eV	γ	4.52-2	1.91-1	4.82-1	7.21-1	9.10-1	1.06+0	1.19+0	1.30+0	1.40+0	1.48+0
	δ	2.17-2	3.49-2	6.01-2	8.53-2	1.10-1	1.35-1	1.59-1	1.83-1	2.07-1	2.30-1
$4f_{5/2}$	σ	1.435+1	5.105+0	1.100+0	3.531-1	1.426-1	6.671-2	3.461-2	1.938-2	1.152-2	7.185-3
$E_b = 2.0 \text{ eV}$	β	1.053 4.48-1	0.989	0.856	0.749 9.31-1	0.666	0.598	0.540 1.17+0	0.487	0.439	0.393 1.30+0
2.0 eV	δ	4.48 – 1 1.08 – 1	5.96-1 1.35-1	7.99-1 1.87-1	2.37-1	1.03+0 2.84-1	1.11+0 3.28-1	3.69-1	1.22+0 4.07-1	1.26+0 4.42-1	4.75-1
46									2.368-2		
$\begin{array}{l} 4f_{7/2} \\ E_b = \end{array}$	$\frac{\sigma}{eta}$	1.829+1 1.044	6.453+0 0.979	1.376+0 0.849	4.387-1 0.746	1.761-1 0.667	8.205-2 0.604	4.241-2 0.549	2.368-2 0.500	1.404-2 0.456	8.733-3 0.414
1.3 eV	γ	4.52-1	6.01-1	8.06-1	9.37-1	1.03+0	1.11+0	1.17+0	1.22+0	1.26+0	1.29+0
-1.0	δ	1.08-1	1.35-1	1.89-1	2.39-1	2.87-1	3.32-1	3.73-1	4.11-1	4.47-1	4.80-1
5s _{1/2}	σ	3.296+0	2.030+0	9.915-1	5.833-1	3.823-1	2.690-1	1.989-1	1.527-1	1.205-1	9.735-2
$E_b =$	β	1.950	1.953	1.959	1.964	1.969	1.972	1.975	1.976	1.977	1.977
36.1 eV	γ	2.16-1	1.19-1	-2.34-2	-1.02-1	-1.34-1	-1.33-1	-1.07 - 1	-6.49 - 2	-1.01-2	5.37-2
	δ	-4.37 - 4	-5.78 - 4	-7.73 - 4	-8.97 - 4	-9.93 - 4	-1.06 - 3	-1.12 - 3	-1.17 - 3	-1.21-3	-1.24 - 3
5p _{1/2}	σ	3.268+0	2.037+0	9.749-1	5.512-1	3.453-1	2.319-1	1.638-1	1.202-1	9.092-2	7.046-2
$E_b =$	β	1.702	1.717	1.702	1.665	1.624	1.581	1.538	1.497	1.457	1.419
24.3 eV	γ	3.66 - 2	-1.91-2	2.11-2	1.49 - 1	3.04 - 1	4.61 - 1	6.14 - 1	7.57 - 1	8.91 - 1	1.02+0
	δ	-2.86-3	-3.09-3	-2.74-3	-1.03-3	2.15-3	6.58-3	1.19-2	1.80-2	2.45-2	3.15-2
$5p_{3/2}$	σ	6.527+0	3.907+0	1.774+0	9.673 - 1	5.896 - 1	3.873 - 1	2.685 - 1	1.939 - 1	1.446 - 1	1.106 - 1
$E_b =$	β	1.702	1.738	1.751	1.733	1.704	1.670	1.635	1.598	1.562	1.526
18.3 eV	γ	2.85-3	-3.81-2	2.50-2	1.72-1	3.44-1	5.18-1	6.85-1	8.43-1	9.89-1	1.12+0
	δ	-3.81-4	1.35-3	4.48-3	7.27-3	1.03-2	1.39-2	1.79-2	2.22-2	2.70-2	3.21-2
$5d_{3/2}$	σ	2.780+0	1.430+0	5.033-1	2.244-1	1.159-1	6.610-2	4.052-2	2.623-2	1.773-2	1.240-2
$E_b = 6.0 \text{ eV}$	β	1.386 4.92-2	1.393 1.88-1	1.338 4.76-1	1.258 7.21-1	1.178 9.21-1	1.102 1.08+0	1.031 1.22+0	0.966 1.33+0	0.905 1.43+0	0.849 1.51+0
0.0 6 V	δ	2.21-2	3.46-2	5.70-2	7.21-1 $7.92-2$	1.02-1	1.25-1	1.47-1	1.69-1	1.45+0	2.11-1
C-											
6s _{1/2}	$\frac{\sigma}{eta}$	2.444-1 1.950	1.497 – 1 1.953	7.273-2 1.958	4.266-2 1.964	2.790-2 1.968	1.960-2 1.972	1.448-2 1.975	1.110-2 1.977	8.763-3 1.977	7.074-3 1.978
$E_b = 6.0 \text{ eV}$	γ	2.14-1	1.17-1	-2.52-2	-1.04-1	-1.36-1	-1.33-1	-1.07 - 1	-6.40-2	-9.46-3	5.40-2
0.0 0.	δ	-4.40-4	-5.83-4	-7.75-4	-9.05-4	-9.99-4	-1.06-3	-1.12-3	-1.16-3	-1.20-3	-1.23-3
Z= 65, Tb: [X	el4f ⁶ 4	1f ³ 6s ²									
	-1-5/2	k (eV)									
a			2222		1000	=000	2222				10000
Shell		1500	2000	3000	4000	5000	6000	7000	8000	9000	10000
$3d_{3/2}$	σ	4.281+2	2.132+2	6.773+1	2.838+1	1.405+1	7.765+0	4.645+0	2.950+0	1.963+0	1.356+0
$E_b =$	β	0.550	1.009	1.225	1.232	1.190	1.132	1.071	1.010	0.952	0.897
1275.0 eV	$\gamma \delta$	-1.26-1 $-1.28-2$	-1.18-1 2.37-2	2.21-1 6.51-2	5.40-1 8.98-2	7.95-1 1.11-1	9.98-1 1.32-1	1.16+0 1.52-1	1.30+0 1.72-1	1.41+0 1.91-1	1.50+0 2.10-1
2.1											
$3d_{5/2}$ $E_b =$	$\frac{\sigma}{eta}$	6.371+2 0.666	3.058+2 1.064	9.521+1 1.218	3.947+1 1.197	1.937+1 1.141	1.064+1 1.077	6.325+0 1.012	3.994+0 0.951	2.643+0 0.894	1.817+0 0.841
1241.2 eV	γ	-1.38 - 1	-9.86-2	2.59-1	5.71-1	8.14-1	1.00+0	1.16+0	1.28+0	1.39+0	1.47+0
12 11.2 CV	δ	-1.21-2	2.30-2	6.40-2	9.12-2	1.16-1	1.40-1	1.63-1	1.85-1	2.07-1	2.28-1
4s _{1/2}	σ	1.998+1	1.260+1	6.291+0	3.745+0	2.473+0	1.750+0	1.299+0	1.000+0	7.915-1	6.405-1
$E_b =$	β	1.941	1.945	1.952	1.959	1.964	1.968	1.972	1.974	1.975	1.976
397.9 eV	γ	3.41 - 1	2.17 - 1	3.27-2	-7.43 - 2	-1.26-1	-1.40-1	-1.27 - 1	-9.44 - 2	-4.72 - 2	1.05 - 2
	δ	-3.70 - 4	-5.65 - 4	-8.09 - 4	-9.64 - 4	-1.07 - 3	-1.16 - 3	-1.23 - 3	-1.28 - 3	-1.33 - 3	-1.37 - 3
$4p_{1/2}$	σ	2.386+1	1.527+1	7.493+0	4.292+0	2.711+0	1.831+0	1.299+0	9.566-1	7.255-1	5.634-1
$E_b =$	β	1 620	1 CO1	4 000				1.550	1.510	1.472	1.434
310.2 eV	Ρ	1.638	1.681	1.689	1.664	1.628	1.589	1.550			
	γ	1.10 - 1	6.63 - 3	-2.59 - 3	1.05 - 1	2.52 - 1	4.08 - 1	5.61 - 1	7.07 - 1	8.43 - 1	9.70 - 1
		1.10-1 -3.84-4	6.63-3 -2.28-3	-2.59-3 -2.51-3	1.05-1 -1.07-3	2.52-1 1.81-3	4.08-1 5.94-3	5.61-1 1.10-2	7.07-1 1.68-2	8.43-1 2.31-2	9.70-1 2.97-2
4p _{3/2}	γ δ	1.10-1 -3.84-4 5.235+1	6.63-3 -2.28-3 3.192+1	-2.59-3 -2.51-3 1.474+1	1.05-1 -1.07-3 8.109+0	2.52-1 1.81-3 4.970+0	4.08-1 5.94-3 3.278+0	5.61-1 1.10-2 2.279+0	7.07-1 1.68-2 1.649+0	8.43-1 2.31-2 1.232+0	9.70-1 2.97-2 9.437-1
$E_b =$	$\frac{\gamma}{\delta}$ $\frac{\sigma}{\beta}$	1.10-1 -3.84-4 5.235+1 1.637	6.63-3 -2.28-3 3.192+1 1.700	-2.59-3 -2.51-3 1.474+1 1.737	1.05-1 -1.07-3 8.109+0 1.731	2.52-1 1.81-3 4.970+0 1.709	4.08-1 5.94-3 3.278+0 1.679	5.61-1 1.10-2 2.279+0 1.647	7.07-1 1.68-2 1.649+0 1.613	8.43-1 2.31-2 1.232+0 1.578	9.70-1 2.97-2 9.437-1 1.544
	γ δ σ β γ	1.10-1 -3.84-4 5.235+1 1.637 5.70-2	6.63-3 -2.28-3 3.192+1 1.700 -2.57-2	-2.59-3 -2.51-3 1.474+1 1.737 -5.29-3	1.05-1 -1.07-3 8.109+0 1.731 1.25-1	2.52-1 1.81-3 4.970+0 1.709 2.91-1	4.08-1 5.94-3 3.278+0 1.679 4.64-1	5.61-1 1.10-2 2.279+0 1.647 6.33-1	7.07-1 1.68-2 1.649+0 1.613 7.94-1	8.43-1 2.31-2 1.232+0 1.578 9.43-1	9.70-1 2.97-2 9.437-1 1.544 1.08+0
$E_b = 285.0 \text{ eV}$	γ δ σ β γ δ	1.10-1 -3.84-4 5.235+1 1.637 5.70-2 8.52-4	6.63-3 -2.28-3 3.192+1 1.700 -2.57-2 1.43-3	-2.59-3 -2.51-3 1.474+1 1.737 -5.29-3 4.64-3	1.05-1 -1.07-3 8.109+0 1.731 1.25-1 7.61-3	2.52-1 1.81-3 4.970+0 1.709 2.91-1 1.06-2	4.08-1 5.94-3 3.278+0 1.679 4.64-1 1.41-2	5.61-1 1.10-2 2.279+0 1.647 6.33-1 1.79-2	7.07-1 1.68-2 1.649+0 1.613 7.94-1 2.21-2	8.43-1 2.31-2 1.232+0 1.578 9.43-1 2.66-2	9.70-1 2.97-2 9.437-1 1.544 1.08+0 3.12-2
$E_b = 285.0 \text{ eV}$	γ δ σ β γ δ	1.10-1 -3.84-4 5.235+1 1.637 5.70-2 8.52-4 5.674+1	6.63-3 -2.28-3 3.192+1 1.700 -2.57-2 1.43-3 2.938+1	-2.59-3 -2.51-3 1.474+1 1.737 -5.29-3 4.64-3 1.040+1	1.05-1 -1.07-3 8.109+0 1.731 1.25-1 7.61-3 4.657+0	2.52-1 1.81-3 4.970+0 1.709 2.91-1 1.06-2 2.411+0	4.08-1 5.94-3 3.278+0 1.679 4.64-1 1.41-2 1.378+0	5.61-1 1.10-2 2.279+0 1.647 6.33-1 1.79-2 8.463-1	7.07-1 1.68-2 1.649+0 1.613 7.94-1 2.21-2 5.487-1	8.43-1 2.31-2 1.232+0 1.578 9.43-1 2.66-2 3.713-1	9.70-1 2.97-2 9.437-1 1.544 1.08+0 3.12-2 2.602-1
$E_b = 285.0 \text{ eV}$ $4d_{3/2}$ $E_b = $	γ δ σ β γ δ σ β	1.10-1 -3.84-4 5.235+1 1.637 5.70-2 8.52-4 5.674+1 1.339	6.63-3 -2.28-3 3.192+1 1.700 -2.57-2 1.43-3 2.938+1 1.371	-2.59-3 -2.51-3 1.474+1 1.737 -5.29-3 4.64-3 1.040+1 1.338	1.05-1 -1.07-3 8.109+0 1.731 1.25-1 7.61-3 4.657+0 1.268	2.52-1 1.81-3 4.970+0 1.709 2.91-1 1.06-2 2.411+0 1.192	4.08-1 5.94-3 3.278+0 1.679 4.64-1 1.41-2 1.378+0 1.118	5.61-1 1.10-2 2.279+0 1.647 6.33-1 1.79-2 8.463-1 1.049	7.07-1 1.68-2 1.649+0 1.613 7.94-1 2.21-2 5.487-1 0.985	8.43-1 2.31-2 1.232+0 1.578 9.43-1 2.66-2 3.713-1 0.925	9.70-1 2.97-2 9.437-1 1.544 1.08+0 3.12-2 2.602-1 0.871
$E_b = 285.0 \text{ eV}$	γ δ σ β γ δ σ β γ	1.10-1 -3.84-4 5.235+1 1.637 5.70-2 8.52-4 5.674+1 1.339 1.41-2	6.63-3 -2.28-3 3.192+1 1.700 -2.57-2 1.43-3 2.938+1 1.371 1.46-1	-2.59-3 -2.51-3 1.474+1 1.737 -5.29-3 4.64-3 1.040+1 1.338 4.36-1	1.05-1 -1.07-3 8.109+0 1.731 1.25-1 7.61-3 4.657+0 1.268 6.88-1	2.52-1 1.81-3 4.970+0 1.709 2.91-1 1.06-2 2.411+0 1.192 8.94-1	4.08-1 5.94-3 3.278+0 1.679 4.64-1 1.41-2 1.378+0 1.118 1.06+0	5.61-1 1.10-2 2.279+0 1.647 6.33-1 1.79-2 8.463-1 1.049 1.20+0	7.07-1 1.68-2 1.649+0 1.613 7.94-1 2.21-2 5.487-1 0.985 1.32+0	8.43-1 2.31-2 1.232+0 1.578 9.43-1 2.66-2 3.713-1 0.925 1.42+0	9.70-1 2.97-2 9.437-1 1.544 1.08+0 3.12-2 2.602-1 0.871 1.51+0
$E_b = 285.0 \text{ eV}$ $4d_{3/2}$ $E_b = 154.5 \text{ eV}$	γ δ σ β γ δ σ β γ δ	1.10-1 -3.84-4 5.235+1 1.637 5.70-2 8.52-4 5.674+1 1.339 1.41-2 2.09-2	6.63-3 -2.28-3 3.192+1 1.700 -2.57-2 1.43-3 2.938+1 1.371 1.46-1 3.43-2	-2.59-3 -2.51-3 1.474+1 1.737 -5.29-3 4.64-3 1.040+1 1.338 4.36-1 5.71-2	1.05-1 -1.07-3 8.109+0 1.731 1.25-1 7.61-3 4.657+0 1.268 6.88-1 7.89-2	2.52-1 1.81-3 4.970+0 1.709 2.91-1 1.06-2 2.411+0 1.192 8.94-1 1.01-1	4.08-1 5.94-3 3.278+0 1.679 4.64-1 1.41-2 1.378+0 1.118 1.06+0 1.22-1	5.61-1 1.10-2 2.279+0 1.647 6.33-1 1.79-2 8.463-1 1.049 1.20+0 1.43-1	7.07-1 1.68-2 1.649+0 1.613 7.94-1 2.21-2 5.487-1 0.985 1.32+0 1.64-1	8.43-1 2.31-2 1.232+0 1.578 9.43-1 2.66-2 3.713-1 0.925 1.42+0 1.85-1	9.70-1 2.97-2 9.437-1 1.544 1.08+0 3.12-2 2.602-1 0.871 1.51+0 2.05-1
$E_b =$ 285.0 eV $4d_{3/2}$ $E_b =$ 154.5 eV	γ δ σ β γ δ σ β γ δ	1.10-1 -3.84-4 5.235+1 1.637 5.70-2 8.52-4 5.674+1 1.339 1.41-2 2.09-2 8.072+1	6.63-3 -2.28-3 3.192+1 1.700 -2.57-2 1.43-3 2.938+1 1.371 1.46-1 3.43-2 4.133+1	-2.59-3 -2.51-3 1.474+1 1.737 -5.29-3 4.64-3 1.040+1 1.338 4.36-1 5.71-2 1.443+1	1.05-1 -1.07-3 8.109+0 1.731 1.25-1 7.61-3 4.657+0 1.268 6.88-1 7.89-2 6.389+0	2.52-1 1.81-3 4.970+0 1.709 2.91-1 1.06-2 2.411+0 1.192 8.94-1 1.01-1 3.281+0	4.08-1 5.94-3 3.278+0 1.679 4.64-1 1.41-2 1.378+0 1.118 1.06+0 1.22-1 1.861+0	5.61-1 1.10-2 2.279+0 1.647 6.33-1 1.79-2 8.463-1 1.049 1.20+0 1.43-1 1.135+0	7.07-1 1.68-2 1.649+0 1.613 7.94-1 2.21-2 5.487-1 0.985 1.32+0 1.64-1 7.319-1	8.43-1 2.31-2 1.232+0 1.578 9.43-1 2.66-2 3.713-1 0.925 1.42+0 1.85-1 4.926-1	9.70-1 2.97-2 9.437-1 1.544 1.08+0 3.12-2 2.602-1 0.871 1.51+0 2.05-1 3.434-1
$E_b = 285.0 \text{ eV}$ $4d_{3/2}$ $E_b = 154.5 \text{ eV}$ $4d_{5/2}$ $E_b = 6$	γ δ σ β γ δ σ β γ δ σ β γ δ	1.10-1 -3.84-4 5.235+1 1.637 5.70-2 8.52-4 5.674+1 1.339 1.41-2 2.09-2 8.072+1 1.351	6.63-3 -2.28-3 3.192+1 1.700 -2.57-2 1.43-3 2.938+1 1.371 1.46-1 3.43-2 4.133+1 1.356	-2.59-3 -2.51-3 1.474+1 1.737 -5.29-3 4.64-3 1.040+1 1.338 4.36-1 5.71-2 1.443+1 1.293	1.05-1 -1.07-3 8.109+0 1.731 1.25-1 7.61-3 4.657+0 1.268 6.88-1 7.89-2 6.389+0 1.209	2.52-1 1.81-3 4.970+0 1.709 2.91-1 1.06-2 2.411+0 1.192 8.94-1 1.01-1 3.281+0 1.127	4.08-1 5.94-3 3.278+0 1.679 4.64-1 1.41-2 1.378+0 1.118 1.06+0 1.22-1 1.861+0 1.051	5.61-1 1.10-2 2.279+0 1.647 6.33-1 1.79-2 8.463-1 1.049 1.20+0 1.43-1 1.135+0 0.982	7.07-1 1.68-2 1.649+0 1.613 7.94-1 2.21-2 5.487-1 0.985 1.32+0 1.64-1 7.319-1 0.919	8.43-1 2.31-2 1.232+0 1.578 9.43-1 2.66-2 3.713-1 0.925 1.42+0 1.85-1 4.926-1 0.863	9.70-1 2.97-2 9.437-1 1.544 1.08+0 3.12-2 2.602-1 0.871 1.51+0 2.05-1 3.434-1 0.812
$E_b = 285.0 \text{ eV}$ $4d_{3/2}$ $E_b = 154.5 \text{ eV}$	γ δ σ β γ δ σ β γ δ	1.10-1 -3.84-4 5.235+1 1.637 5.70-2 8.52-4 5.674+1 1.339 1.41-2 2.09-2 8.072+1	6.63-3 -2.28-3 3.192+1 1.700 -2.57-2 1.43-3 2.938+1 1.371 1.46-1 3.43-2 4.133+1	-2.59-3 -2.51-3 1.474+1 1.737 -5.29-3 4.64-3 1.040+1 1.338 4.36-1 5.71-2 1.443+1	1.05-1 -1.07-3 8.109+0 1.731 1.25-1 7.61-3 4.657+0 1.268 6.88-1 7.89-2 6.389+0	2.52-1 1.81-3 4.970+0 1.709 2.91-1 1.06-2 2.411+0 1.192 8.94-1 1.01-1 3.281+0	4.08-1 5.94-3 3.278+0 1.679 4.64-1 1.41-2 1.378+0 1.118 1.06+0 1.22-1 1.861+0	5.61-1 1.10-2 2.279+0 1.647 6.33-1 1.79-2 8.463-1 1.049 1.20+0 1.43-1 1.135+0	7.07-1 1.68-2 1.649+0 1.613 7.94-1 2.21-2 5.487-1 0.985 1.32+0 1.64-1 7.319-1	8.43-1 2.31-2 1.232+0 1.578 9.43-1 2.66-2 3.713-1 0.925 1.42+0 1.85-1 4.926-1	9.70-1 2.97-2 9.437-1 1.544 1.08+0 3.12-2 2.602-1 0.871 1.51+0 2.05-1 3.434-1
$E_b = 285.0 \text{ eV}$ $4d_{3/2}$ $E_b = 154.5 \text{ eV}$ $4d_{5/2}$ $E_b = 6$	γ δ σ β γ δ σ β γ δ σ β γ γ	1.10-1 -3.84-4 5.235+1 1.637 5.70-2 8.52-4 5.674+1 1.339 1.41-2 2.09-2 8.072+1 1.351 2.91-2	6.63-3 -2.28-3 3.192+1 1.700 -2.57-2 1.43-3 2.938+1 1.371 1.46-1 3.43-2 4.133+1 1.356 1.69-1	-2.59-3 -2.51-3 1.474+1 1.737 -5.29-3 4.64-3 1.040+1 1.338 4.36-1 5.71-2 1.443+1 1.293 4.59-1	1.05-1 -1.07-3 8.109+0 1.731 1.25-1 7.61-3 4.657+0 1.268 6.88-1 7.89-2 6.389+0 1.209 7.02-1	2.52-1 1.81-3 4.970+0 1.709 2.91-1 1.06-2 2.411+0 1.192 8.94-1 1.01-1 3.281+0 1.127 8.97-1	4.08-1 5.94-3 3.278+0 1.679 4.64-1 1.41-2 1.378+0 1.118 1.06+0 1.22-1 1.861+0 1.051 1.05+0	5.61-1 1.10-2 2.279+0 1.647 6.33-1 1.79-2 8.463-1 1.049 1.20+0 1.43-1 1.135+0 0.982 1.19+0	7.07-1 1.68-2 1.649+0 1.613 7.94-1 2.21-2 5.487-1 0.985 1.32+0 1.64-1 7.319-1 0.919 1.30+0	8.43-1 2.31-2 1.232+0 1.578 9.43-1 2.66-2 3.713-1 0.925 1.42+0 1.85-1 4.926-1 0.863 1.39+0	9.70-1 2.97-2 9.437-1 1.544 1.08+0 3.12-2 2.602-1 0.871 1.51+0 2.05-1 3.434-1 0.812 1.47+0

Table 1 (contin	ued)										
$E_b =$	β	1.056	0.997	0.870	0.763	0.677	0.607	0.547	0.495	0.448	0.403
4.0 eV	$\gamma \\ \delta$	4.33-1 1.07-1	5.86-1 1.34-1	7.97-1 1.86-1	9.34-1 2.34-1	1.03+0 2.80-1	1.11+0 3.22-1	1.17+0 3.63-1	1.23+0 4.01-1	1.27+0 4.36-1	1.31+0 4.70-1
4f _{7/2}	σ	1.964+1	6.972+0	1.495+0	4.781-1	1.924-1	8.986-2	4.657-2	2.607-2	1.550-2	9.663-3
$E_b = 1.6 \text{ eV}$	$eta \ \gamma$	1.047 4.39-1	0.988 5.92-1	0.862 8.04-1	0.759 9.40-1	0.678 1.04+0	0.612 1.11+0	0.556 1.17+0	0.507 1.22+0	0.464 1.27+0	0.423 1.30+0
	δ	1.06-1	1.34-1	1.87-1	2.37-1	2.83-1	3.26-1	3.67-1	4.05-1	4.41-1	4.75-1
$5s_{1/2}$ $E_b =$	$\frac{\sigma}{eta}$	3.221+0 1.946	1.991+0 1.949	9.760-1 1.955	5.755-1 1.961	3.777-1 1.966	2.660-1 1.970	1.969-1 1.973	1.512-1 1.974	1.195-1 1.976	9.656-2 1.976
39.0 eV	γ	2.34 - 1	1.37 - 1	-1.00-2	-9.49 - 2	-1.33-1	-1.37 - 1	-1.17 - 1	-8.03 - 2	-3.04 - 2	2.90 - 2
F	δ	-4.48-4	-6.05-4	-8.19-4	-9.58-4	-1.06-3	-1.14-3	-1.21-3	-1.25-3	-1.30-3	-1.34-3
$5p_{1/2}$ $E_b =$	$\frac{\sigma}{eta}$	3.134+0 1.697	1.966+0 1.716	9.487-1 1.704	5.392-1 1.671	3.391-1 1.631	2.284-1 1.590	1.618-1 1.550	1.190-1 1.510	9.022-2 1.471	7.005-2 1.433
26.3 eV	$\gamma \\ \delta$	5.13-2 -2.97-3	-1.43-2 $-3.26-3$	1.05-2 -3.02-3	1.29-1 -1.57-3	2.77-1 1.29-3	4.32-1 5.40-3	5.83-1 1.05-2	7.27-1 1.65-2	8.62-1 2.29-2	9.87 - 1 $2.98 - 2$
5p _{3/2}	σ	6.218+0	3.740+0	1.707+0	9.347-1	5.713-1	3.761-1	2.613-1	1.890-1	1.412-1	1.082-1
$E_b =$	β	1.694	1.735	1.753	1.738	1.712	1.681	1.647	1.612	1.577	1.543
21.3 eV	$\gamma \over \delta$	1.33-2 -5.69-4	-3.66-2 1.13-3	1.19-2 4.34-3	1.50-1 7.07-3	3.16-1 9.97-3	4.87-1 1.33-2	6.54-1 1.71-2	8.12-1 2.14-2	9.60-1 $2.61-2$	1.10+0 3.11-2
6s _{1/2}	σ	2.075-1	1.276-1	6.227-2	3.663-2	2.400-2	1.688-2	1.248-2	9.579-3	7.563-3	6.109-3
$E_b = 6.0 \text{ eV}$	β γ	1.946 2.31-1	1.949 1.34-1	1.955 -1.21-2	1.961 -9.65-2	1.966 1.34 1	1.969 -1.39-1	1.972 -1.18-1	1.974 -8.04-2	1.975 -2.99-2	1.976 2.98-2
0.0 C V	δ	-4.50-4	-6.08-4	-8.21-4	-9.64-4	-1.07 - 3	-1.15-3	-1.21-3	-1.27 - 3	-1.31-3	-1.34-3
Z= 66, Dy: [X	(e]4f ⁶ _{5/2}	4f _{7/2} 6s _{1/2}									
		k (eV)									
Shell		1500	2000	3000	4000	5000	6000	7000	8000	9000	10000
$3d_{3/2}$ $E_b =$	$\frac{\sigma}{eta}$	4.443+2 0.450	2.284+2 0.963	7.328+1 1.216	3.085+1 1.236	1.532+1 1.200	8.498+0 1.146	5.097+0 1.087	3.244+0 1.027	2.163+0 0.970	1.497+0 0.915
1332.5 eV	γ	-9.87 - 2	-1.42 - 1	1.82 - 1	5.04 - 1	7.65 - 1	9.75 - 1	1.15+0	1.28+0	1.40+0	1.50+0
3d _{5/2}	$\frac{\delta}{\sigma}$	-1.22-2 6.657+2	1.80-2 3.273+2	6.26-2 1.028+2	8.76-2 4.280+1	1.09-1 2.109+1	1.29-1 1.161+1	1.49-1 6.921+0	1.68-1 4.380+0	1.87-1 2.905+0	2.06-1 2.000+0
$E_b =$	β	0.575	1.030	1.214	1.203	1.151	1.090	1.027	0.966	0.909	0.856
1294.9 eV	$\gamma \\ \delta$	-1.17-1 $-1.34-2$	-1.25-1 $1.80-2$	2.22-1 $6.12-2$	5.39-1 8.87-2	7.88-1 1.13-1	9.85-1 1.37-1	1.14+0 1.60-1	1.27+0 1.82-1	1.38+0 2.03-1	1.47+0 2.24-1
4s _{1/2}	σ	2.049+1	1.298+1	6.514+0	3.888+0	2.572+0	1.822+0	1.354+0	1.043+0	8.262-1	6.691-1
$E_b = 416.3 \text{ eV}$	β γ	1.937 3.63-1	1.941 2.40-1	1.949 5.00-2	1.955 -6.35-2	1.961 -1.22-1	1.965 -1.42-1	1.969 -1.35-1	1.971 -1.08-1	1.973 -6.54-2	1.974 -1.21-2
410.5 CV	δ	-3.67-4	-5.86-4	-8.59-4	-0.33-2 $-1.03-3$	-1.16-3	-1.42 - 1 -1.25 - 3	-1.32 - 3	-1.38 - 3	-0.34-2 $-1.44-3$	-1.48 - 3
4p _{1/2}	σ	2.449+1	1.579+1	7.820+0	4.504+0	2.856+0	1.935+0	1.377+0	1.016+0	7.723-1	6.010-1
$E_b = 331.8 \text{ eV}$	β γ	1.627 1.35-1	1.676 1.89-2	1.690 -9.58-3	1.668 8.71-2	1.635 2.27-1	1.598 3.79-1	1.560 5.31-1	1.521 6.76-1	1.484 8.13-1	1.447 9.41-1
	δ	3.60-5	-2.29-3	-2.76-3	-1.56-3	1.03-3	4.85-3	9.67-3	1.52-2	2.13-2	2.77-2
$\begin{array}{l} 4p_{3/2} \\ E_b = \end{array}$	$\frac{\sigma}{eta}$	5.405+1 1.626	3.313+1 1.694	1.540+1 1.737	8.510+0 1.735	5.232+0 1.715	3.459+0 1.688	2.411+0 1.658	1.748+0 1.625	1.308+0 1.592	1.003+0 1.558
292.9 eV	γ	7.11 - 2	-1.97 - 2	-1.45 - 2	1.06 - 1	2.66 - 1	4.36 - 1	6.04 - 1	7.64 - 1	9.14 - 1	1.05+0
4.4	δ	9.84-4 5.994+1	1.29-3	4.51-3	7.48-3 5.053+0	1.04-2	1.37-2	1.73-2 9.291-1	2.13-2 6.041-1	2.56-2 4.098-1	3.01-2
$4d_{3/2}$ $E_b =$	$\frac{\sigma}{eta}$	1.331	3.133+1 1.371	1.121+1 1.345	1.280	2.629+0 1.207	1.508+0 1.135	1.067	1.003	0.944	2.878-1 0.889
161.4 eV	$\gamma \\ \delta$	1.49-3 1.95-2	1.26-1 $3.28-2$	4.12-1 5.53-2	6.66-1 $7.66-2$	8.75-1 9.79-2	1.05+0 1.19-1	1.19+0 1.40-1	1.31+0 1.60-1	1.42+0 1.80-1	1.51+0 2.00-1
4d _{5/2}	σ	8.537+1	4.410+1	1.555+1	6.931+0	3.575+0	2.035+0	1.246+0	8.050-1	5.431-1	3.794-1
$E_b =$	β	1.347	1.358	1.301	1.221	1.141	1.065	0.997	0.935	0.878	0.826
149.4 eV	$\gamma \\ \delta$	1.57-2 1.87-2	1.49-1 $3.18-2$	4.37-1 5.61-2	6.82 - 1 $8.05 - 2$	8.81-1 $1.05-1$	1.04+0 1.29-1	1.18+0 1.53-1	1.29+0 1.76-1	1.39+0 1.98-1	1.47+0 2.20-1
4f _{5/2}	σ	1.807+1	6.504+0	1.418+0	4.586-1	1.862-1	8.759-2	4.569-2	2.573-2	1.538-2	9.638-3
$E_b = 5.5 \text{ eV}$	$eta \ \gamma$	1.058 4.19-1	1.005 5.74-1	0.882 7.93-1	0.776 9.35-1	0.689 1.04+0	0.618 1.12+0	0.558 1.18+0	0.504 1.23+0	0.457 1.28+0	0.413 1.31+0
5.5 € 1	δ	1.05-1	1.32-1	1.83-1	2.31-1	2.76-1	3.18-1	3.58-1	3.95-1	4.30-1	4.64-1
$4f_{7/2}$	σ	2.266+1	8.105+0	1.753+0	5.630-1	2.274-1	1.065-1	5.536-2	3.108-2	1.852-2	1.158-2
$E_b = 3.3 \text{ eV}$	$eta \ \gamma$	1.050 4.25-1	0.996 5.81-1	0.874 8.00-1	0.771 9.41-1	0.689 1.04+0	0.622 1.12+0	0.566 1.18+0	0.516 1.23+0	0.472 1.27+0	0.432 1.31+0
	δ	1.05-1	1.32-1	1.84-1	2.33-1	2.79-1	3.22-1	3.62-1	4.00-1	4.35-1	4.69-1
$5s_{1/2} E_b =$	$\frac{\sigma}{eta}$	3.327+0 1.941	2.060+0 1.945	1.012+0 1.952	5.975-1 1.957	3.925-1 1.963	2.765-1 1.967	2.048-1 1.970	1.573-1 1.972	1.244-1 1.974	1.006-1 1.974
62.9 eV	γ	2.58 - 1	1.59 - 1	5.49 - 3	-8.65 - 2	-1.31-1	-1.42 - 1	-1.27 - 1	-9.55 - 2	-5.02 - 2	4.98 - 3
5n	δ	-4.61-4 2.184±0	-6.36-4	-8.73-4 0.780 1	-1.03-3	-1.15-3	-1.23-3	-1.30-3	-1.36-3	-1.41-3	-1.45-3
$5p_{1/2}$ $E_b =$	$\frac{\sigma}{eta}$	3.184+0 1.692	2.010+0 1.715	9.780—1 1.707	5.589-1 1.676	3.528-1 1.639	2.384-1 1.599	1.693-1 1.560	1.249-1 1.521	9.484-2 1.483	7.378-2 1.446
28.2 eV	γ	6.56 - 2	-8.30 - 3	2.08 - 3	1.11 - 1	2.54 - 1	4.05 - 1	5.54 - 1	6.97 - 1	8.32 - 1	9.59 - 1

	δ	-3.06-3	-3.41-3	-3.29-3	-2.06-3	5.14-4	4.30-3	9.13-3	1.48-2	2.10-2	2.76-2
$p_{3/2}$	σ	6.382+0	3.855+0	1.770+0	9.730-1	5.964-1	3.936-1	2.740-1	1.985-1	1.485-1	1.139-1
$E_b =$	β	1.686	1.731	1.754	1.743	1.719	1.690	1.658	1.625	1.591	1.557
22.9 eV	$\frac{\gamma}{\delta}$	2.33-2 $-7.26-4$	-3.41-2 9.33-4	1.08-3 4.22-3	1.30-1 6.96-3	2.92-1 9.74-3	4.60-1 $1.28-2$	6.25 - 1 $1.64 - 2$	7.82 - 1 $2.05 - 2$	9.31-1 2.50-2	1.07+0 2.97-2
$6s_{1/2}$	σ	2.085-1	1.286-1	6.303-2	3.716-2	2.439-2	1.718-2	1.271-2	9.761-3	7.713-3	6.233-
$E_b =$	$\boldsymbol{\beta}$	1.942	1.946	1.952	1.958	1.963	1.967	1.970	1.972	1.973	1.974
6.0 eV	γ	2.46-1 $-4.66-4$	1.49 - 1 $-6.39 - 4$	5.56-4 -8.76-4	-8.91-2 $-1.03-3$	-1.33-1 $-1.15-3$	-1.42-1 $-1.24-3$	-1.28-1 $-1.31-3$	-9.48-2 $-1.37-3$	-4.87-2 $-1.42-3$	7.14-3 -1.46-
Z= 67, Ho: [X			-0.55-4	-0.70-4	-1.05-5	-1,13-3	-1.24-3	-1.51-5	-1.57-5	-1,42-5	-1.40-
2 07,110. [71	115/2	k (eV)									
Shell		1500	2000	3000	4000	5000	6000	7000	8000	9000	10000
3d _{3/2}	σ	4.520+2	2.441+2	7.914+1	3.347+1	1.669+1	9.281+0	5.582+0	3.560+0	2.378+0	1.649+0
$E_b =$	β	0.375	0.914	1.206	1.238	1.209	1.159	1.103	1.045	0.988	0.933
1391.5 eV	δ	-6.50-2 $-6.44-3$	-1.62 - 1 $1.17 - 2$	1.41-1 5.99-2	4.66-1 8.55-2	7.33-1 1.06-1	9.49-1 1.26-1	1.13+0 1.46-1	1.27+0 1.65-1	1.39+0 1.84-1	1.49+0 2.02-1
3d _{5/2}	σ	6.876+2	3.498+2	1.109+2	4.637+1	2.292+1	1.266+1	7.562+0	4.796+0	3.187+0	2.198+0
$E_b =$	β	0.478	0.991	1.209	1.208	1.161	1.102	1.041	0.981	0.925	0.871
1351.4 eV	γ	-8.70-2	-1.48 - 1	1.84-1	5.05-1	7.60-1	9.63-1	1.13+0	1.26+0	1.37+0	1.47+0
	δ	-1.07-2	1.24-2	5.83-2	8.61-2	1.10-1	1.33-1	1.56-1	1.78-1	1.99-1	2.20-1
$4s_{1/2}$ $E_b =$	$\frac{\sigma}{eta}$	2.098+1 1.932	1.335+1 1.936	6.735+0 1.945	4.032+0 1.951	2.672+0 1.957	1.894+0 1.962	1.409+0 1.966	1.087+0 1.969	8.614-1 1.971	6.981- 1.972
435.7 eV	γ	3.87-1 -3.61-4	2.63-1 $-6.06-4$	6.85-2 $-9.11-4$	-5.15-2 $-1.10-3$	-1.17-1 $-1.24-3$	-1.43-1 $-1.34-3$	-1.42-1 $-1.42-3$	-1.19-1 $-1.49-3$	-8.22-2 $-1.55-3$	-3.34- -1.60-
$4p_{1/2}$	σ	2.499+1	1.625+1	8.122+0	4.706+0	2.997+0	2.038+0	1.454+0	1.076+0	8.193-1	6.388-
$E_b =$	β	1.616	1.671	1.691	1.672	1.641	1.605	1.569	1.532	1.495	1.459
343.5 eV	γ	1.57 - 1	3.16 - 2	-1.43-2	7.12 - 2	2.04 - 1	3.52 - 1	5.01 - 1	6.45 - 1	7.82 - 1	9.11 - 1
	δ	4.51-4	-2.29-3	-2.99-3	-2.00-3	3.22-4	3.85-3	8.39-3	1.37-2	1.96-2	2.58-2
$4p_{3/2}$	σ	5.584+1	3.440+1	1.610+1	8.931+0	5.507+0	3.650+0	2.548+0	1.851+0	1.387+0	1.066+0
$E_b = 306.6 \text{ eV}$	β	1.612 8.78-2	1.686 -1.19-2	1.737 -2.29-2	1.738 8.70-2	1.722 2.41-1	1.697 4.07-1	1.668 5.73-1	1.637 7.34-1	1.605 8.84-1	1.573 1.03+0
300.0 EV	δ	1.19-3	1.15-3	4.36-3	7.37-3	1.02-2	1.33-2	1.68-2	2.06-2	2.47-2	2.90-2
4d _{3/2}	σ	6.310+1	3.329+1	1.205+1	5.465+0	2.857+0	1.645+0	1.017+0	6.630-1	4.509-1	3.173-
$E_b =$	β	1.322	1.369	1.352	1.291	1.222	1.152	1.085	1.021	0.962	0.907
167.8 eV	γ	-9.72-3	1.06-1	3.87-1	6.43-1	8.56-1	1.03+0	1.18+0	1.31+0	1.41+0	1.50+0
	δ	1.80-2	3.13-2	5.36-2	7.44-2	9.52-2	1.16-1	1.37-1	1.56-1	1.76-1	1.95-1
$4d_{5/2}$	σ	9.002+1 1.342	4.691+1 1.359	1.671+1 1.309	7.497+0 1.232	3.884+0 1.153	2.220+0 1.080	1.362+0 1.012	8.828-1 0.950	5.970-1 0.893	4.179- 0.841
E _b = 156.5 eV	β γ	3.43-3	1.30-1	4.14-1	6.61-1	8.64–1	1.03+0	1.012	1.28+0	1.38+0	1.47+0
150.5 CV	δ	1.73-2	3.02-2	5.41-2	7.79–2	1.02-1	1.26-1	1.50-1	1.72-1	1.94-1	2.15-1
$4f_{5/2}$	σ	2.059+1	7.470+0	1.644+0	5.341-1	2.176-1	1.027-1	5.375-2	3.036-2	1.819-2	1.143-
$E_b =$	β	1.060	1.012	0.894	0.788	0.702	0.630	0.568	0.514	0.466	0.422
4.8 eV	$_{\delta}^{\gamma}$	4.04-1 1.03-1	5.61-1 1.30-1	7.87-1 1.80-1	9.34-1 2.28-1	1.04+0 2.73-1	1.12+0 3.14-1	1.19+0 3.53-1	1.24+0 3.90-1	1.29+0 4.25-1	1.32+0 4.58-1
4f _{7/2}	σ	2.584+1	9.326+0	2.036+0	6.572-1	2.664-1	1.252-1	6.526-2	3.674-2	2.195-2	1.376-
$E_b =$	β	1.053	1.003	0.885	0.783	0.701	0.633	0.575	0.525	0.481	0.440
2.8 eV	γ	4.11-1	5.69-1	7.94-1	9.41-1	1.04+0	1.12+0	1.19+0	1.24+0	1.28+0	1.32+0
	δ	1.03-1	1.30-1	1.82-1	2.30-1	2.76-1	3.18-1	3.57-1	3.95-1	4.30-1	4.63-1
$5s_{1/2}$	σ	3.380+0	2.101+0	1.038+0	6.149-1	4.047-1	2.856-1	2.117-1	1.628-1	1.288-1	1.042-
$E_b = 51.2 \text{ eV}$	β γ	1.937 2.69-1	1.941 1.71-1	1.948 1.75-2	1.954 -7.87-2	1.959 -1.28-1	1.964 1.44 1	1.967 1.35 1	1.970 1.08 1	1.971 -6.67-2	1.972 1.57
31.2 CV	δ	-4.76-4	-6.68-4	-9.29-4	-1.10-3	-1.23 - 3	-1.33-3	-1.41-3	-1.47 - 3	-1.52 - 3	-1.57 -
5p _{1/2}	σ	3.224+0	2.048+0	1.005+0	5.777-1	3.662-1	2.483-1	1.768-1	1.307-1	9.945-2	7.752-
$E_b = 24.9 \text{ eV}$	β	1.687 7.94_2	1.713 _1.51_3	1.709 _4.73_3	1.681 9.49-2	1.645 2.32—1	1.607 3.80-1	1.569 5.26-1	1.531 6.68-1	1.494 8.03_1	1.458 9.29-1
24.9 eV	δ	7.94-2 $-3.15-3$	-1.51-3 $-3.56-3$	-4.73-3 $-3.54-3$	-2.51-3	2.32 - 1 $-2.02 - 4$	3.80-1 3.29-3	5.26-1 $7.80-3$	1.32-2	8.03-1 1.91-2	9.29—1 2.55—2
$5p_{3/2}$	σ	6.524+0	3.958+0	1.829+0	1.010+0	6.208-1	4.107-1	2.864-1	2.080-1	1.558-1	1.197-
$E_b =$	β	1.679	1.727	1.755	1.747	1.726	1.699	1.668	1.636	1.604	1.572
19.5 eV	$_{\delta}^{\gamma}$	3.29-2 -8.63-4	-3.08-2 $7.42-4$	-8.20-3 4.11-3	1.13-1 6.88-3	2.69-1 9.57-3	4.34-1 $1.25-2$	5.97-1 1.59-2	7.54-1 1.97-2	9.02-1 2.39-2	1.04+0 2.84-2
6s _{1/2}	σ	2.093-1	1.295-1	6.374-2	3.768-2	2.477-2	1.746-2	1.294-2	9.941-3	7.860-3	6.357-
$E_b =$	β	1.938	1.942	1.948	1.954	1.959	1.964	1.967	1.969	1.971	1.972
6.0 eV	γ	2.62 - 1	1.65 - 1	1.38 - 2	-8.07 - 2	-1.30-1	-1.45-1	-1.36-1	-1.08-1	-6.63 - 2	-1.44-
	δ	-4.81-4	-6.72-4	-9.33-4	-1.11-3	-1.23-3	-1.33-3	-1.41-3	-1.48-3	-1.54-3	-1.58-
Z= 68, Er: [X	e]4f ⁶ _{5/2} 4										
21 11		k (eV)	2005	2000	4000	FOOC	C00C	7000	0000	0000	10000
Shell		1500	2000	3000	4000	5000	6000	7000	8000	9000	10000
$3d_{3/2}$	σ	4.115+2	2.603+2	8.540+1	3.629+1	1.815+1	1.012+1	6.103+0	3.901+0	2.611+0	1.813+0

Table 1 (contin	ued)										
$E_b =$	β	0.492	0.856	1.193	1.239	1.216	1.171	1.117	1.061	1.006	0.952
1453.3 eV	$\gamma \\ \delta$	-1.93-2 $-1.80-3$	-1.76-1 $4.95-3$	1.01-1 5.70-2	4.27-1 8.34-2	7.00-1 1.04-1	9.22-1 1.24-1	1.10+0 1.43-1	1.26+0 1.62-1	1.38+0 1.80-1	1.49+0 1.98-1
3d _{5/2}	σ	6.884+2	3.729+2	1.194+2	5.014+1	2.487+1	1.377+1	8.247+0	5.241+0	3.489+0	2.410+0
$E_b =$	β	0.884+2	0.947	1.194+2	1.212	1.170	1.113	1.054	0.996	0.940	0.887
1409.3 eV	γ	-5.21-2	-1.67 - 1	1.45 - 1	4.70 - 1	7.31 - 1	9.39 - 1	1.11+0	1.25+0	1.36+0	1.46+0
	δ	-4.91-3	6.44-3	5.53-2	8.34-2	1.07-1	1.30-1	1.53-1	1.75-1	1.96-1	2.16-1
$4s_{1/2}$	σ	2.140+1	1.369+1	6.943+0	4.169+0	2.769+0	1.966+0	1.464+0	1.130+0	8.963-1	7.269-1
$E_b = 449.1 \text{ eV}$	β γ	1.927 4.07-1	1.932 2.84-1	1.941 8.66-2	1.947 -3.89-2	1.953 -1.11-1	1.959 -1.43-1	1.963 -1.47-1	1.966 -1.30-1	1.968 -9.72-2	1.970 -5.29-2
113.1 € \$	δ	-3.52-4	-6.25-4	-9.63-4	-1.18 - 3	-1.33-3	-1.45 - 3	-1.53-3	-1.61-3	-1.67 - 3	-1.73 - 3
$4p_{1/2}$	σ	2.552+1	1.673+1	8.444+0	4.921+0	3.146+0	2.146+0	1.535+0	1.138+0	8.689-1	6.787-1
$E_b =$	β	1.603	1.665	1.691	1.676	1.647	1.613	1.578	1.542	1.507	1.472
366.2 eV	$\gamma \\ \delta$	1.85-1 1.07-3	4.81-2 $-2.24-3$	-1.78-2 $-3.22-3$	5.55-2 -2.43-3	1.81 - 1 $-3.68 - 4$	3.25-1 2.86-3	4.71 - 1 $7.12 - 3$	6.14-1 1.21-2	7.51-1 1.78-2	8.80-1 2.39-2
4p _{3/2}	σ	5.758+1	3.567+1	1.679+1	9.357+0	5.787+0	3.844+0	2.689+0	1.957+0	1.469+0	1.130+0
$E_b =$	β	1.598	1.679	1.736	1.741	1.727	1.705	1.678	1.649	1.618	1.587
320.0 eV	γ	1.05 - 1	-2.83 - 3	-3.00-2	6.94 - 2	2.17 - 1	3.79 - 1	5.43 - 1	7.02 - 1	8.54 - 1	9.96 - 1
	δ	1.47-3	1.02-3	4.21-3	7.28-3	1.01-2	1.30-2	1.63-2	1.99-2	2.39-2	2.80-2
$4d_{3/2}$	σ	6.636+1	3.534+1 1.366	1.293+1	5.903+0	3.100+0	1.792+0	1.111+0	7.262-1	4.951-1	3.491-1
$E_b = 176.7 \text{ eV}$	β γ	1.312 -1.99-2	8.66-2	1.358 3.62-1	1.302 6.19-1	1.235 8.36-1	1.167 1.02+0	1.102 1.17+0	1.039 1.30+0	0.981 1.41+0	0.925 1.50+0
	δ	1.65-2	2.98-2	5.19-2	7.22-2	9.25-2	1.13-1	1.33-1	1.53-1	1.72-1	1.91-1
4d _{5/2}	σ	9.493+1	4.991+1	1.796+1	8.103+0	4.216+0	2.418+0	1.488+0	9.667-1	6.551-1	4.595-1
$E_b =$	β	1.337	1.360	1.316	1.242	1.166	1.094	1.027	0.965	0.908	0.855
167.6 eV	$\delta \gamma$	-8.34-3 1.59-2	1.10-1 2.86-2	3.91-1 5.21-2	6.40-1 $7.53-2$	8.46-1 $9.90-2$	1.02+0 1.23-1	1.16+0 1.46-1	1.28+0 1.68-1	1.38+0 1.90-1	1.47+0 2.11-1
4f _{5/2}	σ	2.335+1	8.541+0	1.896+0	6.190-1	2.531-1	1.198-1	6.287-2	3.560-2	2.139-2	1.347-2
$E_b =$	β	1.061	1.019	0.905	0.801	0.714	0.641	0.579	0.524	0.476	0.431
5.3 eV	γ	3.90 - 1	5.48 - 1	7.80 - 1	9.33 - 1	1.04+0	1.13+0	1.19+0	1.25+0	1.29+0	1.33+0
	δ	1.02-1	1.28-1	1.78-1	2.25-1	2.69-1	3.10-1	3.48-1	3.85-1	4.19-1	4.52-1
$4f_{7/2}$	σ	2.934+1 1.054	1.068+1 1.009	2.352+0	7.631-1	3.104-1	1.463-1 0.644	7.647-2 0.585	4.317-2	2.586-2	1.624-2
$E_b = 3.6 \text{ eV}$	β γ	3.97—1	5.56-1	0.896 7.88-1	0.795 9.40-1	0.712 1.05+0	1.13+0	0.585 1.19+0	0.535 1.25+0	0.490 1.29+0	0.449 1.33+0
-,	δ	1.02-1	1.28-1	1.79-1	2.27-1	2.72-1	3.14-1	3.53-1	3.90-1	4.24-1	4.57-1
5s _{1/2}	σ	3.458+0	2.155+0	1.069+0	6.347-1	4.184-1	2.955-1	2.192-1	1.687-1	1.335-1	1.081-1
$E_b =$	β	1.933	1.937	1.944	1.950	1.956	1.960	1.964	1.967	1.969	1.970
59.8 eV	$\gamma \\ \delta$	2.88 - 1 $-4.86 - 4$	1.90-1 $-6.97-4$	3.27-2 -9.87-4	-6.90-2 $-1.18-3$	-1.25-1 $-1.33-3$	-1.46-1 $-1.43-3$	-1.42-1 $-1.52-3$	-1.20-1 $-1.58-3$	-8.31-2 $-1.65-3$	-3.62-2 $-1.69-3$
5p _{1/2}	σ	3.266+0	2.087+0	1.033+0	5.971-1	3.800-1	2.584-1	1.845-1	1.367-1	1.042-1	8.140-2
$E_b =$	β	1.681	1.711	1.711	1.685	1.651	1.615	1.578	1.541	1.505	1.470
27.9 eV	γ	9.59-2	7.11-3	-1.07-2	7.92-2	2.10-1	3.54-1	4.99-1	6.39-1	7.73-1	8.99-1
_	δ	-3.24-3	-3.73-3	-3.80-3	-2.95-3	-8.88-4	2.31-3	6.52-3	1.16-2	1.73-2	2.34-2
$5p_{3/2}$ $E_b =$	$\frac{\sigma}{\beta}$	6.678+0 1.670	4.068+0 1.723	1.891+0 1.755	1.048+0 1.751	6.462-1 1.733	4.284-1 1.707	2.994-1 1.678	2.177-1 1.648	1.633-1 1.617	1.257—1 1.585
22.3 eV	γ	4.46-2	-2.61-2	-1.70-2	9.47-2	2.45-1	4.07 – 1	5.69-1	7.24–1	8.73-1	1.01+0
	δ	-1.00 - 3	5.25 - 4	3.99 - 3	6.81 - 3	9.44 - 3	1.22-2	1.54 - 2	1.90 - 2	2.29 - 2	2.71 - 2
6s _{1/2}	σ	2.100 - 1	1.303 - 1	6.441-2	3.818 - 2	2.514 - 2	1.774 - 2	1.316-2	1.012-2	8.006 - 3	6.479 - 3
$E_b = 6.0 \text{ eV}$	β	1.933 2.77-1	1.938 1.82-1	1.944 2.78-2	1.950	1.956 1.26 1	1.960 -1.47-1	1.964	1.966 1.20 1	1.968 -8.26-2	1.970 -3.49-2
0.0 ev	$\gamma \\ \delta$	-4.95-4	-7.03-4	-9.92-4	-7.15-2 $-1.18-3$	-1.20-1 -1.32-3	-1.47-1 -1.43-3	-1.43-1 $-1.52-3$	-1.20-1 -1.60-3	-8.26-2 -1.66-3	-3.49-2 $-1.71-3$
Z= 69, Tm: [X	Xel4f	4f ⁷ - 6s ² -									
2 00, 1111 [.	115/2	k (eV)									
Shell		1500	2000	3000	4000	5000	6000	7000	8000	9000	10000
3d _{5/2}	σ	5.454+2	3.961+2	1.283+2	5.411+1	2.692+1	1.495+1	8.973+0	5.714+0	3.810+0	2.637+0
$E_b =$	β	0.625	0.898	1.193	1.215	1.178	1.124	1.067	1.009	0.955	0.902
1467.7 eV	γ	-3.84 - 3	-1.79 - 1	1.07 - 1	4.34 - 1	7.01 - 1	9.15 - 1	1.09+0	1.23+0	1.35+0	1.45+0
	δ	-2.54-3	4.08-4	5.21-2	8.08-2	1.05-1	1.27-1	1.49-1	1.71-1	1.92-1	2.12-1
$4s_{1/2}$	σ	2.185+1	1.404+1	7.162+0	4.313+0	2.870+0	2.040+0	1.521+0	1.175+0	9.325-1	7.567-1
$E_b = 471.7 \text{ eV}$	β	1.921 4.32-1	1.927 3.09-1	1.936 1.07-1	1.943 -2.44-2	1.949 -1.03-1	1.955 -1.41-1	1.959 1.51 1	1.963 -1.39-1	1.965 -1.11-1	1.967 -7.16-2
1, 1,, 0	$_{\delta}^{\gamma}$	-3.34-4	-6.41-4	-1.02-3	-2.44-2 $-1.26-3$	-1.43-3	-1.55-3	-1.65-3	-1.73-1	-1.80-3	-1.86-3
4p _{1/2}	σ	2.597+1	1.717+1	8.753+0	5.131+0	3.295+0	2.255+0	1.617+0	1.202+0	9.194-1	7.195-1
$E_b =$	β	1.589	1.658	1.691	1.679	1.652	1.620	1.586	1.552	1.517	1.483
385.9 eV	$\gamma \\ \delta$	2.12-1 1.78-3	6.60-2 $-2.16-3$	-1.94-2 $-3.44-3$	4.14-2 $-2.83-3$	1.60-1 $-1.01-3$	2.99-1 1.95-3	4.42 - 1 $5.92 - 3$	5.83-1 1.07-2	7.19-1 1.61-2	8.48 - 1 $2.19 - 2$
4n		5.935+1	3.696+1	1.751+1	9.797+0	6.077+0	4.046+0	2.836+0	2.067+0		
$\begin{array}{l} 4p_{3/2} \\ E_b = \end{array}$	$\frac{\sigma}{eta}$	1.583	1.669	1.731+1	9.797+0 1.743	1.732	4.046+0 1.712	2.836+0 1.687	2.067+0 1.659	1.554+0 1.630	1.197+0 1.600
336.6 eV	γ	1.25-1	8.08-3	-3.58-2	5.25-2	1.93-1	3.52-1	5.13-1	6.71-1	8.23-1	9.65-1

	δ	1.86-3	8.97-4	4.04-3	7.18-3	9.99-3	1.28-2	1.59-2	1.93-2	2.31-2	2.70-2
4d _{3/2}	σ	6.960+1	3.742+1	1.384+1	6.359+0	3.355+0	1.946+0	1.210+0	7.933-1	5.421 - 1	3.831-
$E_b =$	β	1.300	1.363	1.364	1.313	1.249	1.183	1.119	1.057	0.999	0.944
185.5 eV	$\gamma \\ \delta$	-2.85-2 $1.50-2$	6.81-2 2.83-2	3.37-1 5.02-2	5.95-1 7.02-2	8.15-1 8.99-2	1.00+0 1.10-1	1.16+0 1.30-1	1.29+0 1.49-1	1.40+0 1.68-1	1.50+0 1.86-
4.3											
$4d_{5/2}$ $E_b =$	$\frac{\sigma}{eta}$	9.964+1 1.331	5.286+1 1.360	1.922+1 1.323	8.726+0 1.252	4.560+0 1.178	2.624+0 1.107	1.620+0 1.041	1.055+0 0.980	7.165-1 0.923	5.035- 0.870
ւր — 175.7 eV	γ	-1.82-2	9.17-2	3.67-1	6.19-1	8.28-1	1.00+0	1.15+0	1.27+0	1.37+0	1.46+0
	δ	1.46-2	2.71-2	5.02-2	7.30-2	9.62-2	1.19-1	1.42-1	1.65-1	1.86-1	2.07-
$4f_{5/2}$	σ	2.635+1	9.717+0	2.176+0	7.137-1	2.928-1	1.390-1	7.314-2	4.152-2	2.501-2	1.579-
$E_b =$	β	1.061	1.024	0.916	0.813	0.726	0.653	0.590	0.535	0.485	0.440
6.2 eV	γ	3.75 - 1	5.34 - 1	7.72 - 1	9.31 - 1	1.04+0	1.13+0	1.20+0	1.26+0	1.30+0	1.34+0
	δ	1.01-1	1.27-1	1.75-1	2.22-1	2.65-1	3.06-1	3.44-1	3.80-1	4.14-1	4.46-
$4f_{7/2}$	σ	3.313+1	1.216+1	2.703+0	8.813-1	3.597-1	1.700-1	8.910-2	5.042-2	3.027-2	1.906-
$E_b = 4.7 \text{ eV}$	β	1.055 3.82-1	1.015 5.43-1	0.906	0.806	0.724 1.05+0	0.655 1.13+0	0.596 1.20+0	0.544	0.499	0.457
4.7 ev	$\gamma \\ \delta$	1.00-1	1.27-1	7.80-1 1.76-1	9.39-1 2.24-1	2.68-1	3.10-1	3.49-1	1.25+0 3.85-1	1.30+0 4.19-1	1.34+0 4.52-
5s _{1/2}	σ	3.511+0	2.197+0	1.095+0	6.523-1	4.309-1	3.048-1	2.263-1	1.743-1	1.381-1	1.119-
$E_b =$	β	1.928	1.933	1.940	1.946	1.952	1.957	1.961	1.964	1.966	1.968
53.2 eV	γ	3.01-1	2.05-1	4.65-2	-5.91-2	-1.20-1	-1.46-1	-1.47 - 1	-1.30-1	-9.76 - 2	-5.48
	δ	-4.97 - 4	-7.29 - 4	-1.05 - 3	-1.26 - 3	-1.42 - 3	-1.54 - 3	-1.63 - 3	-1.71 - 3	-1.78 - 3	-1.83
5p _{1/2}	σ	3.309+0	2.127+0	1.062+0	6.170-1	3.942-1	2.689-1	1.925-1	1.429-1	1.092-1	8.542-
$E_b =$	β	1.674	1.708	1.712	1.689	1.658	1.623	1.587	1.551	1.516	1.481
36.2 eV	γ	1.15-1	1.78-2	-1.55-2	6.39-2	1.89-1	3.29-1	4.71-1	6.09-1	7.42-1	8.69-
	δ	-3.32-3	-3.90-3	-4.06-3	-3.37-3	-1.54-3	1.41-3	5.34-3	1.01-2	1.55-2	2.14-2
5p _{3/2}	σ_{ρ}	6.841+0 1.659	4.183+0 1.717	1.956+0	1.088+0	6.725-1 1.739	4.468-1 1.715	3.127-1 1.688	2.278-1 1.659	1.711-1 1.629	1.319- 1.599
$E_b = 30.4 \text{ eV}$	β γ	1.659 5.83-2	-2.00-2	1.755 -2.50-2	1.754 7.71–2	1./39 2.22-1	1.715 3.81–1	1.688 5.40—1	1.659 6.95—1	1.629 8.43—1	9.83-
JU.7 CV	δ	-1.14-3	-2.00-2 2.78-4	-2.30-2 3.84-3	6.74-3	9.35-3	1.20-2	1.50-2	1.83-2	2.20-2	2.60-2
6s _{1/2}	σ	2.105-1	1.310-1	6.503-2	3.865-2	2.550-2	1.802-2	1.337-2	1.030-2	8.151-3	6.600-
$E_b =$	β	1.928	1.933	1.940	1.946	1.952	1.957	1.961	1.964	1.966	1.967
6.0 eV	γ	2.93 - 1	1.98 - 1	4.25 - 2	-6.14 - 2	-1.21-1	-1.47 - 1	-1.48-1	-1.30-1	-9.78 - 2	-5.42
											101
	δ	-5.06-4	-7.35-4	-1.05 - 3	-1.26-3	-1.42-3	-1.54-3	-1.63-3	-1.72-3	-1.79-3	-1.84
Z= 70, Yb: [X	δ	-5.06-4	-7.35-4	-1.05-3	-1.26-3	-1.42-3	-1.54-3	-1.63-3	-1.72-3	-1.79-3	-1.84-
	δ	-5.06-4	-7.35-4	-1.05-3	-1.26-3	-1.42-3	-1.54-3	-1.63-3	-1.72-3	-1.79-3	-1.84-
	δ	$-5.06-4$ $4f_{7/2}^8 6s_{1/2}^2$		-1.05-3 3000	-1.26-3 4000	-1.42-3 5000	-1.54-3 6000		-1.72-3 8000	9000	10000
Z= 70, Yb: [X Shell	δ (e]4 $f_{5/2}^6$	$ -5.06-4 $ $ 4f_{7/2}^{8} 6s_{1/2}^{2} $ $ \underline{k (eV)} $ 1500	2000	3000	4000	5000	6000	7000	8000	9000	10000
Z= 70, Yb: [X Shell $4s_{1/2}$	$\frac{\delta}{\delta}$ (e]4 $f_{5/2}^6$	$ -5.06-4 $ $ 4f_{7/2}^{8} 6s_{1/2}^{2} $ $ k (eV) $ $ 1500 $ $ 2.221+1 $	2000 1.435+1	3000 7.364+0	4000 4.450+0	5000 2.967+0	6000 2.112+0	7000 1.576+0	8000 1.219+0	9000 9.683-1	10000
Z= 70, Yb: [X Shell $4s_{1/2}$	δ (e]4 $f_{5/2}^6$	$ -5.06-4 $ $ 4f_{7/2}^{8} 6s_{1/2}^{2} $ $ \underline{k (eV)} $ 1500	2000 1.435+1 1.921 3.32-1	3000	4000	5000	6000 2.112+0 1.951 -1.38-1	7000	8000	9000 9.683-1 1.962 -1.24-1	10000 7.863- 1.964
Z= 70, Yb: [X Shell $4s_{1/2}$ $E_b =$	$\frac{\delta}{\delta}$ (e)4 $f_{5/2}^6$ $\frac{\sigma}{\beta}$	$ -5.06-4 $ $ 4f_{7/2}^8 6s_{1/2}^2 $ $ k (eV) $ $ 1500 $ $ 2.221+1 $ $ 1.915 $	2000 1.435+1 1.921	3000 7.364+0 1.931	4000 4.450+0 1.938	5000 2.967+0 1.945	6000 2.112+0 1.951	7000 1.576+0 1.956	8000 1.219+0 1.959	9000 9.683-1 1.962	10000 7.863- 1.964 -8.85-
Z= 70, Yb: [X Shell $4s_{1/2}$ $E_b =$	$\frac{\delta}{\text{Ce]4f}_{5/2}^6}$ $\frac{\sigma}{\beta}$ γ	$ \begin{array}{r} -5.06-4 \\ \mathbf{4f_{7/2}^8 6s_{1/2}^2} \\ \underline{k \text{ (eV)}} \\ 1500 \\ 2.221+1 \\ 1.915 \\ 4.54-1 \end{array} $	2000 1.435+1 1.921 3.32-1	3000 7.364+0 1.931 1.27-1	4000 4.450+0 1.938 -9.51-3	5000 2.967+0 1.945 -9.36-2	6000 2.112+0 1.951 -1.38-1 -1.67-3 2.361+0	7000 1.576+0 1.956 -1.53-1	8000 1.219+0 1.959 -1.47-1 -1.87-3 1.265+0	9000 9.683-1 1.962 -1.24-1 -1.94-3 9.698-1	10000
Z= 70, Yb: [X Shell $4s_{1/2}$ $E_b = 487.2 \text{ eV}$ $4p_{1/2}$ $E_b = 487.2 \text{ eV}$	$\frac{\delta}{\delta e \mathbf{4f_{5/2}^6}} \frac{\delta}{\delta}$ $\frac{\sigma}{\beta}$ $\frac{\gamma}{\delta}$ $\frac{\sigma}{\delta}$	-5.06-4 4f ⁸ _{7/2} 6s ² _{1/2} k (eV) 1500 2.221+1 1.915 4.54-1 -3.10-4 2.631+1 1.577	2000 1.435+1 1.921 3.32-1 -6.52-4 1.754+1 1.651	3000 7.364+0 1.931 1.27-1 -1.07-3 9.035+0 1.690	4000 4.450+0 1.938 -9.51-3 -1.34-3 5.330+0 1.681	5000 2.967+0 1.945 -9.36-2 -1.53-3 3.438+0 1.657	6000 2.112+0 1.951 -1.38-1 -1.67-3 2.361+0 1.627	7000 1.576+0 1.956 -1.53-1 -1.78-3 1.698+0 1.594	8000 1.219+0 1.959 -1.47-1 -1.87-3 1.265+0 1.561	9000 9.683-1 1.962 -1.24-1 -1.94-3 9.698-1 1.528	10000 7.863- 1.964 -8.85- -2.01- 7.605- 1.495
Z= 70, Yb: [X Shell $4s_{1/2}$ $E_b = 487.2 \text{ eV}$ $4p_{1/2}$	$ \frac{\delta}{\text{Ce}]\mathbf{4f_{5/2}^6}} $ $ \frac{\sigma}{\beta} $ $ \frac{\gamma}{\delta} $ $ \frac{\sigma}{\beta} $ $ \frac{\sigma}{\beta} $ $ \frac{\sigma}{\gamma} $	$\begin{array}{c} -5.06-4 \\ \mathbf{4f_{7/2}^8 6s_{1/2}^2} \\ \underline{k (\text{eV})} \\ 1500 \\ 2.221+1 \\ 1.915 \\ 4.54-1 \\ -3.10-4 \\ 2.631+1 \\ 1.577 \\ 2.37-1 \end{array}$	2000 1.435+1 1.921 3.32-1 -6.52-4 1.754+1 1.651 8.34-2	3000 7.364+0 1.931 1.27-1 -1.07-3 9.035+0 1.690 -1.90-2	4000 4.450+0 1.938 -9.51-3 -1.34-3 5.330+0 1.681 2.95-2	5000 2.967+0 1.945 -9.36-2 -1.53-3 3.438+0 1.657 1.40-1	6000 2.112+0 1.951 -1.38-1 -1.67-3 2.361+0 1.627 2.74-1	7000 1.576+0 1.956 -1.53-1 -1.78-3 1.698+0 1.594 4.14-1	8000 1.219+0 1.959 -1.47-1 -1.87-3 1.265+0 1.561 5.53-1	9000 9.683-1 1.962 -1.24-1 -1.94-3 9.698-1 1.528 6.88-1	10000 7.863- 1.964 -8.85- -2.01- 7.605- 1.495 8.17-1
Z= 70, Yb: [X Shell $4s_{1/2}$ $E_b = 487.2 \text{ eV}$ $4p_{1/2}$ $E_b = 396.7 \text{ eV}$	δ (e]4f _{5/2} σ β γ δ σ β γ δ δ σ β γ δ	$-5.06-4$ $4f_{7/2}^8 6s_{1/2}^2$ $k \text{ (eV)}$ 1500 $2.221+1$ 1.915 $4.54-1$ $-3.10-4$ $2.631+1$ 1.577 $2.37-1$ $2.45-3$	2000 1.435+1 1.921 3.32-1 -6.52-4 1.754+1 1.651 8.34-2 -2.07-3	3000 7.364+0 1.931 1.27-1 -1.07-3 9.035+0 1.690 -1.90-2 -3.63-3	4000 4.450+0 1.938 -9.51-3 -1.34-3 5.330+0 1.681 2.95-2 -3.20-3	5000 2.967+0 1.945 -9.36-2 -1.53-3 3.438+0 1.657 1.40-1 -1.57-3	6000 2.112+0 1.951 -1.38-1 -1.67-3 2.361+0 1.627 2.74-1 1.12-3	7000 1.576+0 1.956 -1.53-1 -1.78-3 1.698+0 1.594 4.14-1 4.81-3	8000 1.219+0 1.959 -1.47-1 -1.87-3 1.265+0 1.561 5.53-1 9.27-3	9000 9.683-1 1.962 -1.24-1 -1.94-3 9.698-1 1.528 6.88-1 1.44-2	10000 7.863– 1.964 -8.85– -2.01- 7.605– 1.495 8.17–1 2.01–2
Z= 70, Yb: [X Shell $4s_{1/2}$ $E_b = 487.2 \text{ eV}$ $4p_{1/2}$ $E_b = 396.7 \text{ eV}$ $4p_{3/2}$	$ \begin{array}{c} \delta \\ \text{Ce]4f}_{5/2}^6 \\ \sigma \\ \beta \\ \gamma \\ \delta \\ \sigma \\ \sigma \end{array} $	$\begin{array}{c} -5.06-4 \\ \textbf{4f}^{8}_{7/2} \ \textbf{6s}^{2}_{1/2} \\ \hline k \ (\text{eV}) \\ \hline 1500 \\ 2.221+1 \\ 1.915 \\ 4.54-1 \\ -3.10-4 \\ 2.631+1 \\ 1.577 \\ 2.37-1 \\ 2.45-3 \\ \hline 6.087+1 \end{array}$	2000 1.435+1 1.921 3.32-1 -6.52-4 1.754+1 1.651 8.34-2 -2.07-3 3.810+1	3000 7.364+0 1.931 1.27-1 -1.07-3 9.035+0 1.690 -1.90-2 -3.63-3 1.818+1	4000 4.450+0 1.938 -9.51-3 -1.34-3 5.330+0 1.681 2.95-2 -3.20-3 1.022+1	5000 2.967+0 1.945 -9.36-2 -1.53-3 3.438+0 1.657 1.40-1 -1.57-3 6.358+0	6000 2.112+0 1.951 -1.38-1 -1.67-3 2.361+0 1.627 2.74-1 1.12-3 4.243+0	7000 1.576+0 1.956 -1.53-1 -1.78-3 1.698+0 1.594 4.14-1 4.81-3 2.980+0	8000 1.219+0 1.959 -1.47-1 -1.87-3 1.265+0 1.561 5.53-1 9.27-3 2.176+0	9000 9.683-1 1.962 -1.24-1 -1.94-3 9.698-1 1.528 6.88-1 1.44-2 1.638+0	10000 7.863– 1.964 -8.85- -2.01- 7.605– 1.495 8.17–1 2.01–2
Z= 70, Yb: [X Shell $4s_{1/2}$ $E_b = 487.2 \text{ eV}$ $4p_{1/2}$ $E_b = 396.7 \text{ eV}$ $4p_{3/2}$ $E_b = 60.7 \text{ eV}$	$ \begin{array}{c} \delta \\ \text{(e)4f}_{5/2}^{6} \\ \sigma \\ \beta \\ \gamma \\ \delta \\ \sigma \\ \beta \\ \beta \end{array} $	$\begin{array}{c} -5.06-4 \\ \textbf{4f}^8_{7/2} \ \textbf{6s}^2_{1/2} \\ \hline k \ (\text{eV}) \\ \hline 1500 \\ 2.221+1 \\ 1.915 \\ 4.54-1 \\ -3.10-4 \\ 2.631+1 \\ 1.577 \\ 2.37-1 \\ 2.45-3 \\ \hline 6.087+1 \\ 1.569 \end{array}$	2000 1.435+1 1.921 3.32-1 -6.52-4 1.754+1 1.651 8.34-2 -2.07-3 3.810+1 1.661	3000 7.364+0 1.931 1.27-1 -1.07-3 9.035+0 1.690 -1.90-2 -3.63-3 1.818+1 1.731	4000 4.450+0 1.938 -9.51-3 -1.34-3 5.330+0 1.681 2.95-2 -3.20-3 1.022+1 1.745	5000 2.967+0 1.945 -9.36-2 -1.53-3 3.438+0 1.657 1.40-1 -1.57-3 6.358+0 1.737	6000 2.112+0 1.951 -1.38-1 -1.67-3 2.361+0 1.627 2.74-1 1.12-3 4.243+0 1.719	7000 1.576+0 1.956 -1.53-1 -1.78-3 1.698+0 1.594 4.14-1 4.81-3 2.980+0 1.696	8000 1.219+0 1.959 -1.47-1 -1.87-3 1.265+0 1.561 5.53-1 9.27-3 2.176+0 1.670	9000 9.683-1 1.962 -1.24-1 -1.94-3 9.698-1 1.528 6.88-1 1.44-2 1.638+0 1.642	10000 7.863- 1.964 -8.85- -2.01- 7.605- 1.495 8.17- 2.01-2
Z= 70, Yb: [X Shell $4s_{1/2}$ $E_b = 487.2$ eV $4p_{1/2}$ $E_b = 396.7$ eV $4p_{3/2}$	$ \begin{array}{c} \delta \\ \text{Ce]4f}_{5/2}^6 \\ \sigma \\ \beta \\ \gamma \\ \delta \\ \sigma \\ \sigma \end{array} $	$\begin{array}{c} -5.06-4 \\ \textbf{4f}^8_{7/2} \ \textbf{6s}^2_{1/2} \\ \hline k \ (\text{eV}) \\ \hline 1500 \\ \hline 2.221+1 \\ 1.915 \\ 4.54-1 \\ -3.10-4 \\ \hline 2.631+1 \\ 1.577 \\ 2.37-1 \\ 2.45-3 \\ \hline 6.087+1 \\ 1.569 \\ 1.40-1 \\ \end{array}$	2000 1.435+1 1.921 3.32-1 -6.52-4 1.754+1 1.651 8.34-2 -2.07-3 3.810+1 1.661 1.86-2	3000 7.364+0 1.931 1.27-1 -1.07-3 9.035+0 1.690 -1.90-2 -3.63-3 1.818+1 1.731 -3.98-2	4000 4.450+0 1.938 -9.51-3 -1.34-3 5.330+0 1.681 2.95-2 -3.20-3 1.022+1 1.745 3.77-2	5000 2.967+0 1.945 -9.36-2 -1.53-3 3.438+0 1.657 1.40-1 -1.57-3 6.358+0 1.737 1.71-1	6000 2.112+0 1.951 -1.38-1 -1.67-3 2.361+0 1.627 2.74-1 1.12-3 4.243+0 1.719 3.26-1	7000 1.576+0 1.956 -1.53-1 -1.78-3 1.698+0 1.594 4.14-1 4.81-3 2.980+0 1.696 4.84-1	8000 1.219+0 1.959 -1.47-1 -1.87-3 1.265+0 1.561 5.53-1 9.27-3 2.176+0 1.670 6.41-1	9000 9.683-1 1.962 -1.24-1 -1.94-3 9.698-1 1.528 6.88-1 1.44-2 1.638+0 1.642 7.91-1	10000 7.863- 1.964 -8.85- -2.01- 7.605- 1.495 8.17- 2.01-2 1.265+ 1.613 9.34-1
Z= 70, Yb: [X Shell $4s_{1/2}$ $E_b = 487.2 \text{ eV}$ $4p_{1/2}$ $E_b = 396.7 \text{ eV}$ $4p_{3/2}$ $E_b = 343.5 \text{ eV}$	δ (ce 4f _{5/2} 4) σ	$\begin{array}{c} -5.06-4 \\ \textbf{4f}^8_{7/2} \ \textbf{6s}^2_{1/2} \\ \hline k \ (\text{eV}) \\ \hline 1500 \\ 2.221+1 \\ 1.915 \\ 4.54-1 \\ -3.10-4 \\ 2.631+1 \\ 1.577 \\ 2.37-1 \\ 2.45-3 \\ \hline 6.087+1 \\ 1.569 \\ 1.40-1 \\ 2.24-3 \\ \end{array}$	2000 1.435+1 1.921 3.32-1 -6.52-4 1.754+1 1.651 8.34-2 -2.07-3 3.810+1 1.661 1.86-2 8.08-4	3000 7.364+0 1.931 1.27-1 -1.07-3 9.035+0 1.690 -1.90-2 -3.63-3 1.818+1 1.731 -3.98-2 3.87-3	4000 4.450+0 1.938 -9.51-3 -1.34-3 5.330+0 1.681 2.95-2 -3.20-3 1.022+1 1.745 3.77-2 7.11-3	5000 2.967+0 1.945 -9.36-2 -1.53-3 3.438+0 1.657 1.40-1 -1.57-3 6.358+0 1.737 1.71-1 9.93-3	6000 2.112+0 1.951 -1.38-1 -1.67-3 2.361+0 1.627 2.74-1 1.12-3 4.243+0 1.719 3.26-1 1.27-2	7000 1.576+0 1.956 -1.53-1 -1.78-3 1.698+0 1.594 4.14-1 4.81-3 2.980+0 1.696 4.84-1 1.56-2	8000 1.219+0 1.959 -1.47-1 -1.87-3 1.265+0 1.561 5.53-1 9.27-3 2.176+0 1.670 6.41-1 1.88-2	9000 9.683-1 1.962 -1.24-1 -1.94-3 9.698-1 1.528 6.88-1 1.44-2 1.638+0 1.642 7.91-1 2.24-2	10000 7.863- 1.964 -8.852.01- 7.605- 1.495 8.17-1 2.01-2 1.265+ 1.613 9.34-1 2.61-2
Z= 70, Yb: [X Shell $4s_{1/2}$ $E_b = 487.2 \text{ eV}$ $4p_{1/2}$ $E_b = 396.7 \text{ eV}$ $4p_{3/2}$ $E_b = 343.5 \text{ eV}$	$ \frac{\delta}{\delta e 4f_{5/2}^6 4} $ $ \frac{\sigma}{\beta} $ $ \frac{\beta}{\gamma} $ $ \frac{\delta}{\delta} $ $ \frac{\sigma}{\beta} $ $ \frac{\beta}{\gamma} $ $ \frac{\delta}{\delta} $ $ \frac{\sigma}{\beta} $ $ \frac{\beta}{\gamma} $ $ \frac{\delta}{\delta} $ $ \frac{\sigma}{\delta} $	$\begin{array}{c} -5.06-4 \\ \textbf{4f}^8_{7/2} \ \textbf{6s}^2_{1/2} \\ \hline k \ (\text{eV}) \\ \hline 1500 \\ \hline 2.221+1 \\ 1.915 \\ 4.54-1 \\ -3.10-4 \\ \hline 2.631+1 \\ 1.577 \\ 2.37-1 \\ 2.45-3 \\ \hline 6.087+1 \\ 1.569 \\ 1.40-1 \\ \end{array}$	2000 1.435+1 1.921 3.32-1 -6.52-4 1.754+1 1.651 8.34-2 -2.07-3 3.810+1 1.661 1.86-2	3000 7.364+0 1.931 1.27-1 -1.07-3 9.035+0 1.690 -1.90-2 -3.63-3 1.818+1 1.731 -3.98-2	4000 4.450+0 1.938 -9.51-3 -1.34-3 5.330+0 1.681 2.95-2 -3.20-3 1.022+1 1.745 3.77-2	5000 2.967+0 1.945 -9.36-2 -1.53-3 3.438+0 1.657 1.40-1 -1.57-3 6.358+0 1.737 1.71-1	6000 2.112+0 1.951 -1.38-1 -1.67-3 2.361+0 1.627 2.74-1 1.12-3 4.243+0 1.719 3.26-1	7000 1.576+0 1.956 -1.53-1 -1.78-3 1.698+0 1.594 4.14-1 4.81-3 2.980+0 1.696 4.84-1	8000 1.219+0 1.959 -1.47-1 -1.87-3 1.265+0 1.561 5.53-1 9.27-3 2.176+0 1.670 6.41-1	9000 9.683-1 1.962 -1.24-1 -1.94-3 9.698-1 1.528 6.88-1 1.44-2 1.638+0 1.642 7.91-1	10000 7.863- 1.964 -8.852.01- 7.605- 1.495 8.17- 2.01-2 1.265+ 1.613 9.34- 2.61-2
Z= 70, Yb: [X Shell $4s_{1/2}$ $E_b = 487.2 \text{ eV}$ $4p_{1/2}$ $E_b = 396.7 \text{ eV}$ $4p_{3/2}$ $E_b = 343.5 \text{ eV}$	δ (ce 4f _{5/2} 4) σ	$\begin{array}{c} -5.06-4 \\ \textbf{4f}^8_{7/2} \ \textbf{6s}^2_{1/2} \\ \hline k \ (\text{eV}) \\ \hline 1500 \\ \hline 2.221+1 \\ 1.915 \\ 4.54-1 \\ -3.10-4 \\ \hline 2.631+1 \\ 1.577 \\ 2.37-1 \\ 2.45-3 \\ \hline 6.087+1 \\ 1.569 \\ 1.40-1 \\ 2.24-3 \\ \hline 7.298+1 \\ \end{array}$	2000 1.435+1 1.921 3.32-1 -6.52-4 1.754+1 1.651 8.34-2 -2.07-3 3.810+1 1.661 1.86-2 8.08-4 3.961+1	3000 7.364+0 1.931 1.27-1 -1.07-3 9.035+0 1.690 -1.90-2 -3.63-3 1.818+1 1.731 -3.98-2 3.87-3 1.481+1	4000 4.450+0 1.938 -9.51-3 -1.34-3 5.330+0 1.681 2.95-2 -3.20-3 1.022+1 1.745 3.77-2 7.11-3 6.846+0	5000 2.967+0 1.945 -9.36-2 -1.53-3 3.438+0 1.657 1.40-1 -1.57-3 6.358+0 1.737 1.71-1 9.93-3 3.628+0	6000 2.112+0 1.951 -1.38-1 -1.67-3 2.361+0 1.627 2.74-1 1.12-3 4.243+0 1.719 3.26-1 1.27-2 2.112+0	7000 1.576+0 1.956 -1.53-1 -1.78-3 1.698+0 1.594 4.14-1 4.81-3 2.980+0 1.696 4.84-1 1.56-2 1.317+0	8000 1.219+0 1.959 -1.47-1 -1.87-3 1.265+0 1.561 5.53-1 9.27-3 2.176+0 1.670 6.41-1 1.88-2 8.654-1 1.075 1.28+0	9000 9.683-1 1.962 -1.24-1 -1.94-3 9.698-1 1.528 6.88-1 1.44-2 1.638+0 1.642 7.91-1 2.24-2 5.926-1	10000 7.863- 1.964 -8.852.01- 7.605- 1.495 8.17-1 2.01-2 1.265+ 1.613 9.34-1 2.61-2
Z= 70, Yb: [X Shell $4s_{1/2}$ $E_b = 487.2$ eV $4p_{1/2}$ $E_b = 396.7$ eV $4p_{3/2}$ $E_b = 343.5$ eV $4d_{3/2}$ $E_b = 4d_{3/2}$	$ \begin{array}{c} \delta \\ \text{Ce]4f}_{5/2}^{6} \cdot 4 \\ \hline \sigma \\ \beta \\ \gamma \\ \delta \\ \hline \sigma \\ \beta \\ \gamma \\ \delta \\ \hline \sigma \\ \beta \\ \gamma \\ \delta \\ \hline \sigma \\ \beta \\ \beta \\ \gamma \\ \delta \\ \hline \sigma \\ \beta \\ \beta$	$\begin{array}{c} -5.06-4 \\ \textbf{4f}^8_{7/2} \ \textbf{6s}^2_{1/2} \\ \hline k \ (\text{eV}) \\ \hline 1500 \\ \hline 2.221+1 \\ 1.915 \\ 4.54-1 \\ -3.10-4 \\ \hline 2.631+1 \\ 1.577 \\ 2.37-1 \\ 2.45-3 \\ \hline 6.087+1 \\ 1.569 \\ 1.40-1 \\ 2.24-3 \\ \hline 7.298+1 \\ 1.287 \\ \end{array}$	2000 1.435+1 1.921 3.32-1 -6.52-4 1.754+1 1.651 8.34-2 -2.07-3 3.810+1 1.661 1.86-2 8.08-4 3.961+1 1.358	3000 7.364+0 1.931 1.27-1 -1.07-3 9.035+0 1.690 -1.90-2 -3.63-3 1.818+1 1.731 -3.98-2 3.87-3 1.481+1 1.368	4000 4.450+0 1.938 -9.51-3 -1.34-3 5.330+0 1.681 2.95-2 -3.20-3 1.022+1 1.745 3.77-2 7.11-3 6.846+0 1.322	5000 2.967+0 1.945 -9.36-2 -1.53-3 3.438+0 1.657 1.40-1 -1.57-3 6.358+0 1.737 1.71-1 9.93-3 3.628+0 1.261	6000 2.112+0 1.951 -1.38-1 -1.67-3 2.361+0 1.627 2.74-1 1.12-3 4.243+0 1.719 3.26-1 1.27-2 2.112+0 1.198	7000 1.576+0 1.956 -1.53-1 -1.78-3 1.698+0 1.594 4.14-1 4.81-3 2.980+0 1.696 4.84-1 1.56-2 1.317+0 1.135	8000 1.219+0 1.959 -1.47-1 -1.87-3 1.265+0 1.561 5.53-1 9.27-3 2.176+0 1.670 6.41-1 1.88-2 8.654-1 1.075	9000 9.683-1 1.962 -1.24-1 -1.94-3 9.698-1 1.528 6.88-1 1.44-2 1.638+0 1.642 7.91-1 2.24-2 5.926-1 1.018	10000 7.863- 1.964 -8.852.01- 7.605- 1.495 8.17- 2.01-2 1.265+ 1.613 9.34- 2.61-2 4.197- 0.963 1.49+0
Z= 70, Yb: [X Shell $4s_{1/2}$ $E_b = 487.2$ eV $4p_{1/2}$ $E_b = 396.7$ eV $4p_{3/2}$ $E_b = 343.5$ eV $4d_{3/2}$ $E_b = 4d_{3/2}$	δ (c) 4f _{5/2} 4 σ σ σ σ σ σ σ σ σ σ σ σ σ σ σ σ σ σ	$\begin{array}{c} -5.06-4 \\ \textbf{4f}^8_{7/2} \ \textbf{6s}^2_{1/2} \\ \hline k \ (\text{eV}) \\ \hline 1500 \\ \hline 2.221+1 \\ 1.915 \\ 4.54-1 \\ -3.10-4 \\ \hline 2.631+1 \\ 1.577 \\ 2.37-1 \\ 2.45-3 \\ \hline 6.087+1 \\ 1.569 \\ 1.40-1 \\ 2.24-3 \\ \hline 7.298+1 \\ 1.287 \\ -3.59-2 \\ \end{array}$	2000 1.435+1 1.921 3.32-1 -6.52-4 1.754+1 1.651 8.34-2 -2.07-3 3.810+1 1.661 1.86-2 8.08-4 3.961+1 1.358 4.97-2	3000 7.364+0 1.931 1.27-1 -1.07-3 9.035+0 1.690 -1.90-2 -3.63-3 1.818+1 1.731 -3.98-2 3.87-3 1.481+1 1.368 3.11-1	4000 4.450+0 1.938 -9.51-3 -1.34-3 5.330+0 1.681 2.95-2 -3.20-3 1.022+1 1.745 3.77-2 7.11-3 6.846+0 1.322 5.69-1	5000 2.967+0 1.945 -9.36-2 -1.53-3 3.438+0 1.657 1.40-1 -1.57-3 6.358+0 1.737 1.71-1 9.93-3 3.628+0 1.261 7.93-1	6000 2.112+0 1.951 -1.38-1 -1.67-3 2.361+0 1.627 2.74-1 1.12-3 4.243+0 1.719 3.26-1 1.27-2 2.112+0 1.198 9.81-1	7000 1.576+0 1.956 -1.53-1 -1.78-3 1.698+0 1.594 4.14-1 4.81-3 2.980+0 1.696 4.84-1 1.56-2 1.317+0 1.135 1.14+0	8000 1.219+0 1.959 -1.47-1 -1.87-3 1.265+0 1.561 5.53-1 9.27-3 2.176+0 1.670 6.41-1 1.88-2 8.654-1 1.075 1.28+0	9000 9.683-1 1.962 -1.24-1 -1.94-3 9.698-1 1.528 6.88-1 1.44-2 1.638+0 1.642 7.91-1 2.24-2 5.926-1 1.018 1.39+0	10000 7.863- 1.964 -8.852.01- 7.605- 1.495 8.17- 2.01- 1.265+ 1.613 9.34- 2.61- 4.197- 0.963 1.49+0 1.82-
Z= 70, Yb: [X Shell $4s_{1/2}$ $E_b =$ 487.2 eV $4p_{1/2}$ $E_b =$ 396.7 eV $4p_{3/2}$ $E_b =$ 343.5 eV $4d_{3/2}$ $E_b =$ 198.1 eV $4d_{5/2}$ $E_b =$	δ (c) 4f _{5/2} 4 σ σ β γ δ σ β γ δ σ β γ δ σ β γ δ σ β γ δ σ β γ δ σ β γ δ σ β γ δ σ β γ δ σ β γ δ σ β γ δ σ β γ δ σ β γ δ σ β γ δ σ β γ δ σ β γ δ δ σ β γ δ δ σ β γ δ δ σ β γ δ δ σ β γ δ δ σ β γ δ δ σ β γ δ δ σ β γ δ δ σ β γ δ δ σ β γ δ δ σ β γ δ δ σ β γ δ δ σ β γ δ δ σ δ β γ δ δ σ δ β γ δ δ σ δ δ σ δ δ γ δ δ σ δ δ σ δ δ δ σ δ δ δ σ δ δ δ δ	$\begin{array}{c} -5.06-4 \\ \mathbf{4f_{7/2}^8 6s_{1/2}^2} \\ \hline k (\text{eV}) \\ \hline 1500 \\ 2.221+1 \\ 1.915 \\ 4.54-1 \\ -3.10-4 \\ 2.631+1 \\ 1.577 \\ 2.37-1 \\ 2.45-3 \\ \hline 6.087+1 \\ 1.569 \\ 1.40-1 \\ 2.24-3 \\ \hline 7.298+1 \\ 1.287 \\ -3.59-2 \\ 1.35-2 \\ \hline 1.044+2 \\ 1.324 \\ \end{array}$	2000 1.435+1 1.921 3.32-1 -6.52-4 1.754+1 1.651 8.34-2 -2.07-3 3.810+1 1.661 1.86-2 8.08-4 3.961+1 1.358 4.97-2 2.67-2 5.588+1 1.359	3000 7.364+0 1.931 1.27-1 -1.07-3 9.035+0 1.690 -1.90-2 -3.63-3 1.818+1 1.731 -3.98-2 3.87-3 1.481+1 1.368 3.11-1 4.87-2 2.053+1 1.329	4000 4.450+0 1.938 -9.51-3 -1.34-3 5.330+0 1.681 2.95-2 -3.20-3 1.022+1 1.745 3.77-2 7.11-3 6.846+0 1.322 5.69-1 6.82-2 9.380+0 1.262	5000 2.967+0 1.945 -9.36-2 -1.53-3 3.438+0 1.657 1.40-1 -1.57-3 6.358+0 1.737 1.71-1 9.93-3 3.628+0 1.261 7.93-1 8.74-2 4.923+0 1.189	6000 2.112+0 1.951 -1.38-1 -1.67-3 2.361+0 1.627 2.74-1 1.12-3 4.243+0 1.719 3.26-1 1.27-2 2.112+0 1.198 9.81-1 1.07-1 2.842+0 1.120	7000 1.576+0 1.956 -1.53-1 -1.78-3 1.698+0 1.594 4.14-1 4.81-3 2.980+0 1.696 4.84-1 1.56-2 1.317+0 1.135 1.14+0 1.26-1 1.760+0 1.055	8000 1.219+0 1.959 -1.47-1 -1.87-3 1.265+0 1.561 5.53-1 9.27-3 2.176+0 1.670 6.41-1 1.88-2 8.654-1 1.075 1.28+0 1.45-1 1.149+0 0.994	9000 9.683-1 1.962 -1.24-1 -1.94-3 9.698-1 1.528 6.88-1 1.44-2 1.638+0 1.642 7.91-1 2.24-2 5.926-1 1.018 1.39+0 1.64-1 7.819-1 0.938	10000 7.863- 1.964 -8.85 -2.01- 7.605- 1.495 8.17- 2.01- 1.265+ 1.613 9.34- 2.61- 4.197- 0.963 1.49+0 1.82- 5.506- 0.885
Z= 70, Yb: [X Shell $4s_{1/2}$ $E_b = 487.2 \text{ eV}$ $4p_{1/2}$ $E_b = 396.7 \text{ eV}$ $4p_{3/2}$ $E_b = 343.5 \text{ eV}$ $4d_{3/2}$ $E_b = 198.1 \text{ eV}$	δ (ce 4f _{5/2} 4) σ	$\begin{array}{c} -5.06-4 \\ \textbf{4f}^{8}_{7/2} \ \textbf{6s}^{2}_{1/2} \\ \hline k \ (\text{eV}) \\ \hline 1500 \\ 2.221+1 \\ 1.915 \\ 4.54-1 \\ -3.10-4 \\ 2.631+1 \\ 1.577 \\ 2.37-1 \\ 2.45-3 \\ \hline 6.087+1 \\ 1.569 \\ 1.40-1 \\ 2.24-3 \\ \hline 7.298+1 \\ 1.287 \\ -3.59-2 \\ 1.35-2 \\ \hline 1.044+2 \\ 1.324 \\ -2.69-2 \\ \end{array}$	2000 1.435+1 1.921 3.32-1 -6.52-4 1.754+1 1.651 8.34-2 -2.07-3 3.810+1 1.661 1.86-2 8.08-4 3.961+1 1.358 4.97-2 2.67-2 5.588+1 1.359 7.39-2	3000 7.364+0 1.931 1.27-1 -1.07-3 9.035+0 1.690 -1.90-2 -3.63-3 1.818+1 1.731 -3.98-2 3.87-3 1.481+1 1.368 3.11-1 4.87-2 2.053+1 1.329 3.44-1	4000 4.450+0 1.938 -9.51-3 -1.34-3 5.330+0 1.681 2.95-2 -3.20-3 1.022+1 1.745 3.77-2 7.11-3 6.846+0 1.322 5.69-1 6.82-2 9.380+0 1.262 5.97-1	5000 2.967+0 1.945 -9.36-2 -1.53-3 3.438+0 1.657 1.40-1 -1.57-3 6.358+0 1.737 1.71-1 9.93-3 3.628+0 1.261 7.93-1 8.74-2 4.923+0 1.189 8.09-1	6000 2.112+0 1.951 -1.38-1 -1.67-3 2.361+0 1.627 2.74-1 1.12-3 4.243+0 1.719 3.26-1 1.27-2 2.112+0 1.198 9.81-1 1.07-1 2.842+0 1.120 9.85-1	7000 1.576+0 1.956 -1.53-1 -1.78-3 1.698+0 1.594 4.14-1 4.81-3 2.980+0 1.696 4.84-1 1.56-2 1.317+0 1.135 1.14+0 1.26-1 1.760+0 1.055 1.13+0	8000 1.219+0 1.959 -1.47-1 -1.87-3 1.265+0 1.561 5.53-1 9.27-3 2.176+0 1.670 6.41-1 1.88-2 8.654-1 1.075 1.28+0 1.45-1 1.149+0 0.994 1.26+0	9000 9.683-1 1.962 -1.24-1 -1.94-3 9.698-1 1.528 6.88-1 1.44-2 1.638+0 1.642 7.91-1 2.24-2 5.926-1 1.018 1.39+0 1.64-1 7.819-1 0.938 1.37+0	10000 7.863- 1.964 -8.852.01- 7.605- 1.495 8.17- 2.01- 1.265+ 1.613 9.34- 2.61- 4.197- 0.963 1.49+0 1.82- 5.506- 0.885 1.46+0
Z= 70, Yb: [X Shell $4s_{1/2}$ $E_b =$ 487.2 eV $4p_{1/2}$ $E_b =$ 396.7 eV $4p_{3/2}$ $E_b =$ 343.5 eV $4d_{3/2}$ $E_b =$ 198.1 eV $4d_{5/2}$ $E_b =$ 184.9 eV	δ (ce 4f _{5/2} · c 4f _{5/2} · c 4f _{5/2} · c 4f _{5/2} · c 6 6 7 8 8	$\begin{array}{c} -5.06-4 \\ \textbf{4f}^{8}_{7/2} \ \textbf{6s}^{2}_{1/2} \\ \hline k \ (\text{eV}) \\ \hline 1500 \\ 2.221+1 \\ 1.915 \\ 4.54-1 \\ -3.10-4 \\ 2.631+1 \\ 1.577 \\ 2.37-1 \\ 2.45-3 \\ \hline 6.087+1 \\ 1.569 \\ 1.40-1 \\ 2.24-3 \\ \hline 7.298+1 \\ 1.287 \\ -3.59-2 \\ 1.35-2 \\ \hline 1.044+2 \\ 1.324 \\ -2.69-2 \\ 1.33-2 \\ \end{array}$	2000 1.435+1 1.921 3.32-1 -6.52-4 1.754+1 1.651 8.34-2 -2.07-3 3.810+1 1.661 1.86-2 8.08-4 3.961+1 1.358 4.97-2 2.67-2 5.588+1 1.359 7.39-2 2.56-2	3000 7.364+0 1.931 1.27-1 -1.07-3 9.035+0 1.690 -1.90-2 -3.63-3 1.818+1 1.731 -3.98-2 3.87-3 1.481+1 1.368 3.11-1 4.87-2 2.053+1 1.329 3.44-1 4.83-2	4000 4.450+0 1.938 -9.51-3 -1.34-3 5.330+0 1.681 2.95-2 -3.20-3 1.022+1 1.745 3.77-2 7.11-3 6.846+0 1.322 5.69-1 6.82-2 9.380+0 1.262 5.97-1 7.06-2	5000 2.967+0 1.945 -9.36-2 -1.53-3 3.438+0 1.657 1.40-1 -1.57-3 6.358+0 1.737 1.71-1 9.93-3 3.628+0 1.261 7.93-1 8.74-2 4.923+0 1.189 8.09-1 9.33-2	6000 2.112+0 1.951 -1.38-1 -1.67-3 2.361+0 1.627 2.74-1 1.12-3 4.243+0 1.719 3.26-1 1.27-2 2.112+0 1.198 9.81-1 1.07-1 2.842+0 1.120 9.85-1 1.16-1	7000 1.576+0 1.956 -1.53-1 -1.78-3 1.698+0 1.594 4.14-1 4.81-3 2.980+0 1.696 4.84-1 1.56-2 1.317+0 1.135 1.14+0 1.26-1 1.760+0 1.055 1.13+0 1.39-1	8000 1.219+0 1.959 -1.47-1 -1.87-3 1.265+0 1.561 5.53-1 9.27-3 2.176+0 1.670 6.41-1 1.88-2 8.654-1 1.075 1.28+0 1.45-1 1.149+0 0.994 1.26+0 1.61-1	9000 9.683-1 1.962 -1.24-1 -1.94-3 9.698-1 1.528 6.88-1 1.44-2 1.638+0 1.642 7.91-1 2.24-2 5.926-1 1.018 1.39+0 1.64-1 7.819-1 0.938 1.37+0 1.82-1	10000 7.863- 1.964 -8.85 -2.01- 7.605- 1.495 8.17- 2.01- 1.265+ 1.613 9.34- 2.61- 2.61- 0.963 1.49+0 0.885 1.46+0 2.03-
Z= 70, Yb: [X Shell $4s_{1/2}$ $E_b = 487.2 \text{ eV}$ $4p_{1/2}$ $E_b = 396.7 \text{ eV}$ $4p_{3/2}$ $E_b = 343.5 \text{ eV}$ $4d_{3/2}$ $E_b = 198.1 \text{ eV}$ $4d_{5/2}$ $E_b = 184.9 \text{ eV}$	δ (ce 4f _{5/2} 4) σ β γ δ σ β γ δ σ β γ δ δ σ β γ δ δ σ β γ δ δ σ β γ δ δ σ β γ δ δ σ β γ δ δ σ β γ δ δ σ β γ δ δ σ β γ δ δ σ β γ δ δ σ β γ δ δ σ β γ δ δ σ β γ δ δ σ β γ δ δ σ β γ δ δ σ β γ δ δ σ β γ δ δ σ β γ δ δ σ β γ δ δ σ σ β γ δ δ σ σ β γ δ δ σ σ β γ δ δ σ σ β γ δ δ σ σ β γ δ δ σ σ σ σ σ σ σ σ σ σ σ σ σ σ σ σ σ	$\begin{array}{c} -5.06-4 \\ \textbf{4f}^{8}_{7/2} \ \textbf{6s}^{2}_{1/2} \\ \hline k \ (\text{eV}) \\ \hline 1500 \\ 2.221+1 \\ 1.915 \\ 4.54-1 \\ -3.10-4 \\ 2.631+1 \\ 1.577 \\ 2.37-1 \\ 2.45-3 \\ \hline 6.087+1 \\ 1.569 \\ 1.40-1 \\ 2.24-3 \\ \hline 7.298+1 \\ 1.287 \\ -3.59-2 \\ 1.35-2 \\ \hline 1.044+2 \\ 1.324 \\ -2.69-2 \\ 1.33-2 \\ \hline 2.959+1 \\ \end{array}$	2000 1.435+1 1.921 3.32-1 -6.52-4 1.754+1 1.651 8.34-2 -2.07-3 3.810+1 1.661 1.86-2 8.08-4 3.961+1 1.358 4.97-2 2.67-2 5.588+1 1.359 7.39-2 2.56-2 1.100+1	3000 7.364+0 1.931 1.27-1 -1.07-3 9.035+0 1.690 -1.90-2 -3.63-3 1.818+1 1.731 -3.98-2 3.87-3 1.481+1 1.368 3.11-1 4.87-2 2.053+1 1.329 3.44-1 4.83-2 2.484+0	4000 4.450+0 1.938 -9.51-3 -1.34-3 5.330+0 1.681 2.95-2 -3.20-3 1.022+1 1.745 3.77-2 7.11-3 6.846+0 1.322 5.69-1 6.82-2 9.380+0 1.262 5.97-1 7.06-2 8.188-1	5000 2.967+0 1.945 -9.36-2 -1.53-3 3.438+0 1.657 1.40-1 -1.57-3 6.358+0 1.737 1.71-1 9.93-3 3.628+0 1.261 7.93-1 8.74-2 4.923+0 1.189 8.09-1 9.33-2 3.370-1	6000 2.112+0 1.951 -1.38-1 -1.67-3 2.361+0 1.627 2.74-1 1.12-3 4.243+0 1.719 3.26-1 1.27-2 2.112+0 1.198 9.81-1 1.07-1 2.842+0 1.120 9.85-1 1.16-1	7000 1.576+0 1.956 -1.53-1 -1.78-3 1.698+0 1.594 4.14-1 4.81-3 2.980+0 1.696 4.84-1 1.56-2 1.317+0 1.135 1.14+0 1.26-1 1.760+0 1.055 1.13+0 1.39-1 8.466-2	8000 1.219+0 1.959 -1.47-1 -1.87-3 1.265+0 1.561 5.53-1 9.27-3 2.176+0 1.670 6.41-1 1.88-2 8.654-1 1.075 1.28+0 1.45-1 1.149+0 0.994 1.26+0 1.61-1 4.818-2	9000 9.683-1 1.962 -1.24-1 -1.94-3 9.698-1 1.528 6.88-1 1.44-2 1.638+0 1.642 7.91-1 2.24-2 5.926-1 1.018 1.39+0 1.64-1 7.819-1 0.938 1.37+0 1.82-1 2.908-2	10000 7.863- 1.964 -8.852.01- 7.605- 1.495 8.17- 2.01- 1.265+ 1.613 9.34- 2.61- 4.197- 0.963 1.49+0 1.82- 5.506- 0.885 1.46+0 2.03- 1.840-
Z= 70, Yb: [X Shell $4s_{1/2}$ $E_b = 487.2 \text{ eV}$ $4p_{1/2}$ $E_b = 396.7 \text{ eV}$ $4p_{3/2}$ $E_b = 343.5 \text{ eV}$ $4d_{3/2}$ $E_b = 198.1 \text{ eV}$ $4d_{5/2}$ $E_b = 184.9 \text{ eV}$	δ (ce 4f _{5/2} 4) σ	$\begin{array}{c} -5.06-4 \\ \textbf{4f}^8_{7/2} \ \textbf{6s}^2_{1/2} \\ \hline k \ (\text{eV}) \\ \hline 1500 \\ 2.221+1 \\ 1.915 \\ 4.54-1 \\ -3.10-4 \\ 2.631+1 \\ 1.577 \\ 2.37-1 \\ 2.45-3 \\ \hline 6.087+1 \\ 1.569 \\ 1.40-1 \\ 2.24-3 \\ \hline 7.298+1 \\ 1.287 \\ -3.59-2 \\ 1.35-2 \\ \hline 1.044+2 \\ 1.324 \\ -2.69-2 \\ 1.33-2 \\ \hline 2.959+1 \\ 1.061 \\ \end{array}$	2000 1.435+1 1.921 3.32-1 -6.52-4 1.754+1 1.651 8.34-2 -2.07-3 3.810+1 1.661 1.86-2 8.08-4 3.961+1 1.358 4.97-2 2.67-2 5.588+1 1.359 7.39-2 2.56-2 1.100+1 1.029	3000 7.364+0 1.931 1.27-1 -1.07-3 9.035+0 1.690 -1.90-2 -3.63-3 1.818+1 1.731 -3.98-2 3.87-3 1.481+1 1.368 3.11-1 4.87-2 2.053+1 1.329 3.44-1 4.83-2 2.484+0 0.926	4000 4.450+0 1.938 -9.51-3 -1.34-3 5.330+0 1.681 2.95-2 -3.20-3 1.022+1 1.745 3.77-2 7.11-3 6.846+0 1.322 5.69-1 6.82-2 9.380+0 1.262 5.97-1 7.06-2 8.188-1 0.825	5000 2.967+0 1.945 -9.36-2 -1.53-3 3.438+0 1.657 1.40-1 -1.57-3 6.358+0 1.737 1.71-1 9.93-3 3.628+0 1.261 7.93-1 8.74-2 4.923+0 1.189 8.09-1 9.33-2 3.370-1 0.738	6000 2.112+0 1.951 -1.38-1 -1.67-3 2.361+0 1.627 2.74-1 1.12-3 4.243+0 1.719 3.26-1 1.27-2 2.112+0 1.198 9.81-1 1.07-1 2.842+0 1.120 9.85-1 1.16-1 1.605-1 0.665	7000 1.576+0 1.956 -1.53-1 -1.78-3 1.698+0 1.594 4.14-1 4.81-3 2.980+0 1.696 4.84-1 1.56-2 1.317+0 1.135 1.14+0 1.26-1 1.760+0 1.055 1.13+0 1.39-1 8.466-2 0.601	8000 1.219+0 1.959 -1.47-1 -1.87-3 1.265+0 1.561 5.53-1 9.27-3 2.176+0 1.670 6.41-1 1.88-2 8.654-1 1.075 1.28+0 1.45-1 1.149+0 0.994 1.26+0 1.61-1 4.818-2 0.546	9000 9.683-1 1.962 -1.24-1 -1.94-3 9.698-1 1.528 6.88-1 1.44-2 1.638+0 1.642 7.91-1 2.24-2 5.926-1 1.018 1.39+0 1.64-1 7.819-1 0.938 1.37+0 1.82-1 2.908-2 0.495	10000 7.863- 1.964 -8.852.01- 7.605- 1.495 8.17- 2.01- 1.265+ 1.613 9.34- 2.61- 4.197- 0.963 1.49+0 1.82- 5.506- 0.885 1.46+0 2.03- 1.840- 0.450
Z= 70, Yb: [X Shell $4s_{1/2}$ $E_b = 487.2 \text{ eV}$ $4p_{1/2}$ $E_b = 396.7 \text{ eV}$ $4p_{3/2}$ $E_b = 343.5 \text{ eV}$ $4d_{3/2}$ $E_b = 198.1 \text{ eV}$ $4d_{5/2}$ $E_b = 184.9 \text{ eV}$	$\begin{array}{c} \delta \\ \text{Ce} \mathbf{4f_{5/2}^6} \\ \\ \sigma \\ \beta \\ \gamma \\ \delta \\ \\ \sigma \\ \beta \\ \gamma \\ \delta \\ \\ \sigma \\ \beta \\ \gamma \\ \delta \\ \\ \sigma \\ \beta \\ \gamma \\ \delta \\ \\ \sigma \\ \beta \\ \gamma \\ \delta \\ \\ \sigma \\ \beta \\ \gamma \\ \delta \\ \\ \sigma \\ \beta \\ \gamma \\ \delta \\ \\ \sigma \\ \beta \\ \gamma \\ \delta \\ \\ \sigma \\ \beta \\ \gamma \\ \delta \\ \\ \sigma \\ \beta \\ \gamma \\ \delta \\ \\ \sigma \\ \beta \\ \gamma \\ \delta \\ \\ \sigma \\ \beta \\ \gamma \\ \delta \\ \\ \sigma \\ \beta \\ \gamma \\ \delta \\ \\ \sigma \\ \beta \\ \gamma \\ \delta \\ \\ \sigma \\ \sigma \\ \beta \\ \gamma \\ \delta \\ \\ \sigma \\ \sigma \\ \beta \\ \gamma \\ \delta \\ \\ \sigma \\ \sigma \\ \beta \\ \gamma \\ \delta \\ \\ \sigma \\ \sigma \\ \beta \\ \gamma \\ \delta \\ \\ \sigma \\ \sigma \\ \delta \\ \sigma \\ \sigma \\ \phi \\ \delta \\ \sigma \\ \sigma \\ \phi \\ \delta \\ \sigma \\ \sigma \\ \phi \\ \sigma \\ \sigma \\ \sigma \\ \sigma \\ \sigma \\ \sigma \\ \sigma$	$\begin{array}{c} -5.06-4 \\ \textbf{4f}^8_{7/2} \ \textbf{6s}^2_{1/2} \\ \hline k \ (\text{eV}) \\ \hline 1500 \\ \hline 2.221+1 \\ 1.915 \\ 4.54-1 \\ -3.10-4 \\ \hline 2.631+1 \\ 1.577 \\ 2.37-1 \\ 2.45-3 \\ \hline 6.087+1 \\ 1.569 \\ 1.40-1 \\ 2.24-3 \\ \hline 7.298+1 \\ 1.287 \\ -3.59-2 \\ 1.35-2 \\ \hline 1.044+2 \\ 1.324 \\ -2.69-2 \\ 1.33-2 \\ \hline 2.959+1 \\ 1.061 \\ 3.60-1 \\ \end{array}$	2000 1.435+1 1.921 3.32-1 -6.52-4 1.754+1 1.651 8.34-2 -2.07-3 3.810+1 1.661 1.86-2 8.08-4 3.961+1 1.358 4.97-2 2.67-2 5.588+1 1.359 7.39-2 2.56-2 1.100+1 1.029 5.20-1	3000 7.364+0 1.931 1.27-1 -1.07-3 9.035+0 1.690 -1.90-2 -3.63-3 1.818+1 1.731 -3.98-2 3.87-3 1.481+1 1.368 3.11-1 4.87-2 2.053+1 1.329 3.44-1 4.83-2 2.484+0 0.926 7.63-1	4000 4.450+0 1.938 -9.51-3 -1.34-3 5.330+0 1.681 2.95-2 -3.20-3 1.022+1 1.745 3.77-2 7.11-3 6.846+0 1.322 5.69-1 6.82-2 9.380+0 1.262 5.97-1 7.06-2 8.188-1 0.825 9.28-1	5000 2.967+0 1.945 -9.36-2 -1.53-3 3.438+0 1.657 1.40-1 -1.57-3 6.358+0 1.737 1.71-1 9.93-3 3.628+0 1.261 7.93-1 8.74-2 4.923+0 1.189 8.09-1 9.33-2 3.370-1 0.738 1.05+0	6000 2.112+0 1.951 -1.38-1 -1.67-3 2.361+0 1.627 2.74-1 1.12-3 4.243+0 1.719 3.26-1 1.27-2 2.112+0 1.198 9.81-1 1.07-1 2.842+0 1.120 9.85-1 1.16-1 1.605-1 0.665 1.13+0	7000 1.576+0 1.956 -1.53-1 -1.78-3 1.698+0 1.594 4.14-1 4.81-3 2.980+0 1.696 4.84-1 1.56-2 1.317+0 1.135 1.14+0 1.26-1 1.760+0 1.055 1.13+0 1.39-1 8.466-2 0.601 1.20+0	8000 1.219+0 1.959 -1.47-1 -1.87-3 1.265+0 1.561 5.53-1 9.27-3 2.176+0 1.670 6.41-1 1.88-2 8.654-1 1.075 1.28+0 1.45-1 1.149+0 0.994 1.26+0 1.61-1 4.818-2 0.546 1.26+0	9000 9.683-1 1.962 -1.24-1 -1.94-3 9.698-1 1.528 6.88-1 1.44-2 1.638+0 1.642 7.91-1 2.24-2 5.926-1 1.018 1.39+0 1.64-1 7.819-1 0.938 1.37+0 1.82-1 2.908-2 0.495 1.31+0	10000 7.863- 1.964 -8.852.01- 7.605- 1.495 8.17- 2.01- 1.265+ 1.613 9.34- 2.61- 4.197- 0.963 1.49+0 1.82- 5.506- 0.885 1.46+0 2.03- 1.840- 0.450 1.35+0
Z= 70, Yb: [X Shell $4s_{1/2}$ $E_b = 487.2 \text{ eV}$ $4p_{1/2}$ $E_b = 396.7 \text{ eV}$ $4p_{3/2}$ $E_b = 343.5 \text{ eV}$ $4d_{3/2}$ $E_b = 198.1 \text{ eV}$ $4d_{5/2}$ $E_b = 184.9 \text{ eV}$ $4f_{5/2}$ $E_b = 7.0 \text{ eV}$	δ (c) 4f _{5/2} 4 σ σ β γ δ σ β γ δ σ β γ δ σ β γ δ σ β γ δ σ β γ δ σ β γ δ δ σ δ β γ δ δ σ δ β γ δ δ σ δ β γ δ δ σ δ β γ δ δ σ δ β γ δ δ σ δ δ δ σ δ δ δ δ σ δ δ δ δ δ δ δ	$\begin{array}{c} -5.06-4 \\ \textbf{4f}^8_{7/2} \ \textbf{6s}^2_{1/2} \\ \hline k \ (\text{eV}) \\ \hline 1500 \\ 2.221+1 \\ 1.915 \\ 4.54-1 \\ -3.10-4 \\ 2.631+1 \\ 1.577 \\ 2.37-1 \\ 2.45-3 \\ \hline 6.087+1 \\ 1.569 \\ 1.40-1 \\ 2.24-3 \\ \hline 7.298+1 \\ 1.287 \\ -3.59-2 \\ 1.35-2 \\ 1.044+2 \\ 1.324 \\ -2.69-2 \\ 1.33-2 \\ \hline 2.959+1 \\ 1.061 \\ 3.60-1 \\ 9.91-2 \\ \end{array}$	2000 1.435+1 1.921 3.32-1 -6.52-4 1.754+1 1.651 8.34-2 -2.07-3 3.810+1 1.661 1.86-2 8.08-4 3.961+1 1.358 4.97-2 2.67-2 5.588+1 1.359 7.39-2 2.56-2 1.100+1 1.029 5.20-1 1.25-1	3000 7.364+0 1.931 1.27-1 -1.07-3 9.035+0 1.690 -1.90-2 -3.63-3 1.818+1 1.731 -3.98-2 3.87-3 1.481+1 1.368 3.11-1 4.87-2 2.053+1 1.329 3.44-1 4.83-2 2.484+0 0.926 7.63-1 1.73-1	4000 4.450+0 1.938 -9.51-3 -1.34-3 5.330+0 1.681 2.95-2 -3.20-3 1.022+1 1.745 3.77-2 7.11-3 6.846+0 1.322 5.69-1 6.82-2 9.380+0 1.262 5.97-1 7.06-2 8.188-1 0.825 9.28-1 2.18-1	5000 2.967+0 1.945 -9.36-2 -1.53-3 3.438+0 1.657 1.40-1 -1.57-3 6.358+0 1.737 1.71-1 9.93-3 3.628+0 1.261 7.93-1 8.74-2 4.923+0 1.189 8.09-1 9.33-2 3.370-1 0.738 1.05+0 2.62-1	6000 2.112+0 1.951 -1.38-1 -1.67-3 2.361+0 1.627 2.74-1 1.12-3 4.243+0 1.719 3.26-1 1.27-2 2.112+0 1.198 9.81-1 1.07-1 2.842+0 1.120 9.85-1 1.16-1 1.605-1 0.665 1.13+0 3.02-1	7000 1.576+0 1.956 -1.53-1 -1.78-3 1.698+0 1.594 4.14-1 4.81-3 2.980+0 1.696 4.84-1 1.56-2 1.317+0 1.135 1.14+0 1.26-1 1.760+0 1.055 1.13+0 1.39-1 8.466-2 0.601 1.20+0 3.40-1	8000 1.219+0 1.959 -1.47-1 -1.87-3 1.265+0 1.561 5.53-1 9.27-3 2.176+0 1.670 6.41-1 1.88-2 8.654-1 1.075 1.28+0 1.45-1 1.149+0 0.994 1.26+0 1.61-1 4.818-2 0.546 1.26+0 3.75-1	9000 9.683-1 1.962 -1.24-1 -1.94-3 9.698-1 1.528 6.88-1 1.44-2 1.638+0 1.642 7.91-1 2.24-2 5.926-1 1.018 1.39+0 1.64-1 7.819-1 0.938 1.37+0 1.82-1 2.908-2 0.495 1.31+0 4.08-1	10000 7.863- 1.964 -8.852.01- 7.605- 1.495 8.17- 2.01- 1.265+ 1.613 9.34- 2.61- 4.197- 0.963 1.49+0 1.82- 5.506- 0.885 1.4640 2.03- 1.840- 0.450 1.35+0 4.40-
Z= 70, Yb: [X Shell $4s_{1/2}$ $E_b = 487.2 \text{ eV}$ $4p_{1/2}$ $E_b = 396.7 \text{ eV}$ $4p_{3/2}$ $E_b = 343.5 \text{ eV}$ $4d_{3/2}$ $E_b = 198.1 \text{ eV}$ $4d_{5/2}$ $E_b = 184.9 \text{ eV}$ $4f_{5/2}$ $E_b = 7.0 \text{ eV}$	$\begin{array}{c} \delta \\ \delta \\ \text{Ce} \mathbf{4f_{5/2}^c} \\ \delta \\ \\ \sigma \\ \beta \\ \gamma \\ \delta \\ \\ \sigma \\ \beta \\ \gamma \\ \delta \\ \\ \sigma \\ \beta \\ \gamma \\ \delta \\ \\ \sigma \\ \beta \\ \gamma \\ \delta \\ \\ \sigma \\ \beta \\ \gamma \\ \delta \\ \\ \sigma \\ \beta \\ \gamma \\ \delta \\ \\ \sigma \\ \beta \\ \gamma \\ \delta \\ \\ \sigma \\ \\ \sigma \\ \beta \\ \gamma \\ \delta \\ \\ \sigma \\ \\ \sigma \\ \\ \beta \\ \gamma \\ \delta \\ \\ \sigma \\ \\ \sigma \\ \\ \beta \\ \gamma \\ \delta \\ \\ \sigma \\ \\ \sigma \\ \\ \sigma \\ \\ \beta \\ \\ \gamma \\ \delta \\ \\ \sigma \\ \\ \sigma \\ \sigma \\ \sigma \\ \\ \sigma \\ \sigma$	$\begin{array}{c} -5.06-4 \\ \textbf{4f}^8_{7/2} \ \textbf{6s}^2_{1/2} \\ \hline k \ (\text{eV}) \\ \hline 1500 \\ \hline 2.221+1 \\ 1.915 \\ 4.54-1 \\ -3.10-4 \\ \hline 2.631+1 \\ 1.577 \\ 2.37-1 \\ 2.45-3 \\ \hline 6.087+1 \\ 1.569 \\ 1.40-1 \\ 2.24-3 \\ \hline 7.298+1 \\ 1.287 \\ -3.59-2 \\ 1.35-2 \\ \hline 1.044+2 \\ 1.324 \\ -2.69-2 \\ 1.33-2 \\ \hline 2.959+1 \\ 1.061 \\ 3.60-1 \\ 9.91-2 \\ \hline 3.719+1 \\ \end{array}$	2000 1.435+1 1.921 3.32-1 -6.52-4 1.754+1 1.651 8.34-2 -2.07-3 3.810+1 1.661 1.86-2 8.08-4 3.961+1 1.358 4.97-2 2.67-2 5.588+1 1.359 7.39-2 2.56-2 1.100+1 1.029 5.20-1 1.25-1 1.377+1	3000 7.364+0 1.931 1.27-1 -1.07-3 9.035+0 1.690 -1.90-2 -3.63-3 1.818+1 1.731 -3.98-2 3.87-3 1.481+1 1.368 3.11-1 4.87-2 2.053+1 1.329 3.44-1 4.83-2 2.484+0 0.926 7.63-1 1.73-1 3.089+0	4000 4.450+0 1.938 -9.51-3 -1.34-3 5.330+0 1.681 2.95-2 -3.20-3 1.022+1 1.745 3.77-2 7.11-3 6.846+0 1.322 5.69-1 6.82-2 9.380+0 1.262 5.97-1 7.06-2 8.188-1 0.825 9.28-1 2.18-1 1.012+0	5000 2.967+0 1.945 -9.36-2 -1.53-3 3.438+0 1.657 1.40-1 -1.57-3 6.358+0 1.737 1.71-1 9.93-3 3.628+0 1.261 7.93-1 8.74-2 4.923+0 1.189 8.09-1 9.33-2 3.370-1 0.738 1.05+0 2.62-1 4.146-1	6000 2.112+0 1.951 -1.38-1 -1.67-3 2.361+0 1.627 2.74-1 1.12-3 4.243+0 1.719 3.26-1 1.27-2 2.112+0 1.198 9.81-1 1.07-1 2.842+0 1.120 9.85-1 1.16-1 1.605-1 0.665 1.13+0 3.02-1	7000 1.576+0 1.956 -1.53-1 -1.78-3 1.698+0 1.594 4.14-1 4.81-3 2.980+0 1.696 4.84-1 1.56-2 1.317+0 1.135 1.14+0 1.26-1 1.760+0 1.055 1.13+0 1.39-1 8.466-2 0.601 1.20+0 3.40-1 1.033-1	8000 1.219+0 1.959 -1.47-1 -1.87-3 1.265+0 1.561 5.53-1 9.27-3 2.176+0 1.670 6.41-1 1.88-2 8.654-1 1.075 1.28+0 1.45-1 1.149+0 0.994 1.26+0 1.61-1 4.818-2 0.546 1.26+0 3.75-1 5.856-2	9000 9.683-1 1.962 -1.24-1 -1.94-3 9.698-1 1.528 6.88-1 1.44-2 1.638+0 1.642 7.91-1 2.24-2 5.926-1 1.018 1.39+0 1.64-1 7.819-1 0.938 1.37+0 1.82-1 2.908-2 0.495 1.31+0 4.08-1 3.524-2	10000 7.863- 1.964 -8.85 -2.01 7.605- 1.495 8.17- 2.01-: 1.265+ 1.613 9.34- 2.61-: 4.197- 0.963 1.49+0 1.82- 5.506- 0.885 1.46+0 2.03- 1.840- 0.450 1.35+0 4.40-
Z= 70, Yb: [X Shell $4s_{1/2}$ $E_b = 487.2 \text{ eV}$ $4p_{1/2}$ $E_b = 396.7 \text{ eV}$ $4d_{3/2}$ $E_b = 198.1 \text{ eV}$ $4d_{5/2}$ $E_b = 184.9 \text{ eV}$ $4f_{5/2}$ $E_b = 7.0 \text{ eV}$	$\begin{array}{c} \delta \\ \delta \\ \text{(e)} 4f_{5/2}^6 \\ \delta \\ \\ \sigma \\ \beta \\ \gamma \\ \delta \\ \\ \sigma \\ \beta \\ \gamma \\ \delta \\ \\ \sigma \\ \beta \\ \gamma \\ \delta \\ \\ \sigma \\ \beta \\ \gamma \\ \delta \\ \\ \sigma \\ \beta \\ \gamma \\ \delta \\ \\ \sigma \\ \beta \\ \gamma \\ \delta \\ \\ \sigma \\ \beta \\ \gamma \\ \delta \\ \\ \sigma \\ \beta \\ \gamma \\ \delta \\ \\ \sigma \\ \\ \beta \\ \gamma \\ \delta \\ \\ \sigma \\ \\ \sigma \\ \beta \\ \gamma \\ \delta \\ \\ \sigma \\ \\ \sigma \\ \\ \beta \\ \gamma \\ \delta \\ \\ \sigma \\ \sigma \\ \sigma \\ \sigma \\ \sigma \\ \sigma \\ \sigma \\ \sigma \\ \sigma \\ \\ \sigma \\ \\ \sigma \\ \\ \sigma \\ \sigma \\ \sigma \\ \sigma \\ \sigma \\ \sigma \\ \sigma \\ \sigma \\ \sigma \\ \sigma \\ \\ \sigma \\ \\ \sigma \\ \\ \sigma \\ \sigma \\ \\ \sigma \\ \sigma \\ \\ \sigma \\ \sigma \\ \sigma \\ \\ \sigma \\ \sigma \\ \\ \sigma \\ \sigma \\ \sigma \\ \\ \sigma \\ \sigma \\ \\ \sigma \\ \sigma \\ \sigma \\ \\ \sigma \\ \sigma \\ \sigma \\ \sigma \\ \sigma \\ \\ \sigma \\$	$\begin{array}{c} -5.06-4 \\ \textbf{4f}^8_{7/2} \ \textbf{6s}^2_{1/2} \\ \hline k \ (\text{eV}) \\ \hline 1500 \\ 2.221+1 \\ 1.915 \\ 4.54-1 \\ -3.10-4 \\ 2.631+1 \\ 1.577 \\ 2.37-1 \\ 2.45-3 \\ \hline 6.087+1 \\ 1.569 \\ 1.40-1 \\ 2.24-3 \\ \hline 7.298+1 \\ 1.287 \\ -3.59-2 \\ 1.35-2 \\ 1.044+2 \\ 1.324 \\ -2.69-2 \\ 1.33-2 \\ \hline 2.959+1 \\ 1.061 \\ 3.60-1 \\ 9.91-2 \\ \end{array}$	2000 1.435+1 1.921 3.32-1 -6.52-4 1.754+1 1.651 8.34-2 -2.07-3 3.810+1 1.661 1.86-2 8.08-4 3.961+1 1.358 4.97-2 2.67-2 5.588+1 1.359 7.39-2 2.56-2 1.100+1 1.029 5.20-1 1.25-1 1.377+1 1.020	3000 7.364+0 1.931 1.27-1 -1.07-3 9.035+0 1.690 -1.90-2 -3.63-3 1.818+1 1.731 -3.98-2 3.87-3 1.481+1 1.368 3.11-1 4.87-2 2.053+1 1.329 3.44-1 4.83-2 2.484+0 0.926 7.63-1 1.73-1 3.089+0 0.915	4000 4.450+0 1.938 -9.51-3 -1.34-3 5.330+0 1.681 2.95-2 -3.20-3 1.022+1 1.745 3.77-2 7.11-3 6.846+0 1.322 5.69-1 6.82-2 9.380+0 1.262 5.97-1 7.06-2 8.188-1 0.825 9.28-1 2.18-1	5000 2.967+0 1.945 -9.36-2 -1.53-3 3.438+0 1.657 1.40-1 -1.57-3 6.358+0 1.737 1.71-1 9.93-3 3.628+0 1.261 7.93-1 8.74-2 4.923+0 1.189 8.09-1 9.33-2 3.370-1 0.738 1.05+0 2.62-1 4.146-1 0.735	6000 2.112+0 1.951 -1.38-1 -1.67-3 2.361+0 1.627 2.74-1 1.12-3 4.243+0 1.719 3.26-1 1.27-2 2.112+0 1.198 9.81-1 1.07-1 2.842+0 1.120 9.85-1 1.16-1 1.605-1 0.665 1.13+0 3.02-1 1.965-1 0.666	7000 1.576+0 1.956 -1.53-1 -1.78-3 1.698+0 1.594 4.14-1 4.81-3 2.980+0 1.696 4.84-1 1.56-2 1.317+0 1.135 1.14+0 1.26-1 1.760+0 1.055 1.13+0 1.39-1 8.466-2 0.601 1.20+0 3.40-1 1.033-1 0.606	8000 1.219+0 1.959 -1.47-1 -1.87-3 1.265+0 1.561 5.53-1 9.27-3 2.176+0 1.670 6.41-1 1.88-2 8.654-1 1.075 1.28+0 1.45-1 1.149+0 0.994 1.26+0 1.61-1 4.818-2 0.546 1.26+0 3.75-1	9000 9.683-1 1.962 -1.24-1 -1.94-3 9.698-1 1.528 6.88-1 1.44-2 1.638+0 1.642 7.91-1 2.24-2 5.926-1 1.018 1.39+0 1.64-1 7.819-1 0.938 1.37+0 1.82-1 2.908-2 0.495 1.31+0 4.08-1 3.524-2 0.508	10000 7.863- 1.964 -8.852.01- 7.605- 1.495 8.17- 2.01- 1.265+ 1.613 9.34- 2.61- 2.61- 5.506- 0.885 1.46+0 2.03- 1.840- 0.450 1.35+0 4.40- 2.223- 0.466
Z= 70, Yb: [X] Shell $4s_{1/2}$ $E_b = 487.2 \text{ eV}$ $4p_{1/2}$ $E_b = 396.7 \text{ eV}$ $4p_{3/2}$ $E_b = 198.1 \text{ eV}$ $4d_{5/2}$ $E_b = 184.9 \text{ eV}$ $4f_{5/2}$ $E_b = 7.0 \text{ eV}$	$\begin{array}{c} \delta \\ \delta \\ \text{Ce} \mathbf{4f_{5/2}^c} \\ \delta \\ \\ \sigma \\ \beta \\ \gamma \\ \delta \\ \\ \sigma \\ \beta \\ \gamma \\ \delta \\ \\ \sigma \\ \beta \\ \gamma \\ \delta \\ \\ \sigma \\ \beta \\ \gamma \\ \delta \\ \\ \sigma \\ \beta \\ \gamma \\ \delta \\ \\ \sigma \\ \beta \\ \gamma \\ \delta \\ \\ \sigma \\ \beta \\ \gamma \\ \delta \\ \\ \sigma \\ \\ \sigma \\ \beta \\ \gamma \\ \delta \\ \\ \sigma \\ \\ \sigma \\ \\ \beta \\ \gamma \\ \delta \\ \\ \sigma \\ \\ \sigma \\ \\ \beta \\ \gamma \\ \delta \\ \\ \sigma \\ \\ \sigma \\ \\ \sigma \\ \\ \beta \\ \\ \gamma \\ \delta \\ \\ \sigma \\ \\ \sigma \\ \sigma \\ \sigma \\ \\ \sigma \\ \sigma$	$\begin{array}{c} -5.06-4 \\ \textbf{4f}^8_{7/2} \ \textbf{6s}^2_{1/2} \\ \hline k \ (\text{eV}) \\ \hline 1500 \\ \hline 2.221+1 \\ 1.915 \\ 4.54-1 \\ -3.10-4 \\ \hline 2.631+1 \\ 1.577 \\ 2.37-1 \\ 2.45-3 \\ \hline 6.087+1 \\ 1.569 \\ 1.40-1 \\ 2.24-3 \\ \hline 7.298+1 \\ 1.287 \\ -3.59-2 \\ 1.35-2 \\ \hline 1.044+2 \\ 1.324 \\ -2.69-2 \\ 1.33-2 \\ \hline 2.959+1 \\ 1.061 \\ 3.60-1 \\ 9.91-2 \\ \hline 3.719+1 \\ 1.056 \\ \end{array}$	2000 1.435+1 1.921 3.32-1 -6.52-4 1.754+1 1.651 8.34-2 -2.07-3 3.810+1 1.661 1.86-2 8.08-4 3.961+1 1.358 4.97-2 2.67-2 5.588+1 1.359 7.39-2 2.56-2 1.100+1 1.029 5.20-1 1.25-1 1.377+1	3000 7.364+0 1.931 1.27-1 -1.07-3 9.035+0 1.690 -1.90-2 -3.63-3 1.818+1 1.731 -3.98-2 3.87-3 1.481+1 1.368 3.11-1 4.87-2 2.053+1 1.329 3.44-1 4.83-2 2.484+0 0.926 7.63-1 1.73-1 3.089+0	4000 4.450+0 1.938 -9.51-3 -1.34-3 5.330+0 1.681 2.95-2 -3.20-3 1.022+1 1.745 3.77-2 7.11-3 6.846+0 1.322 5.69-1 6.82-2 9.380+0 1.262 5.97-1 7.06-2 8.188-1 0.825 9.28-1 2.18-1 1.012+0 0.817	5000 2.967+0 1.945 -9.36-2 -1.53-3 3.438+0 1.657 1.40-1 -1.57-3 6.358+0 1.737 1.71-1 9.93-3 3.628+0 1.261 7.93-1 8.74-2 4.923+0 1.189 8.09-1 9.33-2 3.370-1 0.738 1.05+0 2.62-1 4.146-1	6000 2.112+0 1.951 -1.38-1 -1.67-3 2.361+0 1.627 2.74-1 1.12-3 4.243+0 1.719 3.26-1 1.27-2 2.112+0 1.198 9.81-1 1.07-1 2.842+0 1.120 9.85-1 1.16-1 1.605-1 0.665 1.13+0 3.02-1	7000 1.576+0 1.956 -1.53-1 -1.78-3 1.698+0 1.594 4.14-1 4.81-3 2.980+0 1.696 4.84-1 1.56-2 1.317+0 1.135 1.14+0 1.26-1 1.760+0 1.055 1.13+0 1.39-1 8.466-2 0.601 1.20+0 3.40-1 1.033-1	8000 1.219+0 1.959 -1.47-1 -1.87-3 1.265+0 1.561 5.53-1 9.27-3 2.176+0 1.670 6.41-1 1.88-2 8.654-1 1.075 1.28+0 1.45-1 1.149+0 0.994 1.26+0 1.61-1 4.818-2 0.546 1.26+0 3.75-1 5.856-2 0.554	9000 9.683-1 1.962 -1.24-1 -1.94-3 9.698-1 1.528 6.88-1 1.44-2 1.638+0 1.642 7.91-1 2.24-2 5.926-1 1.018 1.39+0 1.64-1 7.819-1 0.938 1.37+0 1.82-1 2.908-2 0.495 1.31+0 4.08-1 3.524-2	10000 7.863- 1.964 -8.852.01- 7.605- 1.495 8.17- 2.01- 1.265+ 1.613 9.34- 2.61- 2.61- 5.506- 0.885 1.46+0 2.03- 1.840- 0.450 1.35+0 4.40- 2.223- 0.466 1.34+0
Z=70, Yb: [X Shell $4s_{1/2}$ $E_b =$ 487.2 eV $4p_{1/2}$ $E_b =$ 396.7 eV $4p_{3/2}$ $E_b =$ 343.5 eV $4d_{3/2}$ $E_b =$ 198.1 eV $4d_{5/2}$ $E_b =$ 184.9 eV $4f_{5/2}$ $E_b =$ 7.0 eV	δ (c) 4f _{5/2} 4 σ σ σ σ σ σ σ σ σ σ σ σ σ σ σ σ σ σ	$\begin{array}{c} -5.06-4 \\ \textbf{4f}^{8}_{7/2} \ \textbf{6s}^{2}_{1/2} \\ \hline k \ (\text{eV}) \\ \hline 1500 \\ 2.221+1 \\ 1.915 \\ 4.54-1 \\ -3.10-4 \\ 2.631+1 \\ 1.577 \\ 2.37-1 \\ 2.45-3 \\ \hline 6.087+1 \\ 1.569 \\ 1.40-1 \\ 2.24-3 \\ \hline 7.298+1 \\ 1.287 \\ -3.59-2 \\ 1.35-2 \\ \hline 1.044+2 \\ 1.324 \\ -2.69-2 \\ 1.33-2 \\ \hline 2.959+1 \\ 1.061 \\ 3.60-1 \\ 9.91-2 \\ \hline 3.719+1 \\ 1.056 \\ 3.68-1 \\ 9.90-2 \\ \end{array}$	2000 1.435+1 1.921 3.32-1 -6.52-4 1.754+1 1.651 8.34-2 -2.07-3 3.810+1 1.661 1.86-2 8.08-4 3.961+1 1.358 4.97-2 2.67-2 5.588+1 1.359 7.39-2 2.56-2 1.100+1 1.029 5.20-1 1.25-1 1.377+1 1.020 5.29-1 1.25-1	3000 7.364+0 1.931 1.27-1 -1.07-3 9.035+0 1.690 -1.90-2 -3.63-3 1.818+1 1.731 -3.98-2 3.87-3 1.481+1 1.368 3.11-1 4.87-2 2.053+1 1.329 3.44-1 4.83-2 2.484+0 0.926 7.63-1 1.73-1 3.089+0 0.915 7.72-1 1.74-1	4000 4.450+0 1.938 -9.51-3 -1.34-3 5.330+0 1.681 2.95-2 -3.20-3 1.022+1 1.745 3.77-2 7.11-3 6.846+0 1.322 5.69-1 6.82-2 9.380+0 1.262 5.97-1 7.06-2 8.188-1 0.825 9.28-1 2.18-1 1.012+0 0.817 9.36-1 2.20-1	5000 2.967+0 1.945 -9.36-2 -1.53-3 3.438+0 1.657 1.40-1 -1.57-3 6.358+0 1.737 1.71-1 9.93-3 3.628+0 1.261 7.93-1 8.74-2 4.923+0 1.189 8.09-1 9.33-2 3.370-1 0.738 1.05+0 2.62-1 4.146-1 0.735 1.05+0 2.65-1	6000 2.112+0 1.951 -1.38-1 -1.67-3 2.361+0 1.627 2.74-1 1.12-3 4.243+0 1.719 3.26-1 1.27-2 2.112+0 1.198 9.81-1 1.07-1 2.842+0 1.120 9.85-1 1.16-1 1.605-1 0.665 1.13+0 3.02-1 1.965-1 0.666 1.14+0 3.06-1	7000 1.576+0 1.956 -1.53-1 -1.78-3 1.698+0 1.594 4.14-1 4.81-3 2.980+0 1.696 4.84-1 1.56-2 1.317+0 1.135 1.14+0 1.26-1 1.760+0 1.055 1.13+0 1.39-1 8.466-2 0.601 1.20+0 3.40-1 1.033-1 0.606 1.21+0 3.44-1	8000 1.219+0 1.959 -1.47-1 -1.87-3 1.265+0 1.561 5.53-1 9.27-3 2.176+0 1.670 6.41-1 1.88-2 8.654-1 1.075 1.28+0 1.45-1 1.149+0 0.994 1.26+0 1.61-1 4.818-2 0.546 1.26+0 3.75-1 5.856-2 0.554 1.26+0 3.80-1	9000 9.683-1 1.962 -1.24-1 -1.94-3 9.698-1 1.528 6.88-1 1.44-2 1.638+0 1.642 7.91-1 2.24-2 5.926-1 1.018 1.39+0 1.64-1 7.819-1 0.938 1.37+0 1.82-1 2.908-2 0.495 1.31+0 4.08-1 3.524-2 0.508 1.31+0 4.14-1	10000 7.863- 1.964 -8.852.01- 7.605- 1.495 8.17- 2.01- 2.61-2 1.265+ 1.613 9.34- 2.61-2 4.197- 0.963 1.49+0 1.82- 5.506- 0.885 1.46+0 2.03- 1.840- 0.450 1.35+0 4.40- 2.223- 0.466 1.34+0 4.46-
Z=70, Yb: [X Shell $4s_{1/2}$ $E_b =$ 487.2 eV $4p_{1/2}$ $E_b =$ 396.7 eV $4p_{3/2}$ $E_b =$ 343.5 eV $4d_{3/2}$ $E_b =$ 198.1 eV $4d_{5/2}$ $E_b =$ 184.9 eV $4f_{5/2}$ $E_b =$ 7.0 eV	δ (c) 4f _{5/2} c	$\begin{array}{c} -5.06-4 \\ \textbf{4f}^{8}_{7/2} \ \textbf{6s}^{2}_{1/2} \\ \hline k \ (\text{eV}) \\ \hline 1500 \\ 2.221+1 \\ 1.915 \\ 4.54-1 \\ -3.10-4 \\ 2.631+1 \\ 1.577 \\ 2.37-1 \\ 2.45-3 \\ \hline 6.087+1 \\ 1.569 \\ 1.40-1 \\ 2.24-3 \\ \hline 7.298+1 \\ 1.287 \\ -3.59-2 \\ 1.35-2 \\ \hline 1.044+2 \\ 1.324 \\ -2.69-2 \\ 1.33-2 \\ \hline 2.959+1 \\ 1.061 \\ 3.60-1 \\ 9.91-2 \\ \hline 3.719+1 \\ 1.056 \\ 3.68-1 \\ \end{array}$	2000 1.435+1 1.921 3.32-1 -6.52-4 1.754+1 1.651 8.34-2 -2.07-3 3.810+1 1.661 1.86-2 8.08-4 3.961+1 1.358 4.97-2 2.67-2 5.588+1 1.359 7.39-2 2.56-2 1.100+1 1.029 5.20-1 1.25-1 1.377+1 1.020 5.29-1	3000 7.364+0 1.931 1.27-1 -1.07-3 9.035+0 1.690 -1.90-2 -3.63-3 1.818+1 1.731 -3.98-2 3.87-3 1.481+1 1.368 3.11-1 4.87-2 2.053+1 1.329 3.44-1 4.83-2 2.484+0 0.926 7.63-1 1.73-1 3.089+0 0.915 7.72-1	4000 4.450+0 1.938 -9.51-3 -1.34-3 5.330+0 1.681 2.95-2 -3.20-3 1.022+1 1.745 3.77-2 7.11-3 6.846+0 1.322 5.69-1 6.82-2 9.380+0 1.262 5.97-1 7.06-2 8.188-1 0.825 9.28-1 2.18-1 1.012+0 0.817 9.36-1	5000 2.967+0 1.945 -9.36-2 -1.53-3 3.438+0 1.657 1.40-1 -1.57-3 6.358+0 1.737 1.71-1 9.93-3 3.628+0 1.261 7.93-1 8.74-2 4.923+0 1.189 8.09-1 9.33-2 3.370-1 0.738 1.05+0 2.62-1 4.146-1 0.735 1.05+0	6000 2.112+0 1.951 -1.38-1 -1.67-3 2.361+0 1.627 2.74-1 1.12-3 4.243+0 1.719 3.26-1 1.27-2 2.112+0 1.198 9.81-1 1.07-1 2.842+0 1.120 9.85-1 1.16-1 1.605-1 0.665 1.13+0 3.02-1 1.965-1 0.666 1.14+0	7000 1.576+0 1.956 -1.53-1 -1.78-3 1.698+0 1.594 4.14-1 4.81-3 2.980+0 1.696 4.84-1 1.56-2 1.317+0 1.135 1.14+0 1.26-1 1.760+0 1.055 1.13+0 1.39-1 8.466-2 0.601 1.20+0 3.40-1 1.033-1 0.606 1.21+0	8000 1.219+0 1.959 -1.47-1 -1.87-3 1.265+0 1.561 5.53-1 9.27-3 2.176+0 1.670 6.41-1 1.88-2 8.654-1 1.075 1.28+0 1.45-1 1.149+0 0.994 1.26+0 1.61-1 4.818-2 0.546 1.26+0 3.75-1 5.856-2 0.554 1.26+0	9000 9.683-1 1.962 -1.24-1 -1.94-3 9.698-1 1.528 6.88-1 1.44-2 1.638+0 1.642 7.91-1 2.24-2 5.926-1 1.018 1.39+0 1.64-1 7.819-1 0.938 1.37+0 1.82-1 2.908-2 0.495 1.31+0 4.08-1 3.524-2 0.508 1.31+0	10000 7.863- 1.964 -8.852.01- 7.605- 1.495 8.17- 2.01- 2.01- 2.61- 2.61- 2.61- 2.61- 2.61- 2.61- 2.61- 2.61- 2.61- 2.61- 2.03- 1.49+0 1.82- 1.840- 0.450 1.35+0 4.40- 1.2223- 0.466 1.34+0 4.46-
Z= 70, Yb: [X Shell $4s_{1/2}$ $E_b = 487.2 \text{ eV}$ $4p_{1/2}$ $E_b = 396.7 \text{ eV}$ $4p_{3/2}$ $E_b = 343.5 \text{ eV}$ $4d_{3/2}$ $E_b = 198.1 \text{ eV}$ $4d_{5/2}$ $E_b = 7.0 \text{ eV}$ $4f_{5/2}$ $E_b = 5.8 \text{ eV}$ $5s_{1/2}$	δ (c) 4f _{5/2} c σ	$\begin{array}{c} -5.06-4 \\ \textbf{4f}^{8}_{7/2} \ \textbf{6s}^{2}_{1/2} \\ \hline k \ (\text{eV}) \\ \hline 1500 \\ 2.221+1 \\ 1.915 \\ 4.54-1 \\ -3.10-4 \\ 2.631+1 \\ 1.577 \\ 2.37-1 \\ 2.45-3 \\ \hline 6.087+1 \\ 1.569 \\ 1.40-1 \\ 2.24-3 \\ \hline 7.298+1 \\ 1.287 \\ -3.59-2 \\ 1.35-2 \\ \hline 1.044+2 \\ 1.324 \\ -2.69-2 \\ 1.33-2 \\ \hline 2.959+1 \\ 1.061 \\ 3.60-1 \\ 9.91-2 \\ \hline 3.719+1 \\ 1.056 \\ 3.68-1 \\ 9.90-2 \\ \hline 3.571+0 \\ \hline \end{array}$	2000 1.435+1 1.921 3.32-1 -6.52-4 1.754+1 1.651 8.34-2 -2.07-3 3.810+1 1.661 1.86-2 8.08-4 3.961+1 1.358 4.97-2 2.67-2 5.588+1 1.359 7.39-2 2.56-2 1.100+1 1.029 5.20-1 1.25-1 1.377+1 1.020 5.29-1 1.25-1 2.242+0	3000 7.364+0 1.931 1.27-1 -1.07-3 9.035+0 1.690 -1.90-2 -3.63-3 1.818+1 1.731 -3.98-2 3.87-3 1.481+1 1.368 3.11-1 4.87-2 2.053+1 1.329 3.44-1 4.83-2 2.484+0 0.926 7.63-1 1.73-1 3.089+0 0.915 7.72-1 1.74-1 1.123+0	4000 4.450+0 1.938 -9.51-3 -1.34-3 5.330+0 1.681 2.95-2 -3.20-3 1.022+1 1.745 3.77-2 7.11-3 6.846+0 1.322 5.69-1 6.82-2 9.380+0 1.262 5.97-1 7.06-2 8.188-1 0.825 9.28-1 2.18-1 1.012+0 0.817 9.36-1 2.20-1 6.707-1	5000 2.967+0 1.945 -9.36-2 -1.53-3 3.438+0 1.657 1.40-1 -1.57-3 6.358+0 1.737 1.71-1 9.93-3 3.628+0 1.261 7.93-1 8.74-2 4.923+0 1.189 8.09-1 9.33-2 3.370-1 0.738 1.05+0 2.62-1 4.146-1 0.735 1.05+0 2.65-1 4.439-1	6000 2.112+0 1.951 -1.38-1 -1.67-3 2.361+0 1.627 2.74-1 1.12-3 4.243+0 1.719 3.26-1 1.27-2 2.112+0 1.198 9.81-1 1.07-1 2.842+0 1.120 9.85-1 1.16-1 1.605-1 0.665 1.13+0 3.02-1 1.965-1 0.666 1.14+0 3.06-1 3.144-1	7000 1.576+0 1.956 -1.53-1 -1.78-3 1.698+0 1.594 4.14-1 4.81-3 2.980+0 1.696 4.84-1 1.56-2 1.317+0 1.135 1.14+0 1.26-1 1.760+0 1.055 1.13+0 1.39-1 8.466-2 0.601 1.20+0 3.40-1 1.033-1 0.606 1.21+0 3.44-1 2.337-1	8000 1.219+0 1.959 -1.47-1 -1.87-3 1.265+0 1.561 5.53-1 9.27-3 2.176+0 1.670 6.41-1 1.88-2 8.654-1 1.075 1.28+0 1.45-1 1.149+0 0.994 1.26+0 1.61-1 4.818-2 0.546 1.26+0 3.75-1 5.856-2 0.554 1.26+0 3.80-1 1.801-1	9000 9.683-1 1.962 -1.24-1 -1.94-3 9.698-1 1.528 6.88-1 1.44-2 1.638+0 1.642 7.91-1 2.24-2 5.926-1 1.018 1.39+0 1.64-1 7.819-1 0.938 1.37+0 1.82-1 2.908-2 0.495 1.31+0 4.08-1 3.524-2 0.508 1.31+0 4.14-1 1.428-1	10000 7.863- 1.964 -8.852.01- 7.605- 1.495 8.17-1 2.01-2 1.265+ 1.613 9.34-1 2.61-2 4.197- 0.963 1.494- 1.82-1 1.840- 0.450 1.35+0 4.40-1 1.158- 1.158-

$5p_{1/2}$ $E_b = 27.4 \text{ eV}$ $5p_{3/2}$ $E_b = 21.4 \text{ eV}$ $6s_{1/2}$ $E_b = 6.0 \text{ eV}$ $2=71, \text{Lu: [Xe]}$ Shell $4s_{1/2}$ $E_b = 506.2 \text{ eV}$ $4p_{3/2}$ $E_b = 410.1 \text{ eV}$ $4d_{3/2}$ $E_b = 204.8 \text{ eV}$	$ \frac{\sigma}{\beta} $ $ \frac{\gamma}{\gamma} $ $ \frac{\delta}{\delta} $ $ \frac{\sigma}{\beta} $ $ \frac{\beta}{\gamma} $ $ \frac{\delta}{\delta} $ $ \frac{\beta}{\gamma} $ $ \frac{\delta}{\delta} $ $ \frac{\gamma}{\delta} $ $ \frac{\sigma}{\beta} $ $ \frac{\beta}{\gamma} $ $ \frac{\delta}{\delta} $ $ \frac{\sigma}{\beta} $ $ \frac{\sigma}{\delta} $ $ \frac{\beta}{\gamma} $ $ \frac{\delta}{\delta} $ $ \frac{\sigma}{\delta} $ $ \frac{\beta}{\gamma} $ $ \frac{\delta}{\delta} $ $ \frac{\sigma}{\delta} $	$3.329+0$ 1.668 $1.30-1$ $-3.41-3$ $6.948+0$ 1.651 $6.81-2$ $-1.24-3$ $2.108-1$ 1.923 $3.08-1$ $-5.15-4$ $f_{7/2}^{8}$ $5d_{3/2}^{1}$ $6s_{1/2}^{2}$ k (eV) 1500 $2.258+1$ 1.908 $4.74-1$ $-2.89-4$ $2.667+1$ 1.564 $2.58-1$ $3.15-3$ $6.261+1$ 1.553 $1.57-1$	2.154+0 1.705 2.74-2 -4.06-3 4.268+0 1.712 -1.43-2 8.26-5 1.316-1 1.928 2.15-1 -7.66-4 2000 1.466+1 1.916 3.53-1 -6.67-4 1.792+1 1.644 1.00-1 -1.96-3 3.939+1	1.085+0 1.713 -1.83-2 -4.30-3 2.008+0 1.754 -3.07-2 3.71-3 6.562-2 1.935 5.79-2 -1.12-3 3000 7.572+0 1.926 1.47-1 -1.13-3 9.326+0 1.689 -1.73-2 -3.82-3	6.343-1 1.693 5.14-2 -3.74-3 1.122+0 1.757 6.24-2 6.70-3 3.911-2 1.942 -5.05-2 -1.35-3 4000 4.592+0 1.934 6.37-3 -1.42-3 5.538+0 1.683	4.070-1 1.663 1.70-1 -2.11-3 6.961-1 1.744 2.01-1 9.31-3 2.585-2 1.948 -1.15-1 -1.52-3 5000 3.069+0 1.941 -8.30-2 -1.63-3 3.589+0	2.786-1 1.630 3.05-1 5.94-4 4.636-1 1.722 3.56-1 1.19-2 1.829-2 1.953 -1.46-1 -1.65-3 6000 2.189+0 1.947 -1.33-1 -1.78-3 2.473+0	1.999-1 1.595 4.45-1 4.24-3 3.252-1 1.697 5.13-1 1.47-2 1.359-2 1.957 -1.52-1 -1.75-3 7000 1.635+0 1.952 -1.54-1 -1.90-3 1.784+0 1.602	1.488-1 1.560 5.81-1 8.69-3 2.373-1 1.669 6.67-1 1.78-2 1.047-2 1.960 -1.39-1 -1.85-3 8000 1.266+0 1.956 -1.53-1 -2.01-3 1.333+0	1.139-1 1.526 7.13-1 1.38-2 1.785-1 1.640 8.14-1 2.13-2 8.295-3 1.963 -1.12-1 -1.93-3 9000 1.007+0 1.959 -1.35-1 -2.09-3	1.964 -7.23-2 -1.99-3 10000 8.180-1 1.961 -1.04-1
27.4 eV $ 5p_{3/2} E_b = 21.4 \text{ eV} $ $ 6s_{1/2} E_b = 6.0 \text{ eV} $ $ Z=71, Lu: [Xe] $ Shell $ 4s_{1/2} E_b = 506.2 \text{ eV} $ $ 4p_{1/2} E_b = 410.1 \text{ eV} $ $ 4p_{3/2} E_b = 359.3 \text{ eV} $	γ δ σ β γ δ δ σ β β γ δ δ σ β γ δ δ σ β γ δ δ σ β γ γ δ δ σ σ β γ γ δ δ σ σ β γ γ δ δ σ σ β γ γ δ δ σ σ β γ γ δ δ σ σ β γ γ δ δ σ σ β γ γ δ δ σ σ β γ γ δ δ σ σ β γ γ δ δ σ σ β γ γ δ δ σ σ β γ γ δ δ σ σ β γ γ δ δ σ σ β γ γ δ δ σ σ β γ γ δ δ σ σ β γ γ δ δ σ σ β γ γ δ δ σ σ β γ γ δ δ σ σ β γ γ δ δ σ σ β γ γ δ δ σ σ β γ γ δ δ σ σ β γ γ δ δ σ σ β γ γ δ δ σ σ β γ γ δ δ σ σ β γ γ δ δ σ σ ρ γ γ δ δ σ σ γ δ σ σ γ δ σ σ δ σ σ σ σ σ	$\begin{array}{c} 1.30-1\\ -3.41-3\\ \hline 6.948+0\\ 1.651\\ 6.81-2\\ -1.24-3\\ \hline 2.108-1\\ 1.923\\ 3.08-1\\ -5.15-4\\ \hline \mathbf{f_{/2}^8} \mathbf{5d_{3/2}^1} \mathbf{6s_{1/2}^2}\\ \hline k(\text{eV})\\ \hline 1500\\ \hline 2.258+1\\ 1.908\\ 4.74-1\\ -2.89-4\\ 2.667+1\\ 1.564\\ 2.58-1\\ 3.15-3\\ \hline 6.261+1\\ 1.553\\ \end{array}$	2.74-2 -4.06-3 4.268+0 1.712 -1.43-2 8.26-5 1.316-1 1.928 2.15-1 -7.66-4 2000 1.466+1 1.916 3.53-1 -6.67-4 1.792+1 1.644 1.00-1 -1.96-3	-1.83-2 -4.30-3 2.008+0 1.754 -3.07-2 3.71-3 6.562-2 1.935 5.79-2 -1.12-3 3000 7.572+0 1.926 1.47-1 -1.13-3 9.326+0 1.689 -1.73-2	5.14-2 -3.74-3 1.122+0 1.757 6.24-2 6.70-3 3.911-2 1.942 -5.05-2 -1.35-3 4000 4.592+0 1.934 6.37-3 -1.42-3 5.538+0 1.683	1.70-1 -2.11-3 6.961-1 1.744 2.01-1 9.31-3 2.585-2 1.948 -1.15-1 -1.52-3 5000 3.069+0 1.941 -8.30-2 -1.63-3 3.589+0	3.05-1 5.94-4 4.636-1 1.722 3.56-1 1.19-2 1.829-2 1.953 -1.46-1 -1.65-3 6000 2.189+0 1.947 -1.33-1 -1.78-3 2.473+0	4.45-1 4.24-3 3.252-1 1.697 5.13-1 1.47-2 1.359-2 1.957 -1.52-1 -1.75-3 7000 1.635+0 1.952 -1.54-1 -1.90-3 1.784+0	5.81-1 8.69-3 2.373-1 1.669 6.67-1 1.78-2 1.047-2 1.960 -1.39-1 -1.85-3 8000 1.266+0 1.956 -1.53-1 -2.01-3	7.13-1 1.38-2 1.785-1 1.640 8.14-1 2.13-2 8.295-3 1.963 -1.12-1 -1.93-3 9000 1.007+0 1.959 -1.35-1 -2.09-3	8.39-1 1.94-2 1.378-1 1.611 9.54-1 2.50-2 6.721-3 1.964 -7.23-2 -1.99-3 10000 8.180-1 1.961 -1.04-1
$5p_{3/2}$ $E_b =$ 21.4 eV $6s_{1/2}$ $E_b =$ 6.0 eV $2=71, \text{Lu: [Xe]}$ $4s_{1/2}$ $4s_{1/2}$ $4s_{1/2}$ $4s_{1/2}$ $4s_{1/2}$ $5s_{1/2}$ 5	δ σ β γ δ σ β γ δ δ σ β γ δ δ σ σ σ σ σ σ σ σ	$\begin{array}{c} -3.41-3 \\ 6.948+0 \\ 1.651 \\ 6.81-2 \\ -1.24-3 \\ \hline 2.108-1 \\ 1.923 \\ 3.08-1 \\ -5.15-4 \\ \hline {\bf f}_{7/2}^8 {\bf 5d}_{3/2}^1 {\bf 6s}_{1/2}^2 \\ \hline {\bf k (eV)} \\ \hline 1500 \\ \hline 2.258+1 \\ 1.908 \\ 4.74-1 \\ -2.89-4 \\ \hline 2.667+1 \\ 1.564 \\ 2.58-1 \\ 3.15-3 \\ \hline 6.261+1 \\ 1.553 \\ \hline \end{array}$	-4.06-3 4.268+0 1.712 -1.43-2 8.26-5 1.316-1 1.928 2.15-1 -7.66-4 2000 1.466+1 1.916 3.53-1 -6.67-4 1.792+1 1.644 1.00-1 -1.96-3	-4.30-3 2.008+0 1.754 -3.07-2 3.71-3 6.562-2 1.935 5.79-2 -1.12-3 3000 7.572+0 1.926 1.47-1 -1.13-3 9.326+0 1.689 -1.73-2	-3.74-3 1.122+0 1.757 6.24-2 6.70-3 3.911-2 1.942 -5.05-2 -1.35-3 4000 4.592+0 1.934 6.37-3 -1.42-3 5.538+0 1.683	-2.11-3 6.961-1 1.744 2.01-1 9.31-3 2.585-2 1.948 -1.15-1 -1.52-3 5000 3.069+0 1.941 -8.30-2 -1.63-3 3.589+0	5.94-4 4.636-1 1.722 3.56-1 1.19-2 1.829-2 1.953 -1.46-1 -1.65-3 6000 2.189+0 1.947 -1.33-1 -1.78-3 2.473+0	4.24-3 3.252-1 1.697 5.13-1 1.47-2 1.359-2 1.957 -1.52-1 -1.75-3 7000 1.635+0 1.952 -1.54-1 -1.90-3 1.784+0	8.69-3 2.373-1 1.669 6.67-1 1.78-2 1.047-2 1.960 -1.39-1 -1.85-3 8000 1.266+0 1.956 -1.53-1 -2.01-3	1.38-2 1.785-1 1.640 8.14-1 2.13-2 8.295-3 1.963 -1.12-1 -1.93-3 9000 1.007+0 1.959 -1.35-1 -2.09-3	1.94-2 1.378-1 1.611 9.54-1 2.50-2 6.721-3 1.964 -7.23-2 -1.99-3 10000 8.180-1 1.961 -1.04-6
$E_b = 21.4 \text{ eV}$ 21.4 eV $E_b = 6.0 \text{ eV}$	β γ δ σ β γ γ δ δ [4f _{5/2} 4] σ σ β γ γ δ δ σ σ β γ γ δ δ σ σ β γ γ δ δ σ σ β γ γ δ δ σ σ γ δ σ σ γ δ σ σ γ δ σ σ γ δ σ σ γ δ σ σ σ γ δ σ σ σ σ	$\begin{array}{c} 1.651 \\ 6.81-2 \\ -1.24-3 \\ \hline 2.108-1 \\ 1.923 \\ 3.08-1 \\ -5.15-4 \\ \hline {\bf f}_{7/2}^8 {\bf 5d}_{3/2}^1 {\bf 6s}_{1/2}^2 \\ \hline {\it k} ({\rm eV}) \\ \hline 1500 \\ \hline 2.258+1 \\ 1.908 \\ 4.74-1 \\ -2.89-4 \\ \hline 2.667+1 \\ 1.564 \\ 2.58-1 \\ 3.15-3 \\ \hline 6.261+1 \\ 1.553 \\ \end{array}$	1.712 -1.43-2 8.26-5 1.316-1 1.928 2.15-1 -7.66-4 2000 1.466+1 1.916 3.53-1 -6.67-4 1.792+1 1.644 1.00-1 -1.96-3	1.754 -3.07-2 3.71-3 6.562-2 1.935 5.79-2 -1.12-3 3000 7.572+0 1.926 1.47-1 -1.13-3 9.326+0 1.689 -1.73-2	1.757 6.24-2 6.70-3 3.911-2 1.942 -5.05-2 -1.35-3 4000 4.592+0 1.934 6.37-3 -1.42-3 5.538+0 1.683	1.744 2.01-1 9.31-3 2.585-2 1.948 -1.15-1 -1.52-3 5000 3.069+0 1.941 -8.30-2 -1.63-3 3.589+0	1.722 3.56-1 1.19-2 1.829-2 1.953 -1.46-1 -1.65-3 6000 2.189+0 1.947 -1.33-1 -1.78-3 2.473+0	1.697 5.13-1 1.47-2 1.359-2 1.957 -1.52-1 -1.75-3 7000 1.635+0 1.952 -1.54-1 -1.90-3 1.784+0	1.669 6.67-1 1.78-2 1.047-2 1.960 -1.39-1 -1.85-3 8000 1.266+0 1.956 -1.53-1 -2.01-3	1.640 8.14-1 2.13-2 8.295-3 1.963 -1.12-1 -1.93-3 9000 1.007+0 1.959 -1.35-1 -2.09-3	1.611 9.54-1 2.50-2 6.721-3 1.964 -7.23-2 -1.99-3 10000 8.180-1 1.961 -1.04-1
21.4 eV $ 6s_{1/2}E_b = 6.0 \text{ eV} $ Z= 71, Lu: [Xe] Shell $4s_{1/2}E_b = 506.2 \text{ eV}$ $4p_{1/2}E_b = 410.1 \text{ eV}$ $4p_{3/2}E_b = 359.3 \text{ eV}$ $4d_{3/2}E_b = 6$	$ \begin{array}{c} \gamma \\ \delta \\ \hline \sigma \\ \beta \\ \gamma \\ \delta \\ \end{array} $ $ \begin{array}{c} \sigma \\ \beta \\ \gamma \\ \delta \\ \end{array} $ $ \begin{array}{c} \sigma \\ \beta \\ \gamma \\ \delta \\ \end{array} $ $ \begin{array}{c} \sigma \\ \beta \\ \gamma \\ \delta \\ \end{array} $ $ \begin{array}{c} \sigma \\ \beta \\ \gamma \\ \delta \\ \end{array} $ $ \begin{array}{c} \sigma \\ \beta \\ \gamma \\ \delta \\ \end{array} $ $ \begin{array}{c} \sigma \\ \beta \\ \gamma \\ \delta \\ \end{array} $ $ \begin{array}{c} \sigma \\ \beta \\ \gamma \\ \delta \\ \end{array} $	$\begin{array}{c} 6.81-2 \\ -1.24-3 \\ \hline 2.108-1 \\ 1.923 \\ 3.08-1 \\ -5.15-4 \\ \hline \textbf{f}_{7/2}^8 \textbf{5d}_{3/2}^1 \textbf{6s}_{1/2}^2 \\ \hline \textbf{k (eV)} \\ \hline 1500 \\ 2.258+1 \\ 1.908 \\ 4.74-1 \\ -2.89-4 \\ 2.667+1 \\ 1.564 \\ 2.58-1 \\ 3.15-3 \\ \hline 6.261+1 \\ 1.553 \\ \end{array}$	2000 1.466+1 1.916 3.53-1 -6.67-4 1.998 2.15-1 -7.66-4 2000 1.466+1 1.916 3.53-1 -6.67-4 1.792+1 1.644 1.00-1 -1.96-3	-3.07-2 3.71-3 6.562-2 1.935 5.79-2 -1.12-3 3000 7.572+0 1.926 1.47-1 -1.13-3 9.326+0 1.689 -1.73-2	6.24-2 6.70-3 3.911-2 1.942 -5.05-2 -1.35-3 4000 4.592+0 1.934 6.37-3 -1.42-3 5.538+0 1.683	2.01-1 9.31-3 2.585-2 1.948 -1.15-1 -1.52-3 5000 3.069+0 1.941 -8.30-2 -1.63-3 3.589+0	3.56-1 1.19-2 1.829-2 1.953 -1.46-1 -1.65-3 6000 2.189+0 1.947 -1.33-1 -1.78-3 2.473+0	5.13-1 1.47-2 1.359-2 1.957 -1.52-1 -1.75-3 7000 1.635+0 1.952 -1.54-1 -1.90-3 1.784+0	8000 1.266+0 1.956 -1.39-1 -1.85-3	8.14-1 2.13-2 8.295-3 1.963 -1.12-1 -1.93-3 9000 1.007+0 1.959 -1.35-1 -2.09-3	9.54-1 2.50-2 6.721-3 1.964 -7.23-2 -1.99-3 10000 8.180-1 1.961 -1.04-1
$6s_{1/2}$ $E_b =$ 6.0 eV Z= 71, Lu: [Xe] Shell $4s_{1/2}$ $E_b =$ 506.2 eV $4p_{1/2}$ $E_b =$ 410.1 eV $4p_{3/2}$ $E_b =$ 359.3 eV	$\begin{array}{c} \frac{\delta}{\sigma} \\ \frac{\beta}{\beta} \\ \frac{\gamma}{\delta} \\ \frac{\gamma}{\delta} \\ \frac{\delta}{\delta} \\ \frac{\sigma}{\beta} \\ \frac{\gamma}{\delta} \\ \frac{\sigma}{\delta} \\ \frac{\sigma}{\beta} \\ \frac{\gamma}{\delta} \\ \frac{\sigma}{\delta} \\ \frac{\sigma}{\beta} \\ \frac{\sigma}{\beta} \\ \frac{\gamma}{\delta} \\ \frac{\sigma}{\delta} \\$	$\begin{array}{c} -1.24-3 \\ 2.108-1 \\ 1.923 \\ 3.08-1 \\ -5.15-4 \\ f_{7/2}^8 5d_{3/2}^1 6s_{1/2}^2 \\ \hline k (eV) \\ \hline 1500 \\ 2.258+1 \\ 1.908 \\ 4.74-1 \\ -2.89-4 \\ 2.667+1 \\ 1.564 \\ 2.58-1 \\ 3.15-3 \\ \hline 6.261+1 \\ 1.553 \\ \end{array}$	8.26-5 1.316-1 1.928 2.15-1 -7.66-4 2000 1.466+1 1.916 3.53-1 -6.67-4 1.792+1 1.644 1.00-1 -1.96-3	3.71-3 6.562-2 1.935 5.79-2 -1.12-3 3000 7.572+0 1.926 1.47-1 -1.13-3 9.326+0 1.689 -1.73-2	6.70-3 3.911-2 1.942 -5.05-2 -1.35-3 4000 4.592+0 1.934 6.37-3 -1.42-3 5.538+0 1.683	9.31-3 2.585-2 1.948 -1.15-1 -1.52-3 5000 3.069+0 1.941 -8.30-2 -1.63-3 3.589+0	1.19-2 1.829-2 1.953 -1.46-1 -1.65-3 6000 2.189+0 1.947 -1.33-1 -1.78-3 2.473+0	1.47-2 1.359-2 1.957 -1.52-1 -1.75-3 7000 1.635+0 1.952 -1.54-1 -1.90-3 1.784+0	1.78-2 1.047-2 1.960 -1.39-1 -1.85-3 8000 1.266+0 1.956 -1.53-1 -2.01-3	2.13-2 8.295-3 1.963 -1.12-1 -1.93-3 9000 1.007+0 1.959 -1.35-1 -2.09-3	2.50-2 6.721-3 1.964 -7.23-2 -1.99-3 10000 8.180-1 1.961 -1.04-1
$E_b = 6.0 \text{ eV}$ $C = 71, Lu: [Xe]$ Shell $4s_{1/2}$ $E_b = 506.2 \text{ eV}$ $4p_{1/2}$ $E_b = 410.1 \text{ eV}$ $4p_{3/2}$ $E_b = 359.3 \text{ eV}$ $4d_{3/2}$ $E_b = 6.0 \text{ eV}$	β γ δ 4f _{5/2} 4 σ β γ δ σ β γ δ σ β γ δ	$\begin{array}{c} 1.923 \\ 3.08-1 \\ -5.15-4 \\ \textbf{f}_{7/2}^{8} \textbf{5d}_{3/2}^{1} \textbf{6s}_{1/2}^{2} \\ \hline k (\text{eV}) \\ \hline 1500 \\ 2.258+1 \\ 1.908 \\ 4.74-1 \\ -2.89-4 \\ 2.667+1 \\ 1.564 \\ 2.58-1 \\ 3.15-3 \\ \hline 6.261+1 \\ 1.553 \\ \end{array}$	1.928 2.15-1 -7.66-4 2000 1.466+1 1.916 3.53-1 -6.67-4 1.792+1 1.644 1.00-1 -1.96-3	1.935 5.79-2 -1.12-3 3000 7.572+0 1.926 1.47-1 -1.13-3 9.326+0 1.689 -1.73-2	1.942 -5.05-2 -1.35-3 4000 4.592+0 1.934 6.37-3 -1.42-3 5.538+0 1.683	1.948 -1.15-1 -1.52-3 5000 3.069+0 1.941 -8.30-2 -1.63-3 3.589+0	1.953 -1.46-1 -1.65-3 6000 2.189+0 1.947 -1.33-1 -1.78-3 2.473+0	1.957 -1.52-1 -1.75-3 7000 1.635+0 1.952 -1.54-1 -1.90-3 1.784+0	1.960 -1.39-1 -1.85-3 8000 1.266+0 1.956 -1.53-1 -2.01-3	9000 1.007+0 1.959 -1.35-1 -2.09-3	-7.23-2 -1.99-3 10000 8.180-1 1.961 -1.04-1
$E_b = 6.0 \text{ eV}$ Z= 71, Lu: [Xe] Shell $4s_{1/2}$ $E_b = 506.2 \text{ eV}$ $4p_{1/2}$ $E_b = 410.1 \text{ eV}$ $4p_{3/2}$ $E_b = 359.3 \text{ eV}$	γ δ 4f ⁶ _{5/2} 4	$3.08-1 \\ -5.15-4$ $\mathbf{f_{7/2}^8 5d_{3/2}^1 6s_{1/2}^2}$ $\frac{k \text{ (eV)}}{1500}$ $2.258+1$ 1.908 $4.74-1$ $-2.89-4$ $2.667+1$ 1.564 $2.58-1$ $3.15-3$ $6.261+1$ 1.553	2.15-1 -7.66-4 2000 1.466+1 1.916 3.53-1 -6.67-4 1.792+1 1.644 1.00-1 -1.96-3	5.79-2 -1.12-3 3000 7.572+0 1.926 1.47-1 -1.13-3 9.326+0 1.689 -1.73-2	-5.05-2 -1.35-3 4000 4.592+0 1.934 6.37-3 -1.42-3 5.538+0 1.683	5000 3.069+0 1.941 -8.30-2 -1.63-3 3.589+0	6000 2.189+0 1.947 -1.33-1 -1.78-3 2.473+0	7000 1.635+0 1.952 -1.54-1 -1.90-3 1.784+0	8000 1.266+0 1.956 -1.53-1 -2.01-3	9000 1.007+0 1.959 -1.35-1 -2.09-3	-7.23-2 -1.99-3 10000 8.180-1 1.961 -1.04-1
Z= 71, Lu: [Xe] Shell $4s_{1/2}$ $E_b = 506.2 \text{ eV}$ $4p_{1/2}$ $E_b = 410.1 \text{ eV}$ $4p_{3/2}$ $E_b = 359.3 \text{ eV}$ $4d_{3/2}$ $E_b = 6$	δ 4f _{5/2} 4 σ β γ δ σ β γ δ σ β γ δ δ σ β γ δ δ σ β γ δ δ σ β γ δ δ σ β γ δ δ σ β γ δ δ σ β γ δ δ δ σ β γ δ δ δ δ δ δ δ δ δ δ δ δ δ δ δ δ δ δ	$\begin{array}{c} -5.15-4 \\ \mathbf{f}_{7/2}^8 \ \mathbf{5d}_{3/2}^1 \ \mathbf{6s}_{1/2}^2 \\ \underline{k} \ (\text{eV}) \\ 1500 \\ 2.258+1 \\ 1.908 \\ 4.74-1 \\ -2.89-4 \\ 2.667+1 \\ 1.564 \\ 2.58-1 \\ 3.15-3 \\ 6.261+1 \\ 1.553 \end{array}$	2000 1.466+1 1.916 3.53-1 -6.67-4 1.792+1 1.644 1.00-1 -1.96-3	3000 7.572+0 1.926 1.47-1 -1.13-3 9.326+0 1.689 -1.73-2	4000 4.592+0 1.934 6.37-3 -1.42-3 5.538+0 1.683	5000 3.069+0 1.941 -8.30-2 -1.63-3 3.589+0	6000 2.189+0 1.947 -1.33-1 -1.78-3 2.473+0	7000 1.635+0 1.952 -1.54-1 -1.90-3 1.784+0	8000 1.266+0 1.956 -1.53-1 -2.01-3	9000 1.007+0 1.959 -1.35-1 -2.09-3	10000 8.180-1 1.961 -1.04-1
Shell $4s_{1/2}$ $E_b = 506.2 \text{ eV}$ $4p_{1/2}$ $E_b = 410.1 \text{ eV}$ $4p_{3/2}$ $E_b = 359.3 \text{ eV}$ $4d_{3/2}$ $E_b = 6$	σ β γ δ σ β γ δ σ β γ δ δ	f ⁸ _{7/2} 5d ¹ _{3/2} 6s ² _{1/2} k (eV) 1500 2.258+1 1.908 4.74-1 -2.89-4 2.667+1 1.564 2.58-1 3.15-3 6.261+1 1.553	2000 1.466+1 1.916 3.53-1 -6.67-4 1.792+1 1.644 1.00-1 -1.96-3	3000 7.572+0 1.926 1.47-1 -1.13-3 9.326+0 1.689 -1.73-2	4000 4.592+0 1.934 6.37-3 -1.42-3 5.538+0 1.683	5000 3.069+0 1.941 -8.30-2 -1.63-3 3.589+0	6000 2.189+0 1.947 -1.33-1 -1.78-3 2.473+0	7000 1.635+0 1.952 -1.54-1 -1.90-3 1.784+0	8000 1.266+0 1.956 -1.53-1 -2.01-3	9000 1.007+0 1.959 -1.35-1 -2.09-3	10000 8.180-1 1.961 -1.04-1
Shell $4s_{1/2}$ $E_b = 506.2 \text{ eV}$ $4p_{1/2}$ $E_b = 410.1 \text{ eV}$ $4p_{3/2}$ $E_b = 359.3 \text{ eV}$ $4d_{3/2}$ $E_b = 6$	σ β γ δ σ β γ δ σ β γ δ	k(eV) 1500 2.258+1 1.908 4.74-1 -2.89-4 2.667+1 1.564 2.58-1 3.15-3 6.261+1 1.553	1.466+1 1.916 3.53-1 -6.67-4 1.792+1 1.644 1.00-1 -1.96-3	7.572+0 1.926 1.47-1 -1.13-3 9.326+0 1.689 -1.73-2	4.592+0 1.934 6.37-3 -1.42-3 5.538+0 1.683	3.069+0 1.941 -8.30-2 -1.63-3 3.589+0	2.189+0 1.947 -1.33-1 -1.78-3 2.473+0	1.635+0 1.952 -1.54-1 -1.90-3 1.784+0	1.266+0 1.956 -1.53-1 -2.01-3	1.007+0 1.959 -1.35-1 -2.09-3	8.180-1 1.961 -1.04-1
$4s_{1/2}$ $E_b = 506.2 \text{ eV}$ $4p_{1/2}$ $E_b = 410.1 \text{ eV}$ $4p_{3/2}$ $E_b = 359.3 \text{ eV}$ $4d_{3/2}$ $E_b = 60.3 \text{ eV}$	β γ δ σ β γ δ σ β γ δ	2.258+1 1.908 4.74-1 -2.89-4 2.667+1 1.564 2.58-1 3.15-3 6.261+1 1.553	1.466+1 1.916 3.53-1 -6.67-4 1.792+1 1.644 1.00-1 -1.96-3	7.572+0 1.926 1.47-1 -1.13-3 9.326+0 1.689 -1.73-2	4.592+0 1.934 6.37-3 -1.42-3 5.538+0 1.683	3.069+0 1.941 -8.30-2 -1.63-3 3.589+0	2.189+0 1.947 -1.33-1 -1.78-3 2.473+0	1.635+0 1.952 -1.54-1 -1.90-3 1.784+0	1.266+0 1.956 -1.53-1 -2.01-3	1.007+0 1.959 -1.35-1 -2.09-3	8.180-1 1.961 -1.04-1
$E_b = 506.2 \text{ eV}$ $4p_{1/2}$ $E_b = 410.1 \text{ eV}$ $4p_{3/2}$ $E_b = 359.3 \text{ eV}$ $4d_{3/2}$ $E_b = 60.2 \text{ eV}$	β γ δ σ β γ δ σ β γ δ	1.908 4.74-1 -2.89-4 2.667+1 1.564 2.58-1 3.15-3 6.261+1 1.553	1.916 3.53-1 -6.67-4 1.792+1 1.644 1.00-1 -1.96-3	1.926 1.47-1 -1.13-3 9.326+0 1.689 -1.73-2	1.934 6.37-3 -1.42-3 5.538+0 1.683	1.941 -8.30-2 -1.63-3 3.589+0	1.947 -1.33-1 -1.78-3 2.473+0	1.952 -1.54-1 -1.90-3 1.784+0	1.956 -1.53-1 -2.01-3	1.959 -1.35-1 -2.09-3	1.961 -1.04-1
506.2 eV $4p_{1/2}$ $E_b =$ 410.1 eV $4p_{3/2}$ $E_b =$ 359.3 eV $4d_{3/2}$ $E_b =$	γ δ β γ δ σ β γ δ	4.74-1 -2.89-4 2.667+1 1.564 2.58-1 3.15-3 6.261+1 1.553	3.53-1 -6.67-4 1.792+1 1.644 1.00-1 -1.96-3	1.47-1 -1.13-3 9.326+0 1.689 -1.73-2	6.37-3 -1.42-3 5.538+0 1.683	-8.30-2 -1.63-3 3.589+0	-1.33-1 -1.78-3 2.473+0	-1.54-1 -1.90-3 1.784+0	-1.53-1 -2.01-3	-1.35-1 -2.09-3	-1.04-1
$4p_{1/2} E_b = 410.1 \text{ eV}$ $4p_{3/2} E_b = 359.3 \text{ eV}$ $4d_{3/2} E_b = 60.0000000000000000000000000000000000$	δ σ β γ δ σ β γ δ	-2.89-4 2.667+1 1.564 2.58-1 3.15-3 6.261+1 1.553	-6.67-4 1.792+1 1.644 1.00-1 -1.96-3	-1.13-3 9.326+0 1.689 -1.73-2	-1.42-3 5.538+0 1.683	-1.63-3 3.589+0	-1.78-3 2.473+0	-1.90-3 1.784+0	-2.01-3	-2.09-3	-1.04-1 $-2.17-3$
$E_b = 410.1 \text{ eV}$ $4p_{3/2}$ $E_b = 359.3 \text{ eV}$ $4d_{3/2}$ $E_b = 600000000000000000000000000000000000$	β γ δ σ β γ δ	1.564 2.58-1 3.15-3 6.261+1 1.553	1.644 1.00-1 -1.96-3	1.689 -1.73-2	1.683				1.333+0	1.02.4+0	
410.1 eV $4p_{3/2}$ $E_b = 359.3$ eV $4d_{3/2}$ $E_b = 600$	γ δ σ β γ δ	2.58-1 3.15-3 6.261+1 1.553	1.00-1 -1.96-3	-1.73-2				1.602		1.024+0	8.044-1
$4p_{3/2}$ $E_b = 359.3 \text{ eV}$ $4d_{3/2}$ $E_b = 6$	δ σ β γ δ	3.15-3 6.261+1 1.553	-1.96-3		102 2	1.661	1.633		1.569	1.537	1.504
$E_b = 359.3 \text{ eV}$ $4d_{3/2}$ $E_b = $	σ β γ δ	6.261+1 1.553			1.92-2 -3.49-3	1.22 - 1 $-2.03 - 3$	2.51-1 4.94-4	3.88-1 3.96-3	5.26-1 8.19-3	6.60-1 $1.30-2$	7.88 - 1 $1.83 - 2$
$E_b = 359.3 \text{ eV}$ $4d_{3/2}$ $E_b = $	β γ δ	1.553		1.893+1	1.068+1	6.669+0	4.462+0	3.140+0	2.297+0	1.732+0	1.339+0
$4d_{3/2}$ $E_b =$	δ	1.57 - 1	1.651	1.728	1.746	1.741	1.725	1.704	1.679	1.652	1.624
$E_b =$		2.74-3	3.01-2 7.49-4	-4.26-2 3.70-3	2.39-2	1.50-1 9.92-3	3.00-1 1.27-2	4.57-1 1.56-2	6.13-1	7.63-1	9.06-1
$E_b =$		7.615+1	4.174+1	1.580+1	7.03-3 7.358+0	3.919+0	2.291+0	1.433+0	1.86-2 9.443-1	2.19-2 6.482-1	2.54-2 4.601-1
	β	1.275	1.353	1.380+1	7.338+0 1.331	1.273	1.211	1.433+0	9.443-1 1.089	1.033	4.601—1 0.979
204.0 CV	γ	-4.02-2	3.58-2	2.90-1	5.48-1	7.73-1	9.64-1	1.13+0	1.26+0	1.38+0	1.48+0
	δ	1.23-2	2.54-2	4.75-2	6.69-2	8.58-2	1.05-1	1.23-1	1.41-1	1.59-1	1.77 - 1
$4d_{5/2}$	σ	1.093+2	5.902+1	2.193+1	1.009+1	5.320+0	3.082+0	1.914+0	1.253+0	8.545-1	6.029-1
$E_b = 195.0 \text{ eV}$	β γ	1.317 -3.33-2	1.358 5.88-2	1.334 3.24-1	1.271 5.77-1	1.200 7.92-1	1.131 9.71-1	1.066 1.12+0	1.005 1.25+0	0.949 1.36+0	0.898 1.45+0
155.0 CV	δ	1.22-2	2.42-2	4.69-2	6.91-2	9.14-2	1.14-1	1.36-1	1.57-1	1.78-1	1.98-1
$4f_{5/2}$	σ	3.420+1	1.285+1	2.941+0	9.762-1	4.036-1	1.929-1	1.021-1	5.826-2	3.526-2	2.236-2
$E_b =$	β	1.061	1.033	0.934	0.834	0.747	0.673	0.610	0.555	0.505	0.460
7.8 eV	δ	3.45-1 9.72-2	5.06-1 1.23-1	7.53-1 1.70-1	9.23-1 2.15-1	1.04+0 2.57-1	1.13+0 2.97-1	1.21+0 3.34-1	1.27+0 3.70-1	1.32+0 4.04-1	1.36+0 4.35-1
4f _{7/2}	σ	4.331+1	1.621+1	3.685+0	1.216+0	5.003-1	2.380-1	1.254-1	7.134-2	4.304-2	2.722-2
$E_b =$	β	1.056	1.024	0.923	0.825	0.742	0.673	0.614	0.562	0.517	0.475
6.2 eV	δ	3.54-1 9.71-2	5.15-1 1.23-1	7.63-1	9.31-1 2.17-1	1.05+0	1.14+0 3.01-1	1.21+0 3.39-1	1.27+0 3.75-1	1.31+0 4.09-1	1.35+0 4.42-1
50		3.789+0	2.385+0	1.71-1 1.200+0	7.186-1	2.60-1 4.765-1	3.380-1	2.515-1	1.941-1	1.539-1	1.249-1
$5s_{1/2}$ $E_b =$	$\frac{\sigma}{\beta}$	3.789+0 1.917	1.923	1.200+0	1.938	1.944	1.949	1.954	1.941-1	1.960	1.249-1
56.8 eV	γ	3.30-1	2.38 - 1	7.73 - 2	-3.58-2	-1.06-1	-1.43-1	-1.55-1	-1.47 - 1	-1.24-1	-8.90-2
	δ	-5.18-4	-7.94-4	-1.17 - 3	-1.43-3	-1.62-3	-1.77 - 3	-1.88 - 3	-1.98 - 3	-2.06-3	-2.13-3
$5p_{1/2}$	σ_{ρ}	3.559+0 1.661	2.315+0 1.702	1.176+0 1.714	6.912-1 1.696	4.454-1 1.668	3.058-1 1.637	2.201-1 1.603	1.642-1 1.569	1.260-1 1.536	9.890-2 1.503
$E_b = 33.0 \text{ eV}$	β γ	1.47-1	3.89-2	-2.02-2	3.89-2	1.50-1	2.81-1	4.18-1	5.54-1	6.85-1	8.11-1
	δ	-3.49-3	-4.25 - 3	-4.52 - 3	-4.05 - 3	-2.58-3	-6.52-5	3.40-3	7.67-3	1.25-2	1.79-2
$5p_{3/2}$	σ	7.631+0	4.703+0	2.225+0	1.248+0	7.765-1	5.184-1	3.643-1	2.663-1	2.007-1	1.550-1
$E_b = 25.8 \text{ eV}$	β	1.642 7.98-2	1.705 -7.61-3	1.753 -3.57-2	1.759 4.74-2	1.749 1.80-1	1.730 3.30-1	1.706 4.86-1	1.680 6.39-1	1.652 7.86-1	1.624 9.27-1
25.8 eV	$_{\delta}^{\gamma}$	-1.35-3	-7.61-3 -1.50-4	-3.57-2 $3.56-3$	6.64-3	9.29-3	1.19-2	4.86—1 1.47—2	1.77-2	2.10-2	9.27 - 1 2.46 - 2
5d _{3/2}	σ	2.533+0	1.388+0	5.282-1	2.470-1	1.319-1	7.724-2	4.840-2	3.194-2	2.196-2	1.561-2
$E_b =$	β	1.343	1.392	1.387	1.337	1.274	1.210	1.148	1.089	1.033	0.981
4.6 eV	δ	-2.47-2 1.26-2	6.06-2 $2.48-2$	3.16-1 $4.58-2$	5.69-1 $6.46-2$	7.89-1 8.30-2	9.76-1 1.01-1	1.13+0 1.20-1	1.27+0 1.39-1	1.39+0 1.58-1	1.49+0 1.77-1
6s _{1/2}	σ	2.607-1	1.632-1	8.164-2	4.878-2	3.230-2	2.288-2	1.701-2	1.311-2	1.040-2	8.428-3
$E_b =$	β	1.918	1.923	1.931	1.938	1.944	1.949	1.953	1.957	1.959	1.961
7.0 eV	$_{\delta}^{\gamma}$	3.23-1 -5.32-4	2.32-1 $-8.03-4$	7.30-2 $-1.18-3$	-3.89-2 $-1.44-3$	-1.09-1 $-1.63-3$	-1.46-1 $-1.78-3$	-1.57-1 $-1.89-3$	-1.48-1 $-1.99-3$	-1.24-1 $-2.08-3$	-8.86-2 $-2.14-3$
Z= 72, Hf: [Xe]			0.05-4	1,10-5	r	د—دن.،	1.70-3	1,00-0	1,33-3	2.00-3	2,14-3
12, III. [AC]	5/2 4	k (eV)									
Shell		1500	2000	3000	4000	5000	6000	7000	8000	9000	10000
4s _{1/2}	σ	2.302+1	1.502+1	7.801+0	4.746+0	3.179+0	2.270+0	1.698+0	1.316+0	1.047+0	8.514-1
$E_b =$	β	1.900	1.909	1.920	1.929	1.936	1.942	1.947	1.951	1.955	1.957

able 1 (contin	ued)										
538.1 eV	γ δ	5.01-1 -2.50-4	3.79-1 -6.75-4	1.71-1 -1.19-3	2.44-2 -1.51-3	-7.11-2 -1.74-3	-1.27-1 -1.91-3	-1.54-1 $-2.05-3$	-1.59-1 $-2.16-3$	-1.46-1 $-2.26-3$	-1.19-1 -2.34-3
4p _{1/2}	σ	2.708+1	1.835+1	9.645+0	5.764+0	3.753+0	2.595+0	1.877+0	1.405+0	1.082+0	8.514-1
$E_b = 437.0 \text{ eV}$	$eta \gamma$	1.545 2.87-1	1.635 1.23-1	1.687 -1.36-2	1.685 9.52-3	1.665 1.04-1	1.639 2.27-1	1.609 3.62-1	1.578 4.98-1	1.546 6.30-1	1.514 7.57-1
	δ	4.24-3	-1.75 - 3	-3.99 - 3	-3.83 - 3	-2.54 - 3	-2.22-4	2.99-3	6.95-3	1.15-2	1.65 - 2
$4p_{3/2}$	σ	6.450+1	4.077+1	1.972+1	1.118+1	6.999+0	4.694+0	3.309+0	2.425+0	1.831+0	1.417+0
$E_b = 380.4 \text{ eV}$	β γ	1.534 1.76-1	1.640 4.35-2	1.724 -4.41-2	1.746 1.09-2	1.744 1.30-1	1.731 2.76-1	1.711 4.30-1	1.688 5.84-1	1.663 7.33-1	1.636 8.76-1
300.4 C V	δ	3.41-3	7.22-4	3.51-3	6.95-3	9.91-3	1.27-2	1.55-2	1.84-2	2.15-2	2.46-2
4d _{3/2}	σ	8.002+1	4.427+1	1.694+1	7.944+0	4.251+0	2.493+0	1.564+0	1.033+0	7.107-1	5.054-1
$E_b = 223.8 \text{ eV}$	β	1.260 -4.41-2	1.347 2.03-2	1.375 2.66-1	1.339	1.284	1.224 9.45-1	1.164 1.11+0	1.105 1.25+0	1.049 1.37+0	0.997
223.0 EV	$\gamma \\ \delta$	1.10-2	2.39-2	4.60-2	5.23-1 6.53-2	7.51-1 8.37-2	1.02-1	1.20-1	1.37-1	1.55-1	1.48+0 1.72-1
4d _{5/2}	σ	1.149+2	6.260+1	2.350+1	1.088+1	5.761+0	3.349+0	2.085+0	1.368+0	9.349-1	6.608-1
$E_b =$	β	1.309	1.357	1.340	1.280	1.211	1.143	1.078	1.018	0.962	0.911
213.7 eV	$\gamma \\ \delta$	-3.94-2 1.10-2	4.25-2 2.28-2	3.01-1 4.52-2	5.55-1 6.71-2	7.73-1 8.90-2	9.54-1 1.11-1	1.11+0 1.32-1	1.24+0 1.53-1	1.35+0 1.73-1	1.44+0 1.93-1
4f _{5/2}	σ	3.973+1	1.506+1	3.480+0	1.161+0	4.817-1	2.308-1	1.224-1	7.006-2	4.250-2	2.701-2
$E_b =$	β	1.060	1.038	0.943	0.844	0.757	0.684	0.621	0.565	0.516	0.472
18.2 eV	$\gamma \\ \delta$	3.31-1 9.58-2	4.91-1 1.21-1	7.43-1 1.68-1	9.17-1 2.11-1	1.04+0 2.53-1	1.14+0 2.92-1	1.21+0 3.30-1	1.27+0 3.65-1	1.32+0 3.99-1	1.37+0
Af.		5.055+1	1.908+1	4.381+0	1.453+0	5.998-1	2.861-1	1.512-1	8.617-2	5.210-2	4.31-1 3.302-2
$ 4f_{7/2} \\ E_b = $	$\frac{\sigma}{\beta}$	1.056	1.029	0.932	0.835	0.752	0.682	0.623	0.572	0.526	0.485
16.3 eV	γ	3.40-1	5.01-1	7.53 - 1	9.27-1	1.05+0	1.14+0	1.21+0	1.27+0	1.32+0	1.36+0
	δ	9.57-2	1.21-1	1.68-1	2.13-1	2.56-1	2.96-1	3.35-1	3.71-1	4.05-1	4.37-1
$5s_{1/2} E_b =$	$\frac{\sigma}{\beta}$	4.022+0 1.911	2.536+0 1.917	1.280+0 1.926	7.691-1 1.933	5.110-1 1.939	3.629-1 1.945	2.703-1 1.949	2.087-1 1.953	1.657-1 1.956	1.345-1 1.958
64.9 eV	γ	3.46-1	2.55-1	9.39-2	-2.28-2	-9.82-2	-1.40-1	-1.57 - 1	-1.54-1	-1.35-1	-1.05-1
	δ	-5.29-4	-8.28-4	-1.24-3	-1.52-3	-1.73-3	-1.89-3	-2.02-3	-2.13-3	-2.22-3	-2.30-3
$5p_{1/2}$	σ	3.784+0	2.474+0	1.266+0	7.489-1	4.846-1	3.339-1	2.409-1	1.801-1	1.384-1	1.089-1
$E_b = 38.2 \text{ eV}$	β γ	1.655 1.65-1	1.698 5.14-2	1.714 $-2.07-2$	1.699 2.80-2	1.674 1.32-1	1.643 2.59-1	1.611 3.93-1	1.578 5.28-1	1.545 6.58-1	1.513 7.83-1
	δ	-3.59 - 3	-4.44-3	-4.76 - 3	-4.38 - 3	-3.07 - 3	-7.53-4	2.49-3	6.50-3	1.11-2	1.62-2
$5p_{3/2}$	σ	8.322+0	5.144+0	2.447+0	1.378+0	8.597-1	5.753-1	4.050-1	2.965-1	2.238-1	1.731-1
$E_b = 29.0 \text{ eV}$	β γ	1.632 9.14-2	1.699 -1.84-4	1.751 -3.97-2	1.761 3.40-2	1.753 1.60-1	1.736 3.07-1	1.714 4.60-1	1.689 6.12-1	1.663 7.59-1	1.635 9.00-1
23.0 C V	δ	-1.44-3	-3.77-4	3.40-3	6.59-3	9.30-3	1.19-2	1.46-2	1.75-2	2.07-2	2.40-2
5d _{3/2}	σ	3.459+0	1.912+0	7.356-1	3.465-1	1.860-1	1.093-1	6.872-2	4.548-2	3.134-2	2.231-2
$E_b =$	β	1.337	1.390	1.392	1.347	1.288	1.226	1.165	1.106	1.051	0.997
6.6 eV	$\gamma \\ \delta$	-2.95-2 $1.14-2$	4.70-2 2.36-2	2.92-1 4.42-2	5.45-1 6.27-2	7.67-1 8.09-2	9.58-1 9.93-2	1.12+0 1.18-1	1.26+0 1.36-1	1.38+0 1.55-1	1.49+0 1.73-1
6s _{1/2}	σ	2.979-1	1.867-1	9.374-2	5.616-2	3.725-2	2.642-2	1.966-2	1.517-2	1.203-2	9.759-3
$E_b =$	β	1.912	1.918	1.926	1.933	1.939	1.944	1.949	1.953	1.956	1.958
7.0 eV	$\gamma \\ \delta$	3.37-1 -5.49-4	2.47 - 1 $-8.41 - 4$	8.83-2 $-1.25-3$	-2.70-2 $-1.54-3$	-1.02-1 $-1.75-3$	-1.43-1 $-1.91-3$	-1.59-1 $-2.04-3$	-1.55-1 $-2.14-3$	-1.35-1 $-2.23-3$	-1.03-1 -2.30-3
7- 72 Tav [V		$\frac{3.43}{4f_{7/2}^8 5d_{3/2}^3 6s_{1/2}^2}$	0,41 4	1,23 3	1.54 5	1.73 3	1.51 5	2.04 3	2,14 3	2,23 3	2.50
Z- 73, 1a. [A	CJ415/2	k (eV)									
Shell		1500	2000	3000	4000	5000	6000	7000	8000	9000	10000
4s _{1/2}	σ	2.341+1	1.535+1	8.018+0	4.896+0	3.287+0	2.351+0	1.761+0	1.365+0	1.088+0	8.850-1
$E_b =$	β	1.892	1.903	1.915	1.923	1.931	1.937	1.943	1.947	1.951	1.954
565.5 eV	γ	5.25-1	4.03-1	1.94-1	4.29-2	-5.81-2	-1.20-1	-1.53-1	-1.62-1	-1.54-1	-1.32-
	δ	-2.06-4	-6.81-4	-1.24-3	-1.60-3	-1.85-3	-2.04-3	-2.20-3	-2.32-3	-2.43-3	-2.52-3
$\begin{array}{l} 4p_{1/2} \\ E_b = \end{array}$	$\frac{\sigma}{eta}$	2.744+1 1.526	1.876+1 1.626	9.962+0 1.684	5.992+0 1.686	3.919+0 1.669	2.719+0 1.645	1.972+0 1.616	1.480+0 1.586	1.142+0 1.555	9.003-1 1.524
464.8 eV	γ	3.16-1	1.46 - 1	-7.93 - 3	1.40-3	8.63-2	2.04-1	3.35-1	4.69-1	6.00-1	7.25 - 1
	δ	5.47-3	-1.48 - 3	-4.16-3	-4.14 - 3	-3.02 - 3	-9.18 - 4	2.05-3	5.76-3	9.99-3	1.47-2
$4p_{3/2}$	σ	6.648+1	4.221+1	2.054+1	1.169+1	7.343+0	4.936+0	3.487+0	2.559+0	1.935+0	1.499+0
$E_b = 404.5 \text{ eV}$	β γ	1.513 1.95-1	1.628 5.85-2	1.719 -4.43-2	1.746 -1.29-3	1.747 1.10-1	1.736 2.51-1	1.719 4.02-1	1.697 5.54-1	1.673 7.02-1	1.647 8.44-1
	δ	4.21-3	7.30-4	3.30-3	6.85-3	9.89-3	1.26-2	1.54-2	1.81-2	2.10-2	2.40-2
4d _{3/2}	σ	8.387+1	4.684+1	1.812+1	8.557+0	4.600+0	2.708+0	1.703+0	1.128+0	7.778-1	5.542-1
$E_b = 241.3 \text{ eV}$	β	1.245 -4.61-2	1.340 6.40-3	1.377 2.41-1	1.347 4.98-1	1.296 7.27-1	1.237 9.24-1	1.178 1.09+0	1.121 1.23+0	1.066 1.36+0	1.014 1.47+0
∠+1.J EV	$\frac{\gamma}{\delta}$	9.74-3	0.40-3 $2.25-2$	4.46-2	4.98-1 6.36-2	8.17-2	9.24—1 9.93—2	1.09+0 1.17-1	1.23+0	1.51-1	1.47+0 1.67-1
4d _{5/2}	σ	1.204+2	6.615+1	2.510+1	1.169+1	6.221+0	3.629+0	2.265+0	1.489+0	1.020+0	7.227-1
$E_b =$	β	1.300	1.355	1.344	1.288	1.221	1.154	1.090	1.031	0.976	0.925
229.3 eV	$\gamma \\ \delta$	-4.35-2 $9.93-3$	2.79-2 2.14-2	2.78-1 4.35-2	5.32-1 6.50-2	7.53-1 8.65-2	9.37-1 1.08-1	1.09+0 1.29-1	1.22+0 1.49-1	1.34+0 1.69-1	1.44+0 1.89-1
	0	<i>∍.∍</i> ɔ−ɔ	2.14-2	4. JJ−2	0.30-2	0.03-2	1.00-1	1.29-1	1.49-1	1.09-1	1.09-1

Tabl	le 1 i	(continued)	

$4f_{5/2}$ $E_b =$ 27.5 eV	σ	4.565+1	1.745+1	4.076+0	1.368+0	5.696-1	2.737-1	1.456-1	8.349-2	5.076-2	3.233-2
	β	1.059	1.042	0.952	0.855	0.768	0.695	0.631	0.577	0.527	0.482
	γ	3.16-1	4.75-1	7.32-1	9.12-1	1.04+0	1.14+0	1.22+0	1.28+0	1.33+0	1.38+0
	δ	9.40-2	1.19-1	1.65-1	2.08-1	2.49-1	2.88-1	3.25-1	3.61-1	3.94-1	4.26-1
$4f_{7/2}$ $E_b =$ 25.6 eV	$\sigma \ eta \ eta \ \gamma \ \delta$	5.829+1 1.055 3.25-1 9.39-2	2.220+1 1.033 4.86-1 1.19-1	5.149+0 0.940 7.43-1 1.66-1	1.718+0 0.845 9.22-1 2.10-1	7.116-1 0.762 1.05+0 2.53-1	3.404-1 0.692 1.14+0 2.92-1	1.803-1 0.633 1.22+0 3.30-1	1.030-1 0.582 1.28+0 3.67-1	6.241-2 0.536 1.33+0 4.01-1	3.963-2 0.495 1.37+0 4.32-1
$5s_{1/2}$ $E_b = 71.1 \text{ eV}$	σ	4.255+0	2.688+0	1.362+0	8.205-1	5.462-1	3.885-1	2.897-1	2.239-1	1.778-1	1.444-1
	β	1.905	1.912	1.921	1.928	1.934	1.940	1.945	1.949	1.952	1.955
	γ	3.60-1	2.72-1	1.11-1	-9.22-3	-8.92-2	-1.36-1	-1.58-1	-1.59-1	-1.45-1	-1.19-1
	δ	-5.40-4	-8.62-4	-1.31-3	-1.62-3	-1.85-3	-2.03-3	-2.17-3	-2.29-3	-2.40-3	-2.48-3
$5p_{1/2}$ $E_b = 43.7 \text{ eV}$	σ	4.009+0	2.633+0	1.359+0	8.080-1	5.251-1	3.629-1	2.625-1	1.967-1	1.515-1	1.194-1
	β	1.648	1.695	1.715	1.702	1.678	1.649	1.618	1.587	1.555	1.523
	γ	1.83-1	6.49-2	-1.99-2	1.82-2	1.15-1	2.37-1	3.68-1	5.00-1	6.30-1	7.54-1
	δ	-3.68-3	-4.61-3	-4.98-3	-4.71-3	-3.56-3	-1.45-3	1.55-3	5.31-3	9.62-3	1.44-2
$5p_{3/2}$ $E_b = 34.7 \text{ eV}$	σ	9.034+0	5.598+0	2.676+0	1.513+0	9.466-1	6.348-1	4.477-1	3.282-1	2.480-1	1.921-1
	β	1.622	1.692	1.749	1.762	1.757	1.742	1.722	1.698	1.673	1.646
	γ	1.04-1	8.25-3	-4.27-2	2.14-2	1.40-1	2.83-1	4.34-1	5.85-1	7.31-1	8.71-1
	δ	-1.54-3	-6.15-4	3.22-3	6.53-3	9.30-3	1.19-2	1.45-2	1.73-2	2.02-2	2.33-2
$5d_{3/2}$ $E_b = 5.7 \text{ eV}$	σ β γ δ	4.317+0 1.330 -3.31-2 1.03-2	2.406+0 1.388 3.49-2 2.24-2	9.363-1 1.397 2.71-1 4.29-2	4.443-1 1.356 5.22-1 6.12-2	2.397-1 1.300 7.46-1 7.92-2	1.415-1 1.240 9.40-1 9.72-2	8.922-2 1.180 1.11+0 1.15-1	5.919-2 1.122 1.25+0 1.33-1	4.088-2 1.066 1.37+0 1.51-1	2.917-2 1.013 1.48+0 1.68-1
$6s_{1/2}$ $E_b = 8.0 \text{ eV}$	σ	3.302-1	2.072-1	1.043-1	6.267-2	4.164-2	2.957-2	2.203-2	1.701-2	1.350-2	1.096-2
	β	1.906	1.912	1.920	1.928	1.934	1.940	1.945	1.949	1.952	1.955
	γ	3.51-1	2.63-1	1.04-1	-1.42-2	-9.33-2	-1.40-1	-1.60-1	-1.60-1	-1.44-1	-1.17-1
	δ	-5.66-4	-8.79-4	-1.33-3	-1.64-3	-1.87-3	-2.04-3	-2.18-3	-2.29-3	-2.39-3	-2.46-3

Z= 74, W: [Xe] $4f_{5/2}^6 4f_{7/2}^8 5d_{3/2}^4 6s_{1/2}^2$

		k (eV)									
Shell		1500	2000	3000	4000	5000	6000	7000	8000	9000	10000
$4s_{1/2}$ $E_b = 595.0 \text{ eV}$	σ	2.379+1	1.568+1	8.236+0	5.047+0	3.396+0	2.434+0	1.825+0	1.416+0	1.129+0	9.195-1
	β	1.884	1.896	1.909	1.918	1.925	1.932	1.938	1.942	1.946	1.950
	γ	5.50-1	4.28-1	2.17-1	6.26-2	-4.36-2	-1.12-1	-1.50-1	-1.65-1	-1.61-1	-1.44-1
	δ	-1.50-4	-6.82-4	-1.30-3	-1.69-3	-1.97-3	-2.18-3	-2.35-3	-2.49-3	-2.61-3	-2.71-3
$4p_{1/2}$ $E_b =$ 491.6 eV	σ β γ δ	2.777+1 1.507 3.44-1 6.82-3	1.914+1 1.617 1.70-1 -1.17-3	1.027+1 1.681 -4.96-4 -4.31-3	6.219+0 1.687 -5.01-3 -4.44-3	4.086+0 1.673 7.03-2 -3.48-3	2.845+0 1.650 1.82-1 -1.57-3	2.070+0 1.623 3.09-1 1.17-3	1.557+0 1.594 4.40-1 4.61-3	1.203+0 1.564 5.69-1 8.65-3	9.506-1 1.534 6.94-1 1.31-2
$4p_{3/2}$ $E_b = 425.3 \text{ eV}$	σ	6.838+1	4.361+1	2.136+1	1.221+1	7.692+0	5.182+0	3.668+0	2.696+0	2.042+0	1.584+0
	β	1.494	1.617	1.714	1.745	1.750	1.741	1.726	1.705	1.683	1.658
	γ	2.13-1	7.33-2	-4.31-2	-1.18-2	9.10-2	2.26-1	3.74-1	5.24-1	6.71-1	8.12-1
	δ	5.05-3	7.77-4	3.09-3	6.74-3	9.86-3	1.27-2	1.53-2	1.80-2	2.07-2	2.35-2
$4d_{3/2}$ $E_b = 258.8 \text{ eV}$	σ	8.775+1	4.946+1	1.936+1	9.201+0	4.970+0	2.936+0	1.853+0	1.230+0	8.498-1	6.068-1
	β	1.229	1.333	1.379	1.354	1.306	1.251	1.193	1.137	1.083	1.032
	γ	-4.63-2	-6.06-3	2.17-1	4.72-1	7.03-1	9.03-1	1.07+0	1.22+0	1.35+0	1.46+0
	δ	8.61-3	2.10-2	4.31-2	6.20-2	7.98-2	9.70-2	1.14-1	1.30-1	1.47-1	1.63-1
$4d_{5/2}$ $E_b = 245.4 \text{ eV}$	σ	1.259+2	6.980+1	2.677+1	1.255+1	6.708+0	3.926+0	2.458+0	1.620+0	1.112+0	7.891-1
	β	1.292	1.352	1.349	1.296	1.232	1.166	1.103	1.044	0.989	0.939
	γ	-4.62-2	1.44-2	2.56-1	5.09-1	7.32-1	9.19-1	1.08+0	1.21+0	1.33+0	1.43+0
	δ	8.95-3	2.00-2	4.18-2	6.30-2	8.42-2	1.05-1	1.25-1	1.45-1	1.65-1	1.84-1
$4f_{5/2}$ $E_b = 37.4 \text{ eV}$	σ	5.206+1	2.008+1	4.740+0	1.600+0	6.687-1	3.223-1	1.718-1	9.876-2	6.017-2	3.840-2
	β	1.058	1.045	0.961	0.866	0.779	0.706	0.642	0.587	0.538	0.492
	γ	3.00-1	4.59-1	7.20-1	9.06-1	1.04+0	1.14+0	1.22+0	1.28+0	1.34+0	1.38+0
	δ	9.20-2	1.17-1	1.63-1	2.06-1	2.46-1	2.84-1	3.21-1	3.56-1	3.90-1	4.21-1
$4f_{7/2}$ $E_b =$ 35.1 eV	σ β γ δ	6.659+1 1.055 3.09-1 9.20-2	2.559+1 1.037 4.70-1 1.17-1	5.999+0 0.949 7.32-1 1.63-1	2.013+0 0.855 9.16-1 2.07-1	8.370-1 0.772 1.05+0 2.49-1	4.015-1 0.702 1.15+0 2.88-1	2.131-1 0.643 1.22+0 3.26-1	1.220-1 0.591 1.28+0 3.62-1	7.410-2 0.546 1.34+0 3.96-1	4.714-2 0.504 1.38+0 4.28-1
$5s_{1/2}$ $E_b = 77.1 \text{ eV}$	σ	4.491+0	2.842+0	1.445+0	8.728-1	5.822-1	4.147-1	3.096-1	2.394-1	1.903-1	1.547-1
	β	1.899	1.906	1.915	1.923	1.929	1.935	1.940	1.945	1.948	1.951
	γ	3.75-1	2.88-1	1.28-1	5.15-3	-7.90-2	-1.31-1	-1.58-1	-1.64-1	-1.54-1	-1.32-1
	δ	-5.50-4	-8.97-4	-1.38-3	-1.72-3	-1.97-3	-2.17-3	-2.33-3	-2.46-3	-2.58-3	-2.67-3
$5p_{1/2}$ $E_b =$ 46.7 eV	σ	4.230+0	2.791+0	1.451+0	8.677-1	5.663-1	3.928-1	2.849-1	2.139-1	1.651-1	1.303-1
	β	1.642	1.691	1.715	1.705	1.683	1.655	1.626	1.595	1.564	1.533
	γ	2.00-1	7.86-2	-1.79-2	9.85-3	9.86-2	2.15-1	3.44-1	4.74-1	6.01-1	7.24-1
	δ	-3.78-3	-4.80-3	-5.21-3	-5.02-3	-4.02-3	-2.11-3	6.61-4	4.17-3	8.21-3	1.27-2

$5p_{3/2}$ $E_b =$	$\frac{\sigma}{eta}$	9.743+0 1.613	6.052+0 1.686	2.908+0 1.747	1.650+0 1.763	1.035+0 1.760	6.960-1 1.748	4.918-1 1.729	3.611-1 1.707	2.733-1 1.683	2.119-1 1.658
36.5 eV	$_{\delta}^{\gamma}$	1.15-1 -1.61-3	1.66-2 $-8.46-4$	-4.46-2 3.04 -3	1.00-2 $6.47-3$	1.22-1 9.31-3	2.60-1 1.19-2	4.08 - 1 $1.44 - 2$	5.57-1 1.71-2	7.02-1 1.99-2	8.41-1 $2.27-2$
$5d_{3/2}$ $E_b =$	σ β	5.161+0 1.323	2.899+0 1.385	1.141+0 1.401	5.453-1 1.365	2.957-1 1.311	1.752-1 1.253	1.108-1 1.195	7.372-2 1.137	5.103-2 1.082	3.649-2 1.029
6.1 eV	γ δ	-3.57-2 9.27-3	2.35-2 2.12-2	2.50-1 4.16-2	4.99-1 5.97-2	7.24–1 7.73–2	9.21-1 9.49-2	1.195 1.09+0 1.12-1	1.23+0 1.30-1	1.36+0 1.47-1	1.47+0 1.63-1
6s _{1/2}	σ	3.593-1	2.257-1	1.139-1	6.861-2	4.567-2	3.248-2	2.422-2	1.871-2	1.486-2	1.207-2
$E_b = 8.0 \text{ eV}$	β γ	1.899 3.65-1	1.906 2.79-1	1.915 1.21-1	1.922 -5.43-4	1.929 -8.37-2	1.935 -1.34-1	1.940 -1.59-1	1.945 -1.63-1	1.949 -1.52-1	1.952 -1.29-1
	δ	-5.80-4	-9.17-4	-1.40-3	-1.74-3	-1.99-3	-2.18-3	-2.33-3	-2.45-3	-2.56-3	-2.64-3
Z= 75, Re: [X	e]4f _{5/2} 4	k (eV)	6s _{1/2}								
Shell		1500	2000	3000	4000	5000	6000	7000	8000	9000	10000
4s _{1/2}	σ	2.414+1	1.599+1	8.450+0	5.196+0	3.505+0	2.516+0	1.890+0	1.468+0	1.171+0	9.544-1
$E_b =$	β	1.874	1.888	1.902	1.912	1.920	1.926	1.932	1.937	1.942	1.945
625.0 eV	$\frac{\gamma}{\delta}$	5.74-1 -7.97-5	4.53-1 -6.75-4	2.42 - 1 $-1.36 - 3$	8.33-2 $-1.78-3$	-2.80-2 $-2.09-3$	-1.01-1 $-2.32-3$	-1.45-1 $-2.51-3$	-1.65-1 $-2.66-3$	-1.67-1 $-2.80-3$	-1.54-1 $-2.90-3$
$4p_{1/2}$	σ_{β}	2.803+1 1.487	1.949+1 1.606	1.057+1 1.678	6.441+0 1.687	4.252+0 1.675	2.972+0 1.655	2.168+0 1.629	1.635+0 1.602	1.266+0 1.573	1.002+0 1.544
$E_b = 517.9 \text{ eV}$	β γ	3.71 - 1	1.96-1	8.57 - 3	-9.70 - 3	5.58-2	1.61 - 1	2.83 - 1	4.11 - 1	5.38 - 1	6.62-1
	δ	8.30-3	-7.97-4	-4.46-3	-4.72-3	-3.90-3	-2.18-3	3.64-4	3.57-3	7.34-3	1.16-2
$4p_{3/2}$ $E_b =$	$\frac{\sigma}{\beta}$	7.025+1 1.476	4.500+1 1.604	2.217+1 1.708	1.273+1 1.743	8.046+0 1.751	5.434+0 1.745	3.854+0 1.732	2.837+0 1.713	2.152+0 1.692	1.671+0 1.669
444.4 eV	γ	2.30 - 1	8.82-2	-4.07 - 2	-2.09-2	7.34 - 2	2.03 - 1	3.47 - 1	4.95 - 1	6.40 - 1	7.80 - 1
4d _{3/2}	$\frac{\delta}{\sigma}$	5.97-3 9.141+1	8.70-4 5.200+1	2.87-3 2.058+1	6.62-3 9.855+0	9.84-3 5.350+0	1.27-2 3.172+0	1.53-2 2.008+0	1.79-2 1.336+0	2.04-2 9.254-1	2.31-2 6.621-1
$E_b =$	β	1.213	1.324	1.380	1.361	1.316	1.263	1.207	1.152	1.100	1.050
273.7 eV	δ	-4.50-2 $7.65-3$	-1.65-2 $1.97-2$	1.94-1 4.17-2	4.45 - 1 $6.04 - 2$	6.78 - 1 $7.80 - 2$	8.81-1 9.47-2	1.05+0 1.11-1	1.20+0 1.27-1	1.33+0 1.43-1	1.45+0 1.60-1
4d _{5/2}	σ	1.315+2	7.349+1	2.848+1	1.344+1	7.219+0	4.240+0	2.662+0	1.759+0	1.210+0	8.601-1
$E_b = 260.2 \text{ eV}$	β γ	1.282 $-4.74-2$	1.349 2.45-3	1.353 2.34-1	1.304 4.86-1	1.242 7.11-1	1.177 9.01-1	1.115 1.06+0	1.057 1.20+0	1.003 1.32+0	0.953 1.42+0
	δ	8.10-3	1.87-2	4.01-2	6.10-2	8.19-2	1.02-1	1.22-1	1.42-1	1.61-1	1.81-1
$4f_{5/2}$ $E_b =$	$\frac{\sigma}{\beta}$	5.910+1 1.056	2.299+1 1.048	5.486+0 0.970	1.863+0 0.876	7.817—1 0.791	3.778-1 0.716	2.019-1 0.653	1.163-1 0.597	7.100-2 0.548	4.540-2 0.502
48.1 eV	γ	2.84-1 9.00-2	4.43-1 1.14-1	7.08-1 1.60-1	8.98-1 2.03-1	1.04+0 2.42-1	1.14+0 2.80-1	1.22+0 3.17-1	1.29+0 3.52-1	1.34+0 3.85-1	1.39+0 4.16-1
4f _{7/2}	σ	7.545+1	2.924+1	6.930+0	2.339+0	9.763-1	4.696-1	2.499-1	1.434-1	8.722-2	5.559-2
$E_b = 45.7 \text{ eV}$	β γ	1.053 2.94-1	1.040 4.54-1	0.957 7.20-1	0.865 9.10-1	0.782 1.05+0	0.712 1.15+0	0.652 1.23+0	0.601 1.29+0	0.555 1.34+0	0.513 1.39+0
15.7 C V	δ	8.99-2	1.14-1	1.61-1	2.04-1	2.46-1	2.84-1	3.22-1	3.57-1	3.91-1	4.23-1
$5s_{1/2}$ $E_b =$	$\frac{\sigma}{\beta}$	4.732+0 1.892	2.999+0 1.899	1.530+0 1.909	9.266-1 1.917	6.193-1 1.924	4.418-1 1.930	3.302-1 1.935	2.556-1 1.940	2.033-1 1.944	1.653-1 1.947
82.8 eV	γ	3.89 - 1	3.05 - 1	1.45 - 1	2.02 - 2	-6.80 - 2	-1.25-1	-1.56-1	-1.67 - 1	-1.61-1	-1.43-1
F	δ	-5.56-4	-9.30-4	-1.46-3	-1.82-3	-2.10-3	-2.31-3	-2.49-3	-2.64-3	-2.76-3	-2.86-3
$5p_{1/2}$ $E_b =$	$\frac{\sigma}{\beta}$	4.493+0 1.635	2.977+0 1.687	1.559+0 1.714	9.380—1 1.707	6.148-1 1.687	4.278-1 1.661	3.112-1 1.633	2.342-1 1.603	1.811-1 1.573	1.432-1 1.543
48.4 eV	γ	2.17-1	9.28-2	-1.47 - 2	2.77-3	8.36-2	1.95-1	3.19-1	4.47-1	5.73-1	6.94-1
5p _{3/2}	$\frac{\delta}{\sigma}$	-3.90-3 1.043+1	-5.02-3 6.493+0	-5.45-3 3.134+0	-5.31-3 1.785+0	-4.45-3 1.124+0	-2.73-3 7.571-1	-1.78-4 $5.360-1$	3.07-3 3.942-1	6.86-3 2.987-1	1.12-2 2.320-1
$E_b =$	β	1.603	1.678	1.744	1.764	1.763	1.753	1.736	1.715	1.693	1.668
36.8 eV	$\delta \gamma$	1.26-1 -1.67-3	2.51-2 $-1.08-3$	-4.55-2 $2.84-3$	-1.78-4 $6.40-3$	1.05 - 1 $9.32 - 3$	2.38-1 1.19-2	3.83-1 1.44-2	5.29-1 1.70-2	6.73-1 1.96-2	8.12-1 2.23-2
5d _{3/2}	σ	6.037+0	3.416+0	1.359+0	6.545-1	3.568-1	2.123-1	1.347-1	8.984-2	6.233-2	4.466-2
$E_b = 3.8 \text{ eV}$	β γ	1.315 -3.73-2	1.382 1.36-2	1.405 2.31-1	1.372 4.75-1	1.322 7.02-1	1.266 9.01-1	1.208 1.07+0	1.152 1.22+0	1.097 1.35+0	1.045 1.46+0
	δ	8.30-3	2.01-2	4.03-2	5.81-2	7.55-2	9.27-2	1.10-1	1.26-1	1.43-1	1.59-1
$5d_{5/2}$ $E_b =$	$\sigma \ eta$	8.076+0 1.363	4.499+0 1.392	1.754+0 1.367	8.328-1 1.309	4.490-1 1.243	2.646-1 1.177	1.665-1 1.114	1.102-1 1.055	7.597-2 1.000	5.409-2 0.948
2.5 eV	ρ γ δ	-3.44-2	3.42 - 2	2.68 - 1	5.12 - 1	7.30 - 1	9.17 - 1	1.08+0	1.21+0	1.33+0	1.43+0
Co		8.54-3	1.89-2	3.90-2	5.92-2	7.98-2	1.01-1	1.22-1	1.42-1	1.62-1	1.80-1
	σ	3.909 - 1	2.457 - 1	1.244 - 1	7.506 - 2	5.006 - 2	3.565 - 2	2.661 - 2	2.058 - 2	1.636 - 2	1.329 - 2
$6s_{1/2}$ $E_b =$	β	1.892	1.899	1.909	1.917	1.923	1.930	1.935	1.940	1.944	1.948

Table 1 (continued)

Z= 76, Os: [Xe] $4f_{5/2}^6$ $4f_{7/2}^8$ $5d_{3/2}^4$ $5d_{5/2}^2$ $6s_{1/2}^2$

7.423+1

1.430

β

 $4p_{3/2} E_b =$

2.391+1

1.693

4.797+1

1.572

1.384+1

1.738

8.798+0

1.753

5.970+0

1.752

4.250+0

1.743

3.139+0

1.728

Chall		k (eV)	2000	2000	4000	E000	COOC	7000	9000	0000	10000
Shell		1500	2000	3000	4000	5000	6000	7000	8000	9000	10000
ls _{1/2}	$\frac{\sigma}{\beta}$	2.447+1 1.864	1.629+1 1.880	8.657+0 1.895	5.343+0 1.905	3.613+0 1.913	2.599+0 1.921	1.954+0 1.927	1.520+0 1.932	1.214+0 1.937	9.898-1 1.941
$E_b = 654.3 \text{ eV}$	ρ γ	5.97—1	4.78-1	2.67-1	1.905	-1.12-2	-8.98-2	-1.39-1	-1.64-1	-1.71-1	-1.63-1
)34.3 CV	δ	4.10-6	-6.60-4	-1.42-3	-1.88 - 3	-2.21-3	-2.47 - 3	-2.68-3	-2.85-3	-2.99-3	-3.11-3
1p _{1/2}	σ	2.825+1	1.982+1	1.086+1	6.663+0	4.420+0	3.101+0	2.269+0	1.715+0	1.331+0	1.055+0
$E_b =$	β	1.465	1.593	1.674	1.687	1.678	1.659	1.635	1.609	1.581	1.553
546.5 eV	γ	3.99-1	2.23-1	1.96-2	-1.28-2	4.24-2	1.40-1	2.58-1	3.83-1	5.08-1	6.30-1
	δ	1.01 - 2	-3.24 - 4	-4.62 - 3	-5.00 - 3	-4.31 - 3	-2.76 - 3	-4.26 - 4	2.60 - 3	6.16 - 3	1.02 - 2
$4p_{3/2}$	σ	7.221+1	4.646+1	2.303+1	1.327+1	8.416+0	5.698+0	4.049+0	2.985+0	2.267+0	1.763+0
$E_b =$	β	1.455	1.589	1.701	1.741	1.752	1.749	1.737	1.721	1.701	1.679
468.2 eV	γ	2.48-1	1.05-1	-3.71-2	-2.91-2	5.63-2	1.80-1	3.20-1	4.66-1	6.09-1	7.49-1
	δ	7.18-3	1.04-3	2.63-3	6.47-3	9.81-3	1.27-2	1.53-2	1.79-2	2.04-2	2.29-2
$d_{3/2}$	σ	9.510+1	5.459+1	2.185+1	1.054+1	5.749+0	3.422+0	2.172+0	1.449+0	1.006+0	7.212-1
$E_b = 289.4 \text{ eV}$	β	1.195 -4.24-2	1.314 -2.57-2	1.380 1.72-1	1.367 4.19-1	1.326 6.53-1	1.275 8.58-1	1.221 1.03+0	1.168 1.19+0	1.116 1.32+0	1.067 1.44+0
203.4 CV	$_{\delta}^{\gamma}$	6.79-3	1.84-2	4.03-2	5.89-2	7.62-2	9.27-2	1.05+0	1.19+0	1.40-1	1.56-1
4d _{5/2}	σ	1.369+2	7.716+1	3.022+1	1.436+1	7.749+0	4.569+0	2.876+0	1.905+0	1.313+0	9.353-1
$E_b =$	β	1.273	1.345	1.356	1.311	1.251	1.189	1.127	1.069	1.016	0.966
272.8 eV	γ	-4.74-2	-7.87-3	2.14-1	4.63-1	6.89-1	8.82-1	1.05+0	1.18+0	1.31+0	1.41+0
	δ	7.39 - 3	1.76 - 2	3.85 - 2	5.90 - 2	7.96 - 2	9.99 - 2	1.20 - 1	1.39 - 1	1.58 - 1	1.77 - 1
$f_{5/2}$	σ	6.612+1	2.598+1	6.276+0	2.147+0	9.049-1	4.388-1	2.351-1	1.358-1	8.305-2	5.321-2
$E_b =$	β	1.053	1.050	0.977	0.887	0.802	0.727	0.663	0.608	0.558	0.512
53.8 eV	γ	2.69-1	4.27 - 1	6.94-1	8.90-1	1.03+0	1.14+0	1.22+0	1.29+0	1.35+0	1.40+0
	δ	8.80-2	1.12-1	1.58-1	2.00-1	2.39-1	2.77-1	3.13-1	3.47-1	3.80-1	4.11-1
$4f_{7/2}$	σ	8.427+1	3.298+1	7.913+0	2.690+0	1.128+0	5.443-1	2.904-1	1.670-1	1.018-1	6.501-2
$E_b = 51.0 \text{ eV}$	β	1.052	1.042	0.965	0.875	0.792	0.722	0.662	0.610 1.29+0	0.564	0.521
51.0 ev	$_{\delta}^{\gamma}$	2.80-1 8.80-2	4.39-1 1.12-1	7.07-1 1.58-1	9.02-1 $2.02-1$	1.04+0 2.42-1	1.15+0 2.81-1	1.23+0 3.18-1	3.53-1	1.35+0 3.87-1	1.39+0 4.18-1
· c		4.964+0	3.151+0	1.613+0	9.797-1	6.563-1	4.690-1	3.510-1	2.719-1	2.165-1	1.761-1
$\dot{s}_{1/2}$ $\dot{s}_b =$	$\frac{\sigma}{eta}$	1.884	1.892	1.903	9.797—1 1.911	1.918	4.690—1 1.925	3.510—1 1.930	2.719—1 1.935	2.165 – 1 1.939	1.761-1
83.7 eV	γ	4.03-1	3.21-1	1.62-1	3.53-2	-5.61-2	-1.17 - 1	-1.53-1	-1.68-1	-1.67 - 1	-1.53-1
	δ	-5.61-4	-9.63 - 4	-1.53 - 3	-1.93 - 3	-2.23 - 3	-2.46 - 3	-2.66-3	-2.82 - 3	-2.96 - 3	-3.07 - 3
$p_{1/2}$	σ	4.763+0	3.169+0	1.671+0	1.011+0	6.653-1	4.645-1	3.388-1	2.555-1	1.980-1	1.568-1
$E_b =$	β	1.625	1.681	1.713	1.709	1.691	1.666	1.639	1.611	1.581	1.552
58.0 eV	γ	2.39-1	1.10-1	-1.01-2	-3.50-3	6.90-2	1.74-1	2.95-1	4.20-1	5.44-1	6.64-1
	δ	-3.99-3	-5.28-3	-5.73-3	-5.62-3	-4.89-3	-3.33-3	-9.98-4	2.03-3	5.61-3	9.69-3
$p_{3/2}$	σ	1.116+1	6.961+0	3.373+0	1.928+0	1.217+0	8.215-1	5.827-1	4.291-1	3.256-1	2.531-1
$E_b = 45.4 \text{ eV}$	β	1.589 1.40-1	1.669 3.55-2	1.740 -4.56-2	1.763 -1.00-2	1.766 8.73-2	1.757 2.15-1	1.743 3.56-1	1.724 5.01-1	1.702 6.43-1	1.679 7.81-1
43.4 ev	$_{\delta}^{\gamma}$	-1.69-3	-1.34-3	2.60-3	6.31-3	9.32-3	1.20-2	1.44-2	1.69-2	1.94-2	2.19-2
5d _{3/2}	σ	6.910+0	3.938+0	1.584+0	7.681-1	4.210-1	2.515-1	1.601-1	1.071-1	7.446-2	5.346-2
$E_b =$	β	1.306	1.379	1.408	1.380	1.332	1.278	1.222	1.167	1.113	1.062
0.4 eV	γ	-3.80-2	4.73-3	2.12-1	4.53-1	6.80-1	8.80-1	1.05+0	1.20+0	1.33+0	1.45+0
	δ	7.40 - 3	1.90 - 2	3.91 - 2	5.66 - 2	7.37 - 2	9.05 - 2	1.07 - 1	1.23 - 1	1.39 - 1	1.55 - 1
5d _{5/2}	σ	9.315+0	5.224+0	2.057+0	9.834-1	5.328-1	3.152-1	1.990-1	1.320-1	9.119-2	6.506-2
$E_b =$	β	1.361	1.393	1.373	1.317	1.252	1.188	1.126	1.067	1.012	0.960
0.9 eV	γ	-3.69-2	2.42-2	2.50-1	4.92-1	7.11-1	9.00-1	1.06+0	1.20+0	1.32+0	1.42+0
	δ	7.75-3	1.79-2	3.76-2	5.73-2	7.76-2	9.82-2	1.19-1	1.39-1	1.58-1	1.76-1
$5s_{1/2}$	σ	4.203-1	2.643-1	1.341-1	8.114-2	5.421-2	3.866-2	2.889-2	2.236-2	1.779-2	1.447-2
$E_b =$	β	1.885	1.893	1.903	1.911 2.90-2	1.918 -6.16-2	1.924	1.930	1.935 -1.68-1	1.940	1.943
8.0 eV	$\gamma \\ \delta$	3.92-1 $-6.00-4$	3.10-1 $-9.87-4$	1.54-1 -1.55-3	-1.95-3	-6.16-2 -2.25-3	-1.21-1 $-2.48-3$	-1.55-1 $-2.66-3$	-1.68-1 -2.80-3	-1.65-1 $-2.93-3$	-1.51-1 $-3.03-3$
- 77 I [V-				1.55 3	1.55 3	2.23	2.10 3	2.00 3	2.00 3	2.33	3.03 3
z= //, ir: [xe	J41 _{5/2} 4	f _{7/2} 5d _{3/2} 5d _{5/2}	6S _{1/2}								
Chall		k (eV) 1500	2000	2000	4000	5000	6000	7000	9000	0000	10000
Shell			2000	3000	4000	5000	6000	7000	8000	9000	10000
1s _{1/2}	σ	2.480+1	1.659+1	8.871+0 1.887	5.494+0	3.724+0	2.684+0	2.021+0	1.573+0	1.257+0	1.026+0
$E_b = 690.1 \text{ eV}$	β	1.853 6.24-1	1.871 5.08-1	1.887 2.95-1	1.898 1.28-1	1.907 7.20—3	1.914 -7.64-2	1.921 -1.31-1	1.927 -1.61-1	1.931 -1.73-1	1.935 1.701
JJU, 1 CV	δ	1.16-4	-6.31-4	-1.47 - 3	-1.98 - 3	-2.34-3	-7.64-2 $-2.62-3$	-1.31-1 -2.85-3	-3.04-3	-3.20-3	-3.33-3
$1p_{1/2}$	σ	2.843+1	2.012+1	1.115+1	6.885+0	4.589+0	3.231+0	2.371+0	1.797+0	1.398+0	1.110+0
$E_b =$	β	1.440	1.579	1.669	1.686	1.680	1.663	1.641	1.616	1.589	1.562
577.1 eV	γ	4.27-1	2.52-1	3.26-2	-1.42-2	3.05-2	1.21-1	2.34-1	3.55-1	4.78-1	5.99-1
	δ	1.22-2	2.67 - 4	-4.78 - 3	-5.29 - 3	-4.71 - 3	-3.32 - 3	-1.15 - 3	1.66 - 3	5.04 - 3	8.83-3
		7 422 1	4707.1	2 201 - 1	1 20 4 . 1	0.700.0	F 070 · 0	4.250.0	2 120 . 0	2 207 . 0	1.050.0

(continued on next page)

1.859+0

1.689

2.387+0

1.709

	able 1 (continu	ued)										
5 = (a) β 1.172 1.303 1.302 1.322 1.235 1.237 1.135 1.237 1.304 γ -378-2 2.50-1 3.52-2 1.62-2 1.50-1 3.52-2 1.62-2 1.00-1 1.22-2 1.63-1 1.00-1 1.22-2 1.63-1 1.00-1 1.22-2 1.00-1 1.22-2 1.00-1 1.22-2 1.00-1 1.22-2 1.00-1 1.00-1 1.22-2 1.00-1	494.3 eV											7.17-1 2.27-2
131146	$4d_{3/2}$											7.851-1
1 1 1 1 1 1 1 1 1 1												
446/2 σ σ 1,431-2 8,131-1 3215-1 1,577-1 8,332-0 4,928-0 3,111-0 2,005-0 1,428-0 0.00	311.4 ev											1.52-1
5. ± or start of the property of the p	1d- :-											
2949 Y												
4f ₂ /c σ 7,378*1 2,331*1 7,161*0 2,466*0 1,044*0 5,078*1 2,756*1 1,678*1 9,671*2 6,208*6 63.8 w y 2,55*1 411*1 6,80*1 1,81*1 1,30*0 1,14*0 1,23*0 1,30*0												1.40+0
ξ̄s β 1051 1052 0.985 0.897 0.813 0.738 0.673 0.617 0.567 0.521 63 8.62-2 1.10-1 1.55-1 1.97-1 2.36-1 2.73-1 3.08-1 3.42-1 3.75-1 4.06-1 49/2: a 9.416+1 3.716-1 9.016-0 3.08-1 1.29-0 2.08-1 3.63-1 1.93-1 1.55-0 1.60-0 608 eV y 2.66-1 3.13-0 1.00-0 1.03-0 1.04-0 1.15-0 1.23-0 1.05-0 1.05-0 1.05-0 1.06-0 1.05-0 1.04-0 1.15-0 1.23-0 1.06-0 1.05-			6.68 - 3	1.64 - 2	3.70 - 2	5.70 - 2	7.73 - 2	9.74 - 2	1.17 - 1	1.36 - 1	1.54 - 1	1.73 - 1
63.8 (c) y 2.55-1 4.11-1 68.0-1 8.81-1 1.04-0 1.14+0 1.29-0 1.30-0 1.30-0 1.30-0 1.30-0 1.30-0 1.30-0 1.30-0 1.30-0 1.30-0 1.30-0 1.30-0 1.30-0 1.30-0 1.30-0 1.30-0 1.50-0 1.50-0 1.50-0 1.30-0 1.50-0 1.50-0 1.30-0 1.30-0 1.50-0 1.30-0 1.30-0 1.40-0 1.50-0 1.30-0 1.30-0 1.40-0 1.50-0 1.30-0 1.30-0 1.40-0 1.50-0 1.30-0 1.30-0 1.40-0 1.50-0 1.30-0 1.40-0 1.50-0 1.30-0 1.40-0 1.50-0 1.30-0 1.40-0 1.50-0 1.30-0 1.40-0 1.50-0 1.30-0 1.40-0 1.50-0 1.30-0 1.40-0 1.10-0 1.40-0 1.50-0 1.30-0 1.40-0 1.50-0 1.20-0 1.40-0 1.50-0 1.20-0 1.40-0 1.50-0 1.20-0 1.40-0 1.50-0 1.20-0 1.40-0 1.50-0 1.20-0 <td>$4f_{5/2}$</td> <td></td> <td>6.208-2</td>	$4f_{5/2}$											6.208-2
1,	$E_b =$											
β ₀ β ₀ 1.050 1.044 0.972 0.885 0.803 0.732 0.671 0.619 0.572 0.530 08 8.62-2 1.10-1 1.55-1 1.99-1 2.39-1 2.77-1 3.13-1 3.48-1 3.22-1 4.13-2 551/2 α 5.215·0 3.314-0 1.10-10 1.55-1 1.99-1 2.39-1 2.77-1 3.13-1 3.48-1 3.28-1 4.18-2 551/2 α 5.215·0 3.34-0 1.18-2 5.25-2 -4.27-2 -1.08-1 -1.48-1 -1.68-1 -1.72-1 -1.08-1 551/2 α 5.053·0 3.355·0 1.18-1 1.08-2 -4.01-3 -3.56-3 -3.93-3 -5.01-1 5.07-1 -1.68-8 1.17-3 -3.22-3 551/2 α 1.15-1 1.67-1 1.79-1 1.09-1 1.09-1 1.09-1 1.09-1 1.09-1 1.09-1 1.09-1 1.09-1 1.09-1 1.09-1 1.09-1 1.09-1 1.09-1 1.09-1 1.09-1	63.8 eV											1.40+0 4.06-1
60.8 (c) y 2.66-1 4.24-1 6.93-1 8.94-1 1.04-0 1.15-0 1.23-0 1.30-0 1.36-0 1.48-0 55/12 α 5.215-0 3.314-0 1.70-0 1.035-0 6.948-1 2.77-1 3.13-1 3.48-1 3.20-1 1.875 95.2 (c) γ 4.21-1 3.42-1 1.82-1 5.25-2 4.27-2 -1.08-1 -1.48-1 -1.68-1 -1.72-1 -1.68-1 50.9 (c) x 4.21-1 3.42-1 1.82-1 5.25-2 -2.44-3 -2.62-3 -2.3-3 -3.01-3 -3.17-3 -3.25-3 50.9 (c) x 5.91-1 1.675 1.71-1 1.08-9 7.161-1 5.07-1 3.68-3 2.3-3-3 3.31-3 3.47-3 -3.25-3 3.20-3 3.17-3 3.05-3 3.18-1 1.66-6 1.615 1.75 1.712 1.710 1.604 1.61 3.5-4 1.75 1.61 3.5-5 3.62-3 5.59-3 5.59-3 1.51-1 3.59-3 3.11-3	$4f_{7/2}$	σ										7.569-2
S S S S S S S S S S	$E_b =$											0.530
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	60.8 eV											
E _j = mode β 1875 1884 1896 1905 1912 1919 1925 1930 1934 1937 1935 1936 1934 1937 1935 1936 1934 1937 1935 1936 1934 1937 1935 1936 1934 1937 1935 1936 19												
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$5s_{1/2}$											
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$E_b = 95.2 \text{ eV}$											
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	00.2 01											-3.29-
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	5p1/2	σ	5.023+0	3 355+0		1.083+0						1.709-1
630 eV γ 2.59-1 boole 1.27-1 boole -5.56-3 -6.39-3 -5.39-3 -5.29-3 -3.99-3 -3.17-1 3.93-1 5.16-1 6.35-59-3 -3.99-3 -1.75-3 1.08-3 1.08-3 4.46-3 6.35-59-3 -5.59-3 -3.99-3 -7.17-3 1.08-3 1.08-3 4.46-3 6.35-59-3 -3.59-3 -3.75-3 1.08-3 1.08-3 1.08-3 4.46-3 6.35-59-3 1.08-3												1.562
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$												6.35 - 1
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	E.											8.30-3
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$												
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$												7.51-1
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$												2.17-2
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	5d _{3/2}	σ	7.818+0	4.486+0	1.822+0	8.897-1	4.901-1	2.938-1	1.876-1	1.258-1	8.766-2	6.306-2
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$E_b =$	β	1.296	1.374	1.410	1.387	1.343	1.291	1.237	1.182	1.129	1.079
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	4.2 eV											1.44+0
$\begin{array}{c} E_{b} = \\ 3 \\ 2 \\ 2 \\ 3 \\ 2 \\ 2 \\ 4 \\ 2 \\ 3 \\ 2 \\ 2 \\ 4 \\ 2 \\ 3 \\ 2 \\ 2 \\ 2 \\ 3 \\ 2 \\ 2 \\ 2 \\ 3 \\ 2 \\ 2$		δ					7.18-2	8.83-2				1.51-1
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$5d_{5/2}$											7.691-2
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	$E_b =$											
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	J.2 EV											1.72-1
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	6s _{1/2}	σ	4.483-1	2.821-1	1.434-1	8.695-2	5.820-2	4.157-2	3.109-2	2.409-2	1.918-2	1.561-2
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$E_b =$	β	1.877		1.896		1.912	1.918		1.930	1.935	1.939
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	9.0 eV											-1.60-
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$					-1.63-3	-2.06-3	-2.39-3	-2.64-3	-2.83-3	-2.99-3	-3.13-3	-3.25-
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	Z= 78, Pt: [Xe	e]4f ⁶ _{5/2} 4		6s _{1/2}								
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	Shell			2000	3000	4000	5000	6000	7000	8000	9000	10000
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$		σ										1.063+0
$\begin{array}{cccccccccccccccccccccccccccccccccccc$												1.930
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	722.8 eV											-1.75-
$\begin{array}{cccccccccccccccccccccccccccccccccccc$		δ										-3.55-
$\begin{array}{cccccccccccccccccccccccccccccccccccc$												1.167+0
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$												
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	JUU.7 L V											7.74-3
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	4n _{2 /2}											1.959+0
$\begin{array}{cccccccccccccccccccccccccccccccccccc$												1.698
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	519.0 eV	γ	2.87 - 1	1.42 - 1	-2.58-2	-4.21-2	2.55 - 2	1.35 - 1	2.65 - 1	4.05 - 1	5.47 - 1	6.86 - 1
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$												2.28-2
$\begin{array}{cccccccccccccccccccccccccccccccccccc$												8.531-
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$												
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	JJU./ EV											1.41+0
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	Adr in											
$\begin{array}{cccccccccccccccccccccccccccccccccccc$												
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	313.4 eV											1.39+0
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$												1.70-1
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	4f _{5/2}	σ	8.276+1	3.304+1	8.150+0	2.824+0	1.201+0	5.855-1	3.151-1	1.826-1	1.121-1	7.212-2
74.3 eV γ 2.43 – 1 3.98 – 1 6.66 – 1 8.70 – 1 1.02 + 0 1.14 + 0 1.23 + 0 1.30 + 0 1.36 + 0 1.41 + 1	$E_b =$		1.047	1.053	0.990	0.906	0.826	0.751	0.684	0.626	0.575	0.529
δ 8.51-2 1.09-1 1.52-1 1.93-1 2.34-1 2.71-1 3.05-1 3.37-1 3.69-1 4.00-	74.3 eV	γ										1.41+0
		δ	8.51-2	1.09 - 1	1.52 - 1	1.93 - 1	2.34 - 1	2.71 - 1	3.05 - 1	3.37 - 1	3.69 - 1	4.00 - 1

Tah	le 1	(contin	ned)

able 1 (continu	•	1.051.2	4.100.1	1.024.1	2.524.0	1.400+0	7 222 1	2.075 1	2 227 4	1 200 1	0.760 2
$4f_{7/2}$ $E_b =$	$\frac{\sigma}{\beta}$	1.051+2 1.048	4.180+1 1.046	1.024+1 0.977	3.524+0 0.893	1.490+0 0.815	7.232-1 0.744	3.875-1 0.681	2.237-1 0.626	1.368-1 0.579	8.769-2 0.537
70.9 eV	γ	2.54-1	4.11-1	6.80 - 1	8.84-1	1.04+0	1.15+0	1.23+0	1.30+0	1.36+0	1.41+0
	δ	8.52-2	1.09-1	1.52-1	1.95-1	2.36-1	2.75 - 1	3.10-1	3.44-1	3.76-1	4.08-1
$5s_{1/2}$	σ	5.416+0	3.446+0	1.773+0	1.082+0	7.271-1	5.210-1	3.908-1	3.034-1	2.419-1	1.971-1
$E_b =$	β	1.866	1.876	1.888	1.897	1.905	1.913	1.919	1.924	1.929	1.933
101.7 eV	$_{\delta}^{\gamma}$	4.40-1 $-5.33-4$	3.61-1 $-1.01-3$	2.02 - 1 $-1.69 - 3$	7.00-2 $-2.17-3$	-2.90-2 $-2.51-3$	-9.77-2 $-2.78-3$	-1.42-1 $-3.00-3$	-1.66-1 $-3.19-3$	-1.74-1 $-3.37-3$	-1.69-3 -3.51-3
F											
$5p_{1/2}$ $E_b =$	$\frac{\sigma}{\beta}$	5.246+0 1.601	3.518+0 1.668	1.880+0 1.710	1.149+0 1.711	7.628-1 1.697	5.362-1 1.676	3.932-1 1.652	2.981-1 1.626	2.319-1 1.599	1.843-1 1.571
65.3 eV	γ	2.80-1	1.45-1	2.21-3	-1.20-2	4.43-2	1.36-1	2.47-1	3.66-1	4.87-1	6.06-1
	δ	-4.24 - 3	-5.87 - 3	-6.40 - 3	-6.32 - 3	-5.73-3	-4.46 - 3	-2.45 - 3	2.49-4	3.51-3	7.17-3
5p _{3/2}	σ	1.247+1	7.805+0	3.810+0	2.192+0	1.391+0	9.431-1	6.714-1	4.960-1	3.774-1	2.941-1
$E_b =$	β	1.559	1.648	1.730	1.761	1.769	1.765	1.754	1.738	1.720	1.699
51.6 eV	γ	1.66-1	5.67-2	-4.34-2	-2.61-2	5.63-2	1.72-1	3.04-1	4.44-1	5.85-1	7.22-1
	δ	-1.65-3	-1.85 - 3	2.07 - 3	6.10-3	9.33-3	1.20-2	1.45-2	1.69-2	1.94-2	2.18-2
$5d_{3/2}$	σ	8.263+0	4.772+0	1.957+0	9.620-1	5.324-1	3.204-1	2.053-1	1.380-1	9.640-2	6.948-2
$E_b = 2.8 \text{ eV}$	β	1.285	1.369	1.412	1.393	1.352	1.303	1.251	1.199	1.147	1.096
2.8 eV	$_{\delta}^{\gamma}$	-3.70-2 5.45-3	-1.22-2 $1.68-2$	1.75-1 3.70-2	4.08-1 5.40-2	6.31-1 $6.97-2$	8.33-1 8.55-2	1.01+0 1.02-1	1.17+0 1.18-1	1.31+0 1.33-1	1.43+0 1.48-1
Ed			6.307+0	2.530+0	1.225+0	6.698-1		2.535-1	1.690-1		
$5d_{5/2}$ $E_b =$	$\frac{\sigma}{\beta}$	1.111+1 1.355	6.307+0 1.394	2.530+0 1.382	1.225+0	6.698—1 1.270	3.991-1 1.209	2.535—1 1.150	1.690-1	1.172-1 1.039	8.395-2 0.987
1.4 eV	γ	-3.98-2	5.23-3	2.15-1	4.53-1	6.70-1	8.61-1	1.03+0	1.17+0	1.30+0	1.40+0
	δ	6.17-3	1.58-2	3.51-2	5.40-2	7.27-2	9.21-2	1.12-1	1.32-1	1.51-1	1.69-1
6s _{1/2}	σ	4.176-1	2.629-1	1.339-1	8.140-2	5.462-2	3.907-2	2.926-2	2.269-2	1.807-2	1.471-2
$E_b =$	β	1.868	1.877	1.889	1.898	1.906	1.912	1.918	1.924	1.929	1.933
9.0 eV	γ	4.22-1	3.45-1	1.90-1	6.19-2	-3.46-2	-1.03-1	-1.46-1	-1.69 - 1	-1.74-1	-1.67-
	δ	-6.06-4	-1.05-3	-1.70-3	-2.16-3	-2.51-3	-2.80-3	-3.03-3	-3.22-3	-3.36-3	-3.48-
Z= 79, Au: [X	e]4f _{5/2}	4f _{7/2} 5d _{3/2} 5d _{5/2}	2 6s _{1/2}								
CI II		k (eV)	2000	2000	4000	5000	C000	7000	0000	0000	10000
Shell		1500	2000	3000	4000	5000	6000	7000	8000	9000	10000
4s _{1/2}	σ	2.536+1	1.715+1	9.284+0	5.791+0	3.944+0	2.851+0	2.153+0	1.680+0	1.345+0	1.100+0
$E_b = 758.8 \text{ eV}$	β γ	1.827 6.76-1	1.849 5.67-1	1.870 3.52-1	1.882 1.79-1	1.891 4.74-2	1.900 -4.64-2	1.908 -1.10-1	1.915 1.50 1	1.920 -1.72-1	1.925 1.79-
730.0 EV	δ	4.14-4	-5.16-4	-1.55-3	-2.18-3	-2.63-3	-4.04-2 $-2.95-3$	-3.21-3	-3.43-3	-3.62-3	-1.79- -3.79-
4p _{1/2}	σ	2.860+1	2.066+1	1.171+1	7.329+0	4.930+0	3.496+0	2.581+0	1.966+0	1.536+0	1.225+0
$E_b =$	β	1.380	1.543	1.656	1.683	1.683	1.670	1.651	1.629	1.605	1.580
643.7 eV	γ	4.84 - 1	3.18 - 1	6.59 - 2	-1.19 - 2	1.11 - 2	8.55 - 2	1.86 - 1	2.99 - 1	4.18 - 1	5.37 - 1
	δ	1.81-2	1.88-3	-5.08 - 3	-5.98 - 3	-5.58 - 3	-4.43 - 3	-2.58 - 3	-4.96 - 5	3.04 - 3	6.55 - 3
$4p_{3/2}$	σ	7.831+1	5.105+1	2.573+1	1.500+1	9.591+0	6.536+0	4.671+0	3.461+0	2.640+0	2.061+0
$E_b =$	β	1.376	1.534	1.675	1.730	1.752	1.756	1.751	1.740	1.725	1.707
545.4 eV	$_{\delta}^{\gamma}$	3.05-1 1.25-2	1.61-1 $2.06-3$	-1.79-2 1.81-3	-4.65-2 $5.91-3$	1.19-2 9.68-3	1.15 - 1 $1.28 - 2$	2.40-1 $1.55-2$	3.76-1 1.80-2	5.16-1 2.05-2	6.54-1 $2.29-2$
$\begin{array}{l} 4d_{3/2} \\ E_b = \end{array}$	$\frac{\sigma}{\beta}$	1.069+2 1.123	6.310+1 1.276	2.609+1 1.375	1.283+1 1.380	7.095+0 1.351	4.270+0 1.310	2.735+0 1.263	1.838+0 1.213	1.284+0 1.163	9.250-1 1.115
25 – 352.0 eV		-2.36-2	-4.67 - 2	1.10-1	3.42-1	5.70-1	7.80-1	9.67-1	1.13+0	1.105	1.40+0
332.0 € 1	$_{\delta}^{\gamma}$	4.89-3	1.45-2	3.67-2	5.48-2	7.07-2	8.64-2	1.02-1	1.17-1	1.32-1	1.46-1
4d _{5/2}	σ	1.555+2	8.980+1	3.621+1	1.752+1	9.575+0	5.703+0	3.621+0	2.414+0	1.673+0	1.198+0
$E_b =$	β	1.231	1.330	1.364	1.331	1.279	1.222	1.165	1.109	1.055	1.004
333.9 eV	γ	-3.81-2	-3.58 - 2	1.53 - 1	3.94 - 1	6.18 - 1	8.17 - 1	9.91 - 1	1.14+0	1.27+0	1.38+0
	δ	5.68-3	1.41-2	3.44-2	5.37-2	7.23-2	9.17-2	1.11-1	1.31-1	1.49-1	1.66-1
$4f_{5/2}$	σ	9.199+1	3.701+1	9.221+0	3.214+0	1.372+0	6.713-1	3.621-1	2.103-1	1.293-1	8.332-2
$E_b =$	β	1.043	1.054	0.997	0.915	0.836	0.763	0.695	0.636	0.585	0.539
87.3 eV	$_{\delta}^{\gamma}$	2.28-1 8.34-2	3.82-1 1.07-1	6.52-1 1.50-1	8.59-1 1.90-1	1.02+0 2.30-1	1.14+0 2.67-1	1.23+0 3.01-1	1.30+0 3.33-1	1.36+0 3.65-1	1.41+0 3.95-1
Af.											
$4f_{7/2}$ $E_b =$	$\frac{\sigma}{\beta}$	1.168+2 1.045	4.678+1 1.048	1.157+1 0.984	4.008+0 0.901	1.702+0 0.824	8.283-1 0.754	4.448-1 0.691	2.572-1 0.636	1.576-1 0.588	1.012-1 0.545
83.7 eV	γ	2.39-1	3.96-1	6.67-1	8.74–1	1.03+0	1.15+0	1.24+0	1.31+0	1.36+0	1.41+0
	δ	8.35-2	1.07-1	1.50-1	1.92-1	2.33-1	2.71-1	3.06-1	3.39-1	3.72-1	4.03-1
5s _{1/2}	σ	5.655+0	3.602+0	1.858+0	1.136+0	7.652-1	5.492-1	4.124-1	3.205-1	2.558-1	2.085-1
$E_b =$	β	1.856	1.867	1.880	1.890	1.898	1.906	1.913	1.918	1.923	1.927
107.8 eV	γ	4.54 - 1	3.78 - 1	2.22 - 1	8.82 - 2	-1.42 - 2	-8.69 - 2	-1.35-1	-1.64-1	-1.76-1	-1.75-
	δ	-5.16-4	-1.03-3	-1.77-3	-2.28-3	-2.67-3	-2.96-3	-3.20-3	-3.40 - 3	-3.59-3	-3.75-
$5p_{1/2}$	σ	5.494+0	3.698+0	1.990+0	1.223+0	8.148-1	5.746-1	4.226-1	3.211-1	2.503-1	1.993-1
$E_b =$	β	1.590	1.662	1.708	1.712	1.700	1.681	1.658	1.633	1.607	1.580
71.7 eV	δ	3.01-1 -4.39-3	1.64-1 $-6.15-3$	1.05-2 $-6.70-3$	-1.45-2 $-6.66-3$	3.35-2 $-6.14-3$	1.19-1 -4.99-3	2.25-1 $-3.15-3$	3.40-1 $-6.33-4$	4.59-1 2.44-3	5.76-1 5.92-3
E so											
$5p_{3/2}$	σ	1.323+1	8.286+0	4.058+0	2.342+0	1.490+0	1.012+0	7.220-1	5.343-1	4.071 - 1	3.176-1

able 1 (contin	ued)										
$E_b = 56.9 \text{ eV}$	$eta \ \gamma \ \delta$	1.545 1.78-1 -1.61-3	1.638 6.80-2 -2.09-3	1.724 -4.07-2 1.78-3	1.759 -3.28-2 5.96-3	1.770 4.21-2 9.34-3	1.768 1.52-1 1.21-2	1.759 2.80-1 1.46-2	1.745 4.16-1 1.70-2	1.728 5.55-1 1.94-2	1.708 6.91-1 2.17-2
$5d_{3/2}$ $E_b =$ 3.3 eV	σ β γ	9.174+0 1.275 -3.50-2	5.331+0 1.364 -1.91-2	2.207+0 1.413 1.57-1	1.092+0 1.399 3.86-1	6.076-1 1.361 6.08-1	3.671-1 1.314 8.10-1	2.359-1 1.264 9.92-1	1.590-1 1.213 1.15+0	1.113-1 1.162 1.29+0	8.039-2 1.112 1.41+0
5d _{5/2}	$\frac{\delta}{\sigma}$	4.56-3 1.239+1	1.57-2 7.073+0	3.59-2 2.863+0	5.29-2 1.395+0	6.82-2 7.664-1	8.36-2 4.583-1	9.93-2 2.919-1	1.15-1 1.952-1	1.30-1 1.356-1	1.44-1 9.729-2
$E_b = 1.8 \text{ eV}$	$eta \ \gamma \ \delta$	1.352 -3.99-2 5.45-3	1.394 -3.04-3 1.48-2	1.387 1.97-1 3.38-2	1.339 4.33-1 5.24-2	1.279 6.50-1 7.08-2	1.220 8.42-1 8.97-2	1.161 1.01+0 1.09-1	1.105 1.16+0 1.29-1	1.051 1.28+0 1.48-1	1.000 1.39+0 1.66-1
$6s_{1/2}$ $E_b = 9.0 \text{ eV}$	σ β γ	4.389-1 1.858 4.37-1	2.765-1 1.868 3.62-1	1.410-1 1.882 2.09-1	8.590-2 1.891 7.89-2	5.774-2 1.899 -2.02-2	4.138-2 1.906 -9.21-2	3.103-2 1.912 -1.40-1	2.407-2 1.918 -1.67-1	1.919-2 1.923 -1.76-1	1.564-2 1.928 -1.73-1
7= 80 Ha·[Y	δ (a)/4f ⁶	$\frac{-6.01-4}{4\mathbf{f}_{7/2}^8 5\mathbf{d}_{3/2}^4 5\mathbf{d}_{5/2}^6}$	-1.08-3	-1.79-3	-2.28-3	-2.66-3	-2.97-3	-3.23-3	-3.43-3	-3.59-3	-3.72-3
2- 00, 11g. [A	115/2	$\frac{417/2}{k \text{ (eV)}}$	2 031/2								
Shell		1500	2000	3000	4000	5000	6000	7000	8000	9000	10000
$4s_{1/2}$ $E_b =$ 803.0 eV	$\sigma \ eta \ eta \ eta \ eta \ \delta$	2.560+1 1.813 7.03-1 6.01-4	1.742+1 1.837 5.98-1 -4.42-4	9.486+0 1.860 3.83-1 -1.59-3	5.938+0 1.873 2.06-1 -2.28-3	4.054+0 1.884 7.03-2 -2.76-3	2.937+0 1.893 -2.83-2 -3.12-3	2.221+0 1.901 -9.74-2 -3.41-3	1.735+0 1.908 -1.43-1 -3.66-3	1.391+0 1.913 -1.70-1 -3.87-3	1.138+0 1.918 -1.81- -4.06-
$4p_{1/2}$ $E_b =$ 676.9 eV	σ β γ δ	2.860+1 1.343 5.05-1 2.15-2	2.086+1 1.526 3.49-1 2.89-3	1.195+1 1.648 8.45-2 -5.23-3	7.534+0 1.680 -7.76-3 -6.27-3	5.094+0 1.683 3.87-3 -5.93-3	3.627+0 1.673 6.98-2 -4.89-3	2.686+0 1.656 1.64-1 -3.19-3	2.051+0 1.635 2.74-1 -8.67-4	1.606+0 1.612 3.90-1 1.99-3	1.283+0 1.588 5.06-1 5.26-3
$4p_{3/2}$ $E_b =$ 571.0 eV	σ β γ	8.020+1 1.350 3.18-1	5.248+1 1.515 1.79-1	2.660+1 1.664 -9.65-3	1.557+1 1.725 -4.93-2	9.985+0 1.750 -3.50-4	6.823+0 1.758 9.54-2	4.885+0 1.755 2.16-1	3.626+0 1.745 3.49-1	2.769+0 1.732 4.87-1	2.164+0 1.715 6.23-1
$4d_{3/2}$ $E_b =$	$\frac{\delta}{\sigma}$ β	1.44-2 1.108+2 1.098	2.60-3 6.599+1 1.260	1.54-3 2.757+1 1.372	5.67-3 1.365+1 1.383	9.58-3 7.587+0 1.359	1.28-2 4.582+0 1.320	1.56-2 2.943+0 1.274	1.82-2 1.982+0 1.226	2.06-2 1.387+0 1.178	2.28-2 1.002+0 1.131
378.3 eV	$\frac{\gamma}{\delta}$	-1.40-2 $4.69-3$	-5.07-2 1.33-2	8.98-2 3.53-2	3.14-1 5.34-2	5.42-1 6.94-2	7.55-1 8.51-2	9.45-1 1.00-1	1.11+0 1.15-1	1.25+0 1.28-1	1.38+0 1.42-1
$4d_{5/2}$ $E_b =$ 359.8 eV	$\sigma \ eta \ eta \ \gamma \ \delta$	1.616+2 1.216 -3.16-2 5.43-3	9.408+1 1.323 -4.26-2 1.30-2	3.830+1 1.366 1.33-1 3.29-2	1.864+1 1.337 3.68-1 5.17-2	1.024+1 1.288 5.94-1 7.05-2	6.117+0 1.232 7.96-1 8.98-2	3.893+0 1.176 9.73-1 1.09-1	2.601+0 1.120 1.12+0 1.27-1	1.807+0 1.067 1.25+0 1.45-1	1.295+0 1.017 1.37+0 1.62-1
$4f_{5/2}$ $E_b =$ 103.3 eV	σ β γ δ	1.016+2 1.039 2.14-1 8.14-2	4.119+1 1.055 3.66-1 1.05-1	1.037+1 1.003 6.36-1 1.47-1	3.640+0 0.925 8.49-1 1.88-1	1.561+0 0.846 1.01+0 2.27-1	7.655-1 0.772 1.13+0 2.63-1	4.139-1 0.705 1.23+0 2.97-1	2.409-1 0.647 1.30+0 3.29-1	1.485-1 0.596 1.37+0 3.60-1	9.578-2 0.550 1.42+0 3.91-1
$4f_{7/2}$ $E_b = 99.4 \text{ eV}$	σ β γ δ	1.290+2 1.041 2.25-1 8.17-2	5.206+1 1.050 3.80-1 1.05-1	1.301+1 0.990 6.52-1 1.48-1	4.537+0 0.911 8.64-1 1.89-1	1.934+0 0.834 1.02+0 2.30-1	9.442-1 0.763 1.14+0 2.67-1	5.082-1 0.699 1.24+0 3.02-1	2.945-1 0.645 1.31+0 3.35-1	1.808-1 0.597 1.37+0 3.67-1	1.162-1 0.555 1.42+0 3.98-1
$5s_{1/2}$ $E_b =$ 120.3 eV	σ β γ δ	5.946+0 1.845 4.72-1 -4.93-4	3.791+0 1.857 3.98-1 -1.05-3	1.959+0 1.872 2.42-1 -1.85-3	1.201+0 1.882 1.07-1 -2.40-3	8.103-1 1.891 2.35-3 -2.81-3	5.825-1 1.899 -7.42-2 -3.13-3	4.381-1 1.906 -1.27-1 -3.40-3	3.408-1 1.912 -1.60-1 -3.64-3	2.721-1 1.917 -1.77-1 -3.85-3	2.220-1 1.921 -1.80-1 -4.01-3
$5p_{1/2}$ $E_b = 80.5 \text{ eV}$	σ β γ δ	5.769+0 1.577 3.22-1 -4.46-3	3.898+0 1.654 1.83-1 -6.49-3	2.110+0 1.706 2.00-2 -7.06-3	1.304+0 1.712 -1.53-2 -6.96-3	8.725-1 1.702 2.36-2 -6.48-3	6.176-1 1.685 1.03-1 -5.46-3	4.555-1 1.663 2.04-1 -3.79-3	3.468-1 1.639 3.16-1 -1.48-3	2.709-1 1.614 4.32-1 1.35-3	2.161-1 1.588 5.47-1 4.60-3
$5p_{3/2}$ $E_b =$ 61.8 eV	σ β γ δ	1.414+1 1.529 1.90-1 -1.52-3	8.873+0 1.626 7.88-2 -2.33-3	4.359+0 1.718 -3.74-2 1.47-3	2.524+0 1.756 -3.81-2 5.79-3	1.610+0 1.770 2.90-2 9.31-3	1.097+0 1.771 1.33-1 1.22-2	7.835-1 1.763 2.57-1 1.48-2	5.806-1 1.751 3.91-1 1.72-2	4.429-1 1.735 5.27-1 1.94-2	3.459-1 1.717 6.62-1 2.16-2
$5d_{3/2}$ $E_b = $ 7.5 eV	σ β γ δ	1.059+1 1.263 -3.23-2 3.70-3	6.188+0 1.357 -2.49-2 1.47-2	2.585+0 1.414 1.39-1 3.47-2	1.288+0 1.404 3.61-1 5.14-2	7.202-1 1.370 5.83-1 6.68-2	4.369-1 1.325 7.88-1 8.22-2	2.816-1 1.277 9.72-1 9.75-2	1.903-1 1.227 1.13+0 1.12-1	1.335-1 1.177 1.28+0 1.27-1	9.657-2 1.128 1.40+0 1.40-1
$5d_{5/2}$ $E_b = $ 5.7 eV	σ β γ δ	1.448+1 1.348 -3.94-2 4.78-3	8.308+0 1.394 -1.02-2 1.39-2	3.390+0 1.391 1.81-1 3.24-2	1.663+0 1.346 4.11-1 5.05-2	9.179-1 1.289 6.28-1 6.87-2	5.510-1 1.231 8.23-1 8.78-2	3.519-1 1.173 9.94-1 1.07-1	2.358-1 1.116 1.14+0 1.26-1	1.642-1 1.062 1.27+0 1.44-1	1.180-1 1.012 1.38+0 1.62-1
$6s_{1/2}$ $E_b = 9.0 \text{ eV}$	σ β γ	5.248-1 1.849 4.48-1	3.307-1 1.860 3.77-1	1.689-1 1.874 2.26-1	1.031-1 1.884 9.63-2	6.939-2 1.892 -5.77-3	4.978-2 1.899 -8.12-2	3.737-2 1.906 -1.32-1	2.903-2 1.912 -1.63-1	2.316-2 1.918 -1.77-1	1.889-2 1.922 -1.78-1

Table 1	(continued)
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	δ	-5.98 - 4	-1.12 - 3	-1.87 - 3	-2.40 - 3	-2.83 - 3	-3.16 - 3	-3.43 - 3	-3.64 - 3	-3.82 - 3	-3.97 - 3
Z= 81, Tl: [X	e]4f ⁶ _{5/2} 4	$f_{7/2}^8 5d_{3/2}^4 5d_{5/2}^6$	6s _{1/2} 6p _{1/2}								
		k (eV)									
Shell		1500	2000	3000	4000	5000	6000	7000	8000	9000	10000
4s _{1/2}	σ	2.579+1	1.766+1	9.671+0	6.078+0	4.161+0	3.021+0	2.288+0	1.790+0	1.436+0	1.175+0
$E_b =$	β	1.796	1.825	1.851	1.865	1.876	1.885	1.893	1.900	1.906	1.911
845.5 eV	δ	7.27-1 8.31-4	6.23-1 -3.56-4	4.11-1 $-1.62-3$	2.32-1 $-2.37-3$	9.40-2 $-2.89-3$	-9.29-3 $-3.30-3$	-8.40-2 $-3.63-3$	-1.35-1 $-3.91-3$	-1.67-1 $-4.14-3$	-1.82- -4.33-
4p _{1/2}	σ	2.853+1	2.104+1	1.220+1	7.745+0	5.264+0	3.763+0	2.795+0	2.140+0	1.678+0	1.343+0
$E_b =$	β	1.303	1.509	1.641	1.678	1.683	1.675	1.660	1.640	1.619	1.596
721.3 eV	γ	5.30 - 1	3.84 - 1	1.06 - 1	-1.19 - 3	-2.16 - 3	5.52 - 2	1.44 - 1	2.50 - 1	3.61 - 1	4.74 - 1
	δ	2.66-2	4.01-3	-5.27-3	-6.49-3	-6.29-3	-5.40-3	-3.87-3	-1.75-3	8.68-4	3.96-3
$4p_{3/2}$	σ	8.230+1	5.406+1	2.754+1	1.618+1	1.041+1	7.130+0	5.113+0	3.800+0	2.905+0	2.273+0
$E_b = 609.0 \text{ eV}$	$eta \ \gamma$	1.307 3.35-1	1.498 2.00-1	1.655 1.19-3	1.720 -5.07-2	1.748 -1.20-2	1.758 7.69-2	1.757 1.93-1	1.750 3.22-1	1.738 4.56-1	1.723 5.88-1
005.0 € 1	δ	1.76-2	3.26-3	1.26-3	5.37-3	9.44-3	1.29-2	1.58-2	1.83-2	2.06-2	2.28-2
4d _{3/2}	σ	1.147+2	6.886+1	2.908+1	1.450+1	8.098+0	4.907+0	3.160+0	2.134+0	1.496+0	1.082+0
$E_b =$	β	1.073	1.246	1.368	1.385	1.365	1.329	1.285	1.239	1.193	1.148
406.6 eV	$\gamma \\ \delta$	-2.51-3	-5.29-2	6.96-2	2.88-1	5.17-1	7.31-1	9.20-1	1.09+0	1.23+0	1.36+0
4.1		4.77-3	1.20-2	3.38-2	5.22-2	6.85-2	8.37-2	9.79-2	1.11-1	1.25-1	1.39-1
$\begin{array}{l} 4d_{5/2} \\ E_b = \end{array}$	$\frac{\sigma}{eta}$	1.675+2 1.203	9.829+1 1.316	4.040+1 1.367	1.980+1 1.343	1.092+1 1.296	6.545+0 1.241	4.176+0 1.185	2.796+0 1.131	1.946+0 1.080	1.398+0 1.032
386.2 eV	γ	-2.35-2	-4.78-2	1.13-1	3.44-1	5.72-1	7.77-1	9.53-1	1.11+0	1.24+0	1.36+0
	δ	5.41 - 3	1.20 - 2	3.12-2	5.01 - 2	6.91 - 2	8.79 - 2	1.06 - 1	1.24 - 1	1.41 - 1	1.59 - 1
$4f_{5/2}$	σ	1.120+2	4.573+1	1.163+1	4.108+0	1.768+0	8.699-1	4.716-1	2.750-1	1.698-1	1.097-1
$E_b =$	β	1.034	1.055	1.010	0.934	0.854	0.780	0.716	0.659	0.608	0.560
123.0 eV	$\gamma \\ \delta$	1.97-1 7.89-2	3.47-1 1.03-1	6.22-1 1.46-1	8.39-1 1.86-1	1.00+0 2.24-1	1.13+0 2.59-1	1.23+0 2.92-1	1.31+0 3.25-1	1.37+0 3.57-1	1.43+0 3.87-1
$4f_{7/2}$	σ	1.421+2	5.778+1	1.459+1	5.119+0	2.191+0	1.072+0	5.787-1	3.360-1	2.066-1	1.330-1
$E_b =$	β	1.038	1.051	0.998	0.919	0.841	0.770	0.709	0.656	0.608	0.565
118.7 eV	γ	2.08 - 1	3.62 - 1	6.38 - 1	8.55 - 1	1.02+0	1.14+0	1.24+0	1.31+0	1.38+0	1.43+0
	δ	7.92-2	1.03-1	1.46-1	1.88-1	2.26-1	2.62-1	2.97-1	3.31-1	3.64-1	3.94-1
$5s_{1/2}$	σ	6.235+0	3.978+0	2.060+0	1.265+0	8.556-1	6.161-1	4.638-1	3.611-1	2.886-1	2.356-1
$E_b = 136.3 \text{ eV}$	$eta \ \gamma$	1.835 4.87-1	1.848 4.17-1	1.864 2.62-1	1.875 1.27-1	1.884 2.00-2	1.891 -6.08-2	1.898 -1.18-1	1.904 1.56 1	1.910 -1.77-1	1.915 -1.83-
	δ	-4.71-4	-1.07 - 3	-1.92 - 3	-2.51-3	-2.96 - 3	-3.33 - 3	-3.63 - 3	-3.89 - 3	-4.10-3	-4.28-3
5p _{1/2}	σ	6.068+0	4.115+0	2.242+0	1.392+0	9.357-1	6.645-1	4.913-1	3.749-1	2.934-1	2.344-1
$E_b =$	β	1.567	1.647	1.704	1.713	1.705	1.689	1.668	1.646	1.622	1.597
99.6 eV	$_{\delta}^{\gamma}$	3.47-1 $-4.63-3$	2.06-1 $-6.81-3$	3.17-2 -7.36-3	-1.50-2 $-7.25-3$	1.44-2 -6.87-3	8.72-2 $-5.99-3$	1.84 - 1 $-4.49 - 3$	2.92-1 $-2.41-3$	4.04-1 1.85-4	5.16-1 3.28-3
F.,.				4.689+0							
$5p_{3/2}$ $E_b =$	$\frac{\sigma}{\beta}$	1.516+1 1.518	9.519+0 1.616	4.689+0 1.713	2.723+0 1.754	1.742+0 1.770	1.189+0 1.773	8.508-1 1.767	6.313-1 1.756	4.821-1 1.742	3.769-1 1.725
74.5 eV	γ	2.04-1	9.12-2	-3.26-2	-4.25-2	1.65-2	1.15-1	2.36-1	3.66-1	4.98-1	6.29-1
	δ	-1.43 - 3	-2.56 - 3	1.14-3	5.58-3	9.28 - 3	1.23-2	1.50-2	1.73-2	1.94 - 2	2.15 - 2
$5d_{3/2}$	σ	1.205+1	7.085+0	2.986+0	1.498+0	8.419 - 1	5.126 - 1	3.313 - 1	2.244 - 1	1.577 - 1	1.144 - 1
$E_b =$	β	1.253	1.351 -3.01-2	1.414 1.20-1	1.409	1.378	1.336	1.288	1.239	1.191	1.145
15.3 eV	$\gamma \\ \delta$	-2.84-2 2.87-3	-3.01-2 1.35-2	3.34-2	3.37-1 5.03-2	5.60-1 6.59-2	7.67-1 8.09-2	9.51-1 9.52-2	1.11+0 1.09-1	1.26+0 1.23-1	1.38+0 1.37-1
5d _{5/2}	σ	1.681+1	9.698+0	3.990+0	1.969+0	1.092+0	6.580-1	4.214-1	2.830-1	1.975-1	1.422-1
$E_b =$	β	1.345	1.394	1.395	1.353	1.299	1.241	1.182	1.126	1.073	1.024
13.1 eV	γ	-3.79-2	-1.72-2	1.62-1	3.89-1	6.08-1	8.06-1	9.78-1	1.13+0	1.25+0	1.37+0
	δ	4.13-3	1.29-2	3.09-2	4.89-2	6.74-2	8.62-2	1.05-1	1.22-1	1.40-1	1.57-1
6s _{1/2}	σ_{β}	6.470-1 1.838	4.080-1 1.850	2.087-1 1.865	1.275-1	8.598-2	6.179-2 1.892	4.645-2 1.899	3.613-2 1.906	2.885-2 1.911	2.355-2
$E_b = 8.0 \text{ eV}$	$eta \ \gamma$	1.838 4.63–1	1.850 3.94–1	1.865 2.45—1	1.875 1.14-1	1.884 9.29-3	-6.84-2	-1.23-1	-1.57-1	-1.76-1	1.916 1.82-
	δ	-5.84-4	-1.14-3	-1.96-3	-2.55-3	-2.99-3	-3.34 - 3	-3.62 - 3	-3.85 - 3	-4.06-3	-4.25-
6p _{1/2}	σ	3.308-1	2.220-1	1.198-1	7.415-2	4.974-2	3.526-2	2.605-2	1.987-2	1.555-2	1.242-2
$E_b =$	β	1.588	1.662	1.711	1.717	1.707	1.691	1.670	1.647	1.623	1.598
6.0 eV	$\gamma \\ \delta$	3.28-1 $-6.23-3$	1.91-1 -7.44-3	2.56-2 -7.51-3	-1.61-2 $-7.44-3$	1.70-2 -7.08-3	9.17-2 $-6.19-3$	1.88 - 1 $-4.68 - 3$	2.95-1 -2.54-3	4.07 - 1 $2.28 - 4$	5.20-1 3.48-3
7= 02 Db. FV				7.51-5	,J	,.00-3	0.13-3	-1,00-3	2.34-3	2.20-4	J. 1 0-3
∠= 82, PD: [X	ej41 _{5/2} 4	$\frac{\mathbf{4f_{7/2}^8 5d_{3/2}^4 5d_{5/2}^6}}{k (\text{eV})}$	2 0S _{1/2} 6P _{1/2}								
Shell		1500	2000	3000	4000	5000	6000	7000	8000	9000	10000
$4s_{1/2} E_b =$	$\frac{\sigma}{\beta}$	2.595+1 1.777	1.789+1 1.810	9.863+0 1.840	6.221+0 1.855	4.270+0 1.866	3.106+0 1.876	2.355+0 1.884	1.844+0 1.892	1.481+0 1.898	1.213+0 1.905
893.6 eV	γ	7.59-1	6.57-1	4.42-1	2.62-1	1.20-1	1.11-2	-6.90-2	-1.25-1	-1.61-1	-1.80-
	δ	1.13-3	-2.20-4	-1.64 - 3	-2.46 - 3	-3.05 - 3	-3.50 - 3	-3.87 - 3	-4.16 - 3	-4.40 - 3	-4.59-1

able 1 (contin	ued)										
$4p_{1/2}$	σ	2.838+1	2.117+1	1.243+1	7.949+0	5.431+0	3.896+0	2.903+0	2.227+0	1.751+0	1.404+0
$E_b =$	β	1.264	1.484	1.633	1.674	1.683	1.677	1.664	1.646	1.625	1.603
763.9 eV	γ	5.50-1	4.19-1	1.30-1	7.06-3	-6.25-3	4.25-2	1.25-1	2.25-1	3.32-1	4.42-1
4	δ	3.13-2	5.44-3	-5.35-3	-6.82-3	-6.74-3	-5.95-3	-4.54-3	-2.58-3	-9.23-5	2.88-3
$4p_{3/2} E_b =$	$\frac{\sigma}{eta}$	8.429+1 1.273	5.562+1 1.474	2.849+1 1.643	1.680+1 1.713	1.084+1 1.745	7.437+0 1.758	5.342+0 1.760	3.976+0 1.754	3.044+0 1.744	2.384+0 1.730
644.5 eV	γ	3.50-1	2.21-1	1.29-2	-5.10-2	-2.22-2	5.97-2	1.700	2.94-1	4.24-1	5.55-1
	δ	2.08 - 2	4.09 - 3	9.99 - 4	5.06 - 3	9.32 - 3	1.29 - 2	1.59-2	1.85 - 2	2.07 - 2	2.29-2
4d _{3/2}	σ	1.184+2	7.176+1	3.063+1	1.537+1	8.626+0	5.245+0	3.387+0	2.293+0	1.611+0	1.168+0
$E_b =$	β	1.041	1.230	1.363	1.387	1.371	1.338	1.297	1.253	1.209	1.165
435.2 eV	$\gamma \\ \delta$	1.01-2 5.18-3	-5.35-2 $1.09-2$	5.19-2 3.25-2	2.64-1 5.12-2	4.92-1 6.74-2	7.03-1 8.17-2	8.93-1 9.55-2	1.06+0 1.09-1	1.21+0 1.23-1	1.35+0 1.37-1
1d	σ	1.735+2	1.026+2	4.257+1	2.099+1	1.162+1	6.989+0	4.471+0	3.001+0	2.093+0	1.506+0
$4d_{5/2}$ $E_b =$	β	1.735+2	1.309	1.368	1.348	1.303	1.250	1.196	1.143	1.093	1.046
412.9 eV	γ	-1.41-2	-5.16 - 2	9.46 - 2	3.23 - 1	5.50 - 1	7.53 - 1	9.31 - 1	1.09+0	1.22+0	1.34+0
	δ	5.59-3	1.10-2	2.99-2	4.88-2	6.73-2	8.52-2	1.03-1	1.20-1	1.38-1	1.56-1
$4f_{5/2}$	σ	1.228+2	5.051+1	1.298+1	4.611+0	1.994+0	9.842-1	5.350-1	3.126-1	1.933-1	1.251-1
$E_b = 141.8 \text{ eV}$	β	1.028 1.83-1	1.055 3.32-1	1.016 6.08-1	0.941 8.26-1	0.863 9.93-1	0.791 1.12+0	0.728 1.23+0	0.671 1.31+0	0.618 1.38+0	0.569 1.43+0
141.0 67	$\frac{\gamma}{\delta}$	7.71–2	1.01-1	1.44-1	1.83-1	2.20-1	2.55-1	2.89-1	3.22-1	3.53-1	3.82-1
4f _{7/2}	σ	1.558+2	6.380+1	1.627+1	5.744+0	2.469+0	1.213+0	6.561-1	3.818-1	2.351-1	1.516-1
$E_b =$	β	1.033	1.051	1.003	0.926	0.849	0.780	0.720	0.667	0.618	0.573
136.9 eV	γ	1.94-1	3.47-1	6.26-1	8.44-1	1.01+0	1.14+0	1.24+0	1.32+0	1.38+0	1.43+0
	δ	7.74-2	1.01-1	1.44-1	1.84-1	2.22-1	2.58-1	2.94-1	3.28-1	3.60-1	3.90-1
$5s_{1/2}$	σ	6.519+0	4.166+0	2.161+0	1.330+0	9.014-1	6.500-1	4.899-1	3.818-1 1.897	3.054-1 1.903	2.495-1
$E_b = 147.3 \text{ eV}$	β γ	1.822 5.02-1	1.838 4.34-1	1.855 2.83-1	1.866 1.47-1	1.875 3.75-2	1.883 -4.71-2	1.890 -1.09-1	-1.50-1	-1.74-1	1.908 1.84 1
	δ	-4.32 - 4	-1.08 - 3	-1.99 - 3	-2.64 - 3	-3.14 - 3	-3.54 - 3	-3.87 - 3	-4.13 - 3	-4.36 - 3	-4.54 - 3
$5p_{1/2}$	σ	6.358+0	4.327+0	2.372+0	1.480+0	9.994-1	7.120-1	5.279-1	4.038-1	3.167-1	2.535-1
$E_b =$	β	1.554	1.641	1.701	1.712	1.706	1.692	1.673	1.652	1.629	1.605
104.8 eV	$\gamma \\ \delta$	3.66-1 $-4.85-3$	2.25-1 -7.18-3	4.30-2 $-7.72-3$	-1.36-2 $-7.64-3$	7.54-3 -7.31-3	7.39-2 -6.52-3	1.65-1 -5.15-3	2.68-1 $-3.22-3$	3.76-1 -7.44-4	4.86-1 2.24-3
5p _{3/2}	σ	1.622+1	1.019+1	5.034+0	2.931+0	1.879+0	1.285+0	9.213-1	6.846-1	5.234-1	4.097-1
$E_b =$	β	1.502	1.605	1.706	1.750	1.769	1.774	1.771	1.761	1.749	1.733
้84.5 eV	γ	2.16 - 1	1.03 - 1	-2.73-2	-4.62 - 2	5.44 - 3	9.83-2	2.13 - 1	3.39 - 1	4.68 - 1	5.97 - 1
	δ	-1.32-3	-2.79-3	7.90-4	5.36-3	9.25-3	1.24-2	1.51-2	1.74-2	1.95-2	2.16-2
$5d_{3/2}$	σ	1.353+1	7.996+0	3.399+0	1.716+0	9.690-1	5.921-1	3.839-1	2.606-1	1.837-1	1.334-1
$E_b = 21.8 \text{ eV}$	β γ	1.241 -2.37-2	1.345 -3.42-2	1.414 1.04-1	1.413 3.17-1	1.385 5.38-1	1.345 7.43-1	1.300 9.27-1	1.254 1.09+0	1.208 1.24+0	1.162 1.37+0
21.0 01	δ	2.12-3	1.24-2	3.23-2	4.94-2	6.47-2	7.88-2	9.25-2	1.06-1	1.20-1	1.34-1
5d _{5/2}	σ	1.916+1	1,111+1	4.606+0	2.286+0	1.274+0	7.700-1	4.945-1	3.329-1	2.328-1	1.679-1
$E_b =$	β	1.342	1.394	1.399	1.360	1.307	1.249	1.192	1.138	1.087	1.039
19.2 eV	$\gamma \\ \delta$	-3.57-2 3.56-3	-2.31-2 1.20-2	1.47-1 2.98-2	3.71-1 4.77-2	5.90-1 6.57-2	7.86-1 8.35-2	9.58-1 1.01-1	1.11+0 1.19-1	1.24+0 1.36-1	1.36+0 1.54-1
C-											
$6s_{1/2} E_b =$	$\frac{\sigma}{\beta}$	7.619-1 1.828	4.807-1 1.841	2.463-1 1.856	1.508-1 1.867	1.019—1 1.877	7.333-2 1.885	5.521-2 1.892	4.299-2 1.898	3.437-2 1.904	2.806-2 1.909
3.1 eV	γ	4.72-1	4.07-1	2.62-1	1.31-1	2.56-2	-5.46-2	-1.13-1	-1.52 - 1	-1.75-1	-1.85 - 1
	δ	-5.88 - 4	-1.19 - 3	-2.05 - 3	-2.67 - 3	-3.14 - 3	-3.51-3	-3.83 - 3	-4.11-3	-4.35 - 3	-4.55 - 3
$6p_{1/2}$	σ	4.376 - 1	2.944 - 1	1.597 - 1	9.923 - 2	6.683 - 2	4.756 - 2	3.524 - 2	2.695 - 2	2.113 - 2	1.691 - 2
$E_b = 0.7 \text{ eV}$	β	1.575	1.653 2.08-1	1.708 3.51-2	1.717 -1.49-2	1.710	1.694 7.76-2	1.675 1.68-1	1.653 2.73-1	1.629 3.83-1	1.605
0.7 ev	$\gamma \delta$	3.45-1 -6.54-3	-7.94-3	-8.01-3	-7.81-3	1.02-2 -7.41-3	-6.58-3	-5.18-3	-3.19-3	-6.62-4	4.95-1 $2.32-3$
7= 83 Ri· [Y	al4f ⁶ 4		$6s_{1/2}^2 6p_{1/2}^2 6p_3^1$								
Z- 03, DI. [X	5/2		$os_{1/2} op_{1/2} op_3$	/2							
Ch -II		k (eV)	2000	2000	4000	5000	C000	7000	0000	0000	10000
Shell		1500	2000	3000	4000	5000	6000	7000	8000	9000	10000
$4s_{1/2}$ $E_b =$	$\frac{\sigma}{eta}$	2.605+1 1.759	1.808+1 1.795	1.004+1 1.828	6.354+0 1.844	4.373+0 1.856	3.186+0 1.866	2.420+0 1.875	1.897+0 1.884	1.525+0 1.891	1.251+0 1.898
938.2 eV	γ	7.81-1	6.88-1	4.74-1	2.92-1	1.46-1	3.25-2	-5.19-2	-1.12-1	-1.52-1	-1.76-1
	δ	1.42 - 3	-6.88 - 5	-1.65 - 3	-2.56 - 3	-3.21-3	-3.70 - 3	-4.08 - 3	-4.39 - 3	-4.64 - 3	-4.86 - 3
4p _{1/2}	σ	2.818+1	2.126+1	1.263+1	8.140+0	5.588+0	4.025+0	3.008+0	2.315+0	1.824+0	1.466+0
$E_b =$	β	1.216	1.458	1.622	1.669	1.682	1.678	1.667	1.650	1.631	1.610
805.3 eV	$\delta \gamma$	5.62-1 3.67-2	4.53-1 7.21-3	1.56-1 -5.45-3	1.71-2 -7.23-3	-8.25 - 3 $-7.20 - 3$	3.14-2 $-6.45-3$	1.06-1 -5.12-3	2.00-1 $-3.27-3$	3.04-1 $-9.01-4$	4.12-1 1.99-3
4p _{3/2}	σ	8.621+1	5.714+1	2.942+1	1.742+1	1.126+1	7.745+0	5.574+0	4.155+0	3.185+0	2.499+0
$E_b =$	β	1.240	1.449	1.629	1.742+1	1.741	1.757	1.761	1.758	1.749	1.737
678.9 eV	γ	3.62 - 1	2.40 - 1	2.52 - 2	-5.03-2	-3.10-2	4.32 - 2	1.47 - 1	2.66 - 1	3.93 - 1	5.23 - 1
	δ	2.42-2	5.14-3	7.43-4	4.74-3	9.16-3	1.29-2	1.60-2	1.86-2	2.10-2	2.32-2
$4d_{3/2}$	σ_{ρ}	1.220+2	7.464+1	3.220+1	1.626+1	9.166+0	5.594+0	3.624+0	2.459+0	1.732+0	1.258+0
$E_b =$	β	1.009	1.211	1.357	1.388	1.376	1.346	1.308	1.266	1.223	1.179

4400 γ σ.3.3 σ.5.40 7.2.2 3.01 5.05 7.28 1.08 1.07 1.01	
44-γ2-γ σ 1.79-γ 1.069-γ 4.477-1 2.291-γ 1.310 1.381-1 1.210-1 1.381-	1.33+0 1.35-1
	1.620+0
	1.020+0
18-1 18-1	1.33+0
E/s β 10.22 10.54 10.02 0.949 0.874 0.894 0.234 0.81 0.236 0.226 1.38-1 1.38-1 1.38-1 1.38-1 1.38-1 1.38-1 1.38-1 1.38-1 1.38-1 1.38-1 1.38-1 1.38-1 1.38-1 1.38-1 1.38-1 1.38-1 1.38-1 2.58-1 2.58-1 2.58-1 0.38-1 0.38-1 2.68-1 2.58-1 0.38-1 0.38-1 2.68-1 2.58-1 0.38-1 0.58-1 1.38-1 1.38-1 1.18-1 1.19-1 1.19-0 1.21-0 1.24-0 1.32-0 0.35-1 3.58-1 3.58-1 3.58-1 3.58-1 3.58-1 3.58-1 3.58-1 3.58-1 3.28-1	1.54 - 1
E/ε β 10.22 10.54 10.00 0.949 0.874 0.894 0.314 0.836 10.120 11.20 11.20 11.20 11.20 13.96 0.836 10.104 2.886 11.20 12.39 13.81 3.866 14.60 2.896 12.20 13.81 3.866 1.866 1.866 1.866 1.866 1.866 1.866 1.866 1.866 1.866 1.866 1.866 1.866 1.866 1.866 1.876 2.754 0.866 0.866 1	1.421-1
	0.577
4fyz σ 11/94°2 7,05°1 1,808°1 6,624°0 2,775°0 1,310°0 7,415°1 332°1 2,606°1 157.2 v y 1,801°1 3,33°1 6,11°1 8,30°1 1,00°0 1,31°0 1,24°0 1,32°0 1,38°0 157.2 v y 1,808 3,33°1 6,11°1 8,30°1 1,00°0 1,30°1 1,20°1 3,35°1 3,53°1 51/2 v σ 6,804°0 4,33°4 2,26°1 1,20°1 2,26°1 3,20°1 1,80°1 <td>1.43+0</td>	1.43+0
\$μ̄ = 10 / 10 / 10 / 10 / 10 / 10 / 10 / 10	3.76-1
1572 Y 180-0 333-1 611-1 8.30-1 100-0 1.31-0 1.24-0 1.32-0 3.55-1 3.55-1 3.55-1 5.51-2 3 5.51-2 3.55-1 3.55-1 3.55-1 5.51-2 3 5.51-2 3.55-1 3.55	1.721-1
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $	0.579
55/10 σ 68/940 43540 22/9410 13.9960 43/6-1 6.163-1 4.029-1 32.56 1.844 18.56 1.866 18.76 1.872 1.814 1.856 1.866 1.876 1.872 -1.81-1 4.51-1 4.51-1 4.51-1 3.06-1 1.69-1 5.59-2 -3.17-2 -9.63-2 -1.41-1 -1.68-1 5.91 σ 6.8390 4.534-0 2.01-0 1.5690 1.063-0 7.75-3 -3.23-3 -3.68-3 5.51-1 3.33-1 3.06-1 1.16.8 V 3.8391 2.47-1 5.62-2 -1.09-2 1.82-3 6.08-2 1.16-1 2.44-1 3.04-1 5.91 σ 7.75-2 7.75-2 3.08-2 3.08-1 1.51-1 3.09-1 1.51-1 3.08-1 1.51-1 3.09-1 1.51-1 3.01-1 1.25-2 1.73-1 1.76-1 1.75-1 1.32-1 1.33-1 1.25-2 1.73-1 1.76-1 1.75-1 1.52-1 1.52-1 1.52-1 1.72-1	1.44+0 3.84-1
	2.638-1
1991 1991 1991 1991 1991 1991 1992	1.902
1.6 1.6	-1.83-1
E/ε B/E 1.536 1.630 1.896 1.711 1.708 1.695 1.678 1.637 1.636 1.168 eV 3 3.891 2.477-1 5.522-2 -8.10-3 -7.75-3 -6.96-3 -5.71-3 -3.89-3 -1.51-3 5.92.2 α 1.723 1.090-1 5.398-0 1.315-0 1.202-0 1.755 1.775 1.754 1.773 1.742-1 1.567-1 29.9 eV 2.271 1.15-1 1.200-2 4.490-2 1.666-3 1.812-1 1.752-1 1.752-1 1.775-1 1.775-1 1.775-1 1.752-1	-4.82 - 3
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $	2.732-1
Page	1.613
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $	4.57 - 1
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$ \begin{array}{c c c c c c c c c c c c c c c c c c c $	1.178
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	1.35+0
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$6s_{1/2}$ a <t< td=""><td>1.053</td></t<>	1.053
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	1.35+0
$E_b = \beta \ \ \ \ \ \ \ \ \ \ \ \ \$	1.52-1
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	3.274-2 1.901
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $	-1.86-1
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	-4.85 - 3
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	2.241-2
6p _{3/2} σ 1.203+0 -8.41-3 -8.37-3 -8.09-3 -7.75-3 -7.03-3 -5.79-3 -4.01-3 -1.71-3 6p _{3/2} σ 1.203+0 7.512-1 3.693-1 2.150-1 1.380-1 9.448-2 6.782-2 5.046-2 3.856-2 b_{e} β 1.504 1.604 1.705 1.751 1.777 1.775 1.767 1.755 0.2 eV γ 2.13-1 1.04-1 -2.60-2 -4.78-2 -1.36-3 8.56-2 1.96-1 3.20-1 4.49-1 0.2 eV γ 2.13-3 1.04-1 -2.60-2 -4.78-2 -1.36-3 8.56-2 1.96-1 3.20-1 4.49-1 0.2 eV γ 2.13-3 1.04-1 -2.60-2 -4.78-2 -1.36-3 8.56-2 1.96-1 3.20-1 4.49-1 2.0 -2.49-3 -3.30-3 405-3 -3.00-3 400 500 6000 7000 800 900 45 1.373 1.35 1.814 1.833	1.613
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	4.67 - 1
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	1.05-3
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δ -2.49-3 -3.50-3 4.05-4 5.14-3 9.10-3 1.23-2 1.51-2 1.75-2 1.97-2 Z= 84, Po: [Xe] $4f_{5/2}^2$ $4f_{7/2}^2$ $5f_{3/2}^4$ $5f_{5/2}^6$ $6f_{7/2}^2$ $6f_$	1.741 5.78-1
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	2.17-2
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Shell 1500 2000 3000 4000 5000 6000 7000 8000 9000 $4s_{1/2}$ σ 2.612+1 1.825+1 1.020+1 6.484+0 4.474+0 3.267+0 2.485+0 1.951+0 1.570+0 $E_b =$ β 1.736 1.778 1.814 1.833 1.846 1.857 1.867 1.876 1.883 987.5 eV γ 8.07-1 7.20-1 5.09-1 3.24-1 1.74-1 5.62-2 -3.23-2 -9.69-2 -1.42-1 δ 1.83-3 1.16-4 -1.64-3 -2.65-3 -3.36-3 -3.88-3 -4.29-3 -4.63-3 -4.92-3 $4p_{1/2}$ σ 2.789+1 2.130+1 1.283+1 8.324+0 5.744+0 4.154+0 3.114+0 2.49-3 -4.63-3 -4.92-3 $E_b =$ β 1.157 1.430 1.610 1.664 1.680 1.679 1.670 1.655 1.637 85.9 eV γ 5.70-1 4.89-1	
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$\begin{array}{cccccccccccccccccccccccccccccccccccc$	1.289+0 1.890
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$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	1.743
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	4.94-1 $2.36-2$
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	1.353+0
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	1.353+0
δ 7.21-3 9.00-3 3.01-2 4.88-2 6.43-2 7.87-2 9.27-2 1.06-1 1.20-1 $4d_{5/2}$ $σ$ 1.852+2 1.113+2 4.705+1 2.346+1 1.310+1 7.934+0 5.105+0 3.442+0 2.410+0 $E_b = β$ 1.145 1.291 1.368 1.357 1.318 1.270 1.219 1.168 1.118 469.9 eV $γ$ 9.29-3 -5.51-2 6.15-2 2.78-1 4.99-1 7.04-1 8.87-1 1.05+0 1.19+0	1.31+0
$E_b = \beta$ 1.145 1.291 1.368 1.357 1.318 1.270 1.219 1.168 1.118 469.9 eV γ 9.29-3 -5.51-2 6.15-2 2.78-1 4.99-1 7.04-1 8.87-1 1.05+0 1.19+0	1.33 - 1
$E_b = \beta$ 1.145 1.291 1.368 1.357 1.318 1.270 1.219 1.168 1.118 469.9 eV γ 9.29-3 -5.51-2 6.15-2 2.78-1 4.99-1 7.04-1 8.87-1 1.05+0 1.19+0	1.740+0
	1.069
0 0.75-3 9.45-3 2.74-2 4.30-2 b.30-2 8.05-2 9.84-2 1.16-1 1.34-1	1.32+0
2 2.2 3 2.2 3 2 2 1 2 0.00 2 0.00 2 0.01 2 1 1	1.51-1

Tab	nle 1	l (c	nnt	inı	ed)

abic i (contin	aca,										
$4f_{5/2}$	σ	1.466+2	6.111+1	1.600+1	5.757+0	2.512+0	1.249+0	6.818-1	3.999-1	2.481-1	1.610-1
$E_b =$	β	1.015	1.053	1.025	0.957	0.885	0.815	0.749	0.689	0.635	0.585
184.6 eV	γ	1.54 - 1	3.01 - 1	5.76 - 1	7.98 - 1	9.75 - 1	1.11+0	1.22+0	1.31+0	1.38+0	1.44+0
	δ	7.33-2	9.75-2	1.39-1	1.77-1	2.14-1	2.50-1	2.83-1	3.14-1	3.43-1	3.71-1
$4f_{7/2}$	σ	1.860+2	7.715+1	2.004+1	7.166+0	3.109+0	1.537+0	8.353 - 1	4.878 - 1	3.014 - 1	1.948 - 1
$E_b =$	β	1.023	1.051	1.013	0.941	0.869	0.802	0.739	0.683	0.632	0.586
178.9 eV	γ	1.66-1	3.17-1	5.95-1	8.17-1	9.93-1	1.13+0	1.24+0	1.32+0	1.38+0	1.44+0
	δ	7.38-2	9.76-2	1.39-1	1.78-1	2.16-1	2.53-1	2.88-1	3.20-1	3.50-1	3.79-1
$5s_{1/2}$	σ	7.103+0	4.551+0	2.370+0	1.464+0	9.951-1	7.198-1	5.440-1	4.249-1	3.405 - 1	2.787-1
$E_b =$	β	1.794	1.813	1.833	1.846	1.857	1.866	1.875	1.882	1.888	1.894
177.5 eV	$\gamma \\ \delta$	5.37-1 -3.11-4	4.75 - 1 $-1.07 - 3$	3.28 - 1 $-2.15 - 3$	1.91-1 -2.91-3	7.61-2 $-3.49-3$	-1.42-2 $-3.94-3$	-8.20-2 $-4.30-3$	-1.31-1 $-4.62-3$	-1.63-1 $-4.89-3$	-1.82-1 $-5.13-3$
$5p_{1/2}$	σ	6.914+0 1.519	4.743+0 1.619	2.631+0 1.692	1.658+0 1.710	1.128+0 1.709	8.092-1 1.698	6.036-1 1.682	4.640-1 1.663	3.655-1 1.642	2.938-1 1.620
$E_b = 131.8 \text{ eV}$	β γ	4.12-1	2.72-1	7.11–2	-6.42 - 3	-2.82 - 3	4.84-2	1.062	2.21–1	3.24-1	4.31-1
131.0 01	δ	-5.04-3	-8.03 - 3	-8.73-3	-8.52 - 3	-8.13-3	-7.40-3	-6.22 - 3	-4.52 - 3	-2.29 - 3	4.02-4
5p _{3/2}	σ	1.848+1	1.164+1	5.775+0	3.379+0	2.176+0	1.494+0	1.075+0	8.012-1	6.143-1	4.821-1
$E_b =$	β	1.464	1.576	1.688	1.740	1.765	1.775	1.776	1.770	1.760	1.747
103.7 eV	γ	2.40-1	1.28-1	-1.56-2	-5.07 - 2	-1.40-2	6.53-2	1.69-1	2.87-1	4.13-1	5.40-1
	δ	-8.84 - 4	-3.21-3	6.44 - 7	4.85 - 3	9.06 - 3	1.25 - 2	1.53-2	1.78 - 2	2.01-2	2.23 - 2
5d _{3/2}	σ	1.675+1	1.001+1	4.322+0	2.208+0	1.259+0	7.752-1	5.059-1	3.454-1	2.445-1	1.783-1
$E_b =$	β	1.214	1.328	1.411	1.420	1.399	1.365	1.325	1.281	1.237	1.192
33.8 eV	γ	-1.25-2	-3.94-2	7.58 - 2	2.74 - 1	4.85 - 1	6.89 - 1	8.78 - 1	1.05+0	1.20+0	1.34+0
	δ	7.89 - 4	1.05 - 2	3.04 - 2	4.70 - 2	6.16 - 2	7.55 - 2	8.94 - 2	1.03 - 1	1.16 - 1	1.30 - 1
$5d_{5/2}$	σ	2.386+1	1.396+1	5.874+0	2.948+0	1.658+0	1.009+0	6.523-1	4.414 - 1	3.099 - 1	2.243 - 1
$E_b =$	β	1.334	1.393	1.406	1.372	1.323	1.270	1.216	1.163	1.113	1.064
30.6 eV	γ	-2.94-2	-3.23-2	1.19-1	3.32-1	5.45-1	7.42-1	9.19-1	1.08+0	1.21+0	1.33+0
	δ	2.55-3	1.04-2	2.76-2	4.45-2	6.14-2	7.86-2	9.65-2	1.14-1	1.32-1	1.49-1
$6s_{1/2}$	σ	9.964 - 1	6.294 - 1	3.230 - 1	1.983 - 1	1.343 - 1	9.694 - 2	7.314 - 2	5.705 - 2	4.568 - 2	3.734 - 2
$E_b =$	β	1.802	1.818	1.836	1.848	1.858	1.867	1.874	1.882	1.888	1.894
11.0 eV	$\gamma \\ \delta$	5.00-1 -5.31-4	4.40-1 $-1.22-3$	3.01-1 $-2.22-3$	1.71 - 1 $-2.94 - 3$	6.11-2 -3.51-3	-2.57-2 $-3.97-3$	-9.12-2 $-4.34-3$	-1.38-1 $-4.66-3$	-1.68-1 $-4.92-3$	-1.84-1 $-5.13-3$
$6p_{1/2}$	σ	6.855-1	4.635-1	2.538-1	1.591-1	1.080-1	7.738-2	5.764-2	4.427-2	3.485-2	2.799-2
$E_b = 3.2 \text{ eV}$	β	1.557 3.82-1	1.642 2.45-1	1.704 5.90-2	1.717 -9.42-3	1.713 -1.35-3	1.701 5.30-2	1.684 1.34-1	1.664 2.30-1	1.643 3.33-1	1.621 4.38-1
3.2 ev	$\gamma \\ \delta$	-7.53-3	-8.97 - 3	-8.83-3	-9.42-3 -8.54-3	-8.23-3	-7.58-3	-6.45 - 3	-4.80-3	-2.66-3	-3.17-5
6n		1.518+0	9.485-1	4.671-1	2.725-1	1.753-1	1.203-1	8.646-2	6.441-2	4.936-2	3.871-2
$6p_{3/2}$ $E_b =$	$\frac{\sigma}{\beta}$	1.492	1.594	1.699	2.723—1 1.747	1.755-1	1.778	1.778	1.771	4.930—2 1.761	1.748
1.4 eV	γ	2.23-1	1.14-1	-2.02-2	-4.96-2	-1.04-2	7.11-2	1.77-1	2.96-1	4.21-1	5.46-1
	δ	-2.55 - 3	-3.78 - 3	3.49 - 5	4.87 - 3	9.03 - 3	1.24 - 2	1.53 - 2	1.77 - 2	1.99 - 2	2.18 - 2
Z= 85. At: [X	el4f ⁶ 4	If ⁸ , 5d ⁴ , 5d ⁶ ,	$6s_{1/2}^2 6p_{1/2}^2 6p_3^3$	1/2							
,	3/2	k (eV)	2 - 1/2 - 1/2 - 1/3	5/2							
Shell		1500	2000	3000	4000	5000	6000	7000	8000	9000	10000
$4s_{1/2}$	σ	2.613+1	1.840+1	1.036+1	6.611+0	4.574+0	3.346+0	2.550+0	2.005+0	1.615+0	1.327+0
$E_b = 1038.2 \text{ eV}$	$eta \gamma$	1.712 8.34-1	1.760 7.51-1	1.801 5.42-1	1.821 3.57-1	1.835 2.03-1	1.847 8.14-2	1.857 1.14-2	1.866 -8.09-2	1.874 -1.31-1	1.880 -1.65-1
1030.2 CV	δ	2.29-3	3.41-4	-1.62 - 3	-2.74-3	-3.50-3	-4.07 - 3	-4.52 - 3	-4.90-3	-5.23-3	-5.52 - 3
4n. /2	σ	2.753+1	2.130+1	1.300+1	8.498+0	5.895+0	4.281+0	3.221+0	2.493+0	1.973+0	1.592+0
$4p_{1/2} E_b =$	β	1.093	2.130+1 1.400	1.500+1	1.658	1.678	1.680	3.221+0 1.672	2.493+0 1.659	1.642	1.592+0
897.7 eV	γ	5.70-1	5.24-1	2.14-1	4.45-2	-6.46 - 3	1.30-2	7.27-2	1.56-1	2.53-1	3.56-1
	δ	5.30-2	1.19-2	-5.50-3	-7.97 - 3	-8.03 - 3	-7.36-3	-6.22 - 3	-4.60-3	-2.49 - 3	4.34-5
4p _{3/2}	σ	9.005+1	6.022+1	3.134+1	1.867+1	1.214+1	8.385+0	6.058+0	4.531+0	3.483+0	2.738+0
$E_b =$	β	1.161	1.396	1.598	1.687	1.731	1.753	1.762	1.763	1.758	1.748
753.7 eV	γ	3.81 - 1	2.80 - 1	5.35 - 2	-4.44-2	-4.47 - 2	1.31-2	1.05 - 1	2.16 - 1	3.38 - 1	4.64 - 1
	δ	3.25 - 2	7.83 - 3	2.98 - 4	3.98 - 3	8.67 - 3	1.27 - 2	1.62 - 2	1.91 - 2	2.16-2	2.39 - 2
4d _{3/2}	σ	1.293+2	8.053+1	3.547+1	1.814+1	1.032+1	6.347+0	4.136+0	2.820+0	1.994+0	1.453+0
$E_b =$	β	0.939	1.168	1.341	1.387	1.385	1.362	1.328	1.289	1.248	1.206
527.6 eV	γ	5.53-2	-4.57 - 2	5.15 - 3	1.90 - 1	4.04 - 1	6.16 - 1	8.13 - 1	9.91 - 1	1.15+0	1.29+0
	δ	8.97-3	8.19-3	2.88-2	4.75-2	6.31-2	7.77-2	9.15-2	1.05-1	1.17-1	1.29-1
$4d_{5/2}$	σ	1.910+2	1.157+2	4.936+1	2.476+1	1.389+1	8.438+0	5.444+0	3.679+0	2.580+0	1.866+0
$E_b =$	β	1.124	1.281	1.367	1.361	1.325	1.279	1.229	1.178	1.128	1.080
500.1 eV	γ	2.33-2	-5.47-2	4.56-2	2.55-1	4.74-1	6.81-1	8.67-1	1.03+0	1.17+0	1.30+0
	δ	7.78-3	8.75-3	2.62-2	4.40-2	6.13-2	7.88-2	9.66-2	1.14-1	1.31-1	1.47-1
$4f_{5/2}$	σ	1.595+2	6.690+1	1.767+1	6.402+0	2.806+0	1.399+0	7.658 - 1	4.501 - 1	2.797 - 1	1.818 - 1
$E_b =$	β	1.007	1.051	1.030	0.965	0.894	0.824	0.758	0.698	0.644	0.596
207.0 eV	γ	1.39-1	2.84-1	5.59-1	7.84-1	9.65-1	1.11+0	1.22+0	1.31+0	1.38+0	1.44+0
	δ	7.10-2	9.54-2	1.37-1	1.75-1	2.12-1	2.47-1	2.79-1	3.09-1	3.38-1	3.66-1
$4f_{7/2}$	σ	2.023+2	8.443+1	2.213+1	7.964+0	3.471+0	1.721+0	9.376 - 1	5.486 - 1	3.395 - 1	2.198 - 1

table i (contin	uea)										
$E_b = 200.8 \text{ eV}$	$eta \ \gamma \ \delta$	1.017 1.51-1 7.16-2	1.051 3.01-1 9.55-2	1.018 5.79-1 1.37-1	0.949 8.04-1 1.75-1	0.878 9.84-1 2.14-1	0.810 1.12+0 2.50-1	0.747 1.23+0 2.83-1	0.691 1.32+0 3.15-1	0.640 1.39+0 3.45-1	0.596 1.44+0 3.74-1
$5s_{1/2}$ $E_b =$ 193.4 eV	σ	7.395+0	4.745+0	2.476+0	1.532+0	1.043+0	7.556-1	5.718-1	4.471-1	3.587-1	2.938-1
	β	1.779	1.799	1.821	1.836	1.847	1.857	1.866	1.873	1.879	1.885
	γ	5.54-1	4.95-1	3.51-1	2.14-1	9.70-2	4.16-3	-6.73-2	-1.20-1	-1.57-1	-1.80-1
	δ	-2.35-4	-1.06-3	-2.23-3	-3.04-3	-3.65-3	-4.14-3	-4.55-3	-4.90-3	-5.21-3	-5.48-3
$5p_{1/2}$ $E_b = 145.6 \text{ eV}$	σ	7.177+0	4.944+0	2.759+0	1.747+0	1.193+0	8.592-1	6.428-1	4.954-1	3.911-1	3.148-1
	β	1.501	1.608	1.687	1.709	1.710	1.700	1.686	1.668	1.648	1.627
	γ	4.36-1	2.96-1	8.70-2	-6.08-4	-6.19-3	3.73-2	1.10-1	2.01-1	3.01-1	4.05-1
	δ	-5.17-3	-8.49-3	-9.25-3	-8.95-3	-8.51-3	-7.85-3	-6.77-3	-5.20-3	-3.15-3	-6.43-4
$5p_{3/2}$ $E_b = 113.6 \text{ eV}$	σ	1.967+1	1.240+1	6.166+0	3.615+0	2.333+0	1.606+0	1.157+0	8.638-1	6.632-1	5.210-1
	β	1.446	1.562	1.678	1.735	1.763	1.775	1.777	1.773	1.765	1.753
	γ	2.51-1	1.40-1	-8.55-3	-5.13-2	-2.23-2	5.05-2	1.50-1	2.65-1	3.87-1	5.13-1
	δ	-6.09-4	-3.39-3	-4.16-4	4.53-3	8.91-3	1.25-2	1.55-2	1.81-2	2.05-2	2.26-2
$5d_{3/2}$ $E_b = 40.9 \text{ eV}$	σ	1.839+1	1.105+1	4.807+0	2.471+0	1.415+0	8.750-1	5.728-1	3.920-1	2.780-1	2.031-1
	β	1.199	1.319	1.409	1.423	1.405	1.374	1.335	1.293	1.249	1.206
	γ	-5.71-3	-4.08-2	6.18-2	2.52-1	4.61-1	6.65-1	8.56-1	1.03+0	1.18+0	1.32+0
	δ	1.91-4	9.52-3	2.94-2	4.59-2	6.05-2	7.46-2	8.82-2	1.01-1	1.14-1	1.26-1
$5d_{5/2}$ $E_b =$ 37.4 eV	σ	2.627+1	1.544+1	6.540+0	3.301+0	1.864+0	1.139+0	7.384-1	5.008-1	3.523-1	2.555-1
	β	1.329	1.392	1.410	1.378	1.331	1.279	1.226	1.173	1.122	1.074
	γ	-2.52-2	-3.60-2	1.05-1	3.12-1	5.23-1	7.22-1	9.01-1	1.06+0	1.20+0	1.32+0
	δ	2.10-3	9.56-3	2.65-2	4.30-2	5.97-2	7.71-2	9.48-2	1.12-1	1.29-1	1.46-1
$6s_{1/2}$ $E_b =$ 15.0 eV	$\sigma \ eta \ eta \ \gamma \ \delta$	1.109+0 1.788 5.14-1 -4.91-4	7.008-1 1.805 4.58-1 -1.23-3	3.600-1 1.825 3.22-1 -2.31-3	2.212-1 1.838 1.91-1 -3.09-3	1.500-1 1.848 8.01-2 -3.70-3	1.084-1 1.858 -9.05-3 -4.18-3	8.189-2 1.866 -7.71-2 -4.57-3	6.395-2 1.874 -1.27-1 -4.91-3	5.125-2 1.881 -1.61-1 -5.20-3	4.193-2 1.887 -1.81-1 -5.44-3
$6p_{1/2}$ $E_b = 5.7 \text{ eV}$	σ	8.037-1	5.450-1	2.998-1	1.887-1	1.286-1	9.238-2	6.901-2	5.313-2	4.191-2	3.373-2
	β	1.543	1.634	1.700	1.716	1.714	1.704	1.688	1.670	1.649	1.628
	γ	4.02-1	2.66-1	7.27-2	-5.07-3	-5.02-3	4.24-2	1.17-1	2.08-1	3.07-1	4.10-1
	δ	-8.03-3	-9.59-3	-9.40-3	-9.05-3	-8.70-3	-8.07-3	-7.00-3	-5.45-3	-3.41-3	-8.81-4
$6p_{3/2}$ $E_b =$ 2.8 eV	σ	1.838+0	1.149+0	5.668-1	3.313-1	2.135-1	1.468-1	1.057-1	7.882-2	6.048-2	4.750-2
	β	1.478	1.583	1.691	1.742	1.767	1.778	1.780	1.775	1.766	1.754
	γ	2.33-1	1.25-1	-1.40-2	-5.10-2	-1.86-2	5.68-2	1.57-1	2.72-1	3.93-1	5.16-1
	δ	-2.59-3	-4.08-3	-3.75-4	4.59-3	8.94-3	1.25-2	1.54-2	1.79-2	2.01-2	2.21-2
Z= 86, Rn: [X	(e]4f ⁶ _{5/2}	$\frac{4f_{7/2}^8 5d_{3/2}^4 5d_{5/2}^6}{k(2V)}$	2 6s _{1/2} 6p _{1/2} 6p	4 3/2							
Shell		k (eV) 1500	2000	3000	4000	5000	6000	7000	8000	9000	10000
$4s_{1/2}$ $E_b =$ 1090.5 eV	σ β γ δ	2.611+1 1.684 8.62-1 2.89-3	1.853+1 1.740 7.83-1 6.13-4	1.051+1 1.786 5.77-1 -1.59-3	6.734+0 1.808 3.90-1 -2.81-3	4.671+0 1.824 2.33-1 -3.65-3	3.425+0 1.837 1.08-1 -4.27-3	2.615+0 1.847 1.09-2 -4.77-3	2.058+0 1.856 -6.35-2 -5.19-3	1.660+0 1.863 -1.19-1 -5.56-3	1.366+0 1.870 -1.58-1 -5.88-3
$4p_{1/2}$ $E_b = 946.2 \text{ eV}$	σ	2.708+1	2.124+1	1.314+1	8.663+0	6.042+0	4.406+0	3.326+0	2.581+0	2.048+0	1.656+0
	β	1.034	1.367	1.584	1.652	1.676	1.680	1.674	1.662	1.647	1.629
	γ	5.65-1	5.58-1	2.47-1	6.17-2	-2.59-3	6.40-3	5.83-2	1.36-1	2.29-1	3.28-1
	δ	6.27-2	1.48-2	-5.45-3	-8.36-3	-8.47-3	-7.87-3	-6.81-3	-5.31-3	-3.36-3	-9.94-4
$4p_{3/2}$ $E_b =$ 791.2 eV	σ β γ δ	9.190+1 1.118 3.87-1 3.73-2	6.173+1 1.369 3.00-1 9.49-3	3.229+1 1.583 6.90-2 1.30-4	1.931+1 1.677 -3.95-2 3.57-3	1.258+1 1.726 -4.95-2 8.37-3	8.713+0 1.751 1.68-4 1.26-2	6.307+0 1.762 8.57-2 1.62-2	4.724+0 1.764 1.93-1 1.93-2	3.637+0 1.761 3.11-1 2.19-2	2.862+0 1.753 4.35-1 2.42-2
$4d_{3/2}$ $E_b = 560.4 \text{ eV}$	$\sigma \ eta \ eta \ \gamma \ \delta$	1.327+2 0.901 7.24-2 1.13-2	8.344+1 1.146 -3.98-2 7.53-3	3.714+1 1.332 -8.47-3 2.74-2	1.911+1 1.385 1.67-1 4.63-2	1.093+1 1.388 3.77-1 6.21-2	6.745+0 1.368 5.88-1 7.67-2	4.408+0 1.337 7.86-1 9.02-2	3.012+0 1.300 9.65-1 1.03-1	2.134+0 1.261 1.12+0 1.15-1	1.557+0 1.220 1.27+0 1.27-1
$4d_{5/2}$ $E_b =$ 531.1 eV	$\sigma \ eta$	1.967+2 1.102	1.201+2 1.270	5.172+1 1.366	2.609+1 1.364	1.470+1 1.331	8.961+0 1.287	5.796+0 1.238	3.925+0 1.188	2.758+0 1.139	1.997+0 1.091
	γ	3.88-2	-5.28-2	3.04-2	2.33-1	4.50-1	6.58-1	8.46-1	1.01+0	1.16+0	1.28+0
	δ	9.20-3	8.19-3	2.49-2	4.25-2	5.96-2	7.71-2	9.46-2	1.11-1	1.28-1	1.43-1
$4f_{5/2}$ $E_b =$ 230.1 eV	γ	3.88-2 9.20-3 1.730+2 0.999 1.24-1 6.87-2	-5.28-2 8.19-3 7.303+1 1.049 2.67-1 9.32-2	3.04-2 2.49-2 1.946+1 1.034 5.43-1 1.35-1	2.33-1 4.25-2 7.096+0 0.973 7.70-1 1.72-1	4.50-1 5.96-2 3.125+0 0.903 9.55-1 2.09-1	6.58-1 7.71-2 1.563+0 0.833 1.10+0 2.43-1	8.46-1 9.46-2 8.576-1 0.767 1.21+0 2.74-1	1.01+0 1.11-1 5.050-1 0.708 1.30+0 3.05-1	1.16+0 1.28-1 3.144-1 0.655 1.38+0 3.34-1	1.28+0 1.43-1 2.047-1 0.607 1.44+0 3.62-1
$E_b =$	γ	3.88-2	-5.28-2	3.04-2	2.33-1	4.50-1	6.58-1	8.46-1	1.01+0	1.16+0	1.28+0
	δ	9.20-3	8.19-3	2.49-2	4.25-2	5.96-2	7.71-2	9.46-2	1.11-1	1.28-1	1.43-1
	σ	1.730+2	7.303+1	1.946+1	7.096+0	3.125+0	1.563+0	8.576-1	5.050-1	3.144-1	2.047-1
	β	0.999	1.049	1.034	0.973	0.903	0.833	0.767	0.708	0.655	0.607
	γ	1.24-1	2.67-1	5.43-1	7.70-1	9.55-1	1.10+0	1.21+0	1.30+0	1.38+0	1.44+0

$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	ble 1 (continu	δ	-1.42-4	-1.04 - 3	-2.29 - 3	-3.17 - 3	-3.83 - 3	-4.37 - 3	-4.82 - 3	-5.21-3	-5.55-3	-5.84-3
1935 Y 459-1 321-1 104-1 659-3 -8.23-3 276-2 948-2 181-1 277-1 -403-3 -303-3												3.364-1
\$\begin{array}{c c c c c c c c c c c c c c c c c c c												1.634
1	159.5 eV											3.78-1 -1.73-
1239 Y												5.616-1
		-										1.759 4.85-1
fb. = 6, state β 1.184 1.309 1.406 1.425 1.411 1.382 1.345 1.304 1.562 1.616 1.660 8 -3.41-4 8.54-3 2.83-2 2.31-1 4.37-1 6.41-1 8.22-1 1.00-1 1.616 1.625 1.62	123.3 6											2.28-2
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $												2.296-1
1												1.220 1.30+0
fs, = β β 1.325 1.391 1.413 1.334 1.339 1.238 1.236 1.130 1.31 1.32 42 2 v γ -0.02 2.09 1.040 1.136 1.266 1.136 1.266 1.136 1.266<	40.0 6											1.23-1
44.2 γ γ −2.02 - 2 −3.88 - 2 −3.14 - 2 −3.91 −3.03 - 1 −7.02 - 1 −8.87 −3.05 - 1 −3.05 −3.0												2.886-1
1												1.085 1.30+0
E _j = β β 1.772 1.792 1.813 1.827 1.838 1.848 1.848 1.845 1.856 1.872 β 5.28 - 4.42 - 4 -1.23 - 3 -3.24 - 3 -3.88 - 3 -6.21 - 2 -1.15 - 1 -1.53 - 1 -1.55 - 1	44,2 CV											1.41-1
18.7e												4.653-2
$β$ $-4.42-4$ $-1.23-3$ $-3.24-3$ $-3.88-3$ $-4.39-3$ $-4.82-3$ $-5.91-3$ $-5.51-3$ $4.91-2$ E_8 $β$ 1.529 1.625 1.696 1.715 1.706 1.626 1.625 1.685 1.685 1.685 1.685 1.685 1.685 1.685 1.685 1.682 1.682 1.682 1.715 1.706 1.682 1.682 1.612 $3.78-2$ $-0.63-3$ -0.63												1.878 -1.78-
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	10.7 € \$											-1.78- -5.79-
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$												3.965-2
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $												1.635 3.84-1
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$,,o c v											-1.74-1
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$												5.666-2
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$		-										1.760 4.89-1
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $	4.1 CV											2.25-2
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	Z= 87, Fr: [Rn	1]7s _{1/2}										
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$												
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$												10000
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$												1.403+0 1.861
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$												-1.47-1
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$												-6.22 - 3
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$												1.719+0
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$												1.635 2.99-1
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	1000.7 ev											-2.00-1
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$												2.988+0
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$												1.757 4.02-1
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	333.1 EV											2.44-2
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$4d_{3/2}$											1.667+0
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$												1.235 1.24+0
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$)96.7 EV											1.24+0
$\begin{array}{cccccccccccccccccccccccccccccccccccc$												2.135+0
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$									1.246			1.105 1.26+0
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	JU1.J EV											1.26+0 1.40-1
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$4f_{5/2}$											2.299-1
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	$E_b =$	β										0.619
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	258.6 eV											1.45+0 3.60-1
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\frac{1}{4f_{7/2}}$			1.003+2								2.775-1
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	$E_b =$											0.616
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	251.6 eV											1.45+0 3.68-1
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	5s _{1/2}							8.285-1				3.246-1
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	$E_b =$	β										1.867
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	230.9 eV											-1.70-6
$\stackrel{\longleftarrow}{E_b} = \begin{array}{ccccccccccccccccccccccccccccccccccc$	5p _{1/2}											3.586-1
	$E_b =$		1.460	1.585	1.678	1.705	1.710	1.704	1.693	1.677	1.660	1.641
δ -5.33-3 -9.48-3 -1.03-2 -9.93-3 -9.52-3 -8.94-3 -8.00-3 -6.65-3 -4.88-3	178.7 eV											3.49-1
		δ	-5.33-3	-9.48-3	-1.03-2	-9.93-3	-9.52-3	-8.94-3	-8.00-3	-6.65-3	-4.88-3	-2.68-

Table 1 (contin	ued)										
5p _{3/2}	σ	2.211+1	1.397+1	6.974+0	4.109+0	2.663+0	1.840+0	1.330+0	9.954-1	7.661-1	6.030-1
$E_b =$	β	1.406	1.534	1.661	1.722	1.755	1.772	1.779	1.778	1.773	1.764
138.7 eV	γ	2.73 - 1	1.66 - 1	7.97 - 3	-5.00-2	-3.60-2	2.46 - 2	1.14 - 1	2.19 - 1	3.34 - 1	4.53 - 1
	δ	1.24 - 4	-3.70 - 3	-1.27 - 3	3.82 - 3	8.58 - 3	1.26 - 2	1.59 - 2	1.86 - 2	2.09 - 2	2.30-2
5d _{3/2}	σ	2.174+1	1.319+1	5.827+0	3.031+0	1.752+0	1.091+0	7.181 - 1	4.939 - 1	3.519-1	2.580 - 1
$E_b =$	β	1.168	1.300	1.404	1.426	1.416	1.389	1.355	1.317	1.277	1.236
60.0 eV	γ	9.90-3	-4.06-2	3.56-2	2.13-1	4.16-1	6.16-1	8.03-1	9.75-1	1.13+0	1.27+0
	δ	-8.12-4	7.58-3	2.71-2	4.42-2	5.89-2	7.19-2	8.43-2	9.65-2	1.09-1	1.21-1
$5d_{5/2}$	σ	3.127+1	1.854+1	7.956+0	4.059+0	2.312+0	1.422+0	9.268-1	6.315-1	4.461-1	3.246-1
$E_b =$	β	1.319	1.390	1.415	1.389	1.346	1.296	1.244	1.194	1.146	1.099
55.6 eV	$\gamma \\ \delta$	-1.47-2 1.34-3	-4.09-2 $8.05-3$	7.75-2 2.42-2	2.76-1 $4.06-2$	4.86-1 5.71-2	6.82-1 7.33-2	8.60-1 $8.93-2$	1.02+0 1.06-1	1.16+0 1.22-1	1.29+0 1.38-1
Co				4.524-1							
$6s_{1/2} E_b =$	$\frac{\sigma}{eta}$	1.389+0 1.756	8.792-1 1.778	4.524-1 1.802	2.785-1 1.817	1.894-1 1.828	1.373-1 1.837	1.040-1 1.846	8.134-2 1.854	6.530-2 1.861	5.352-2 1.868
26.3 eV	γ	5.42-1	4.92-1	3.62-1	2.33-1	1.21-1	2.77-2	-4.70-2	-1.04-1	-1.46-1	-1.75-1
	δ	-3.85 - 4	-1.24 - 3	-2.48 - 3	-3.37 - 3	-4.06 - 3	-4.63 - 3	-5.12 - 3	-5.54 - 3	-5.90 - 3	-6.19 - 3
6p _{1/2}	σ	1.094+0	7.459-1	4.140-1	2.627-1	1.803-1	1.304-1	9.801-2	7.583-2	6.007-2	4.851-2
$E_b =$	β	1.513	1.616	1.693	1.715	1.716	1.708	1.696	1.679	1.661	1.641
13.2 eV	γ	4.43 - 1	3.09 - 1	1.03 - 1	7.87 - 3	-8.99 - 3	2.35 - 2	8.71 - 2	1.70 - 1	2.62 - 1	3.61 - 1
	δ	-9.16-3	-1.09-2	-1.06-2	-9.94-3	-9.50-3	-8.96-3	-8.07-3	-6.76-3	-4.99-3	-2.81-3
$6p_{3/2}$	σ	2.739+0	1.714+0	8.470 - 1	4.968 - 1	3.213 - 1	2.217 - 1	1.602 - 1	1.199 - 1	9.221 - 2	7.257 - 2
$E_b =$	β	1.446	1.557	1.674	1.731	1.762	1.776	1.782	1.780	1.775	1.765
8.8 eV	γ	2.52-1	1.47-1	-6.15-4	-5.06-2	-3.23-2	3.01-2	1.21-1	2.28-1	3.44-1	4.65-1
	δ	-2.59-3	-4.64-3	-1.28-3	3.92-3	8.58-3	1.25-2	1.57-2	1.84-2	2.08-2	2.29-2
$7s_{1/2}$	σ	8.657-2	5.463-2 1.777	2.802-2 1.802	1.722-2 1.816	1.170-2 1.827	8.470-3 1.837	6.410-3	5.014-3 1.855	4.024-3	3.297-3 1.869
$E_b = 4.0 \text{ eV}$	$eta \gamma$	1.755 5.45-1	4.94—1	3.61-1	2.33-1	1.827	2.63-2	1.846 -4.79-2	-1.04-1	1.863 -1.45-1	-1.73-1
4.0 C V	δ	-3.90-4	-1.26-3	-2.48-3	-3.39-3	-4.09 - 3	-4.65-3	-5.11-3	-5.51-3	-5.84-3	-6.14-3
Z= 88, Ra: [R	n 17c ²										
Z- 00, Nd. [N	11]/S _{1/2}	k (eV)									
Shell		1500	2000	3000	4000	5000	6000	7000	8000	9000	10000
4s _{1/2}	σ_{ρ}	2.587+1 1.622	1.870+1 1.694	1.078+1 1.753	6.961+0 1.779	4.857+0 1.797	3.576+0 1.811	2.739+0 1.823	2.162+0 1.834	1.748+0 1.843	1.440+0 1.851
$E_b = 1208.4 \text{ eV}$	$eta \ \gamma$	9.07-1	8.47-1	6.49-1	4.61-1	2.99-1	1.66-1	6.01-2	-2.28-2	-8.62-2	-1.33-1
1200.4 CV	δ	4.33-3	1.34-3	-1.45 - 3	-2.94-3	-3.94-3	-4.70-3	-5.29 - 3	-5.77 - 3	-6.19 - 3	-6.54-3
$4p_{1/2}$	σ	2.595+1	2.097+1	1.337+1	8.958+0	6.320+0	4.647+0	3.532+0	2.756+0	2.197+0	1.784+0
$E_b =$	β	0.861	1.289	1.553	1.636	1.668	1.678	1.676	1.668	1.656	1.640
1057.6 eV	γ	5.08 - 1	6.23 - 1	3.19 - 1	1.04 - 1	1.16 - 2	-8.95 - 4	3.45 - 2	9.87 - 2	1.80 - 1	2.72 - 1
	δ	9.01-2	2.29-2	-5.06 - 3	-9.18 - 3	-9.56 - 3	-9.01 - 3	-8.04 - 3	-6.68 - 3	-4.92 - 3	-2.77 - 3
$4p_{3/2}$	σ	9.547+1	6.470+1	3.421+1	2.060+1	1.350+1	9.385+0	6.816+0	5.120+0	3.951+0	3.117+0
$E_b =$	β	1.016	1.308	1.547	1.654	1.711	1.742	1.758	1.765	1.765	1.761
879.1 eV	γ	3.87-1	3.37-1	1.03-1	-2.56-2	-5.55-2	-2.20-2	5.01-2	1.46-1	2.55-1	3.72-1
	δ	4.97-2	1.38-2	-3.36-5	2.67-3	7.67-3	1.23-2	1.63-2	1.96-2	2.24-2	2.49-2
$4d_{3/2}$	σ	1.392+2	8.916+1	4.052+1	2.113+1	1.219+1	7.576+0	4.980+0	3.420+0	2.434+0	1.783+0
$E_b = 635.9 \text{ eV}$	β	0.819 1.07-1	1.095 -2.35-2	1.310 -3.17-2	1.379 1.23-1	1.392 3.23-1	1.379 5.28-1	1.354 7.24-1	1.322 9.06-1	1.286 1.07+0	1.248 1.22+0
033.3 CV	$_{\delta}^{\gamma}$	1.82-2	6.79-3	2.47-2	4.40-2	6.00-2	7.40-2	8.71-2	9.97-2	1.12-1	1.24-1
4d _{5/2}	σ	2.078+2	1.289+2	5.652+1	2.884+1	1.638+1	1.005+1	6.536+0	4.447+0	3.137+0	2.280+0
$E_b =$	β	1.052	1.244	1.362	1.370	1.343	1.303	1.257	1.210	1.163	1.117
602.7 eV	γ	7.27-2	-4.47 - 2	2.96-3	1.90-1	4.03-1	6.08-1	7.96-1	9.66-1	1.12+0	1.25+0
	δ	1.34 - 2	7.44 - 3	2.24 - 2	3.97 - 2	5.63 - 2	7.28 - 2	8.94 - 2	1.06 - 1	1.23 - 1	1.39 - 1
4f _{5/2}	σ	2.021+2	8.634+1	2.342+1	8.643+0	3.839+0	1.934+0	1.067+0	6.310-1	3.941-1	2.573-1
$E_b =$	β	0.979	1.043	1.042	0.986	0.920	0.854	0.790	0.730	0.676	0.625
287.9 eV	γ	9.49-2	2.33-1	5.07-1	7.40-1	9.29-1	1.08+0	1.20+0	1.30+0	1.38+0	1.45+0
	δ	6.41-2	8.86-2	1.30-1	1.67-1	2.03-1	2.37-1	2.69-1	2.99-1	3.27-1	3.54-1
$4f_{7/2}$	σ	2.563+2	1.089+2	2.929+1	1.074+1	4.741+0	2.375+0	1.304+0	7.675-1	4.774-1	3.104-1
$E_b = 280.4 \text{ eV}$	β	0.995 1.06-1	1.046 2.50-1	1.031 5.30-1	0.970	0.903	0.838 1.10+0	0.776 1.22+0	0.720 1.32+0	0.669 1.39+0	0.622 1.45+0
280.4 eV	$_{\delta}^{\gamma}$	6.50-2	8.90-2	1.30-1	7.64-1 1.67-1	9.52-1 2.04-1	2.40-1	2.73-1	3.05-1	3.34-1	3.62-1
Fo											
$5s_{1/2}$ $E_b =$	$\frac{\sigma}{\beta}$	8.258+0 1.725	5.325+0 1.753	2.795+0 1.782	1.738+0 1.799	1.189+0 1.813	8.652-1 1.824	6.572-1 1.834	5.156-1 1.843	4.148-1 1.851	3.405-1 1.858
254.4 eV	γ	6.04-1	5.58-1	4.24-1	2.87-1	1.66-1	6.50-2	-1.61-2	-7.94-2	-1.27-1	-1.61-1
2J7,7 € V	δ	9.39-5	-9.59-4	-2.42-3	-3.45-3	-4.23-3	-4.85 - 3	-5.36-3	-7.34-2 $-5.80-3$	-6.18-3	-6.51-1
5p _{1/2}	σ	7.891+0	5.509+0	3.133+0	2.013+0	1.392+0	1.012+0	7.637-1	5.929-1	4.711-1	3.815-1
$E_b =$	β	1.441	1.568	1.669	1.702	1.709	1.706	1.695	1.681	1.665	1.647
200.4 eV	γ	5.08 - 1	3.75 - 1	1.43 - 1	2.52 - 2	-8.07 - 3	1.26 - 2	6.66 - 2	1.41 - 1	2.28 - 1	3.23-1
	δ	-5.34-3	-9.93-3	-1.11-2	-1.06-2	-1.00-2	-9.37 - 3	-8.47 - 3	-7.20-3	-5.52-3	-3.41-3
$5p_{3/2} E_b =$	$\frac{\sigma}{eta}$	2.335+1 1.389	1.478+1 1.514	7.390+0 1.647	4.361+0 1.714	2.832+0 1.751	1.959+0 1.770	1.419+0 1.778	1.064+0 1.780	8.198-1 1.776	6.462-1 1.769

able 1 (contin	ued)										
152.8 eV	$_{\delta}^{\gamma}$	2.84-1 6.09-4	1.79-1 -3.75-3	1.65-2 -1.76-3	-4.84-2 3.41-3	-4.12-2 8.33-3	1.24-2 1.25-2	9.53-2 1.59-2	1.96-1 1.88-2	3.08-1 2.13-2	4.26-1 2.35-2
5d _{3/2}	σ	2.344+1	1.429+1	6.359+0	3.325+0	1.930+0	1.207+0	7.971-1	5.498-1	3.926-1	2.884-1
$E_b =$	β	1.151	1.286	1.399	1.427	1.420	1.397	1.365	1.328	1.290	1.250
69.4 eV	γ	1.79 - 2	-3.95 - 2	2.50-2	1.93 - 1	3.89 - 1	5.88 - 1	7.77 - 1	9.53 - 1	1.11+0	1.26+0
	δ	-1.20-3	6.71-3	2.63-2	4.31-2	5.74-2	7.07-2	8.34-2	9.59-2	1.08-1	1.20-1
$5d_{5/2}$	σ	3.383+1	2.015+1	8.703+0	4.461+0	2.551+0	1.575+0	1.030+0	7.035 - 1	4.981 - 1	3.631 - 1
$E_b =$	β	1.313	1.387	1.418	1.394	1.353	1.305	1.256	1.206	1.158	1.111
63.8 eV	γ	-9.14-3	-4.24-2	6.67-2	2.58-1	4.62-1	6.58-1	8.38-1	1.00+0	1.15+0	1.27+0
	δ	1.04-3	7.42-3	2.33-2	3.91-2	5.49-2	7.10-2	8.75-2	1.04 - 1	1.21-1	1.37 - 1
$6s_{1/2}$	σ	1.567+0	9.927 - 1	5.113 - 1	3.151 - 1	2.145 - 1	1.556 - 1	1.179 - 1	9.236 - 2	7.421 - 2	6.086 - 2
$E_b =$	β	1.738	1.761	1.787	1.803	1.815	1.826	1.836	1.844	1.852	1.859
35.5 eV	$\gamma \\ \delta$	5.58-1 -3.09-4	5.14-1 $-1.23-3$	3.86-1 -2.56-3	2.57-1 -3.53-3	1.43 - 1 $-4.28 - 3$	4.69-2 $-4.89-3$	-3.02-2 $-5.39-3$	-9.03-2 $-5.83-3$	-1.35-1 $-6.20-3$	-1.67-1 $-6.52-3$
$\begin{array}{l} 6p_{1/2} \\ E_b = \end{array}$	$\frac{\sigma}{eta}$	1.263+0 1.496	8.644-1 1.601	4.821-1 1.686	3.071-1 1.712	2.115-1 1.716	1.534-1 1.710	1.156-1 1.699	8.963-2 1.684	7.115-2 1.667	5.757-2 1.648
19.2 eV	γ	4.64-1	3.33-1	1.20-1	1.57-2	-9.14-3	1.67-2	7.42-2	1.51-1	2.39-1	3.33-1
10.2 01	δ	-9.62 - 3	-1.17-2	-1.14-2	-1.06-2	-1.01-2	-9.52 - 3	-8.66-3	-7.43 - 3	-5.79-3	-3.73-3
6p _{3/2}	σ	3.302+0	2.068+0	1.023+0	6.011-1	3.895-1	2.691-1	1.947-1	1.458-1	1.123-1	8.850-2
$E_b =$	β	1.427	1.539	1.662	1.723	1.757	1.774	1.782	1.782	1.778	1.770
13.7 eV	γ	2.61-1	1.58-1	6.92-3	-4.99-2	-3.80-2	1.89-2	1.04-1	2.06-1	3.18-1	4.35-1
	δ	-2.40 - 3	-4.90 - 3	-1.78 - 3	3.54 - 3	8.42 - 3	1.25 - 2	1.58 - 2	1.86 - 2	2.10-2	2.31 - 2
7s _{1/2}	σ	1.380-1	8.712-2	4.470-2	2.748-2	1.869-2	1.355-2	1.027-2	8.040-3	6.458-3	5.296-3
$E_b =$	β	1.738	1.761	1.787	1.804	1.817	1.827	1.836	1.844	1.851	1.858
5.0 eV	γ	5.58 - 1	5.12 - 1	3.84 - 1	2.54 - 1	1.40 - 1	4.59 - 2	-3.07 - 2	-9.07 - 2	-1.36-1	-1.68-1
	δ	-3.35-4	-1.24 - 3	-2.58 - 3	-3.55-3	-4.27-3	-4.86 - 3	-5.38 - 3	-5.84 - 3	-6.22 - 3	-6.58-3
Z= 89, Ac: [R	n]6d _{3/2}										
		k (eV)									
Shell		1500	2000	3000	4000	5000	6000	7000	8000	9000	10000
$4s_{1/2}$	σ	2.565+1	1.875+1	1.089+1	7.066+0	4.944+0	3.649+0	2.800+0	2.213+0	1.791+0	1.478+0
$E_b = 1269.4 \text{ eV}$	β	1.585 9.31-1	1.667 8.79-1	1.735 6.85-1	1.764 4.96-1	1.784 3.33-1	1.799 1.97—1	1.811 8.80-2	1.822 7.89-4	1.831 -6.75-2	1.839 1.20 1
1209.4 ev	$\gamma \\ \delta$	5.33-3	1.81-3	-1.35-3	-2.98-3	-4.07 - 3	-4.89 - 3	-5.54-3	-6.08-3	-6.75-2 -6.55-3	-6.96 - 3
4		2.529+1	2.075+1	1.344+1	9.082+0	6.445+0	4.761+0	3.631+0	2.842+0	2.272+0	
$\begin{array}{l} 4p_{1/2} \\ E_b = \end{array}$	$\frac{\sigma}{eta}$	0.750	2.075+1 1.244	1.544+1	1.628	1.664	1.677	1.677	2.842+0 1.670	1.659	1.848+0 1.645
1112.8 eV	γ	4.53-1	6.51-1	3.58-1	1.28-1	2.23-2	-1.70-3	2.47-2	8.22-2	1.59-1	2.47-1
	δ	1.07 - 1	2.80-2	-4.79 - 3	-9.56 - 3	-1.00-2	-9.54 - 3	-8.63 - 3	-7.36 - 3	-5.70 - 3	-3.68 - 3
4p _{3/2}	σ	9.720+1	6.620+1	3.518+1	2.125+1	1.396+1	9.729+0	7.079+0	5.326+0	4.116+0	3.251+0
$E_b =$	β	0.958	1.274	1.530	1.642	1.703	1.737	1.756	1.765	1.767	1.764
924.3 eV	γ	3.81 - 1	3.54 - 1	1.21 - 1	-1.65-2	-5.61-2	-3.13-2	3.40-2	1.25 - 1	2.30 - 1	3.45 - 1
	δ	5.73-2	1.66-2	-2.70-5	2.20-3	7.23-3	1.21-2	1.62-2	1.98-2	2.27-2	2.53-2
$4d_{3/2}$	σ	1.422+2	9.201+1	4.225+1	2.217+1	1.285+1	8.017+0	5.285+0	3.638+0	2.594+0	1.903+0
$E_b =$	β	0.775	1.067	1.299	1.374	1.392	1.384	1.361	1.331	1.296	1.260
673.9 eV	γ	1.25-1 2.31-2	-1.29-2	-4.13-2	1.00-1	2.95-1	5.00-1	6.98-1	8.81-1	1.05+0	1.20+0
	δ		6.78-3	2.33-2	4.26-2	5.89-2	7.33-2	8.64-2	9.87-2	1.10-1	1.21-1
$4d_{5/2}$	σ	2.134+2	1.335+2	5.904+1	3.029+1	1.728+1	1.064+1	6.935+0	4.728+0	3.341+0	2.432+0
$E_b = 641.1 \text{ eV}$	β	1.023 9.25-2	1.230 -3.80-2	1.359 -9.82-3	1.373 1.68-1	1.349 3.78-1	1.311 5.84-1	1.266 7.75-1	1.220 9.46-1	1.173 1.10+0	1.127 1.23+0
041.1 CV	$\gamma \\ \delta$	1.65-2	7.29-3	2.11-2	3.81-2	5.47-2	7.14-2	8.80-2	1.04-1	1.20-1	1.36-1
1f	σ	2.176+2	9.354+1	2.559+1	9.501+0	4.240+0	2.142+0	1.185+0	7.021-1	4.393-1	2.873-1
$ 4f_{5/2} E_b = $	β	0.968	1.039	1.045	0.994	0.929	0.862	0.798	0.738	0.684	0.635
316.4 eV	γ	8.04-2	2.15-1	4.89-1	7.25 - 1	9.18-1	1.07+0	1.20+0	1.30+0	1.38+0	1.45+0
	δ	6.17-2	8.63-2	1.28-1	1.65-1	2.01-1	2.34-1	2.65-1	2.94-1	3.22-1	3.49-1
4f _{7/2}	σ	2.761+2	1.179+2	3.199+1	1.180+1	5.233+0	2.630+0	1.447+0	8.535-1	5.318-1	3.463-1
$E_b =$	β	0.985	1.043	1.035	0.977	0.911	0.845	0.783	0.727	0.676	0.630
308.4 eV	γ	9.06 - 2	2.33 - 1	5.13-1	7.50 - 1	9.42 - 1	1.09+0	1.21+0	1.31+0	1.39+0	1.46+0
	δ	6.26-2	8.67-2	1.28-1	1.66-1	2.02 - 1	2.37-1	2.69-1	2.99-1	3.29-1	3.57-1
$5s_{1/2}$	σ	8.526+0	5.509+0	2.898+0	1.805+0	1.237+0	9.014 - 1	6.857 - 1	5.386 - 1	4.338 - 1	3.564-1
$E_b =$	β	1.704	1.735	1.768	1.787	1.801	1.813	1.823	1.832	1.839	1.847
273.5 eV	$\gamma \over \delta$	6.20-1 2.47-4	5.77-1 -9.06-4	4.46-1 $-2.48-3$	3.11-1 -3.57-3	1.90-1 -4.41-3	8.78-2 $-5.09-3$	3.94-3 -5.65-3	-6.30-2 $-6.14-3$	-1.15-1 $-6.57-3$	-1.53-1 -6.94-3
En											-6.94-3
5p _{1/2}	σ_{β}	8.096+0 1.417	5.677+0 1.555	3.250+0 1.663	2.098+0 1.699	1.457+0 1.709	1.063+0 1.707	8.046-1 1.698	6.264-1 1.685	4.988-1 1.670	4.047-1 1.653
$E_b = 216.9 \text{ eV}$	$eta \ \gamma$	5.31-1	4.01–1	1.64–1	3.68-2	-5.73-3	6.69-3	5.43-2	1.085	2.08-1	1.053 2.99—1
_ 10,5 CV	δ	-5.38-3	-1.05-2	-1.17-2	-1.11-2	-3.75-3 -1.05-2	-9.87 - 3	-9.03-3	-7.86 - 3	-6.29-3	-4.34-3
5p _{3/2}	σ	2.463+1	1.560+1	7.818+0	4.622+0	3.007+0	2.085+0	1.512+0	1.135+0	8.761-1	6.913-1
$E_b =$	β	1.367	1.498	1.637	1.707	1.746	1.767	1.778	1.781	1.779	1.773
167.8 eV	γ	2.95 - 1	1.92 - 1	2.62 - 2	-4.53-2	-4.55-2	1.46 - 3	7.91 - 2	1.76 - 1	2.85 - 1	4.00 - 1
167.8 eV		2.95 - 1 $1.14 - 3$	1.92-1 -3.83-3	2.62-2 $-2.23-3$	-4.53-2 $2.96-3$	-4.55-2 8.03-3	1.46-3 1.24-2	7.91-2 1.60-2	1.76—1 1.91—2	2.85 - 1 $2.17 - 2$	4.00-1 $2.40-2$

Tab	le 1 (continued)

ible 1 (contini	ued)										
$5d_{3/2}$	σ	2.525+1	1.548+1	6.933+0	3.644+0	2.125+0	1.333+0	8.832-1	6.107-1	4.369-1	3.216-1
$E_b =$	β	1.132	1.275	1.395	1.427	1.424	1.404 5.64-1	1.374	1.339	1.301	1.262
83.3 eV	$_{\delta}^{\gamma}$	2.79-2 -1.55-3	-3.72-2 5.75-3	1.36-2 2.51-2	1.72-1 4.20-2	3.66-1 $5.66-2$	7.01-2	7.54-1 8.27-2	9.30-1 $9.46-2$	1.09+0 1.06-1	1.23+0 1.17-1
- d											
5d _{5/2}	σ_{ρ}	3.657+1 1.307	2.187+1 1.385	9.501+0 1.420	4.893+0 1.400	2.810+0 1.360	1.741+0 1.314	1.141+0 1.265	7.813-1 1.216	5.541-1 1.167	4.046-1 1.120
$E_b = 77.7 \text{ eV}$	β	-1.70-3	-4.31-2	5.40-2	2.39-1	4.42-1	6.38-1	8.20-1	9.83-1	1.107	1.120
77.7 CV	$\delta \gamma$	7.47-4	6.69-3	2.21-2	3.77-2	5.36-2	6.98-2	8.61-2	1.02-1	1.18-1	1.34-1
6s _{1/2}	σ	1.722+0	1.092+0	5.632-1	3.474-1	2.368-1	1.719-1	1.305-1	1.023-1	8.230-2	6.755-2
$E_b =$	β	1.719	1.745	1.773	1.791	1.804	1.815	1.825	1.834	1.842	1.849
39.8 eV	$_{\delta}^{\gamma}$	5.70-1 $-2.32-4$	5.29 - 1 $-1.22 - 3$	4.06-1 $-2.64-3$	2.79-1 -3.68-3	1.64-1 $-4.47-3$	6.77 - 2 $-5.11 - 3$	-1.16-2 $-5.66-3$	-7.45-2 $-6.13-3$	-1.23-1 $-6.54-3$	-1.58- -6.90-
6p _{1/2}	σ	1.394+0	9.563-1	5.359-1	3.427-1	2.368-1	1.724-1	1.302-1	1.012-1	8.054-2	6.530-2
$E_b =$	β	1.479	1.592	1.682	1.711	1.717	1.712	1.702	1.688	1.672	1.654
24.1 eV	γ	4.85 - 1	3.56 - 1	1.38 - 1	2.53 - 2	-7.75 - 3	1.04 - 2	6.12 - 2	1.33 - 1	2.17 - 1	3.08 - 1
	δ	-1.03-2	-1.25-2	-1.21-2	-1.12-2	-1.06-2	-9.95 - 3	-9.14 - 3	-7.97 - 3	-6.42 - 3	-4.46-
6p _{3/2}	σ	3.823+0	2.395+0	1.187+0	6.979-1	4.529-1	3.134-1	2.271-1	1.704-1	1.314-1	1.036-
$E_b =$	β	1.411	1.527	1.652	1.717	1.753	1.772	1.782	1.784	1.781	1.774
17.0 eV	γ	2.70 - 1	1.69 - 1	1.48 - 2	-4.79 - 2	-4.25 - 2	7.85 - 3	8.71 - 2	1.84 - 1	2.93 - 1	4.07 - 1
	δ	-2.36-3	-5.17-3	-2.27 - 3	3.12-3	8.16-3	1.24-2	1.59-2	1.88-2	2.13-2	2.36-2
$6d_{3/2}$	σ	1.544+0	9.415-1	4.201-1	2.206-1	1.286-1	8.065-2	5.343-2	3.694-2	2.643-2	1.946-2
$E_b =$	β	1.158	1.294	1.405	1.433	1.428	1.406	1.375	1.340	1.303	1.264
6.0 eV	$_{\delta}^{\gamma}$	2.37-2 $-2.48-3$	-3.68-2 $5.67-3$	1.92-2 2.51-2	1.81-1 4.20-2	3.75-1 5.65-2	5.71-1 6.93-2	7.57-1 8.13-2	9.30-1 9.29-2	1.09+0 1.04-1	1.24+0 1.16-1
7.										8.124-3	6.666-3
$7s_{1/2}$ $E_b =$	$\frac{\sigma}{\beta}$	1.724-1 1.720	1.089-1 1.746	5.591-2 1.774	3.441-2 1.791	2.342-2 1.804	1.700-2 1.814	1.289-2 1.824	1.011-2 1.832	8.124-3 1.840	1.848
6.0 eV	γ	5.68-1	5.26-1	4.03-1	2.76-1	1.63-1	6.61-2	-1.36-2	-7.71-2	-1.26-1	-1.60-
	δ	-2.75-4	-1.25 - 3	-2.67 - 3	-3.69 - 3	-4.48 - 3	-5.14 - 3	-5.71-3	-6.21-3	-6.60 - 3	-6.98-
Z= 90, Th: [R	n]6d _{3/2}	7s _{1/2}									
		k (eV)									
Shell		1500	2000	3000	4000	5000	6000	7000	8000	9000	10000
4s _{1/2}	σ	2.535+1	1.876+1	1.099+1	7.163+0	5.027+0	3.718+0	2.858+0	2.263+0	1.834+0	1.514+0
$E_b =$	β	1.543	1.638	1.714	1.747	1.769	1.784	1.797	1.808	1.818	1.826
1329.5 eV	γ	9.53 - 1	9.08 - 1	7.22 - 1	5.34 - 1	3.68 - 1	2.30-1	1.17 - 1	2.57 - 2	-4.72 - 2	-1.04-
	δ	6.56-3	2.35-3	-1.20-3	-3.00-3	-4.20-3	-5.09-3	-5.82-3	-6.42-3	-6.94 - 3	-7.38-
$4p_{1/2}$	σ	2.455+1	2.048+1	1.348+1	9.192+0	6.563+0	4.870+0	3.728+0	2.926+0	2.345+0	1.912+0
$E_b =$	β	0.633	1.197	1.517	1.618	1.659	1.674	1.677	1.672	1.662	1.650
1168.2 eV	$_{\delta}^{\gamma}$	3.77-1	6.75-1	3.98-1	1.55-1	3.52-2	-4.04-4	1.69-2	6.77-2	1.39-1	2.23-1
		1.28-1	3.41-2	-4.39-3	-1.00-2	-1.06-2	-1.02-2	-9.31-3	-8.11-3	-6.54-3	-4.64-
$4p_{3/2}$	σ	9.883+1	6.763+1	3.613+1 1.509	2.190+1	1.443+1	1.007+1	7.344+0	5.534+0 1.763	4.282+0 1.767	3.386+0
$E_b = 967.2 \text{ eV}$	β	0.899 3.70-1	1.238 3.70-1	1.509 1.40-1	1.629 -6.49-3	1.694 -5.56-2	1.731 -3.92-2	1.752 1.94-2	1.763 1.05—1	2.06-1	1.766 3.17-1
307.2 EV	$\frac{\gamma}{\delta}$	6.54-2	1.97-2	7.38-5	1.73-3	-3.30-2 6.78-3	-3.92-2 1.18-2	1.62-2	1.99-2	2.31-2	2.57 - 2
4d _{3/2}	σ	1.452+2	9.488+1	4.403+1	2.325+1	1.354+1	8.476+0	5.603+0	3.866+0	2.761+0	2.029+0
$E_b =$	β	0.727	1.035	1.285	1.369	1.392	1.387	1.368	1.340	1.307	1.272
713.7 eV	γ	1.42 - 1	-7.49 - 4	-4.96-2	7.99 - 2	2.69 - 1	4.72 - 1	6.69 - 1	8.51 - 1	1.02+0	1.17+0
	δ	2.93-2	7.09-3	2.19-2	4.14-2	5.80-2	7.25-2	8.54-2	9.72-2	1.08-1	1.19-1
$4d_{5/2}$	σ	2.186+2	1.379+2	6.153+1	3.175+1	1.819+1	1.123+1	7.342+0	5.016+0	3.551+0	2.589+0
$E_b =$	β	0.993	1.213	1.356	1.375	1.354	1.318	1.275	1.229	1.183	1.138
676.6 eV	$\delta ^{\gamma }$	1.12-1 2.01-2	-3.01-2 7.33-3	-2.09-2 $1.99-2$	1.48-1 3.67-2	3.55-1 5.34-2	5.62 - 1 $6.99 - 2$	7.52-1 8.61-2	9.24-1 1.02-1	1.08+0 1.17-1	1.21+0 1.32-1
$4f_{5/2}$	σ	2.337+2	1.010+2	2.787+1	1.041+1	4.667+0	2.366+0	1.312+0	7.791-1	4.884-1	3.199-
$E_b =$	β	0.956	1.034	1.047	1.000	0.936	0.870	0.807	0.748	0.695	0.646
344.4 eV	γ	6.66 - 2	1.99 - 1	4.71 - 1	7.10 - 1	9.06 - 1	1.06+0	1.19+0	1.29+0	1.38+0	1.45+0
	δ	5.94-2	8.41-2	1.26-1	1.63-1	1.98-1	2.30-1	2.61-1	2.90-1	3.18-1	3.45-1
$4f_{7/2}$	σ	2.962+2	1.273+2	3.480+1	1.291+1	5.754+0	2.901+0	1.601+0	9.461-1	5.905-1	3.852-
$E_b =$	β	0.976	1.040	1.038	0.984	0.918	0.852	0.791	0.735	0.685	0.640
335.0 eV	$\gamma \\ \delta$	7.65-2 6.04-2	2.16-1 $8.46-2$	4.96-1	7.37-1 1.64-1	9.31-1 2.00-1	1.08+0 2.33_1	1.21+0 2.65—1	1.31+0 2.95-1	1.39+0 3.25-1	1.46+0 3.53_1
F.o.		6.04-2		1.25-1	1.64-1	2.00-1	2.33-1	2.65-1			3.53-1
5s _{1/2}	σ_{β}	8.778+0 1.681	5.685+0 1.716	2.998+0	1.871+0 1.773	1.284+0	9.372-1 1.700	7.139-1	5.614-1	4.526-1	3.722- 1.835
$E_b = 290.2 \text{ eV}$	β	1.681 6.36-1	1.716 5.97-1	1.752 4.70-1	1.773 3.36-1	1.788 2.15-1	1.799 1.11-1	1.810 2.47-2	1.819 -4.56-2	1.827 -1.01-1	1.835 1.43-
2JU.2 CV	$\frac{\gamma}{\delta}$	4.16-4	-8.28-4	-2.53-3	-3.70-3	-4.60-3	-5.35-3	-5.97-3	-4.30-2 -6.51-3	-6.97 - 3	-1.43- -7.37-
5p _{1/2}	σ	8.281+0	5.835+0	3.362+0	2.181+0	1.521+0	1.114+0	8.455-1	6.599-1	5.266-1	4.280-
$E_b =$	β	1.391	1.539	1.656	1.696	1.708	1.707	1.700	1.689	1.674	1.658
232.0 eV	γ	5.53-1	4.28-1	1.86-1	4.95-2	-2.11-3	2.37-3	4.35-2	1.08-1	1.88-1	2.76-1
	δ	-5.26-3	-1.11-2	-1.25-2	-1.18-2	-1.11-2	-1.05-2	-9.66-3	-8.56-3	-7.09-3	-5.28-
$5p_{3/2}$	σ	2.591+1	1.644+1	8.252+0	4.887+0	3.186+0	2.212+0	1.607+0	1.209+0	9.337 - 1	7.375

$ble 1 (continut)$ $E_b = $	β	1.343	1.480	1.625	1.699	1.740	1.764	1.776	1.781	1.780	1.776
180.8 eV	γ	3.05 - 1	2.04 - 1	3.62-2	-4.17-2	-4.89-2	-8.33 - 3	6.41-2	1.57 - 1	2.62 - 1	3.74 - 1
	δ	1.83-3	-3.86-3	-2.72-3	2.49-3	7.72-3	1.23-2	1.61-2	1.93-2	2.20-2	2.44-2
$d_{3/2}$	σ	2.707+1	1.668+1	7.521+0	3.973+0	2.327+0	1.465+0	9.735 - 1	6.746 - 1	4.837 - 1	3.566-
$E_b =$	β	1.111	1.262	1.389	1.427	1.427	1.410	1.382	1.349	1.312	1.275
94.1 eV	$\gamma \\ \delta$	3.78-2 $-1.79-3$	-3.42-2 $4.86-3$	3.75-3 2.41-2	1.54-1 4.11-2	3.43-1 5.59-2	5.40-1 6.92-2	7.28-1 8.14-2	9.03-1 9.28-2	1.06+0 1.04-1	1.21+0 1.15-1
. d		3.927+1	2.359+1	1.031+1	5.334+0	3.075+0	1.911+0	1.256+0	8.621-1	6.127-1	4.481-
$5d_{5/2}$ $E_b =$	$\frac{\sigma}{eta}$	1.299	1.383	1.423	1.405	3.075+0 1.367	1.322	1.256+0	1.225	6.127 — 1 1.177	1.131
87.3 eV	γ	5.63-3	-4.31-2	4.30-2	2.22-1	4.23-1	6.19-1	8.00-1	9.63-1	1.11+0	1.24+0
	δ	5.24 - 4	6.04 - 3	2.11-2	3.66-2	5.23-2	6.83-2	8.40-2	9.95 - 2	1.15 - 1	1.30-1
6s _{1/2}	σ	1.868+0	1.186+0	6.126-1	3.783-1	2.581-1	1.877-1	1.426-1	1.120-1	9.012-2	7.404-
$E_b =$	β	1.699	1.727	1.758	1.777	1.791	1.803	1.813	1.821	1.830	1.837
41.4 eV	γ	5.83-1	5.46-1	4.27-1	3.01-1	1.87-1	8.91-2	7.51-3	-5.86-2	-1.10-1	-1.49
	δ	-1.36-4	-1.20-3	-2.72-3	-3.82-3	-4.67-3	-5.38-3	-5.97-3	-6.50-3	-6.95-3	-7.35-
$6p_{1/2}$	σ	1.507+0	1.038+0	5.844-1	3.752-1	2.602-1	1.900-1	1.439-1	1.122-1	8.946-2	7.267-
$E_b = 25.8 \text{ eV}$	β	1.460 5.05-1	1.580 3.79-1	1.677 1.56-1	1.708 3.59-2	1.716 -5.40-3	1.713 5.33-3	1.704 5.00-2	1.692 1.16-1	1.677 1.97—1	1.660 2.86-1
23.6 EV	$_{\delta}^{\gamma}$	-1.09-2	-1.34-2	-1.29-2	-1.18-2	-3.40-3 -1.11-2	-1.05-2	-9.71-3	-8.62 - 3	-7.18 - 3	-5.35
Cn.									1.945-1		
$6p_{3/2}$ $E_b =$	$\frac{\sigma}{eta}$	4.320+0 1.391	2.708+0 1.512	1.344+0 1.642	7.914—1 1.710	5.144-1 1.748	3.566-1 1.770	2.588-1 1.781	1.945 – 1 1.784	1.502-1 1.783	1.186- 1.778
17.3 eV	γ	2.78-1	1.79-1	2.31-2	-4.50-2	-4.60-2	-1.90-3	7.21–2	1.66-1	2.71-1	3.83-1
	δ	-2.22-3	-5.42 - 3	-2.76 - 3	2.68-3	7.86-3	1.23-2	1.60-2	1.91-2	2.17-2	2.41-2
$6d_{3/2}$	σ	2.074+0	1.270+0	5.703-1	3.009-1	1.761-1	1.109-1	7.368-2	5.108-2	3.664-2	2.702-
$E_b =$	β	1.143	1.283	1.400	1.434	1.432	1.413	1.384	1.351	1.315	1.277
6.0 eV	γ	3.18-2	-3.44-2	1.04-2	1.64-1	3.51-1	5.44-1	7.30-1	9.05-1	1.07+0	1.22+0
	δ	-2.92 - 3	4.81-3	2.42-2	4.11-2	5.53-2	6.80-2	8.02-2	9.20-2	1.04-1	1.15-1
$7s_{1/2}$	σ	2.013-1	1.273-1	6.542-2	4.029-2	2.745-2	1.994-2	1.514-2	1.188-2	9.555-3	7.846-
$E_b =$	β	1.700	1.728	1.759	1.777	1.790	1.801	1.811	1.821	1.830	1.838
6.0 eV	$\frac{\gamma}{\delta}$	5.80-1 $-1.89-4$	5.42-1 -1.23-3	4.24-1 -2.75-3	2.99-1 -3.85-3	1.86-1 -4.72-3	8.70-2 -5.43-3	4.97 - 3 $-6.02 - 3$	-6.09-2 $-6.54-3$	-1.12-1 $-6.95-3$	1.50- 7.35-
7 04 5 7=			1,25-5	2.13-3	J.UJ-J	1,12-3	J. 1 J-J	5.02-5	3,34-3	5.55-5	1.55
Z= 91, Pa: [R	nj5t _{5/2} (
		k (eV)									
Shell		1500	2000	3000	4000	5000	6000	7000	8000	9000	10000
4s _{1/2}	σ	2.496+1	1.875+1	1.109+1	7.257+0	5.108+0	3.786+0	2.914+0	2.311+0	1.875+0	1.550+0
$E_b =$	β	1.495	1.606	1.691	1.727	1.751	1.768	1.783	1.795	1.805	1.814
1387.1 eV	γ	9.65-1	9.41-1	7.64-1	5.76-1	4.08-1	2.66-1	1.48-1	5.31-2	-2.34-2	-8.40-
	δ	8.22-3	3.04-3	-9.80-4	-3.00-3	-4.33-3	-5.32-3	-6.09-3	-6.72-3	-7.27-3	-7.75-
$4p_{1/2}$	σ	2.368+1	2.013+1 1.133	1.350+1 1.492	9.295+0	6.677+0	4.976+0	3.822+0 1.676	3.009+0 1.673	2.418+0	1.976+0
$E_b = 1224.3 \text{ eV}$	β γ	0.472 2.54-1	6.95—1	1.492 4.45—1	1.604 1.87-1	1.651 5.13-2	1.671 3.45-3	1.076	5.36–2	1.665 1.18-1	1.654 1.97—1
1224.5 CV	δ	1.57-1	4.24-2	-3.70-3	-1.06-2	-1.14-2	-1.09-2	-9.99-3	-8.79 - 3	-7.29 - 3	-5.45-
$4p_{3/2}$	σ	1.005+2	6.913+1	3.713+1	2.258+1	1.491+1	1.043+1	7.613+0	5.745+0	4.451+0	3.524+0
$E_b =$	β	0.824	1.199	1.484	1.612	1.682	1.724	1.748	1.761	1.767	1.767
1006.7 eV	γ	3.52-1	3.85-1	1.61-1	4.90-3	-5.41-2	-4.60-2	5.19-3	8.40-2	1.80-1	2.88-1
	δ	7.50-2	2.35 - 2	3.10-4	1.21-3	6.25 - 3	1.15-2	1.60-2	1.99-2	2.32-2	2.60-2
4d _{3/2}	σ	1.480+2	9.765+1	4.580+1	2.434+1	1.423+1	8.939+0	5.927+0	4.100+0	2.935+0	2.161+0
$E_b =$	β	0.677	1.003	1.269	1.362	1.391	1.390	1.374	1.348	1.318	1.284
743.4 eV	γ	1.57-1	1.26-2	-5.62-2	6.14-2	2.42-1	4.40-1	6.35-1	8.20-1	9.90-1	1.15+0
	δ	3.62-2	7.70-3	2.06-2	4.04-2	5.68-2	7.11-2	8.41-2	9.63-2	1.08-1	1.18-1
$4d_{5/2}$	σ	2.240+2	1.425+2	6.418+1	3.329+1	1.914+1	1.185+1	7.768+0	5.319+0	3.773+0	2.755+0
$E_b = 7.08.3 \text{ eV}$	β	0.959	1.195	1.351	1.376	1.359	1.325	1.284	1.240	1.195	1.150
708.2 eV	γ	1.33-1 2.47-2	-1.98-2 7.57-3	-3.12-2 $1.89-2$	1.29-1 3.55-2	3.31-1 5.16-2	5.33-1 6.75-2	7.25-1 8.36-2	8.99-1 9.97-2	1.06+0 1.15-1	1.19+0 1.31-1
	λ			1.03-2		5.152+0					
A.F.	δ			2 0E1 · 1		つ コンノナロ	2.620+0	1.457+0	8.667 - 1	5.441 - 1	3.568-
$4f_{5/2}$	σ	2.531+2	1.099+2	3.051+1 1.050	1.145+1 1.005			0.818	() 759	0.704	() 654
$E_b =$	$\frac{\sigma}{\beta}$	2.531+2 0.942		3.051+1 1.050 4.54-1	1.145+1 1.005 6.92-1	0.945 8.90-1	0.881	0.818 1.18+0	0.759 1.29+0	0.704 1.37+0	0.654 1.45+0
$E_b =$	σ	2.531+2	1.099+2 1.028	1.050	1.005	0.945					1.45+0
E _b = 371.2 eV	σ β γ δ	2.531+2 0.942 5.16-2 5.67-2	1.099+2 1.028 1.82-1 8.22-2	1.050 4.54-1 1.24-1	1.005 6.92-1 1.60-1	0.945 8.90-1 1.95-1	0.881 1.05+0 2.28-1	1.18+0 2.59-1	1.29+0 2.88-1	1.37+0 3.15-1	1.45+0 3.41-1
$4f_{5/2}$ $E_b = 371.2 \text{ eV}$ $4f_{7/2}$ $E_b = 6$	σ β γ	2.531+2 0.942 5.16-2	1.099+2 1.028 1.82-1	1.050 4.54-1	1.005 6.92-1	0.945 8.90-1	0.881 1.05+0	1.18+0	1.29+0	1.37+0	1.45+0 3.41-1
$E_b = 371.2 \text{ eV}$ $4f_{7/2}$ $E_b = $	σ β γ δ σ β γ	2.531+2 0.942 5.16-2 5.67-2 3.197+2 0.964 6.14-2	1.099+2 1.028 1.82-1 8.22-2 1.380+2 1.036 2.00-1	1.050 4.54-1 1.24-1 3.798+1 1.041 4.80-1	1.005 6.92-1 1.60-1 1.416+1 0.989 7.19-1	0.945 8.90-1 1.95-1 6.332+0 0.926 9.16-1	0.881 1.05+0 2.28-1 3.203+0 0.863 1.08+0	1.18+0 2.59-1 1.772+0 0.802 1.20+0	1.29+0 2.88-1 1.049+0 0.746 1.31+0	1.37+0 3.15-1 6.558-1 0.694 1.39+0	1.45+0 3.41-1 4.283- 0.647
$E_b = 371.2 \text{ eV}$ $4f_{7/2}$ $E_b = $	σ β γ δ	2.531+2 0.942 5.16-2 5.67-2 3.197+2 0.964	1.099+2 1.028 1.82-1 8.22-2 1.380+2 1.036	1.050 4.54-1 1.24-1 3.798+1 1.041	1.005 6.92-1 1.60-1 1.416+1 0.989	0.945 8.90-1 1.95-1 6.332+0 0.926	0.881 1.05+0 2.28-1 3.203+0 0.863	1.18+0 2.59-1 1.772+0 0.802	1.29+0 2.88-1 1.049+0 0.746	1.37+0 3.15-1 6.558-1 0.694	1.45+0 3.41-1 4.283- 0.647 1.46+0
$E_b = 371.2 \text{ eV}$ $4f_{7/2}$ $E_b = 359.5 \text{ eV}$	σ β γ δ σ β γ	2.531+2 0.942 5.16-2 5.67-2 3.197+2 0.964 6.14-2	1.099+2 1.028 1.82-1 8.22-2 1.380+2 1.036 2.00-1	1.050 4.54-1 1.24-1 3.798+1 1.041 4.80-1	1.005 6.92-1 1.60-1 1.416+1 0.989 7.19-1	0.945 8.90-1 1.95-1 6.332+0 0.926 9.16-1 1.96-1	0.881 1.05+0 2.28-1 3.203+0 0.863 1.08+0	1.18+0 2.59-1 1.772+0 0.802 1.20+0 2.63-1 7.394-1	1.29+0 2.88-1 1.049+0 0.746 1.31+0	1.37+0 3.15-1 6.558-1 0.694 1.39+0	1.45+0 3.41-1 4.283- 0.647 1.46+0 3.48-1
$E_b = 371.2 \text{ eV}$ $4f_{7/2}$ $E_b = 359.5 \text{ eV}$ $5s_{1/2}$ $E_b = 6$	σ β γ δ σ β γ δ σ δ δ δ δ δ	2.531+2 0.942 5.16-2 5.67-2 3.197+2 0.964 6.14-2 5.80-2 9.016+0 1.655	1.099+2 1.028 1.82-1 8.22-2 1.380+2 1.036 2.00-1 8.28-2 5.850+0 1.693	1.050 4.54-1 1.24-1 3.798+1 1.041 4.80-1 1.24-1 3.091+0 1.732	1.005 6.92-1 1.60-1 1.416+1 0.989 7.19-1 1.60-1 1.932+0 1.755	0.945 8.90-1 1.95-1 6.332+0 0.926 9.16-1 1.96-1 1.327+0 1.772	0.881 1.05+0 2.28-1 3.203+0 0.863 1.08+0 2.30-1 9.697-1 1.786	1.18+0 2.59-1 1.772+0 0.802 1.20+0 2.63-1 7.394-1 1.797	1.29+0 2.88-1 1.049+0 0.746 1.31+0 2.93-1 5.821-1 1.807	1.37+0 3.15-1 6.558-1 0.694 1.39+0 3.21-1 4.698-1 1.816	1.45+0 3.41-1 4.283- 0.647 1.46+0 3.48-1 3.867- 1.823
$E_b = 371.2 \text{ eV}$ $4f_{7/2}$	σ β γ δ σ β γ δ	2.531+2 0.942 5.16-2 5.67-2 3.197+2 0.964 6.14-2 5.80-2 9.016+0 1.655 6.56-1	1.099+2 1.028 1.82-1 8.22-2 1.380+2 1.036 2.00-1 8.28-2 5.850+0 1.693 6.23-1	1.050 4.54-1 1.24-1 3.798+1 1.041 4.80-1 1.24-1 3.091+0 1.732 5.00-1	1.005 6.92-1 1.60-1 1.416+1 0.989 7.19-1 1.60-1 1.932+0 1.755 3.67-1	0.945 8.90-1 1.95-1 6.332+0 0.926 9.16-1 1.96-1 1.327+0 1.772 2.43-1	0.881 1.05+0 2.28-1 3.203+0 0.863 1.08+0 2.30-1 9.697-1 1.786 1.37-1	1.18+0 2.59-1 1.772+0 0.802 1.20+0 2.63-1 7.394-1 1.797 4.79-2	1.29+0 2.88-1 1.049+0 0.746 1.31+0 2.93-1 5.821-1 1.807 -2.51-2	1.37+0 3.15-1 6.558-1 0.694 1.39+0 3.21-1 4.698-1 1.816 -8.36-2	1.45+0 3.41-1 4.283- 0.647 1.46+0 3.48-1 3.867- 1.823 -1.29-
$E_b = 371.2 \text{ eV}$ $4f_{7/2}$ $E_b = 359.5 \text{ eV}$ $55s_{1/2}$ $E_b = 309.6 \text{ eV}$	σ β γ δ σ β γ δ σ β γ δ	2.531+2 0.942 5.16-2 5.67-2 3.197+2 0.964 6.14-2 5.80-2 9.016+0 1.655 6.56-1 6.53-4	1.099+2 1.028 1.82-1 8.22-2 1.380+2 1.036 2.00-1 8.28-2 5.850+0 1.693 6.23-1 -6.93-4	1.050 4.54-1 1.24-1 3.798+1 1.041 4.80-1 1.24-1 3.091+0 1.732 5.00-1 -2.56-3	1.005 6.92-1 1.60-1 1.416+1 0.989 7.19-1 1.60-1 1.932+0 1.755 3.67-1 -3.85-3	0.945 8.90-1 1.95-1 6.332+0 0.926 9.16-1 1.96-1 1.327+0 1.772 2.43-1 -4.82-3	0.881 1.05+0 2.28-1 3.203+0 0.863 1.08+0 2.30-1 9.697-1 1.786 1.37-1 -5.61-3	1.18+0 2.59-1 1.772+0 0.802 1.20+0 2.63-1 7.394-1 1.797 4.79-2 -6.26-3	1.29+0 2.88-1 1.049+0 0.746 1.31+0 2.93-1 5.821-1 1.807 -2.51-2 -6.83-3	1.37+0 3.15-1 6.558-1 0.694 1.39+0 3.21-1 4.698-1 1.816 -8.36-2 -7.32-3	1.45+0 3.41-1 4.283- 0.647 1.46+0 3.48-1 3.867- 1.823 -1.29- -7.76-
$E_b = 371.2 \text{ eV}$ $4f_{7/2}$ $E_b = 359.5 \text{ eV}$ $55s_{1/2}$ $E_b = 309.6 \text{ eV}$	σ β γ δ σ β γ δ δ σ β γ δ	2.531+2 0.942 5.16-2 5.67-2 3.197+2 0.964 6.14-2 5.80-2 9.016+0 1.655 6.56-1 6.53-4 8.382+0	1.099+2 1.028 1.82-1 8.22-2 1.380+2 1.036 2.00-1 8.28-2 5.850+0 1.693 6.23-1 -6.93-4 5.938+0	1.050 4.54-1 1.24-1 3.798+1 1.041 4.80-1 1.24-1 3.091+0 1.732 5.00-1 -2.56-3 3.446+0	1.005 6.92-1 1.60-1 1.416+1 0.989 7.19-1 1.60-1 1.932+0 1.755 3.67-1 -3.85-3 2.246+0	0.945 8.90-1 1.95-1 6.332+0 0.926 9.16-1 1.96-1 1.327+0 1.772 2.43-1 -4.82-3 1.572+0	0.881 1.05+0 2.28-1 3.203+0 0.863 1.08+0 2.30-1 9.697-1 1.786 1.37-1 -5.61-3 1.155+0	1.18+0 2.59-1 1.772+0 0.802 1.20+0 2.63-1 7.394-1 1.797 4.79-2 -6.26-3 8.796-1	1.29+0 2.88-1 1.049+0 0.746 1.31+0 2.93-1 5.821-1 1.807 -2.51-2 -6.83-3 6.883-1	1.37+0 3.15-1 6.558-1 0.694 1.39+0 3.21-1 4.698-1 1.816 -8.36-2 -7.32-3 5.506-1	1.45+0 3.41-1 4.283- 0.647 1.46+0 3.48-1 3.867- 1.823 -1.29- -7.76- 4.485-
$E_b = 371.2 \text{ eV}$ $4f_{7/2} = E_b = 359.5 \text{ eV}$ $55s_{1/2} = 309.6 \text{ eV}$	σ β γ δ σ β γ δ δ σ β γ δ	2.531+2 0.942 5.16-2 5.67-2 3.197+2 0.964 6.14-2 5.80-2 9.016+0 1.655 6.56-1 6.53-4 8.382+0 1.360	1.099+2 1.028 1.82-1 8.22-2 1.380+2 1.036 2.00-1 8.28-2 5.850+0 1.693 6.23-1 -6.93-4 5.938+0 1.517	1.050 4.54-1 1.24-1 3.798+1 1.041 4.80-1 1.24-1 3.091+0 1.732 5.00-1 -2.56-3 3.446+0 1.645	1.005 6.92-1 1.60-1 1.416+1 0.989 7.19-1 1.60-1 1.932+0 1.755 3.67-1 -3.85-3 2.246+0 1.690	0.945 8.90-1 1.95-1 6.332+0 0.926 9.16-1 1.96-1 1.327+0 1.772 2.43-1 -4.82-3 1.572+0 1.706	0.881 1.05+0 2.28-1 3.203+0 0.863 1.08+0 2.30-1 9.697-1 1.786 1.37-1 -5.61-3 1.155+0 1.707	1.18+0 2.59-1 1.772+0 0.802 1.20+0 2.63-1 7.394-1 1.797 4.79-2 -6.26-3 8.796-1 1.702	1.29+0 2.88-1 1.049+0 0.746 1.31+0 2.93-1 5.821-1 1.807 -2.51-2 -6.83-3 6.883-1 1.692	1.37+0 3.15-1 6.558-1 0.694 1.39+0 3.21-1 4.698-1 1.816 -8.36-2 -7.32-3 5.506-1 1.679	1.45+0 3.41-1 4.283- 0.647 1.46+0 3.48-1 3.867- 1.823 -1.29- -7.76- 4.485- 1.664
$E_b = 871.2 \text{ eV}$ $A_{7/2} = E_b = 859.5 \text{ eV}$ $E_b = 809.6 \text{ eV}$	σ β γ δ σ β γ δ δ σ β γ δ	2.531+2 0.942 5.16-2 5.67-2 3.197+2 0.964 6.14-2 5.80-2 9.016+0 1.655 6.56-1 6.53-4 8.382+0	1.099+2 1.028 1.82-1 8.22-2 1.380+2 1.036 2.00-1 8.28-2 5.850+0 1.693 6.23-1 -6.93-4 5.938+0	1.050 4.54-1 1.24-1 3.798+1 1.041 4.80-1 1.24-1 3.091+0 1.732 5.00-1 -2.56-3 3.446+0	1.005 6.92-1 1.60-1 1.416+1 0.989 7.19-1 1.60-1 1.932+0 1.755 3.67-1 -3.85-3 2.246+0	0.945 8.90-1 1.95-1 6.332+0 0.926 9.16-1 1.96-1 1.327+0 1.772 2.43-1 -4.82-3 1.572+0	0.881 1.05+0 2.28-1 3.203+0 0.863 1.08+0 2.30-1 9.697-1 1.786 1.37-1 -5.61-3 1.155+0	1.18+0 2.59-1 1.772+0 0.802 1.20+0 2.63-1 7.394-1 1.797 4.79-2 -6.26-3 8.796-1	1.29+0 2.88-1 1.049+0 0.746 1.31+0 2.93-1 5.821-1 1.807 -2.51-2 -6.83-3 6.883-1	1.37+0 3.15-1 6.558-1 0.694 1.39+0 3.21-1 4.698-1 1.816 -8.36-2 -7.32-3 5.506-1	1.45+0 3.41- 4.283- 0.647 1.46+0 3.48- 3.867- 1.823 -1.29- -7.76- 4.485-

	δ	-5.12-3	-1.17-2	-1.35-2	-1.26-2	-1.18-2	-1.11-2	-1.02-2	-9.16-3	-7.77-3	-6.04-3
$5p_{3/2}$	σ	2.700+1	1.715+1	8.627+0	5.118+0	3.341+0	2.324+0	1.691+0	1.273+0	9.848-1	7.788-1
$E_b = 186.3 \text{ eV}$	β γ	1.318 3.15-1	1.458 2.18-1	1.609 4.69-2	1.688 -3.76-2	1.733 -5.15-2	1.759 -1.73-2	1.774 4.88-2	1.781 1.36-1	1.782 2.37-1	1.779 3.47-1
100.5 € 1	δ	2.56-3	-3.82 - 3	-3.26 - 3	1.94-3	7.36-3	1.21-2	1.61-2	1.94-2	2.23-2	2.48-2
5d _{3/2}	σ	2.814+1	1.742+1	7.911+0	4.200+0	2.469+0	1.560+0	1.040+0	7.226-1	5.192-1	3.836-1
$E_b = 97.3 \text{ eV}$	β γ	1.089 4.84-2	1.245 -3.04-2	1.382 -4.96-3	1.425 1.37-1	1.430 3.19-1	1.415 5.11-1	1.390 6.99-1	1.359 8.76-1	1.324 1.04+0	1.288 1.19+0
	δ	-1.94-3	3.98-3	2.31-2	4.02-2	5.47-2	6.79-2	8.03-2	9.20-2	1.03-1	1.14-1
5d _{5/2}	σ	4.127+1 1.291	2.489+1 1.379	1.094+1 1.424	5.687+0 1.409	3.291+0 1.374	2.052+0 1.330	1.352+0 1.284	9.303-1 1.237	6.625-1 1.189	4.854-1 1.143
$E_b = 89.2 \text{ eV}$	β γ	1.291	-4.24-2	3.31-2	2.06-1	4.01-1	5.95–1	7.77—1	9.43-1	1.189	1.143
	δ	3.15-4	5.39-3	2.03-2	3.54-2	5.05-2	6.60-2	8.19-2	9.77-2	1.13-1	1.28-1
5f _{5/2}	σ	1.559+1	7.137+0	2.112+0	8.240-1	3.802-1	1.967-1	1.107-1	6.640-2	4.196-2	2.765-2
$E_b = 6.0 \text{ eV}$	β γ	1.075 1.06-1	1.104 2.36-1	1.074 4.90-1	1.012 7.12-1	0.945 9.00-1	0.879 1.06+0	0.815 1.19+0	0.756 1.29+0	0.701 1.38+0	0.650 1.45+0
	δ	5.47-2	7.79-2	1.18-1	1.55-1	1.90-1	2.24-1	2.55-1	2.85-1	3.13-1	3.39-1
6s _{1/2}	σ	1.894+0	1.204+0	6.225-1	3.847-1	2.627-1	1.912-1	1.454-1	1.143-1	9.207-2	7.569-2
$E_b = 46.7 \text{ eV}$	β γ	1.675 6.02-1	1.706 5.69-1	1.740 4.54-1	1.761 3.28-1	1.776 2.13-1	1.789 1.12-1	1.800 2.85-2	1.810 $-4.01-2$	1.818 -9.48-2	1.826 1.371
	δ	1.61-5	-1.13-3	-2.79-3	-3.99-3	-4.91-3	-5.66-3	-6.28-3	-6.83-3	-7.31-3	-7.73-3
6p _{1/2}	σ	1.529+0 1.433	1.056+0 1.562	5.982-1 1.668	3.857-1 1.704	2.684-1 1.715	1.966-1 1.714	1.493-1 1.706	1.167-1 1.695	9.323-2 1.681	7.589-2 1.665
$E_b = 28.1 \text{ eV}$	β γ	5.31–1	4.07-1	1.79-1	4.85-2	-1.57-3	1.714	4.00-2	1.095	1.76-1	2.60-1
	δ	-1.15-2	-1.43-2	-1.39-2	-1.27-2	-1.18-2	-1.11-2	-1.03-2	-9.27 - 3	-7.90-3	-6.17-3
$6p_{3/2}$	σ	4.275+0	2.682+0	1.332+0	7.859-1	5.116-1	3.551-1	2.581-1	1.941-1	1.501-1	1.186-1
$E_b = 18.9 \text{ eV}$	β γ	1.368 2.89-1	1.491 1.92-1	1.628 3.30-2	1.699 -4.19-2	1.741 -4.95-2	1.765 -1.13-2	1.779 5.72-2	1.784 1.45-1	1.784 2.46-1	1.781 3.55-1
10.0 0 1	δ	-1.88 - 3	-5.62-3	-3.35 - 3	2.15-3	7.54-3	1.22-2	1.60-2	1.92-2	2.20-2	2.44-2
6d _{3/2}	σ	1.928+0	1.186+0	5.362-1	2.844-1	1.672-1	1.056-1	7.037-2	4.890-2	3.514-2	2.596-2
$E_b = 6.0 \text{ eV}$	β γ	1.127 4.20-2	1.272 -3.08-2	1.396 7.08-4	1.433 1.46-1	1.435 3.30-1	1.418 5.22-1	1.392 7.06-1	1.360 8.79-1	1.326 1.04+0	1.290 1.19+0
0.0 0.	δ	-3.29-3	3.87-3	2.31-2	4.02-2	5.48-2	6.76-2	7.92-2	9.03-2	1.01-1	1.12-1
$7s_{1/2}$	σ	1.777-1	1.125-1	5.791-2	3.570-2	2.435-2	1.771-2	1.347-2	1.058-2	8.517-3	7.000-3
$E_b = 6.0 \text{ eV}$	β γ	1.677 5.97-1	1.707 5.64-1	1.741 4.49-1	1.762 3.24-1	1.777 2.10-1	1.789 1.10-1	1.799 2.65-2	1.808 -4.27-2	1.816 -9.78-2	1.825 1.40 1
	δ	-5.43 - 5	-1.18 - 3	-2.82 - 3	-4.00 - 3	-4.91 - 3	-5.67 - 3	-6.32 - 3	-6.91 - 3	-7.38 - 3	-7.82 - 3
											7.02
Z= 92, U : [Ri	n]5f ³ _{5/2} 6	6d _{3/2} 7s _{1/2}									7.02
	n]5f ³ _{5/2} 6	k (eV)									
Shell	·	k (eV) 1500	2000	3000	4000	5000	6000	7000	8000	9000	10000
Shell 4s _{1/2}	σ	k (eV) 1500 2.438+1	2000 1.869+1	1.115+1	4000 7.335+0	5.179+0	6000 3.847+0	7000 2.967+0	2.356+0	9000	10000 1.584+0
Shell	·	k (eV) 1500	2000 1.869+1 1.572 9.65-1		4000 7.335+0 1.707 6.15-1	5.179+0 1.732 4.47-1	6000	7000		9000	10000
Shell $4s_{1/2}$ $E_b = 1440.8 \text{ eV}$	$\frac{\sigma}{\beta}$	k (eV) 1500 2.438+1 1.444 9.57-1 1.05-2	2000 1.869+1 1.572 9.65-1 3.73-3	1.115+1 1.666 8.01-1 -7.35-4	4000 7.335+0 1.707 6.15-1 -2.97-3	5.179+0 1.732 4.47-1 -4.45-3	6000 3.847+0 1.751 3.02-1 -5.53-3	7000 2.967+0 1.767 1.81-1 -6.38-3	2.356+0 1.780 8.15-2 -7.06-3	9000 1.914+0 1.791 1.09-3 -7.64-3	10000 1.584+0 1.801 -6.33-2 -8.16-3
Shell $4s_{1/2}$ $E_b = 1440.8 \text{ eV}$	σ β γ δ	k (eV) 1500 2.438+1 1.444 9.57-1 1.05-2 2.287+1	2000 1.869+1 1.572 9.65-1 3.73-3 1.976+1	1.115+1 1.666 8.01-1 -7.35-4 1.348+1	4000 7.335+0 1.707 6.15-1 -2.97-3 9.367+0	5.179+0 1.732 4.47-1 -4.45-3 6.771+0	6000 3.847+0 1.751 3.02-1 -5.53-3 5.070+0	7000 2.967+0 1.767 1.81-1 -6.38-3 3.909+0	2.356+0 1.780 8.15-2 -7.06-3 3.087+0	9000 1.914+0 1.791 1.09-3 -7.64-3 2.486+0	10000 1.584+0 1.801 -6.33-2 -8.16-3 2.037+0
Shell $4s_{1/2}$ $E_b = 1440.8 \text{ eV}$	σ β γ δ	k (eV) 1500 2.438+1 1.444 9.57-1 1.05-2	2000 1.869+1 1.572 9.65-1 3.73-3	1.115+1 1.666 8.01-1 -7.35-4	4000 7.335+0 1.707 6.15-1 -2.97-3	5.179+0 1.732 4.47-1 -4.45-3	6000 3.847+0 1.751 3.02-1 -5.53-3	7000 2.967+0 1.767 1.81-1 -6.38-3	2.356+0 1.780 8.15-2 -7.06-3	9000 1.914+0 1.791 1.09-3 -7.64-3	10000 1.584+0 1.801 -6.33-2 -8.16-3
Shell $4s_{1/2}$ $E_b = 1440.8 \text{ eV}$ $4p_{1/2}$ $E_b = 1490.8 \text{ eV}$	σ β γ δ	k (eV) 1500 2.438+1 1.444 9.57-1 1.05-2 2.287+1 0.332 1.26-1 1.84-1	2000 1.869+1 1.572 9.65-1 3.73-3 1.976+1 1.075 7.04-1 5.04-2	1.115+1 1.666 8.01-1 -7.35-4 1.348+1 1.469 4.88-1 -3.05-3	4000 7.335+0 1.707 6.15-1 -2.97-3 9.367+0 1.592 2.19-1 -1.11-2	5.179+0 1.732 4.47-1 -4.45-3 6.771+0 1.644 6.89-2 -1.21-2	6000 3.847+0 1.751 3.02-1 -5.53-3 5.070+0 1.667 9.21-3 -1.16-2	7000 2.967+0 1.767 1.81-1 -6.38-3 3.909+0 1.675 7.44-3 -1.07-2	2.356+0 1.780 8.15-2 -7.06-3 3.087+0 1.674 4.23-2 -9.53-3	9000 1.914+0 1.791 1.09-3 -7.64-3 2.486+0 1.667 1.01-1 -8.07-3	10000 1.584+0 1.801 -6.33-2 -8.16-3 2.037+0 1.657 1.74-1 -6.31-3
Shell $4s_{1/2}$ $E_b = 1440.8 \text{ eV}$ $4p_{1/2}$ $E_b = 1271.8 \text{ eV}$ $4p_{3/2}$	σ β γ δ σ β γ δ σ δ σ δ σ σ	k (eV) 1500 2.438+1 1.444 9.57-1 1.05-2 2.287+1 0.332 1.26-1 1.84-1 1.021+2	2000 1.869+1 1.572 9.65-1 3.73-3 1.976+1 1.075 7.04-1 5.04-2 7.052+1	1.115+1 1.666 8.01-1 -7.35-4 1.348+1 1.469 4.88-1 -3.05-3 3.807+1	4000 7.335+0 1.707 6.15-1 -2.97-3 9.367+0 1.592 2.19-1 -1.11-2 2.323+1	5.179+0 1.732 4.47-1 -4.45-3 6.771+0 1.644 6.89-2 -1.21-2 1.538+1	6000 3.847+0 1.751 3.02-1 -5.53-3 5.070+0 1.667 9.21-3 -1.16-2 1.078+1	7000 2.967+0 1.767 1.81-1 -6.38-3 3.909+0 1.675 7.44-3 -1.07-2 7.882+0	2.356+0 1.780 8.15-2 -7.06-3 3.087+0 1.674 4.23-2 -9.53-3 5.956+0	9000 1.914+0 1.791 1.09-3 -7.64-3 2.486+0 1.667 1.01-1 -8.07-3 4.621+0	10000 1.584+0 1.801 -6.33-2 -8.16-3 2.037+0 1.657 1.74-1 -6.31-3 3.662+0
Shell $4s_{1/2}$ $E_b = 1440.8 \text{ eV}$ $4p_{1/2}$ $E_b = 1271.8 \text{ eV}$	σ β γ δ σ β γ δ σ δ δ	k (eV) 1500 2.438+1 1.444 9.57-1 1.05-2 2.287+1 0.332 1.26-1 1.84-1	2000 1.869+1 1.572 9.65-1 3.73-3 1.976+1 1.075 7.04-1 5.04-2	1.115+1 1.666 8.01-1 -7.35-4 1.348+1 1.469 4.88-1 -3.05-3	4000 7.335+0 1.707 6.15-1 -2.97-3 9.367+0 1.592 2.19-1 -1.11-2	5.179+0 1.732 4.47-1 -4.45-3 6.771+0 1.644 6.89-2 -1.21-2	6000 3.847+0 1.751 3.02-1 -5.53-3 5.070+0 1.667 9.21-3 -1.16-2	7000 2.967+0 1.767 1.81-1 -6.38-3 3.909+0 1.675 7.44-3 -1.07-2	2.356+0 1.780 8.15-2 -7.06-3 3.087+0 1.674 4.23-2 -9.53-3	9000 1.914+0 1.791 1.09-3 -7.64-3 2.486+0 1.667 1.01-1 -8.07-3	10000 1.584+0 1.801 -6.33-2 -8.16-3 2.037+0 1.657 1.74-1 -6.31-3
Shell $4s_{1/2}$ $E_b = 1440.8 \text{ eV}$ $4p_{1/2}$ $E_b = 1271.8 \text{ eV}$ $4p_{3/2}$ $E_b = 1280.8 \text{ eV}$	σ β γ δ σ β γ δ σ δ σ δ σ σ	k (eV) 1500 2.438+1 1.444 9.57-1 1.05-2 2.287+1 0.332 1.26-1 1.84-1 1.021+2 0.751	2000 1.869+1 1.572 9.65-1 3.73-3 1.976+1 1.075 7.04-1 5.04-2 7.052+1 1.159	1.115+1 1.666 8.01-1 -7.35-4 1.348+1 1.469 4.88-1 -3.05-3 3.807+1 1.460	4000 7.335+0 1.707 6.15-1 -2.97-3 9.367+0 1.592 2.19-1 -1.11-2 2.323+1 1.595	5.179+0 1.732 4.47-1 -4.45-3 6.771+0 1.644 6.89-2 -1.21-2 1.538+1 1.670	6000 3.847+0 1.751 3.02-1 -5.53-3 5.070+0 1.667 9.21-3 -1.16-2 1.078+1 1.715	7000 2.967+0 1.767 1.81-1 -6.38-3 3.909+0 1.675 7.44-3 -1.07-2 7.882+0 1.743	2.356+0 1.780 8.15-2 -7.06-3 3.087+0 1.674 4.23-2 -9.53-3 5.956+0 1.758	9000 1.914+0 1.791 1.09-3 -7.64-3 2.486+0 1.667 1.01-1 -8.07-3 4.621+0 1.766	10000 1.584+0 1.801 -6.33-2 -8.16-3 2.037+0 1.657 1.74-1 -6.31-3 3.662+0 1.768
Shell $4s_{1/2}$ $E_b = 1440.8 \text{ eV}$ $4p_{1/2}$ $E_b = 1271.8 \text{ eV}$ $4p_{3/2}$ $E_b = 1044.9 \text{ eV}$ $4d_{3/2}$	σ β γ δ σ β γ δ σ δ	k (eV) 1500 2.438+1 1.444 9.57-1 1.05-2 2.287+1 0.332 1.26-1 1.84-1 1.021+2 0.751 3.28-1 8.55-2 1.507+2	2000 1.869+1 1.572 9.65-1 3.73-3 1.976+1 1.075 7.04-1 5.04-2 7.052+1 1.159 3.97-1 2.74-2 1.005+2	1.115+1 1.666 8.01-1 -7.35-4 1.348+1 1.469 4.88-1 -3.05-3 3.807+1 1.460 1.80-1 6.25-4	4000 7.335+0 1.707 6.15-1 -2.97-3 9.367+0 1.592 2.19-1 -1.11-2 2.323+1 1.595 1.71-2 7.23-4 2.547+1	5.179+0 1.732 4.47-1 -4.45-3 6.771+0 1.644 6.89-2 -1.21-2 1.538+1 1.670 -5.12-2 5.71-3 1.496+1	6000 3.847+0 1.751 3.02-1 -5.53-3 5.070+0 1.667 9.21-3 -1.16-2 1.078+1 1.715 -5.13-2 1.11-2 9.426+0	7000 2.967+0 1.767 1.81-1 -6.38-3 3.909+0 1.675 7.44-3 -1.07-2 7.882+0 1.743 -7.09-3 1.59-2 6.266+0	2.356+0 1.780 8.15-2 -7.06-3 3.087+0 1.674 4.23-2 -9.53-3 5.956+0 1.758 6.57-2 1.99-2 4.345+0	9000 1.914+0 1.791 1.09-3 -7.64-3 2.486+0 1.667 1.01-1 -8.07-3 4.621+0 1.766 1.57-1 2.34-2 3.117+0	10000 1.584+0 1.801 -6.33-2 -8.16-3 2.037+0 1.657 1.74-1 -6.31-3 3.662+0 1.768 2.60-1 2.63-2 2.299+0
Shell $4s_{1/2}$ $E_b = 1440.8 \text{ eV}$ $4p_{1/2}$ $E_b = 1271.8 \text{ eV}$ $4p_{3/2}$ $E_b = 1044.9 \text{ eV}$ $4d_{3/2}$ $E_b = 1046.9 \text{ eV}$	σ β γ δ σ β γ δ σ δ σ δ σ δ	k (eV) 1500 2.438+1 1.444 9.57-1 1.05-2 2.287+1 0.332 1.26-1 1.84-1 1.021+2 0.751 3.28-1 8.55-2 1.507+2 0.621	2000 1.869+1 1.572 9.65-1 3.73-3 1.976+1 1.075 7.04-1 5.04-2 7.052+1 1.159 3.97-1 2.74-2 1.005+2 0.968	1.115+1 1.666 8.01-1 -7.35-4 1.348+1 1.469 4.88-1 -3.05-3 3.807+1 1.460 1.80-1 6.25-4 4.763+1 1.252	4000 7.335+0 1.707 6.15-1 -2.97-3 9.367+0 1.592 2.19-1 -1.11-2 2.323+1 1.595 1.71-2 7.23-4 2.547+1 1.354	5.179+0 1.732 4.47-1 -4.45-3 6.771+0 1.644 6.89-2 -1.21-2 1.538+1 1.670 -5.12-2 5.71-3 1.496+1 1.389	6000 3.847+0 1.751 3.02-1 -5.53-3 5.070+0 1.667 9.21-3 -1.16-2 1.078+1 1.715 -5.13-2 1.11-2 9.426+0 1.392	7000 2.967+0 1.767 1.81-1 -6.38-3 3.909+0 1.675 7.44-3 -1.07-2 7.882+0 1.743 -7.09-3 1.59-2 6.266+0 1.379	2.356+0 1.780 8.15-2 -7.06-3 3.087+0 1.674 4.23-2 -9.53-3 5.956+0 1.758 6.57-2 1.99-2 4.345+0 1.356	9000 1.914+0 1.791 1.09-3 -7.64-3 2.486+0 1.667 1.01-1 -8.07-3 4.621+0 1.766 1.57-1 2.34-2 3.117+0 1.327	10000 1.584+0 1.801 -6.33-2 -8.16-3 2.037+0 1.657 1.74-1 -6.31-3 3.662+0 1.768 2.60-1 2.63-2 2.299+0 1.296
Shell $4s_{1/2}$ $E_b = 1440.8 \text{ eV}$ $4p_{1/2}$ $E_b = 1271.8 \text{ eV}$ $4p_{3/2}$ $E_b = 1044.9 \text{ eV}$ $4d_{3/2}$ $E_b = 780.2 \text{ eV}$	σ β γ δ σ β γ δ σ δ	k (eV) 1500 2.438+1 1.444 9.57-1 1.05-2 2.287+1 0.332 1.26-1 1.84-1 1.021+2 0.751 3.28-1 8.55-2 1.507+2	2000 1.869+1 1.572 9.65-1 3.73-3 1.976+1 1.075 7.04-1 5.04-2 7.052+1 1.159 3.97-1 2.74-2 1.005+2	1.115+1 1.666 8.01-1 -7.35-4 1.348+1 1.469 4.88-1 -3.05-3 3.807+1 1.460 1.80-1 6.25-4	4000 7.335+0 1.707 6.15-1 -2.97-3 9.367+0 1.592 2.19-1 -1.11-2 2.323+1 1.595 1.71-2 7.23-4 2.547+1	5.179+0 1.732 4.47-1 -4.45-3 6.771+0 1.644 6.89-2 -1.21-2 1.538+1 1.670 -5.12-2 5.71-3 1.496+1	6000 3.847+0 1.751 3.02-1 -5.53-3 5.070+0 1.667 9.21-3 -1.16-2 1.078+1 1.715 -5.13-2 1.11-2 9.426+0	7000 2.967+0 1.767 1.81-1 -6.38-3 3.909+0 1.675 7.44-3 -1.07-2 7.882+0 1.743 -7.09-3 1.59-2 6.266+0	2.356+0 1.780 8.15-2 -7.06-3 3.087+0 1.674 4.23-2 -9.53-3 5.956+0 1.758 6.57-2 1.99-2 4.345+0	9000 1.914+0 1.791 1.09-3 -7.64-3 2.486+0 1.667 1.01-1 -8.07-3 4.621+0 1.766 1.57-1 2.34-2 3.117+0	10000 1.584+0 1.801 -6.33-2 -8.16-3 2.037+0 1.657 1.74-1 -6.31-3 3.662+0 1.768 2.60-1 2.63-2 2.299+0
Shell $4s_{1/2}$ $E_b = 1440.8 \text{ eV}$ $4p_{1/2}$ $E_b = 1271.8 \text{ eV}$ $4p_{3/2}$ $E_b = 1044.9 \text{ eV}$ $4d_{3/2}$ $E_b = 780.2 \text{ eV}$	σ β γ δ σ β γ δ σ β γ δ σ β γ δ σ β γ δ σ β γ δ σ σ β γ δ σ σ σ σ σ σ σ σ σ σ σ σ σ	k(eV) 1500 2.438+1 1.444 9.57-1 1.05-2 2.287+1 0.332 1.26-1 1.84-1 1.021+2 0.751 3.28-1 8.55-2 1.507+2 0.621 1.71-1 4.52-2 2.288+2	2000 1.869+1 1.572 9.65-1 3.73-3 1.976+1 1.075 7.04-1 5.04-2 7.052+1 1.159 3.97-1 2.74-2 1.005+2 0.968 2.79-2 8.79-3 1.467+2	1.115+1 1.666 8.01-1 -7.35-4 1.348+1 1.469 4.88-1 -3.05-3 3.807+1 1.460 1.80-1 6.25-4 4.763+1 1.252 -6.16-2 1.93-2 6.669+1	4000 7.335+0 1.707 6.15-1 -2.97-3 9.367+0 1.592 2.19-1 -1.11-2 2.323+1 1.595 1.71-2 7.23-4 2.547+1 1.354 4.30-2 3.92-2 3.479+1	5.179+0 1.732 4.47-1 -4.45-3 6.771+0 1.644 6.89-2 -1.21-2 1.538+1 1.670 -5.12-2 5.71-3 1.496+1 1.389 2.17-1 5.59-2 2.008+1	6000 3.847+0 1.751 3.02-1 -5.53-3 5.070+0 1.667 9.21-3 -1.16-2 1.078+1 1.715 -5.13-2 1.11-2 9.426+0 1.392 4.10-1 7.01-2 1.248+1	7000 2.967+0 1.767 1.81-1 -6.38-3 3.909+0 1.675 7.44-3 -1.07-2 7.882+0 1.743 -7.09-3 1.59-2 6.266+0 1.379 6.03-1 8.29-2 8.196+0	2.356+0 1.780 8.15-2 -7.06-3 3.087+0 1.674 4.23-2 -9.53-3 5.956+0 1.758 6.57-2 1.99-2 4.345+0 1.356 7.88-1 9.50-2 5.625+0	9000 1.914+0 1.791 1.09-3 -7.64-3 2.486+0 1.667 1.01-1 -8.07-3 4.621+0 1.766 1.57-1 2.34-2 3.117+0 1.327 9.60-1 1.06-1 3.998+0	10000 1.584+0 1.801 -6.33-2 -8.16-3 2.037+0 1.657 1.74-1 -6.31-3 3.662+0 1.768 2.60-1 2.63-2 2.299+0 1.12+0 1.17-1 2.924+0
Shell $4s_{1/2}$ $E_b = 1440.8 \text{ eV}$ $4p_{1/2}$ $E_b = 1271.8 \text{ eV}$ $4p_{3/2}$ $E_b = 1044.9 \text{ eV}$ $4d_{3/2}$ $E_b = 780.2 \text{ eV}$ $4d_{5/2}$ $E_b = 60.2 \text{ eV}$	σ β γ δ σ β γ δ σ β γ δ σ β γ δ σ β γ δ σ β γ δ σ σ β ρ γ δ δ σ σ σ σ σ σ σ σ σ σ σ σ σ	k(eV) 1500 2.438+1 1.444 9.57-1 1.05-2 2.287+1 0.332 1.26-1 1.84-1 1.021+2 0.751 3.28-1 8.55-2 1.507+2 0.621 1.71-1 4.52-2 2.288+2 0.926	2000 1.869+1 1.572 9.65-1 3.73-3 1.976+1 1.075 7.04-1 5.04-2 7.052+1 1.159 3.97-1 2.74-2 1.005+2 0.968 2.79-2 8.79-3 1.467+2 1.178	1.115+1 1.666 8.01-1 -7.35-4 1.348+1 1.469 4.88-1 -3.05-3 3.807+1 1.460 1.80-1 6.25-4 4.763+1 1.252 -6.16-2 1.93-2 6.669+1 1.347	4000 7.335+0 1.707 6.15-1 -2.97-3 9.367+0 1.592 2.19-1 -1.11-2 2.323+1 1.595 1.71-2 7.23-4 2.547+1 1.354 4.30-2 3.92-2 3.479+1 1.377	5.179+0 1.732 4.47-1 -4.45-3 6.771+0 1.644 6.89-2 -1.21-2 1.538+1 1.670 -5.12-2 5.71-3 1.496+1 1.389 2.17-1 5.59-2 2.008+1 1.363	6000 3.847+0 1.751 3.02-1 -5.53-3 5.070+0 1.667 9.21-3 -1.16-2 1.078+1 1.715 -5.13-2 1.11-2 9.426+0 1.392 4.10-1 7.01-2 1.248+1 1.331	7000 2.967+0 1.767 1.81-1 -6.38-3 3.909+0 1.675 7.44-3 -1.07-2 7.882+0 1.743 -7.09-3 1.59-2 6.266+0 1.379 6.03-1 8.29-2 8.196+0 1.292	2.356+0 1.780 8.15-2 -7.06-3 3.087+0 1.674 4.23-2 -9.53-3 5.956+0 1.758 6.57-2 1.99-2 4.345+0 1.356 7.88-1 9.50-2 5.625+0 1.249	9000 1.914+0 1.791 1.09-3 -7.64-3 2.486+0 1.667 1.01-1 -8.07-3 4.621+0 1.766 1.57-1 2.34-2 3.117+0 1.327 9.60-1 1.06-1 3.998+0 1.205	10000 1.584+0 1.801 -6.33-2 -8.16-3 2.037+0 1.657 1.74-1 -6.31-3 3.662+0 1.768 2.60-1 2.63-2 2.299+0 1.12+0 1.17-1 2.924+0 1.161
Shell $4s_{1/2}$ $E_b = 1440.8 \text{ eV}$ $4p_{1/2}$ $E_b = 1271.8 \text{ eV}$ $4p_{3/2}$ $E_b = 1044.9 \text{ eV}$ $4d_{3/2}$ $E_b = 780.2 \text{ eV}$	σ β γ δ σ β γ δ σ β γ δ σ β γ δ σ β γ δ σ β γ δ σ σ β γ δ σ σ σ σ σ σ σ σ σ σ σ σ σ	k(eV) 1500 2.438+1 1.444 9.57-1 1.05-2 2.287+1 0.332 1.26-1 1.84-1 1.021+2 0.751 3.28-1 8.55-2 1.507+2 0.621 1.71-1 4.52-2 2.288+2	2000 1.869+1 1.572 9.65-1 3.73-3 1.976+1 1.075 7.04-1 5.04-2 7.052+1 1.159 3.97-1 2.74-2 1.005+2 0.968 2.79-2 8.79-3 1.467+2	1.115+1 1.666 8.01-1 -7.35-4 1.348+1 1.469 4.88-1 -3.05-3 3.807+1 1.460 1.80-1 6.25-4 4.763+1 1.252 -6.16-2 1.93-2 6.669+1	4000 7.335+0 1.707 6.15-1 -2.97-3 9.367+0 1.592 2.19-1 -1.11-2 2.323+1 1.595 1.71-2 7.23-4 2.547+1 1.354 4.30-2 3.92-2 3.479+1	5.179+0 1.732 4.47-1 -4.45-3 6.771+0 1.644 6.89-2 -1.21-2 1.538+1 1.670 -5.12-2 5.71-3 1.496+1 1.389 2.17-1 5.59-2 2.008+1	6000 3.847+0 1.751 3.02-1 -5.53-3 5.070+0 1.667 9.21-3 -1.16-2 1.078+1 1.715 -5.13-2 1.11-2 9.426+0 1.392 4.10-1 7.01-2 1.248+1	7000 2.967+0 1.767 1.81-1 -6.38-3 3.909+0 1.675 7.44-3 -1.07-2 7.882+0 1.743 -7.09-3 1.59-2 6.266+0 1.379 6.03-1 8.29-2 8.196+0	2.356+0 1.780 8.15-2 -7.06-3 3.087+0 1.674 4.23-2 -9.53-3 5.956+0 1.758 6.57-2 1.99-2 4.345+0 1.356 7.88-1 9.50-2 5.625+0	9000 1.914+0 1.791 1.09-3 -7.64-3 2.486+0 1.667 1.01-1 -8.07-3 4.621+0 1.766 1.57-1 2.34-2 3.117+0 1.327 9.60-1 1.06-1 3.998+0	10000 1.584+0 1.801 -6.33-2 -8.16-3 2.037+0 1.657 1.74-1 -6.31-3 3.662+0 1.768 2.60-1 2.63-2 2.299+0 1.12+0 1.17-1 2.924+0
Shell $4s_{1/2}$ $E_b = 1440.8 \text{ eV}$ $4p_{1/2}$ $E_b = 1271.8 \text{ eV}$ $4p_{3/2}$ $E_b = 1044.9 \text{ eV}$ $4d_{3/2}$ $E_b = 780.2 \text{ eV}$ $4d_{5/2}$ $E_b = 737.7 \text{ eV}$	σ β γ δ σ β γ δ σ β γ δ σ β γ δ σ β γ δ σ β γ δ σ β γ δ σ σ σ σ σ σ σ σ σ σ σ σ σ	k(eV) 1500 2.438+1 1.444 9.57-1 1.05-2 2.287+1 0.332 1.26-1 1.84-1 1.021+2 0.751 3.28-1 8.55-2 1.507+2 0.621 1.71-1 4.52-2 2.288+2 0.926 1.52-1 2.96-2 2.696+2	2000 1.869+1 1.572 9.65-1 3.73-3 1.976+1 1.075 7.04-1 5.04-2 7.052+1 1.159 3.97-1 2.74-2 1.005+2 0.968 2.79-2 8.79-3 1.467+2 1.178 -8.95-3 8.01-3 1.179+2	1.115+1 1.666 8.01-1 -7.35-4 1.348+1 1.469 4.88-1 -3.05-3 3.807+1 1.460 1.80-1 6.25-4 4.763+1 1.252 -6.16-2 1.93-2 6.669+1 1.347 -3.98-2 1.78-2 3.300+1	4000 7.335+0 1.707 6.15-1 -2.97-3 9.367+0 1.592 2.19-1 -1.11-2 2.323+1 1.595 1.71-2 7.23-4 2.547+1 1.354 4.30-2 3.92-2 3.479+1 1.377 1.11-1 3.43-2 1.246+1	5.179+0 1.732 4.47-1 -4.45-3 6.771+0 1.644 6.89-2 -1.21-2 1.538+1 1.670 -5.12-2 5.71-3 1.496+1 1.389 2.17-1 5.59-2 2.008+1 1.363 3.09-1 5.03-2 5.635+0	6000 3.847+0 1.751 3.02-1 -5.53-3 5.070+0 1.667 9.21-3 -1.16-2 1.078+1 1.715 -5.13-2 1.11-2 9.426+0 1.392 4.10-1 7.01-2 1.248+1 1.331 5.09-1 6.58-2 2.876+0	7000 2.967+0 1.767 1.81-1 -6.38-3 3.909+0 1.675 7.44-3 -1.07-2 7.882+0 1.743 -7.09-3 1.59-2 6.266+0 1.379 6.03-1 8.29-2 8.196+0 1.292 6.99-1 8.14-2 1.604+0	2.356+0 1.780 8.15-2 -7.06-3 3.087+0 1.674 4.23-2 -9.53-3 5.956+0 1.758 6.57-2 1.99-2 4.345+0 1.356 7.88-1 9.50-2 5.625+0 1.249 8.74-1 9.73-2 9.566-1	9000 1.914+0 1.791 1.09-3 -7.64-3 2.486+0 1.667 1.01-1 -8.07-3 4.621+0 1.766 1.57-1 2.34-2 3.117+0 1.327 9.60-1 1.06-1 3.998+0 1.205 1.03+0 1.13-1 6.017-1	10000 1.584+0 1.801 -6.33-2 -8.16-3 2.037+0 1.657 1.74-1 -6.31-3 3.662+0 1.768 2.60-1 2.63-2 2.299+0 1.12+0 1.17-1 2.924+0 1.17-0 1.161 1.17+0 1.28-1 3.952-1
Shell $4s_{1/2}$ $E_b = 1440.8 \text{ eV}$ $4p_{1/2}$ $E_b = 1271.8 \text{ eV}$ $4p_{3/2}$ $E_b = 1044.9 \text{ eV}$ $4d_{3/2}$ $E_b = 780.2 \text{ eV}$ $4d_{5/2}$ $E_b = 737.7 \text{ eV}$ $4f_{5/2}$ $E_b = 6$	$ \begin{array}{c} \sigma \\ \beta \\ \gamma \\ \delta \\ \sigma \\ \beta \\ \beta \\ \gamma \\ \delta \\ \sigma \\ \sigma \\ \beta \\ \gamma \\ \delta \\ \sigma \\ \sigma \\ \beta \\ \gamma \\ \delta \\ \sigma \\ \sigma \\ \rho \\ \sigma \\ \sigma \\ \sigma \\ \rho \\ \sigma \\ \sigma \\ \sigma \\ \sigma \\ \rho \\ \sigma \\ \sigma$	k(eV) 1500 2.438+1 1.444 9.57-1 1.05-2 2.287+1 0.332 1.26-1 1.84-1 1.021+2 0.751 3.28-1 8.55-2 1.507+2 0.621 1.71-1 4.52-2 2.288+2 0.926 1.52-1 2.96-2 2.696+2 0.930	2000 1.869+1 1.572 9.65-1 3.73-3 1.976+1 1.075 7.04-1 5.04-2 7.052+1 1.159 3.97-1 2.74-2 1.005+2 0.968 2.79-2 8.79-3 1.467+2 1.178 -8.95-3 8.01-3 1.179+2 1.023	1.115+1 1.666 8.01-1 -7.35-4 1.348+1 1.469 4.88-1 -3.05-3 3.807+1 1.460 1.80-1 6.25-4 4.763+1 1.252 -6.16-2 1.93-2 6.669+1 1.347 -3.98-2 1.78-2 3.300+1 1.051	4000 7.335+0 1.707 6.15-1 -2.97-3 9.367+0 1.592 2.19-1 -1.11-2 2.323+1 1.595 1.71-2 7.23-4 2.547+1 1.354 4.30-2 3.92-2 3.479+1 1.377 1.11-1 3.43-2 1.246+1 1.010	5.179+0 1.732 4.47-1 -4.45-3 6.771+0 1.644 6.89-2 -1.21-2 1.538+1 1.670 -5.12-2 5.71-3 1.496+1 1.389 2.17-1 5.59-2 2.008+1 1.363 3.09-1 5.03-2 5.635+0 0.952	6000 3.847+0 1.751 3.02-1 -5.53-3 5.070+0 1.667 9.21-3 -1.16-2 1.078+1 1.715 -5.13-2 1.11-2 9.426+0 1.392 4.10-1 7.01-2 1.248+1 1.331 5.09-1 6.58-2 2.876+0 0.890	7000 2.967+0 1.767 1.81-1 -6.38-3 3.909+0 1.675 7.44-3 -1.07-2 7.882+0 1.743 -7.09-3 1.59-2 6.266+0 1.379 6.03-1 8.29-2 8.196+0 1.292 6.99-1 8.14-2 1.604+0 0.829	2.356+0 1.780 8.15-2 -7.06-3 3.087+0 1.674 4.23-2 -9.53-3 5.956+0 1.758 6.57-2 1.99-2 4.345+0 1.356 7.88-1 9.50-2 5.625+0 1.249 8.74-1 9.73-2 9.566-1 0.770	9000 1.914+0 1.791 1.09-3 -7.64-3 2.486+0 1.667 1.01-1 -8.07-3 4.621+0 1.766 1.57-1 2.34-2 3.117+0 1.327 9.60-1 1.06-1 3.998+0 1.205 1.03+0 1.13-1 6.017-1 0.715	10000 1.584+0 1.801 -6.33-2 -8.16-3 2.037+0 1.657 1.74-1 -6.31-3 3.662+0 1.768 2.60-1 2.63-2 2.299+0 1.12+0 1.17-1 2.924+0 1.161 1.17+0 1.28-1 3.952-1 0.664
Shell $4s_{1/2}$ $E_b = 1440.8 \text{ eV}$ $4p_{1/2}$ $E_b = 1271.8 \text{ eV}$ $4p_{3/2}$ $E_b = 1044.9 \text{ eV}$ $4d_{3/2}$ $E_b = 780.2 \text{ eV}$ $4d_{5/2}$ $E_b = 737.7 \text{ eV}$	σ β γ δ σ β γ δ σ β γ δ σ β γ δ σ β γ δ σ β γ δ σ β γ δ σ σ σ σ σ σ σ σ σ σ σ σ σ	k(eV) 1500 2.438+1 1.444 9.57-1 1.05-2 2.287+1 0.332 1.26-1 1.84-1 1.021+2 0.751 3.28-1 8.55-2 1.507+2 0.621 1.71-1 4.52-2 2.288+2 0.926 1.52-1 2.96-2 2.696+2	2000 1.869+1 1.572 9.65-1 3.73-3 1.976+1 1.075 7.04-1 5.04-2 7.052+1 1.159 3.97-1 2.74-2 1.005+2 0.968 2.79-2 8.79-3 1.467+2 1.178 -8.95-3 8.01-3 1.179+2	1.115+1 1.666 8.01-1 -7.35-4 1.348+1 1.469 4.88-1 -3.05-3 3.807+1 1.460 1.80-1 6.25-4 4.763+1 1.252 -6.16-2 1.93-2 6.669+1 1.347 -3.98-2 1.78-2 3.300+1	4000 7.335+0 1.707 6.15-1 -2.97-3 9.367+0 1.592 2.19-1 -1.11-2 2.323+1 1.595 1.71-2 7.23-4 2.547+1 1.354 4.30-2 3.92-2 3.479+1 1.377 1.11-1 3.43-2 1.246+1	5.179+0 1.732 4.47-1 -4.45-3 6.771+0 1.644 6.89-2 -1.21-2 1.538+1 1.670 -5.12-2 5.71-3 1.496+1 1.389 2.17-1 5.59-2 2.008+1 1.363 3.09-1 5.03-2 5.635+0	6000 3.847+0 1.751 3.02-1 -5.53-3 5.070+0 1.667 9.21-3 -1.16-2 1.078+1 1.715 -5.13-2 1.11-2 9.426+0 1.392 4.10-1 7.01-2 1.248+1 1.331 5.09-1 6.58-2 2.876+0	7000 2.967+0 1.767 1.81-1 -6.38-3 3.909+0 1.675 7.44-3 -1.07-2 7.882+0 1.743 -7.09-3 1.59-2 6.266+0 1.379 6.03-1 8.29-2 8.196+0 1.292 6.99-1 8.14-2 1.604+0	2.356+0 1.780 8.15-2 -7.06-3 3.087+0 1.674 4.23-2 -9.53-3 5.956+0 1.758 6.57-2 1.99-2 4.345+0 1.356 7.88-1 9.50-2 5.625+0 1.249 8.74-1 9.73-2 9.566-1	9000 1.914+0 1.791 1.09-3 -7.64-3 2.486+0 1.667 1.01-1 -8.07-3 4.621+0 1.766 1.57-1 2.34-2 3.117+0 1.327 9.60-1 1.06-1 3.998+0 1.205 1.03+0 1.13-1 6.017-1	10000 1.584+0 1.801 -6.33-2 -8.16-3 2.037+0 1.657 1.74-1 -6.31-3 3.662+0 1.768 2.60-1 2.63-2 2.299+0 1.12+0 1.17-1 2.924+0 1.17-0 1.161 1.17+0 1.28-1 3.952-1
Shell $4s_{1/2}$ $E_b = 1440.8 \text{ eV}$ $4p_{1/2}$ $E_b = 1271.8 \text{ eV}$ $4p_{3/2}$ $E_b = 1044.9 \text{ eV}$ $4d_{3/2}$ $E_b = 780.2 \text{ eV}$ $4d_{5/2}$ $E_b = 737.7 \text{ eV}$ $4f_{5/2}$ $E_b = 390.7 \text{ eV}$	σ β γ δ σ β γ δ σ β γ δ σ β γ δ σ β γ δ σ β γ δ σ β γ δ σ σ β γ δ σ σ σ σ σ σ σ σ σ σ σ σ σ	k (eV) 1500 2.438+1 1.444 9.57-1 1.05-2 2.287+1 0.332 1.26-1 1.84-1 1.021+2 0.751 3.28-1 8.55-2 1.507+2 0.621 1.71-1 4.52-2 2.288+2 0.926 1.52-1 2.96-2 2.696+2 0.930 3.90-2 5.42-2 3.409+2	2000 1.869+1 1.572 9.65-1 3.73-3 1.976+1 1.075 7.04-1 5.04-2 7.052+1 1.159 3.97-1 2.74-2 1.005+2 0.968 2.79-2 8.79-3 1.467+2 1.178 -8.95-3 8.01-3 1.179+2 1.023 1.66-1 8.00-2 1.480+2	1.115+1 1.666 8.01-1 -7.35-4 1.348+1 1.469 4.88-1 -3.05-3 3.807+1 1.460 1.80-1 6.25-4 4.763+1 1.252 -6.16-2 1.93-2 6.669+1 1.347 -3.98-2 1.78-2 3.300+1 1.051 4.38-1 1.22-1 4.107+1	4000 7.335+0 1.707 6.15-1 -2.97-3 9.367+0 1.592 2.19-1 -1.11-2 2.323+1 1.595 1.71-2 7.23-4 2.547+1 1.354 4.30-2 3.92-2 3.479+1 1.377 1.11-1 3.43-2 1.246+1 1.010 6.76-1 1.58-1 1.540+1	5.179+0 1.732 4.47-1 -4.45-3 6.771+0 1.644 6.89-2 -1.21-2 1.538+1 1.670 -5.12-2 5.71-3 1.496+1 1.389 2.17-1 5.59-2 2.008+1 1.363 3.09-1 5.03-2 5.635+0 0.952 8.75-1 1.92-1 6.920+0	6000 3.847+0 1.751 3.02-1 -5.53-3 5.070+0 1.667 9.21-3 -1.16-2 1.078+1 1.715 -5.13-2 1.11-2 9.426+0 1.392 4.10-1 7.01-2 1.248+1 1.331 5.09-1 6.58-2 2.876+0 0.890 1.04+0 2.25-1 3.513+0	7000 2.967+0 1.767 1.81-1 -6.38-3 3.909+0 1.675 7.44-3 -1.07-2 7.882+0 1.743 -7.09-3 1.59-2 6.266+0 1.379 6.03-1 8.29-2 8.196+0 1.292 6.99-1 8.14-2 1.604+0 0.829 1.17+0 2.56-1 1.949+0	2.356+0 1.780 8.15-2 -7.06-3 3.087+0 1.674 4.23-2 -9.53-3 5.956+0 1.758 6.57-2 1.99-2 4.345+0 1.356 7.88-1 9.50-2 5.625+0 1.249 8.74-1 9.73-2 9.566-1 0.770 1.28+0 2.85-1 1.157+0	9000 1.914+0 1.791 1.09-3 -7.64-3 2.486+0 1.667 1.01-1 -8.07-3 4.621+0 1.766 1.57-1 2.34-2 3.117+0 1.327 9.60-1 1.06-1 3.998+0 1.205 1.03+0 1.13-1 6.017-1 0.715 1.37+0 3.12-1 7.244-1	10000 1.584+0 1.801 -6.33-2 -8.16-3 2.037+0 1.657 1.74-1 -6.31-3 3.662+0 1.768 2.60-1 2.63-2 2.299+0 1.12+0 1.17-1 2.924+0 1.161 1.17+0 1.161 1.17+0 1.28-1 3.952-1 0.664 1.44+0 3.37-1 4.737-1
Shell $4s_{1/2}$ $E_b = 1440.8 \text{ eV}$ $4p_{1/2}$ $E_b = 1271.8 \text{ eV}$ $4p_{3/2}$ $E_b = 1044.9 \text{ eV}$ $4d_{3/2}$ $E_b = 780.2 \text{ eV}$ $4d_{5/2}$ $E_b = 737.7 \text{ eV}$ $4f_{5/2}$ $E_b = 390.7 \text{ eV}$	σ β γ δ σ β γ δ σ β γ δ σ β γ δ σ β γ δ σ β γ δ σ β γ δ δ σ σ β ρ γ δ δ σ σ σ σ σ σ σ σ σ σ σ σ σ	k(eV) 1500 2.438+1 1.444 9.57-1 1.05-2 2.287+1 0.332 1.26-1 1.84-1 1.021+2 0.751 3.28-1 8.55-2 1.507+2 0.621 1.71-1 4.52-2 2.288+2 0.926 1.52-1 2.96-2 2.696+2 0.930 3.90-2 5.42-2	2000 1.869+1 1.572 9.65-1 3.73-3 1.976+1 1.075 7.04-1 5.04-2 7.052+1 1.159 3.97-1 2.74-2 1.005+2 0.968 2.79-2 8.79-3 1.467+2 1.178 -8.95-3 8.01-3 1.179+2 1.023 1.66-1 8.00-2	1.115+1 1.666 8.01-1 -7.35-4 1.348+1 1.469 4.88-1 -3.05-3 3.807+1 1.460 1.80-1 6.25-4 4.763+1 1.252 -6.16-2 1.93-2 6.669+1 1.349 -3.98-2 1.78-2 3.300+1 1.051 4.38-1 1.22-1	4000 7.335+0 1.707 6.15-1 -2.97-3 9.367+0 1.592 2.19-1 -1.11-2 2.323+1 1.595 1.71-2 7.23-4 2.547+1 1.354 4.30-2 3.92-2 3.479+1 1.377 1.11-1 3.43-2 1.246+1 1.010 6.76-1 1.58-1	5.179+0 1.732 4.47-1 -4.45-3 6.771+0 1.644 6.89-2 -1.21-2 1.538+1 1.670 -5.12-2 5.71-3 1.496+1 1.389 2.17-1 5.59-2 2.008+1 1.363 3.09-1 5.03-2 5.635+0 0.952 8.75-1 1.92-1	6000 3.847+0 1.751 3.02-1 -5.53-3 5.070+0 1.667 9.21-3 -1.16-2 1.078+1 1.715 -5.13-2 1.11-2 9.426+0 1.392 4.10-1 7.01-2 1.248+1 1.331 5.09-1 6.58-2 2.876+0 0.890 1.04+0 2.25-1	7000 2.967+0 1.767 1.81-1 -6.38-3 3.909+0 1.675 7.44-3 -1.07-2 7.882+0 1.743 -7.09-3 1.59-2 6.266+0 1.379 6.03-1 8.29-2 8.196+0 1.292 6.99-1 8.14-2 1.604+0 0.829 1.17+0 2.56-1	2.356+0 1.780 8.15-2 -7.06-3 3.087+0 1.674 4.23-2 -9.53-3 5.956+0 1.758 6.57-2 1.99-2 4.345+0 1.356 7.88-1 9.50-2 5.625+0 1.249 8.74-1 9.73-2 9.566-1 0.770 1.28+0 2.85-1	9000 1.914+0 1.791 1.09-3 -7.64-3 2.486+0 1.667 1.01-1 -8.07-3 4.621+0 1.766 1.57-1 2.34-2 3.117+0 1.327 9.60-1 1.06-1 3.998+0 1.205 1.03+0 1.13-1 6.017-1 0.715 1.37+0 3.12-1	10000 1.584+0 1.801 -6.33-2 -8.16-3 2.037+0 1.657 1.74-1 -6.31-3 3.662+0 1.768 2.60-1 2.63-2 2.299+0 1.12+0 1.17-1 2.924+0 1.17+0 1.161 1.17+0 1.28-1 3.952-1 0.664 1.44+0

able 1 (<i>contini</i> 5s _{1/2}	ued) σ	9.227+0	6.002+0	3.180+0	1.990+0	1.370+0	1.002+0	7.651-1	6.030-1	4.871-1	4.013-1
$E_b =$	β	1.627	1.669	1.713	1.738	1.756	1.771	1.783	1.794	1.803	1.811
323.3 eV	γ	6.71 - 1	6.43 - 1	5.27 - 1	3.95 - 1	2.71 - 1	1.63 - 1	7.15 - 2	-4.19 - 3	-6.57 - 2	-1.15-
	δ	8.98-4	-5.59-4	-2.58-3	-3.98-3	-5.03-3	-5.88-3	-6.58-3	-7.18-3	-7.71-3	-8.19-3
$5p_{1/2}$	σ	8.484+0	6.043+0	3.532+0	2.314+0	1.626+0	1.199+0	9.157-1	7.184-1	5.760-1	4.702-1
$E_b = 259.3 \text{ eV}$	β γ	1.327 6.02-1	1.496 4.91-1	1.635 2.38-1	1.685 8.11-2	1.703 1.03-2	1.707 1.44-3	1.703 2.54-2	1.694 7.76-2	1.682 1.47-1	1.668 2.27-1
233.3 C V	δ	-4.96 - 3	-1.24-2	-1.44-2	-1.35-2	-1.26-2	-1.17-2	-1.09-2	-9.83-3	-8.51-3	-6.87-3
$5p_{3/2}$	σ	2.817+1	1.792+1	9.030+0	5.366+0	3.509+0	2.444+0	1.781+0	1.342+0	1.040+0	8.232-1
$E_b =$	β	1.291	1.437	1.594	1.677	1.725	1.754	1.771	1.780	1.782	1.781
195.9 eV	$\gamma \\ \delta$	3.25-1 3.41-3	2.31-1 -3.76-3	5.83-2 -3.79-3	-3.25-2 1.37-3	-5.32-2 $6.95-3$	-2.53-2 1.19-2	3.52-2 1.60-2	1.17-1 1.96-2	2.14-1 2.26-2	3.20-1 2.52-2
5d _{3/2}	σ	2.952+1	1.837+1	8.399+0	4.481+0	2.645+0	1.677+0	1.121+0	7.808-1	5.623-1	4.162-1
$E_b =$	β	1.067	1.230	1.374	1.423	1.431	1.420	1.397	1.368	1.335	1.300
104.4 eV	γ	5.94 - 2	-2.56-2	-1.32-2	1.20 - 1	2.96 - 1	4.84 - 1	6.70 - 1	8.48 - 1	1.01+0	1.16+0
	δ	-1.98-3	3.12-3	2.21-2	3.94-2	5.39-2	6.69-2	7.91-2	9.08-2	1.02-1	1.12-1
$5d_{5/2}$	σ	4.355+1	2.638+1	1.166+1	6.088+0	3.535+0	2.211+0	1.461+0	1.007+0	7.189-1	5.276-1
$E_b = 95.2 \text{ eV}$	β γ	1.283 2.28-2	1.376 -4.08-2	1.426 2.33-2	1.414 1.90-1	1.380 3.82-1	1.338 5.73-1	1.293 7.54-1	1.247 9.21-1	1.201 1.07+0	1.155 1.21+0
33.2 CV	δ	1.72-4	4.77-3	1.93-2	3.43-2	4.91-2	6.42-2	7.97-2	9.54-2	1.11-1	1.26-1
5f _{5/2}	σ	1.821+1	8.402+0	2.513+0	9.877-1	4.583-1	2.382-1	1.345-1	8.098-2	5.129-2	3.387-2
$E_b =$	β	1.074	1.106	1.080	1.019	0.952	0.887	0.825	0.766	0.711	0.660
6.0 eV	γ	9.62-2	2.24-1	4.77-1	6.98-1	8.87-1	1.05+0	1.18+0	1.29+0	1.38+0	1.45+0
C-	δ	5.26-2	7.58-2	1.16-1	1.52-1	1.87-1	2.20-1	2.52-1	2.82-1	3.09-1	3.35-1
$6s_{1/2} E_b =$	$\frac{\sigma}{\beta}$	1.965+0 1.650	1.251+0 1.684	6.479-1 1.721	4.008-1 1.744	2.740-1 1.760	1.996-1 1.774	1.520-1 1.786	1.195-1 1.796	9.639-2 1.805	7.932-2 1.814
49.5 eV	γ	6.17-1	5.88-1	4.78 - 1	3.55-1	2.39 - 1	1.37 - 1	5.04 - 2	-2.09-2	-7.85-2	-1.24-1
	δ	1.78 - 4	-1.05 - 3	-2.85 - 3	-4.14 - 3	-5.14 - 3	-5.94 - 3	-6.62 - 3	-7.20 - 3	-7.71 - 3	-8.17-3
$6p_{1/2}$	σ	1.580+0	1.096+0	6.241 - 1	4.041 - 1	2.822 - 1	2.073 - 1	1.579 - 1	1.237 - 1	9.906 - 2	8.078 - 2
$E_b = 30.8 \text{ eV}$	β	1.408	1.546 4.35-1	1.660 2.01-1	1.700 6.25-2	1.713 3.64-3	1.714 -5.38-4	1.708 3.11-2	1.698 8.63-2	1.685 1.57-1	1.671 2.37-1
30.6 EV	$\gamma \\ \delta$	5.54-1 -1.22-2	-1.53-1	-1.49-2	-1.35-2	-1.26-2	-3.38-4 -1.18-2	-1.10-2	-9.94-3	-8.65-3	-7.02-3
6p _{3/2}	σ	4.456+0	2.798+0	1.392+0	8.222-1	5.360-1	3.727-1	2.712-1	2.042-1	1.581-1	1.251-1
$E_b =$	β	1.345	1.473	1.615	1.690	1.734	1.761	1.776	1.783	1.785	1.783
18.6 eV	γ	2.98-1	2.04-1	4.28-2	-3.77-2	-5.17-2	-1.94-2	4.38-2	1.27-1	2.24-1	3.29-1
	δ	-1.60-3	-5.82-3	-3.91-3	1.60-3	7.16-3	1.20-2	1.60-2	1.94-2	2.23-2	2.48-2
$6d_{3/2}$ $E_b =$	$\frac{\sigma}{\beta}$	2.064+0 1.110	1.275+0 1.260	5.802-1 1.390	3.092-1 1.432	1.825-1 1.437	1.157-1 1.423	7.731-2 1.399	5.385-2 1.370	3.878-2 1.337	2.871-2 1.302
6.0 eV	γ	5.19-2	-2.68-2	-7.35-3	1.29-1	3.08-1	4.97-1	6.80-1	8.53-1	1.01+0	1.16+0
	δ	-3.62 - 3	2.98 - 3	2.20-2	3.92-2	5.39-2	6.68 - 2	7.84 - 2	8.92-2	9.99-2	1.11-1
$7s_{1/2}$	σ	1.787 - 1	1.133 - 1	5.840 - 2	3.604-2	2.461-2	1.792 - 2	1.363-2	1.072 - 2	8.641 - 3	7.107 - 3
$E_b = 6.0 \text{ eV}$	β	1.652 6.12-1	1.685 5.84-1	1.723 4.73-1	1.746 3.49-1	1.762 2.35-1	1.775 1.34-1	1.785 4.86-2	1.795 -2.32-2	1.803 -8.15-2	1.812 -1.27-1
0.0 6	$\gamma \\ \delta$	9.05-5	-1.11-3	-2.89-3	-4.16-3	-5.14-3	-5.94-3	-6.64-3	-2.32-2 -7.27-3	-7.79 - 3	-8.27 - 3
Z= 93, Np: [R	n 5f _{5/2}	$6d_{3/2}^{1} 7s_{1/2}^{2}$									
	- 3/2	k (eV)									
Shell		1500	2000	3000	4000	5000	6000	7000	8000	9000	10000
$4p_{1/2}$	σ	2.191+1	1.931+1	1.343+1	9.427+0	6.860+0	5.161+0	3.994+0	3.164+0	2.555+0	2.098+0
$E_b =$	β	0.113	1.000	1.441	1.577	1.635	1.662	1.673	1.674	1.669	1.660
1327.7 eV	γ	-7.36-2	7.04-1	5.35-1	2.55-1	9.02-2	1.75-2	5.64-3	3.25-2	8.43-2	1.52-1
4	δ	2.22-1	6.17-2	-2.12-3	-1.16-2	-1.29-2	-1.25-2	-1.15-2	-1.03-2	-8.89-3	-7.20-3
$4p_{3/2}$ $E_b =$	$\frac{\sigma}{\beta}$	1.035+2 0.685	7.192+1 1.116	3.903+1 1.435	2.389+1 1.578	1.586+1 1.657	1.114+1 1.706	8.157+0 1.736	6.173+0 1.754	4.794+0 1.764	3.804+0 1.768
$L_b = 1086.0 \text{ eV}$	γ	3.02-1	4.08-1	2.01-1	3.09-2	-4.67 - 2	-5.54-2	-1.83-2	4.85-2	1.764	2.34-1
	δ	9.71-2	3.20-2	1.08-3	2.35-4	5.11-3	1.06-2	1.56-2	1.99-2	2.35-2	2.66-2
4d _{3/2}	σ	1.531+2	1.032+2	4.944+1	2.660+1	1.570+1	9.924+0	6.615+0	4.597+0	3.305+0	2.442+0
$E_b = 816.1 \text{ eV}$	β	0.563 1.82-1	0.931 4.40-2	1.234	1.345 2.56—2	1.386 1.93_1	1.394 3.82_1	1.383 5.72-1	1.363 7.55-1	1.337	1.307
0 10.1 EV	$_{\delta}^{\gamma}$	5.55-2	4.40—2 1.04—2	-6.52-2 $1.79-2$	2.56-2 3.79-2	1.93-1 5.50-2	3.82-1 6.93-2	5.72-1 8.19-2	9.38-2	9.28-1 1.05-1	1.09+0 1.16-1
4d _{5/2}	σ	2.337+2	1.511+2	6.931+1	3.635+1	2.106+1	1.313+1	8.645+0	5.946+0	4.234+0	3.102+0
$E_b =$	β	0.889	1.159	1.342	1.378	1.367	1.337	1.300	1.258	1.216	1.173
770.8 eV	γ	1.72-1	4.03-3	-4.76-2	9.28-2	2.87-1	4.85-1	6.74-1	8.50-1	1.01+0	1.15+0
46	δ	3.58-2	8.74-3	1.67-2	3.30-2	4.89-2	6.42-2	7.94-2	9.50-2	1.10-1	1.26-1
$4f_{5/2}$ $E_b =$	$\frac{\sigma}{\beta}$	2.881+2 0.916	1.267+2 1.017	3.574+1 1.053	1.357+1 1.016	6.162+0 0.959	3.156+0 0.898	1.765+0 0.838	1.055+0 0.780	6.649-1 0.725	4.373-1 0.674
$E_b = 414.3 \text{ eV}$	γ	2.57-2	1.50-1	4.21–1	6.60-1	8.60-1	1.03+0	1.16+0	1.28+0	1.37+0	1.44+0
	δ	5.14-2	7.76-2	1.20-1	1.56-1	1.89-1	2.21-1	2.53-1	2.81-1	3.08-1	3.34-1
4f _{7/2}	σ	3.641+2	1.589+2	4.443+1	1.675+1	7.557+0	3.849+0	2.141+0	1.274+0	7.990-1	5.233-1
$E_b =$	β	0.941	1.027	1.045	0.999	0.940	0.879	0.820	0.764	0.713	0.665

8.89-1

1.05+0

1.19+0

1.30+0

1.39+0

4.48-1 6.90-1

Table 1 (continued)

403.4 eV γ 3.40-2

1.67 - 1

1.46+0

403.4 eV	γ	5.40-2	7.06	4.48-1	0.90-1	8.89-1	1.05+0	1.19+0	1.30+0	1.39+0	1.40+0
	δ	5.30-2	7.86-2	1.20-1	1.56-1	1.90-1	2.23-1	2.56-1	2.86-1	3.15-1	3.41-1
$5s_{1/2}$	σ	9.428+0	6.149+0	3.266+0	2.048+0	1.411+0	1.034+0	7.902 - 1	6.235 - 1	5.042 - 1	4.157 - 1
$E_b =$	β	1.597	1.644	1.693	1.719	1.739	1.754	1.767	1.779	1.789	1.798
339.8 eV	γ	6.88-1	6.65-1	5.53-1	4.24-1	3.01-1	1.91-1	9.69-2	1.84-2	-4.61-2	-9.80-2
	δ	1.20-3	-3.93-4	-2.58-3	-4.10-3	-5.25-3	-6.16-3	-6.92-3	-7.56-3	-8.12-3	-8.63-3
$5p_{1/2}$	σ	8.565+0	6.137+0	3.614+0	2.381+0	1.680+0	1.243+0	9.517 - 1	7.486 - 1	6.016 - 1	4.920 - 1
$E_b =$	β	1.287	1.471	1.623	1.678	1.700	1.706	1.704	1.697	1.686	1.673
283.4 eV	γ	6.30 - 1	5.27 - 1	2.69 - 1	1.01 - 1	1.94 - 2	-1.26 - 3	1.83 - 2	6.43 - 2	1.28 - 1	2.04 - 1
	δ	-4.50 - 3	-1.31-2	-1.55-2	-1.45 - 2	-1.34-2	-1.25-2	-1.16-2	-1.06-2	-9.28 - 3	-7.72 - 3
5p _{3/2}	σ	2.934+1	1.868+1	9.433+0	5.615+0	3.678+0	2.565+0	1.872+0	1.413+0	1.095+0	8.682-1
$E_b =$	β	1.264	1.415	1.579	1.665	1.716	1.748	1.767	1.778	1.782	1.782
206.0 eV	γ	3.34 - 1	2.44 - 1	7.03 - 2	-2.65-2	-5.40-2	-3.24-2	2.25 - 2	9.96 - 2	1.92 - 1	2.94 - 1
	δ	4.34 - 3	-3.65 - 3	-4.32 - 3	7.65 - 4	6.48 - 3	1.16 - 2	1.60 - 2	1.97 - 2	2.28 - 2	2.56 - 2
5d _{3/2}	σ	3.085+1	1.929+1	8.883+0	4.763+0	2.823+0	1.795+0	1.203+0	8.403-1	6.065-1	4.498-1
$E_b =$	β	1.044	1.214	1.366	1.420	1.432	1.424	1.404	1.377	1.346	1.312
109.3 eV	γ	7.03 - 2	-2.01-2	-2.03-2	1.04 - 1	2.75 - 1	4.59 - 1	6.42 - 1	8.19 - 1	9.85 - 1	1.14+0
	δ	-1.92 - 3	2.33 - 3	2.11-2	3.86 - 2	5.32 - 2	6.61 - 2	7.81 - 2	8.96 - 2	1.01 - 1	1.11 - 1
5d _{5/2}	σ	4.579+1	2.785+1	1.239+1	6.494+0	3.783+0	2.373+0	1.572+0	1.087+0	7.769-1	5.712-1
$E_b =$	β	1.275	1.373	1.427	1.418	1.386	1.345	1.302	1.257	1.211	1.167
101.2 eV	γ	3.24 - 2	-3.85 - 2	1.40 - 2	1.75 - 1	3.63 - 1	5.52 - 1	7.32 - 1	8.99 - 1	1.05+0	1.19+0
	δ	8.62 - 5	4.17 - 3	1.84 - 2	3.33 - 2	4.78 - 2	6.25 - 2	7.77 - 2	9.30 - 2	1.08 - 1	1.23 - 1
5f _{5/2}	σ	2.081+1	9.673+0	2.923+0	1.157+0	5.401-1	2.820-1	1.598-1	9.650-2	6.128-2	4.054-2
$E_b =$	β	1.073	1.108	1.085	1.025	0.960	0.896	0.835	0.776	0.722	0.670
6.0 eV	γ	8.60 - 2	2.11 - 1	4.65 - 1	6.86 - 1	8.74 - 1	1.04+0	1.17+0	1.28+0	1.37+0	1.45+0
	δ	5.05 - 2	7.37 - 2	1.14 - 1	1.50 - 1	1.84 - 1	2.17 - 1	2.48 - 1	2.78 - 1	3.06 - 1	3.31 - 1
6s _{1/2}	σ	2.028+0	1.294+0	6.711-1	4.156-1	2.844-1	2.074-1	1.581-1	1.245-1	1.005-1	8.274-2
$E_b =$	β	1.623	1.661	1.702	1.726	1.744	1.758	1.771	1.782	1.792	1.800
50.0 eV	γ	6.30 - 1	6.06 - 1	5.02 - 1	3.81 - 1	2.65 - 1	1.62 - 1	7.36 - 2	-3.16 - 4	-6.08 - 2	-1.09 - 1
	δ	3.54 - 4	-9.70 - 4	-2.90 - 3	-4.29 - 3	-5.36 - 3	-6.24 - 3	-6.96 - 3	-7.59 - 3	-8.14 - 3	-8.63 - 3
6p _{1/2}	σ	1.622+0	1.130+0	6.471-1	4.208-1	2.950-1	2.174-1	1.661-1	1.304-1	1.046-1	8.550-2
$E_b =$	β	1.382	1.530	1.652	1.695	1.711	1.714	1.710	1.701	1.689	1.675
29.3 eV	γ	5.76-1	4.61 - 1	2.24 - 1	7.75-2	1.02-2	-1.55 - 3	2.37 - 2	7.33-2	1.39 - 1	2.15 - 1
	δ	-1.30-2	-1.65-2	-1.59 - 2	-1.44-2	-1.33-2	-1.25-2	-1.16-2	-1.06-2	-9.39 - 3	-7.85 - 3
6p _{3/2}	σ	4.618+0	2.903+0	1.446+0	8.555-1	5.586-1	3.889-1	2.834-1	2.137-1	1.656-1	1.311-1
	β	1.323	1.456	1.602	1.680	1.726	1.755	1.773	1.782	1.785	1.785
$E_b = 17.5 \text{ eV}$	γ	3.06-1	2.15-1	5.29-2	-3.27-2	-5.30-2	-2.67 - 2	3.12-2	1.10-1	2.03-1	3.04-1
	δ	-1.31 - 3	-6.01 - 3	-4.48 - 3	1.03 - 3	6.74 - 3	1.18 - 2	1.60 - 2	1.96 - 2	2.26 - 2	2.52 - 2
6d _{3/2}	σ	2.177+0	1.351+0	6.185-1	3.312-1	1.962-1	1.248-1	8.366-2	5.841-2	4.216-2	3.126-2
$E_b =$	β	1.092	1.247	1.383	1.430	1.439	1.428	1.406	1.378	1.347	1.314
$E_b = 6.0 \text{ eV}$	γ	6.21 - 2	-2.20-2	-1.46 - 2	1.12 - 1	2.86 - 1	4.72 - 1	6.54 - 1	8.27 - 1	9.88 - 1	1.14+0
	δ	-3.88 - 3	2.11 - 3	2.10 - 2	3.82 - 2	5.31 - 2	6.61 - 2	7.77 - 2	8.83-2	9.87 - 2	1.09 - 1
7s _{1/2}	σ	1.793-1	1.139-1	5.879-2	3.632-2	2.482-2	1.809-2	1.378-2	1.084-2	8.750-3	7.203-3
$E_b =$	β	1.625	1.662	1.703	1.728	1.746	1.760	1.771	1.781	1.790	1.798
6.0 eV	γ	6.27 - 1	6.02 - 1	4.98 - 1	3.76 - 1	2.61 - 1	1.59 - 1	7.19 - 2	-2.14 - 3	-6.34 - 2	-1.12 - 1
	δ	2.68 - 4	-1.03 - 3	-2.94 - 3	-4.32 - 3	-5.37 - 3	-6.22 - 3	-6.97 - 3	-7.65 - 3	-8.22 - 3	-8.74 - 3
Z= 94, Pu: [R	n15f ⁶	7s ²									
Z- 34, Fu. [K	11]315/2										
		k (eV)									
Shell		1500	2000	3000	4000	5000	6000	7000	8000	9000	10000
4p _{1/2}	σ	2.094+1	1.882+1	1.335+1	9.463+0	6.934+0	5.244+0	4.075+0	3.238+0	2.622+0	2.157+0
$E_b =$	β		0.924	1.413	1.564	1.627	1.657	1.670	1.673	1.670	1.663
1377.4 eV	γ	-3.12 - 1	6.95 - 1	5.81 - 1	2.92 - 1	1.14 - 1	2.83 - 2	5.72 - 3	2.47 - 2	7.03 - 2	1.33 - 1
	δ	2.62 - 1	7.46 - 2	-1.12 - 3	-1.21-2	-1.37 - 2	-1.33-2	-1.25 - 2	-1.13-2	-9.84 - 3	-8.17 - 3
4p _{3/2}	σ	1.050+2	7.328+1	3.997+1	2.455+1	1.633+1	1.150+1	8.435+0	6.392+0	4.970+0	3.947+0
$E_b =$	β	0.593	1.072	1.411	1.562	1.645	1.696	1.729	1.749	1.761	1.767
1120.9 eV	γ	2.63 - 1	4.15 - 1	2.21 - 1	4.56 - 2	-4.06-2	-5.81-2	-2.82 - 2	3.30 - 2	1.14 - 1	2.08 - 1
	δ	1.10 - 1	3.69 - 2	1.58 - 3	-2.29 - 4	4.48 - 3	1.01 - 2	1.54 - 2	1.99 - 2	2.37 - 2	2.69 - 2
4d _{3/2}	σ	1.555+2	1.058+2	5.126+1	2.776+1	1.646+1	1.044+1	6.978+0	4.860+0	3.499+0	2.590+0
$E_b =$	β	0.500	0.892	1.216	1.336	1.382	1.394	1.387	1.369	1.345	1.317
848.9 eV	γ	1.89-1	6.14-2	-6.71-2	8.80-3	1.69-1	3.55-1	5.43-1	7.23-1	8.94-1	1.05+0
	δ	6.79 - 2	1.25-2	1.65 - 2	3.64 - 2	5.41-2	6.89-2	8.13-2	9.26 - 2	1.03-1	1.14 - 1
4d _{5/2}	σ	2.385+2	1.556+2	7.200+1	3.797+1	2.209+1	1.381+1	9.115+0	6.280+0	4.479+0	3.287+0
$E_b =$	β	0.847	1.138	1.336	1.378	1.371	1.343	1.307	1.266	1.225	1.184
801.5 eV	γ	1.92-1	1.91-2	-5.43-2	7.42-2	2.64-1	4.63-1	6.52-1	8.25-1	9.84-1	1.13+0
•	δ	4.33-2	9.80-3	1.55-2	3.15-2	4.76-2	6.31-2	7.79-2	9.24-2	1.07-1	1.22-1
$4f_{5/2}$	σ	3.088+2	1.365+2	3.876+1	1.480+1	6.744+0	3.464+0	1.942+0	1.163+0	7.345-1	4.839-1
$E_b =$	β	0.900	1.009	1.054	1.021	0.965	0.905	0.846	0.790	0.737	0.687
437.4 eV	γ	1.22-2	1.32-1	4.02-1	6.46-1	8.47-1	1.01+0	1.15+0	1.27+0	1.36+0	1.44+0
-	δ	4.84-2	7.49-2	1.18-1	1.55-1	1.87-1	2.18-1	2.48-1	2.77-1	3.05-1	3.31-1
	0	1.01 2									

Tab	nle 1	l (c	nnt	inı	ed)

$4f_{7/2}$ $E_b = 425.2 \text{ eV}$	σ β γ δ	3.895+2 0.927 1.99-2 5.03-2	1.708+2 1.022 1.50-1 7.61-2	4.808+1 1.047 4.30-1 1.18-1	1.822+1 1.005 6.76-1 1.55-1	8.250+0 0.946 8.78-1 1.88-1	4.213+0 0.885 1.04+0 2.19-1	2.349+0 0.827 1.18+0 2.51-1	1.400+0 0.773 1.29+0 2.82-1	8.802-1 0.723 1.39+0 3.11-1	5.775-1 0.676 1.46+0 3.39-1
5s _{1/2}	σ	9.602+0	6.280+0	3.344+0	2.101+0	1.450+0	1.064+0	8.139-1	6.428-1	5.202-1	4.293-1
$E_b = 351.9 \text{ eV}$	$eta \ \gamma \ \delta$	1.563 7.03-1 1.54-3	1.616 6.85-1 -1.97-4	1.672 5.78-1 -2.58-3	1.701 4.53-1 -4.20-3	1.720 3.31-1 -5.44-3	1.736 2.21-1 -6.45-3	1.749 1.24-1 -7.30-3	1.762 4.22-2 -8.00-3	1.773 -2.56-2 -8.59-3	1.783 -8.04- -9.11-
$5p_{1/2}$ $E_b =$	σ β	8.580+0 1.255	6.182+0 1.452	3.668+0 1.614	2.429+0 1.673	1.722+0 1.696	1.279+0 1.704	9.823-1 1.704	7.746-1 1.698	6.238-1 1.689	5.112-1 1.677
282.5 eV	γ δ	6.47 - 1 $-4.61 - 3$	5.53-1 -1.41-2	2.95-1 $-1.66-2$	1.20-1 -1.54-2	2.93-2 -1.43-2	2.08-4 $-1.33-2$	1.31-2 -1.24-2	5.37-2 -1.14-2	1.12-1 -1.01-2	1.83-1 -8.56-
5p _{3/2}	σ	3.044+1	1.941+1	9.815+0	5.851+0	3.839+0	2.682+0	1.959+0	1.480+0	1.149+0	9.113-1
$E_b =$	β	1.233	1.394	1.565	1.654	1.707	1.741	1.762	1.775	1.781	1.783
215.3 eV	$\frac{\gamma}{\delta}$	3.44-1 5.44-3	2.59-1 -3.53-3	8.35-2 $-4.86-3$	-1.90-2 $1.15-4$	-5.37-2 5.94-3	-3.87-2 1.13-2	1.07-2 1.59-2	8.30-2 1.98-2	1.71-1 2.31-2	2.68-1 2.59-2
5d _{3/2}	σ	3.190+1	2.005+1	9.293+0	5.008+0	2.980+0	1.901+0	1.277+0	8.939-1	6.464-1	4.803-
$E_b =$	β	1.019	1.198	1.358	1.416	1.432	1.427	1.409	1.385	1.356	1.324
116.0 eV	δ	8.34-2 $-1.72-3$	-1.31-2 1.50-3	-2.72-2 $1.98-2$	8.79-2 3.76-2	2.55-1 5.27-2	4.36-1 6.56-2	6.15-1 7.71-2	7.89-1 8.80-2	9.53-1 9.87-2	1.11+0 1.09-1
5d _{5/2}	σ	4.774+1	2.916+1	1.304+1	6.865+0	4.015+0	2.525+0	1.676+0	1.161+0	8.316-1	6.125-
$E_b =$	β	1.267	1.369	1.428	1.422	1.392	1.352	1.309	1.265	1.221	1.178
105.2 eV	δ	4.33-2 4.54-5	-3.52-2 3.57-3	4.69-3 1.73-2	1.59-1 3.21-2	3.46-1 4.69-2	5.34-1 6.14-2	7.12-1 7.57-2	8.76-1 $9.02-2$	1.03+0 1.05-1	1.17+0 1.20-1
$5f_{5/2}$	σ	2.189+1	1.025+1	3.125+0	1.246+0	5.843-1	3.063-1	1.742-1	1.055-1	6.713-2	4.450-2
$E_b =$	β	1.070	1.109	1.090	1.033	0.967	0.903	0.842	0.786	0.733	0.683
6.0 eV	$_{\delta}^{\gamma}$	7.50-2 4.82-2	1.97—1 7.13—2	4.50-1 1.12-1	6.74-1 1.49-1	8.64-1 1.82-1	1.02+0 2.13-1	1.16+0 2.43-1	1.27+0 2.73-1	1.37+0 3.02-1	1.45+0 3.28-1
6s _{1/2}	σ	2.029+0	1.297+0	6.739-1	4.180-1	2.864-1	2.091-1	1.595-1	1.257-1	1.016-1	8.370-
$E_b =$	β	1.593	1.636	1.683	1.709	1.727	1.741	1.753	1.765	1.775	1.785
48.6 eV	$_{\delta}^{\gamma}$	6.44-1 5.70-4	6.23-1 -8.77-4	5.24-1 -2.94-3	4.07 - 1 $-4.42 - 3$	2.93-1 -5.58-3	1.89-1 -6.54-3	9.88-2 $-7.35-3$	2.18-2 -8.04-3	-4.21-2 $-8.63-3$	-9.37- -9.14-
$6p_{1/2}$	σ	1.616+0	1.130+0	6.512-1	4.254-1	2.994-1	2.214-1	1.696-1	1.335-1	1.074-1	8.789—
$E_b =$	β	1.352	1.513	1.644	1.691	1.709	1.713	1.711	1.703	1.693	1.680
30.6 eV	δ	6.01-1 $-1.39-2$	4.91-1 $-1.77-2$	2.50-1 $-1.71-2$	9.51-2 -1.53-2	1.87 - 2 $-1.41 - 2$	-1.56-3 $-1.33-2$	1.70-2 -1.24-2	6.14-2 $-1.15-2$	1.23-1 -1.03-2	1.95-1 -8.78-
$6p_{3/2}$	σ	4.483+0	2.821+0	1.407+0	8.334-1	5.449-1	3.800-1	2.773-1	2.094-1	1.624-1	1.288-
$E_b =$	β	1.299	1.439	1.590	1.671	1.719	1.749	1.769	1.780	1.785	1.786
18.4 eV	δ	3.16-1 $-9.01-4$	2.28-1 $-6.18-3$	6.43-2 $-5.06-3$	-2.64-2 $4.02-4$	-5.31-2 $6.22-3$	-3.34-2 $1.15-2$	1.91-2 1.60-2	9.39-2 1.98-2	1.83-1 2.30-2	2.81-1 2.57-2
7s _{1/2}	σ	1.520-1	9.674-2	5.005-2	3.095-2	2.117-2	1.544-2	1.177-2	9.275-3	7.492-3	6.174-
$E_b = 6.0 \text{ eV}$	β	1.595	1.638	1.683	1.708	1.727	1.742	1.756	1.767	1.776	1.785
6.0 ev	$\frac{\gamma}{\delta}$	6.41-1 $4.90-4$	6.20-1 $-9.39-4$	5.22-1 $-2.98-3$	4.05-1 $-4.47-3$	2.90-1 $-5.62-3$	1.86 - 1 $-6.54 - 3$	9.65-2 $-7.30-3$	2.08-2 $-8.00-3$	-4.26-2 $-8.61-3$	-9.46- -9.19-
Z= 95, Am: [F	Rn]5f ⁶ _{5/2}										
Chall		k (eV) 1500	2000	2000	4000	5000	6000	7000	9000	0000	10000
Shell 4p _{1/2}	σ	1.986+1	2000 1.827+1	3000 1.323+1	9.481+0	5000 6.995+0	5.319+0	7000 4.150+0	8000 3.308+0	9000 2.686+0	10000 2.215+0
$E_b =$	β		0.842	1.381	1.548	1.617	1.651	1.666	1.672	1.671	1.665
1435.1 eV	$\delta \gamma$	-6.14-1 $2.94-1$	6.72-1 8.99-2	6.31-1 3.83-4	3.33-1 -1.27-2	1.41-1 $-1.45-2$	4.21-2 $-1.42-2$	8.38 - 3 $-1.33 - 2$	1.84-2 $-1.22-2$	5.72-2 $-1.08-2$	1.14-1 -9.12-
$4p_{3/2}$	σ	1.063+2	7.469+1	4.097+1	2.523+1	1.683+1	1.187+1	8.723+0	6.620+0	5.153+0	4.097+0
$E_b =$	β	0.496	1.020	1.383	1.543	1.631	1.685	1.721	1.744	1.758	1.765
1168.0 eV	$\gamma \\ \delta$	2.12-1 1.26-1	4.22-1 4.33-2	2.44-1 2.40-3	6.20-2 $-6.89-4$	−3.31−2 3.78−3	-5.93-2 9.54-3	-3.72-2 1.50-2	1.77-2 1.98-2	9.40-2 2.38-2	1.84-1 2.72-2
4d _{3/2}	σ	1.575+2	1.082+2	5.298+1	2.887+1	1.720+1	1.095+1	7.340+0	5.123+0	3.697+0	2.741+0
$E_b =$	β	0.443	0.855	1.197	1.326	1.378	1.394	1.390	1.374	1.352	1.326
880.4 eV	$\frac{\gamma}{\delta}$	1.90-1 8.04-2	7.73-2 1.51-2	-6.74-2 $1.53-2$	-5.82-3 3.50-2	1.45-1 5.30-2	3.27-1 6.81-2	5.14-1 8.08-2	6.93-1 9.20-2	8.63-1 1.02-1	1.02+0 1.13-1
4d _{5/2}	σ	2.428+2	1.597+2	7.452+1	3.951+1	2.308+1	1.448+1	9.581+0	6.615+0	4.727+0	3.474+0
$E_b =$	β	0.808	1.118	1.330	1.378	1.374	1.349	1.314	1.275	1.234	1.194
830.0 eV	$_{\delta}^{\gamma}$	2.07-1 5.08-2	3.35-2 1.10-2	-5.90-2 $1.46-2$	5.78-2 3.02-2	2.42-1 4.61-2	4.39-1 6.16-2	6.28-1 7.64-2	8.03-1 9.07-2	9.61-1 1.05-1	1.11+0 1.19-1
$4f_{5/2}$	σ	3.291+2	1.462+2	4.182+1	1.605+1	7.345+0	3.785+0	2.127+0	1.277+0	8.077-1	5.330-
$E_b =$	β	0.883	1.001	1.054	1.026	0.972	0.913	0.854	0.799	0.747	0.697
463.3 eV	γ	-5.88-4	1.15-1	3.83-1	6.28-1	8.33-1	1.00+0	1.14+0	1.26+0	1.36+0	1.44+0
$4f_{7/2}$	δ	4.53-2	7.22-2	1.15-1	1.52-1	1.85-1	2.15-1	2.44-1	2.73-1	3.01-1	3.28-1
41- /n	σ	4.147+2	1.828+2	5.181+1	1.974+1	8.976+0	4.599+0	2.571+0	1.536+0	9.671 - 1	6.354 -

(continued on next page)

0.953

8.65 - 1

1.86 - 1

0.892

1.03+0

2.17 - 1

0.835

1.17+0

2.47 - 1

0.781

1.29+0

2.78 - 1

1.010

6.60 - 1

1.52 - 1

Table 1 (continued)

β

γ δ

 $E_b =$

449.0 eV

0.914

6.34 - 3

4.73 - 2

1.016

1.32 - 1

7.36 - 2

1.049

4.11 - 1

1.16 - 1

0.685

1.46+0

3.35 - 1

0.732

1.38+0

3.07 - 1

	δ	4.73-2	7.36-2	1.16 - 1	1.52 - 1	1.86 - 1	2.17 - 1	2.47 - 1	2.78 - 1	3.07 - 1	3.35 - 1
5s _{1/2}	σ	9.787+0	6.419+0	3.427+0	2.156+0	1.490+0	1.094+0	8.384-1	6.629 - 1	5.370-1	4.435 - 1
$E_b =$	β	1.527	1.587	1.648	1.680	1.702	1.718	1.732	1.744	1.756	1.767
373.0 eV	$\gamma \over \delta$	7.19-1 1.98-3	7.07-1	6.07-1	4.83-1 -4.29-3	3.63-1	2.52-1	1.53-1	6.88-2	-2.27-3 $-9.05-3$	-6.07 - 2
			5.01-5	-2.54-3		-5.63-3	-6.72-3	-7.64-3	-8.40-3		-9.63-3
$5p_{1/2}$	σ	8.619+0	6.249+0 1.426	3.738+0	2.489+0	1.772+0	1.321+0	1.018+0 1.704	8.045-1	6.494-1	5.332-1
$E_b = 303.0 \text{ eV}$	β	1.210 6.72-1	1.426 5.89—1	1.601 3.28-1	1.666 1.43-1	1.692 4.21-2	1.703 3.80-3	1.704 8.80—3	1.700 4.31-2	1.692 9.66-2	1.681 1.63-1
303.0 CV	$_{\delta}^{\gamma}$	-4.15-3	-1.50-2	-1.78-2	-1.65-2	-1.52-2	-1.42-2	-1.32-2	-1.22-2	-1.09-2	-9.47 - 3
5p _{3/2}	σ	3.147+1	2.011+1	1.019+1	6.087+0	4.000+0	2.799+0	2.048+0	1.550+0	1.204+0	9.561-1
$E_b =$	β	1.209	1.374	1.550	1.642	1.698	1.734	1.757	1.771	1.779	1.782
216.4 eV	γ	3.49 - 1	2.69 - 1	9.47 - 2	-1.19 - 2	-5.24-2	-4.35 - 2	4.12 - 4	6.81 - 2	1.51 - 1	2.45 - 1
	δ	6.25 - 3	-3.39 - 3	-5.34 - 3	-5.04 - 4	5.41 - 3	1.10 - 2	1.58 - 2	1.99 - 2	2.33-2	2.63 - 2
5d _{3/2}	σ	3.329+1	2.103+1	9.811+0	5.312+0	3.174+0	2.031+0	1.369+0	9.603 - 1	6.959 - 1	5.180 - 1
$E_b =$	β	0.998	1.182	1.349	1.412	1.432	1.430	1.415	1.392	1.365	1.335
118.0 eV	γ	9.41-2	-6.47-3	-3.24-2	7.32-2	2.34-1	4.12-1	5.89-1	7.61-1	9.24-1	1.08+0
	δ	-1.45-3	8.16-4	1.87-2	3.66-2	5.20-2	6.51-2	7.65-2	8.72-2	9.75-2	1.08-1
$5d_{5/2}$	σ	4.978+1 1.260	3.053+1 1.366	1.373+1 1.429	7.260+0 1.425	4.260+0 1.397	2.688+0 1.359	1.789+0 1.317	1.242+0 1.274	8.912-1 1.231	6.575-1 1.189
$E_b = 107.9 \text{ eV}$	β γ	5.29–2	-3.16-2	-2.87 - 3	1.425	3.27-1	5.14-1	6.91–1	8.56—1	1.231	1.15+0
107.5 CV	δ	8.25-5	3.06-3	1.64-2	3.10-2	4.57-2	6.01-2	7.41-2	8.83-2	1.03-1	1.17-1
5f _{5/2}	σ	2.462+1	1.161+1	3.575+0	1.435+0	6.769-1	3.564-1	2.034-1	1.235-1	7.881-2	5.236-2
$E_b =$	β	1.068	1.110	1.095	1.040	0.975	0.911	0.851	0.795	0.742	0.692
$E_b = 6.0 \text{ eV}$	γ	6.52 - 2	1.85 - 1	4.36 - 1	6.61 - 1	8.51 - 1	1.01+0	1.15+0	1.27+0	1.36+0	1.45+0
	δ	4.60-2	6.90-2	1.09-1	1.46-1	1.79-1	2.10-1	2.40-1	2.69-1	2.97-1	3.24-1
5f _{7/2}	σ	2.918+1	1.365+1	4.155+0	1.653+0	7.735 - 1	4.045 - 1	2.294 - 1	1.385 - 1	8.797 - 2	5.818 - 2
$E_b = 6.0 \text{ eV}$	β	1.083	1.112	1.082	1.020	0.954	0.889	0.830	0.776	0.726	0.680
6.0 eV	$\gamma \over \delta$	7.23-2 4.77-2	2.00-1 6.99-2	4.61-1 1.09-1	6.90-1	8.83-1	1.04+0	1.18+0	1.29+0	1.39+0	1.47+0
C-					1.46-1	1.80-1	2.12-1	2.43-1	2.74-1	3.04-1	3.32-1
6s _{1/2}	$\frac{\sigma}{eta}$	2.086+0 1.562	1.336+0 1.610	6.956-1 1.661	4.319-1 1.689	2.962-1 1.708	2.165-1 1.723	1.654-1 1.736	1.305-1 1.748	1.055-1 1.759	8.701-2 1.769
$E_b = 50.4 \text{ eV}$	γ	6.56-1	6.41-1	5.49-1	4.34-1	3.21-1	2.17-1	1.25-1	4.59-2	-2.09-2	-7.56-2
	δ	8.12-4	-7.56-4	-2.98 - 3	-4.56-3	-5.79-3	-6.83-3	-7.71-3	-8.46 - 3	-9.10-3	-9.66-3
6p _{1/2}	σ	1.637+0	1.150+0	6.668-1	4.376-1	3.091-1	2.293-1	1.762-1	1.390-1	1.121-1	9.192-2
$E_b =$	β	1.323	1.494	1.635	1.686	1.706	1.712	1.711	1.705	1.696	1.684
31.1 eV	γ	6.24-1	5.20-1	2.77-1	1.14-1	2.86-2	4.20-4	1.18-2	5.03-2	1.07-1	1.75-1
	δ	-1.48-2	-1.91-2	-1.83-2	-1.64-2	-1.50-2	-1.40-2	-1.32-2	-1.22-2	-1.10-2	-9.63-3
$6p_{3/2}$	σ	4.654+0	2.931+0	1.465+0	8.687-1	5.687-1	3.971-1	2.902-1	2.194-1	1.704-1	1.352-1
$E_b = 18.1 \text{ eV}$	β	1.277 3.24-1	1.421 2.39-1	1.576 7.53-2	1.659 -2.00-2	1.710 -5.26-2	1.743 -3.88-2	1.764 8.10-3	1.777 7.80—2	1.783 1.63-1	1.786 2.58-1
10.1 6	$_{\delta}^{\gamma}$	-5.17-4	-6.29-3	-5.66-3	-2.50-2 $-2.50-4$	5.69-3	1.11-2	1.59-2	1.99-2	2.33-2	2.61-2
7s _{1/2}	σ	1.525-1	9.723-2	5.040-2	3.121-2	2.136-2	1.560-2	1.190-2	9.385-3	7.588-3	6.259-3
$E_b =$	β	1.564	1.612	1.661	1.688	1.708	1.724	1.739	1.751	1.761	1.770
6.0 eV	γ	6.53 - 1	6.38 - 1	5.46 - 1	4.32 - 1	3.18 - 1	2.14 - 1	1.22 - 1	4.45 - 2	-2.13-2	-7.61-2
	δ	7.18 - 4	-8.22 - 4	-3.01-3	-4.61-3	-5.86 - 3	-6.85 - 3	-7.66 - 3	-8.41-3	-9.05 - 3	-9.67 - 3
Z= 96, Cm: [R	n]5f ⁶ _{5/2}	5f _{7/2} 6d _{3/2} 7s _{1/2}	2								
	5,2	k (eV)									
Shell		1500	2000	3000	4000	5000	6000	7000	8000	9000	10000
	~	1300	1.766+1	1.307+1	9.481+0	7.047+0	5.386+0	4.219+0	3.375+0	2.748+0	2.272+0
$\begin{array}{l} 4p_{1/2} \\ E_b = \end{array}$	$\frac{\sigma}{eta}$		0.736	1.307+1	9.481+0 1.527	7.047+0 1.605	5.386+0 1.643	4.219+0 1.662	3.375+0 1.670	2.748+0 1.671	2.272+0 1.667
1499.9 eV	γ		6.25-1	6.81-1	3.79-1	1.71-1	5.88-2	1.38-2	1.46-2	4.56-2	9.65-2
	δ		1.09 - 1	2.42 - 3	-1.32 - 2	-1.56-2	-1.53-2	-1.43-2	-1.31-2	-1.17 - 2	-1.00-2
4p _{3/2}	σ	1.075+2	7.594+1	4.188+1	2.588+1	1.730+1	1.223+1	9.000+0	6.839+0	5.331+0	4.244+0
$E_b =$	β	0.398	0.970	1.353	1.522	1.615	1.673	1.712	1.737	1.754	1.763
1211.0 eV	γ	1.55-1	4.23-1	2.64-1	7.81-2	-2.51-2	-5.93-2	-4.43-2	4.15-3	7.48-2	1.60-1
	δ	1.42-1	4.96-2	3.41-3	-1.08-3	3.09-3	8.93-3	1.46-2	1.96-2	2.38-2	2.74-2
$4d_{3/2}$	σ	1.593+2	1.106+2	5.476+1	3.003+1	1.796+1	1.148+1	7.713+0	5.398+0	3.903+0	2.899+0
$E_b = 919.3 \text{ eV}$	β	0.380 1.86-1	0.814 9.41-2	1.175 -6.64-2	1.313 -1.91-2	1.372 1.23-1	1.392 2.99-1	1.392 4.81-1	1.379 6.60-1	1.359 8.31-1	1.335
J 13.3 EV	$_{\delta}^{\gamma}$	9.55-2	9.41-2 1.85-2	-6.64-2 1.41-2	-1.91-2 3.37-2	5.19-2	2.99—1 6.71—2	4.81—1 7.98—2	9.11–2	8.31-1 1.02-1	9.92-1 1.12-1
4d _{5/2}	σ	2.470+2	1.637+2	7.710+1	4.110+1	2.410+1	1.516+1	1.006+1	6.961+0	4.983+0	3.669+0
$E_b =$	β	0.766	1.037+2	1.323	1.377	1.377	1.354	1.321	1.284	1.244	1.204
864.8 eV	γ	2.20-1	4.93-2	-6.28-2	4.29-2	2.21-1	4.15-1	6.02-1	7.77 – 1	9.38-1	1.09+0
	δ	5.97-2	1.27 - 2	1.37 - 2	2.90-2	4.48 - 2	5.99-2	7.44-2	8.86-2	1.03-1	1.18 - 1
4f _{5/2}	σ	3.475+2	1.554+2	4.481+1	1.730+1	7.954+0	4.114+0	2.319+0	1.396+0	8.846-1	5.847-1
$E_b =$	β	0.867	0.993	1.055	1.030	0.979	0.921	0.864	0.809	0.756	0.706
487.4 eV	γ	-1.20-2	9.93 - 2	3.66 - 1	6.11 - 1	8.16 - 1	9.87 - 1	1.13+0	1.25+0	1.35+0	1.44+0

able 1 (continu	ued) δ	4.22-2	6.96-2	1.13-1	1.50-1	1.82-1	2.12-1	2.42-1	2.71-1	2.98-1	3.24-1
$4f_{7/2}$	σ	4.380+2	1.942+2	5.549+1	2.126+1	9.711+0	4.994+0	2.800+0	1.677+0	1.058+0	6.962-1
$E_b =$	β	0.900	1.010	1.050	1.015	0.959	0.900	0.843	0.790	0.740	0.693
472.7 eV	γ	-6.07 - 3	1.16-1	3.95-1	6.44-1	8.50-1	1.02+0	1.16+0	1.28+0	1.38+0	1.46+0
r-	δ	4.44-2	7.11–2	1.14-1	1.50-1	1.82-1	2.14-1	2.45-1	2.75-1	3.04-1	3.31-1
$5s_{1/2}$ $E_b =$	$\frac{\sigma}{\beta}$	9.951+0 1.488	6.545+0 1.554	3.506+0 1.622	2.209+0 1.657	1.529+0 1.680	1.124+0 1.698	8.625-1 1.714	6.827-1 1.727	5.536-1 1.740	4.577 – 1 1.751
392.7 eV	γ	7.31-1	7.27-1	6.36-1	5.16-1	3.95-1	2.83-1	1.83-1	9.64-2	2.29-2	-3.84-2
	δ	2.43 - 3	3.28 - 4	-2.48 - 3	-4.38 - 3	-5.83 - 3	-7.01 - 3	-7.98 - 3	-8.80 - 3	-9.49 - 3	-1.01-2
$5p_{1/2}$	σ	8.636+0	6.298+0	3.799+0	2.544+0	1.819+0	1.360+0	1.051+0	8.334-1	6.744-1	5.551-1
$E_b = 317.7 \text{ eV}$	β	1.170 6.91-1	1.398 6.21-1	1.586 3.60-1	1.656 1.66-1	1.687 5.60-2	1.700 9.18-3	1.703 6.68-3	1.701 3.43-2	1.694 8.21-2	1.684 1.44-1
317.7 EV	$_{\delta}^{\gamma}$	-3.92-3	-1.58-2	-1.92-2	-1.78-2	-1.63-2	-1.51-2	-1.40-2	-1.29-2	-1.17-2	-1.03-2
5p _{3/2}	σ	3.269+1	2.092+1	1.063+1	6.356+0	4.183+0	2.930+0	2.147+0	1.626+0	1.265+0	1.006+0
$E_b =$	β	1.179	1.348	1.531	1.627	1.687	1.725	1.751	1.768	1.777	1.782
231.7 eV	$_{\delta}^{\gamma}$	3.57-1 7.51-3	2.82-1 $-3.02-3$	1.08-1 -5.88-3	-3.60-3 $-1.22-3$	-5.03-2 4.79-3	-4.75-2 $1.05-2$	-9.47-3 1.56-2	5.28-2 1.98-2	1.32-1 2.35-2	2.22-1 $2.66-2$
5d _{3/2}	σ	3.491+1	2.216+1	1.041+1	5.663+0	3.395+0	2.179+0	1.473+0	1.036+0	7.522-1	5.609-1
$E_b =$	β	0.972	1.162	1.337	1.407	1.431	1.432	1.419	1.399	1.374	1.345
130.4 eV	γ	1.07-1	1.55 - 3	-3.70-2	5.92 - 2	2.12 - 1	3.85 - 1	5.61 - 1	7.32 - 1	8.97 - 1	1.05+0
	δ	-9.78-4	1.08-4	1.77-2	3.57-2	5.11-2	6.42-2	7.57-2	8.65-2	9.70-2	1.07-1
$5d_{5/2}$ $E_b =$	$\frac{\sigma}{eta}$	5.213+1 1.252	3.211+1 1.361	1.453+1 1.430	7.711+0 1.429	4.540+0 1.403	2.872+0 1.366	1.917+0 1.325	1.334+0 1.283	9.591-1 1.241	7.089-1 1.199
$E_b = 113.1 \text{ eV}$	P γ	6.23-2	-2.76-2	-9.43-3	1.429 1.31–1	3.09-1	4.93–1	6.69—1	8.34—1	9.88-1	1.13+0
	δ	1.68-4	2.60-3	1.56-2	3.00-2	4.44-2	5.84-2	7.23–2	8.64-2	1.01-1	1.16-1
5f _{5/2}	σ	2.876+1	1.368+1	4.254+0	1.720+0	8.159-1	4.316-1	2.473-1	1.506-1	9.638-2	6.417-2
$E_b = 6.0 \text{ eV}$	β	1.066	1.111	1.100	1.046	0.983	0.920	0.861	0.805	0.752	0.701
6.0 ev	$\frac{\gamma}{\delta}$	5.66-2 4.39-2	1.74-1 6.71-2	4.24-1 1.07-1	6.47-1 1.43-1	8.37-1 1.76-1	1.00+0 2.07-1	1.14+0 2.37-1	1.26+0 2.67-1	1.36+0 2.94-1	1.44+0 3.20-1
5f _{7/2}	σ	3.531+1	1.665+1	5.120+0	2.051+0	9.651-1	5.071-1	2.887-1	1.749-1	1.113-1	7.378-2
$E_b =$	β	1.083	1.115	1.087	1.026	0.960	0.897	0.839	0.785	0.735	0.688
6.0 eV	γ	6.31-2	1.89-1	4.50-1	6.78-1	8.70-1	1.03+0	1.17+0	1.29+0	1.38+0	1.46+0
	δ	4.58-2	6.81-2 1.407+0	1.07-1 7.345-1	1.43-1 4.565-1	1.77-1	2.09-1 2.293-1	2.40-1	2.71-1	3.00-1	3.28-1 9.245-2
$6s_{1/2}$ $E_b =$	$\frac{\sigma}{eta}$	2.194+0 1.528	1.407+0	7.345 – 1 1.636	4.565 — I 1.667	3.134-1 1.687	2.293—1 1.704	1.753-1 1.718	1.384-1 1.731	1.120-1 1.743	9.245-2 1.754
56.9 eV	γ	6.70-1	6.61-1	5.76-1	4.64-1	3.51-1	2.47-1	1.53-1	7.14-2	2.37-3	-5.51-2
	δ	1.09-3	-5.79 - 4	-2.98 - 3	-4.69 - 3	-6.03 - 3	-7.14 - 3	-8.08 - 3	-8.87 - 3	-9.55 - 3	-1.02-2
$6p_{1/2}$	σ	1.702+0	1.200+0	7.003-1	4.617-1	3.273-1	2.436-1	1.877-1	1.485-1	1.199-1	9.859-2
$E_b = 32.1 \text{ eV}$	β γ	1.293 6.46-1	1.472 5.49-1	1.622 3.04-1	1.679 1.33-1	1.702 3.99-2	1.711 4.01-3	1.711 8.61-3	1.707 4.10-2	1.698 9.21-2	1.688 1.56-1
32.1 0	δ	-1.58-2	-2.04-2	-1.98-2	-1.76-2	-1.60-2	-1.49-2	-1.40-2	-1.29-2	-1.18-2	-1.04-2
6p _{3/2}	σ	5.081+0	3.205+0	1.604+0	9.527-1	6.245-1	4.366-1	3.194-1	2.417-1	1.879-1	1.493-1
$E_b =$	β	1.254	1.399	1.559	1.646	1.700	1.735	1.758	1.773	1.782	1.785
18.9 eV	$\frac{\gamma}{\delta}$	3.30-1 -8.04-5	2.50-1 $-6.37-3$	8.64-2 $-6.27-3$	-1.33-2 $-9.33-4$	-5.14-2 5.14-3	-4.32-2 $1.08-2$	-1.59-3 1.57-2	6.33-2 1.99-2	1.44-1 2.34-2	2.35-1 $2.64-2$
6d _{3/2}	σ	2.318+0	1.459+0	6.804-1	3.692-1	2.212-1	1.421-1	9.604-2	6.755-2	4.906-2	3.658-2
$E_b =$	β	1.032	1.200	1.358	1.419	1.439	1.438	1.424	1.402	1.375	1.346
6.0 eV	γ	9.49-2	-3.60-3	-3.12-2	6.80-2	2.21 - 1	3.96 - 1	5.74 - 1	7.47 - 1	9.09 - 1	1.06+0
	δ	-4.21-3	-4.23-4	1.78-2	3.54-2	5.05-2	6.37-2	7.57-2	8.64-2	9.62-2	1.06-1
$7s_{1/2}$	σ	1.811 - 1									
L			1.156-1	6.004-2	3.721-2	2.549-2	1.863-2	1.423-2	1.123-2	9.089-3	7.502-3
$E_b = 6.0 \text{ eV}$	β	1.531	1.582 6.58-1	1.636	1.666	1.689	1.707	1.721	1.733	1.743	1.753
$E_b = 6.0 \text{ eV}$			1.582								
6.0 eV	$eta \ \gamma \ \delta$	1.531 6.67-1	1.582 6.58-1 -6.54-4	1.636 5.73-1	1.666 4.60-1	1.689 3.46-1	1.707 2.42-1	1.721 1.50-1	1.733 6.97-2	1.743 1.04-3	1.753 -5.69-2
6.0 eV	$eta \ \gamma \ \delta$	1.531 6.67-1 9.71-4	1.582 6.58-1 -6.54-4	1.636 5.73-1	1.666 4.60-1	1.689 3.46-1	1.707 2.42-1	1.721 1.50-1	1.733 6.97-2	1.743 1.04-3	1.753 -5.69-2
6.0 eV	$eta \ \gamma \ \delta$	$ \begin{array}{r} 1.531 \\ 6.67 - 1 \\ 9.71 - 4 \end{array} $ $ \mathbf{5f}_{7/2}^{2} \mathbf{6d}_{3/2}^{1} \mathbf{7s}_{1/2}^{2} $	1.582 6.58-1 -6.54-4	1.636 5.73-1	1.666 4.60-1	1.689 3.46-1	1.707 2.42-1	1.721 1.50-1	1.733 6.97-2	1.743 1.04-3	1.753 -5.69-2
6.0 eV Z= 97, Bk: [Rt Shell 4p _{3/2}	$\frac{\beta}{\delta}$ n]5 $\mathbf{f}_{5/2}^{6}$	$ \begin{array}{c} 1.531 \\ 6.67 - 1 \\ 9.71 - 4 \end{array} $ $ \begin{array}{c} 5f_{7/2}^2 6d_{3/2}^1 7s_{1/2}^2 \\ \underline{k (eV)} \\ 1500 \\ 1.085 + 2 \end{array} $	1.582 6.58-1 -6.54-4 2000 7.715+1	1.636 5.73-1 -3.02-3 3000 4.277+1	1.666 4.60-1 -4.75-3 4000 2.652+1	1.689 3.46-1 -6.08-3 5000 1.777+1	1.707 2.42-1 -7.14-3 6000 1.258+1	1.721 1.50-1 -8.02-3 7000 9.278+0	1.733 6.97-2 -8.84-3 8000 7.062+0	1.743 1.04-3 -9.56-3 9000 5.511+0	1.753 -5.69-2 -1.02-2 10000 4.392+0
6.0 eV Z= 97, Bk: [Ri Shell $4p_{3/2}$ $E_b =$	β γ δ $n]5f_{5/2}^6$	$ \begin{array}{c} 1.531 \\ 6.67 - 1 \\ 9.71 - 4 \end{array} $ $ \begin{array}{c} \mathbf{5f_{7/2}^2 6d_{3/2}^1 7s_{1/2}^2} \\ \underline{k \text{ (eV)}} \\ 1500 \\ 1.085 + 2 \\ 0.294 \end{array} $	1.582 6.58-1 -6.54-4 2000 7.715+1 0.919	1.636 5.73-1 -3.02-3 3000 4.277+1 1.325	1.666 4.60-1 -4.75-3 4000 2.652+1 1.502	1.689 3.46-1 -6.08-3 5000 1.777+1 1.600	1.707 2.42-1 -7.14-3 6000 1.258+1 1.661	1.721 1.50-1 -8.02-3 7000 9.278+0 1.702	1.733 6.97-2 -8.84-3 8000 7.062+0 1.730	1.743 1.04-3 -9.56-3 9000 5.511+0 1.748	1.753 -5.69-2 -1.02-2 10000 4.392+0 1.760
6.0 eV Z= 97, Bk: [Rt Shell 4p _{3/2}	β γ δ n]5 $f_{5/2}^6$:	$ \begin{array}{c} 1.531 \\ 6.67 - 1 \\ 9.71 - 4 \end{array} $ $ \begin{array}{c} \mathbf{567_{7/2}} \ \mathbf{6d_{3/2}} \ \mathbf{7s_{1/2}^2} \\ \underline{k \ (eV)} \\ 1500 \\ 1.085 + 2 \\ 0.294 \\ 9.10 - 2 \end{array} $	1.582 6.58-1 -6.54-4 2000 7.715+1 0.919 4.20-1	1.636 5.73-1 -3.02-3 3000 4.277+1 1.325 2.83-1	1.666 4.60-1 -4.75-3 4000 2.652+1 1.502 9.46-2	1.689 3.46-1 -6.08-3 5000 1.777+1 1.600 -1.57-2	1.707 2.42-1 -7.14-3 6000 1.258+1 1.661 -5.77-2	1.721 1.50-1 -8.02-3 7000 9.278+0 1.702 -5.01-2	1.733 6.97-2 -8.84-3 8000 7.062+0 1.730 -7.91-3	1.743 1.04-3 -9.56-3 9000 5.511+0 1.748 5.76-2	1.753 -5.69-2 -1.02-2 10000 4.392+0 1.760 1.38-1
6.0 eV Z= 97, Bk: [Ri Shell $4p_{3/2}$ $E_b = 1248.0 \text{ eV}$	β γ δ $n]5f_{5/2}^6$ β γ β γ β	$ \begin{array}{c} 1.531 \\ 6.67 - 1 \\ 9.71 - 4 \end{array} $ $ \begin{array}{c} 5f_{7/2}^2 6d_{3/2}^1 7s_{1/2}^2 \\ \underline{k \text{ (eV)}} \\ 1500 \\ 1.085 + 2 \\ 0.294 \\ 9.10 - 2 \\ 1.58 - 1 \end{array} $	1.582 6.58-1 -6.54-4 2000 7.715+1 0.919 4.20-1 5.61-2	1.636 5.73-1 -3.02-3 3000 4.277+1 1.325 2.83-1 4.48-3	1.666 4.60-1 -4.75-3 4000 2.652+1 1.502 9.46-2 -1.43-3	1.689 3.46-1 -6.08-3 5000 1.777+1 1.600 -1.57-2 2.39-3	1.707 2.42-1 -7.14-3 6000 1.258+1 1.661 -5.77-2 8.26-3	1.721 1.50-1 -8.02-3 7000 9.278+0 1.702 -5.01-2 1.41-2	8000 7.062+0 1.730 -7.91-3 1.93-2	9000 5.511+0 1.748 5.76-2 2.38-2	1.753 -5.69-2 -1.02-2 10000 4.392+0 1.760 1.38-1 2.76-2
6.0 eV Z= 97, Bk: [Rt Shell $4p_{3/2}$ $E_b =$	β γ δ n]5 $f_{5/2}^6$:	$ \begin{array}{c} 1.531 \\ 6.67 - 1 \\ 9.71 - 4 \end{array} $ $ \begin{array}{c} \mathbf{567_{7/2}} \ \mathbf{6d_{3/2}} \ \mathbf{7s_{1/2}^2} \\ \hline k \ (eV) \\ \hline 1500 \\ 1.085 + 2 \\ 0.294 \\ 9.10 - 2 \end{array} $	1.582 6.58-1 -6.54-4 2000 7.715+1 0.919 4.20-1	1.636 5.73-1 -3.02-3 3000 4.277+1 1.325 2.83-1	1.666 4.60-1 -4.75-3 4000 2.652+1 1.502 9.46-2	1.689 3.46-1 -6.08-3 5000 1.777+1 1.600 -1.57-2	1.707 2.42-1 -7.14-3 6000 1.258+1 1.661 -5.77-2	1.721 1.50-1 -8.02-3 7000 9.278+0 1.702 -5.01-2	1.733 6.97-2 -8.84-3 8000 7.062+0 1.730 -7.91-3	1.743 1.04-3 -9.56-3 9000 5.511+0 1.748 5.76-2	1.753 -5.69-2 -1.02-2 10000 4.392+0 1.760 1.38-1
6.0 eV Z= 97, Bk: [Ri Shell $4p_{3/2}$ $E_b = 1248.0 \text{ eV}$ $4d_{3/2}$	$ \begin{array}{c} \beta \\ \gamma \\ \delta \end{array} $ $ \begin{array}{c} \sigma \\ \beta \\ \gamma \\ \delta \end{array} $ $ \begin{array}{c} \sigma \\ \beta \\ \gamma \\ \delta \end{array} $	1.531 6.67-1 9.71-4 56 ⁷ _{7/2} 6d ¹ _{3/2} 7s ² _{1/2} k (eV) 1500 1.085+2 0.294 9.10-2 1.58-1 1.610+2 0.313 1.76-1	1.582 6.58-1 -6.54-4 2000 7.715+1 0.919 4.20-1 5.61-2 1.130+2 0.770 1.12-1	1.636 5.73-1 -3.02-3 3000 4.277+1 1.325 2.83-1 4.48-3 5.658+1 1.153 -6.35-2	1.666 4.60-1 -4.75-3 4000 2.652+1 1.502 9.46-2 -1.43-3 3.122+1 1.301 -3.18-2	1.689 3.46-1 -6.08-3 5000 1.777+1 1.600 -1.57-2 2.39-3 1.876+1 1.365 1.00-1	1.707 2.42-1 -7.14-3 6000 1.258+1 1.661 -5.77-2 8.26-3 1.203+1 1.390 2.71-1	1.721 1.50-1 -8.02-3 7000 9.278+0 1.702 -5.01-2 1.41-2 8.106+0 1.393 4.51-1	1.733 6.97-2 -8.84-3 8000 7.062+0 1.730 -7.91-3 1.93-2 5.685+0 1.383 6.28-1	1.743 1.04-3 -9.56-3 9000 5.511+0 1.748 5.76-2 2.38-2 4.118+0 1.366 7.98-1	1.753 -5.69-2 -1.02-2 10000 4.392+0 1.760 1.38-1 2.76-2 3.064+0 1.343 9.59-1
6.0 eV Z= 97, Bk: [Rn Shell $4p_{3/2}$ $E_b = 1248.0 \text{ eV}$ $4d_{3/2}$ $E_b = 957.7 \text{ eV}$	β γ δ $n]5f_{5/2}^6$ β γ δ δ δ δ	$ \begin{array}{c} 1.531 \\ 6.67 - 1 \\ 9.71 - 4 \end{array} $ $ \begin{array}{c} \mathbf{5f_{7/2}^2 6d_{3/2}^1 7s_{1/2}^2} \\ \underline{k \text{ (eV)}} \\ 1500 \\ 1.085 + 2 \\ 0.294 \\ 9.10 - 2 \\ 1.58 - 1 \end{array} $ $ \begin{array}{c} 1.610 + 2 \\ 0.313 \\ 1.76 - 1 \\ 1.14 - 1 \end{array} $	1.582 6.58-1 -6.54-4 2000 7.715+1 0.919 4.20-1 5.61-2 1.130+2 0.770 1.12-1 2.29-2	1.636 5.73-1 -3.02-3 3000 4.277+1 1.325 2.83-1 4.48-3 5.658+1 1.153 -6.35-2 1.30-2	1.666 4.60-1 -4.75-3 4000 2.652+1 1.502 9.46-2 -1.43-3 3.122+1 1.301 -3.18-2 3.22-2	1.689 3.46-1 -6.08-3 5000 1.777+1 1.600 -1.57-2 2.39-3 1.876+1 1.365 1.00-1 5.07-2	1.707 2.42-1 -7.14-3 6000 1.258+1 1.661 -5.77-2 8.26-3 1.203+1 1.390 2.71-1 6.63-2	1.721 1.50-1 -8.02-3 7000 9.278+0 1.702 -5.01-2 1.41-2 8.106+0 1.393 4.51-1 7.93-2	1.733 6.97-2 -8.84-3 8000 7.062+0 1.730 -7.91-3 1.93-2 5.685+0 1.383 6.28-1 9.06-2	1.743 1.04-3 -9.56-3 9000 5.511+0 1.748 5.76-2 2.38-2 4.118+0 1.366 7.98-1 1.01-1	1.753 -5.69-2 -1.02-2 10000 4.392+0 1.760 1.38-1 2.76-2 3.064+0 1.343 9.59-1 1.11-1
6.0 eV Z= 97, Bk: [Rn Shell $4p_{3/2}$ $E_b = 1248.0 \text{ eV}$ $4d_{3/2}$ $E_b = 957.7 \text{ eV}$	$ \frac{\beta}{\delta} $ $ \gamma \qquad \delta $ $ \mathbf{n]5f_{5/2}^6} \qquad \vdots $ $ \frac{\sigma}{\beta} $ $ \gamma \qquad \delta $ $ \frac{\sigma}{\beta} $ $ \gamma \qquad \delta $ $ \frac{\sigma}{\beta} $ $ \frac{\sigma}{\delta} $	1.531 6.67-1 9.71-4 56 ² 7 _{/2} 6d ¹ _{3/2} 7s ² _{1/2} k (eV) 1500 1.085+2 0.294 9.10-2 1.58-1 1.610+2 0.313 1.76-1 1.14-1 2.511+2	1.582 6.58-1 -6.54-4 2000 7.715+1 0.919 4.20-1 5.61-2 1.130+2 0.770 1.12-1 2.29-2 1.680+2	1.636 5.73-1 -3.02-3 3000 4.277+1 1.325 2.83-1 4.48-3 5.658+1 1.153 -6.35-2 1.30-2 7.985+1	1.666 4.60-1 -4.75-3 4000 2.652+1 1.502 9.46-2 -1.43-3 3.122+1 1.301 -3.18-2 3.22-2 4.278+1	1.689 3.46-1 -6.08-3 5000 1.777+1 1.600 -1.57-2 2.39-3 1.876+1 1.365 1.00-1 5.07-2 2.518+1	1.707 2.42-1 -7.14-3 6000 1.258+1 1.661 -5.77-2 8.26-3 1.203+1 1.390 2.71-1 6.63-2 1.589+1	1.721 1.50-1 -8.02-3 7000 9.278+0 1.702 -5.01-2 1.41-2 8.106+0 1.393 4.51-1 7.93-2 1.057+1	8000 7.062+0 1.730 -7.91-3 1.93-2 5.685+0 1.383 6.28-1 9.06-2 7.328+0	9000 5.511+0 1.748 5.76-2 2.38-2 4.118+0 1.366 7.98-1 1.01-1 5.255+0	1.753 -5.69-2 -1.02-2 10000 4.392+0 1.760 1.38-1 2.76-2 3.064+0 1.343 9.59-1 1.11-1 3.875+0
6.0 eV Z= 97, Bk: [Rr Shell $4p_{3/2}$ $E_b = 1248.0 \text{ eV}$ $4d_{3/2}$ $E_b = 957.7 \text{ eV}$	β γ δ n]5f ⁶ _{5/2} ! σ β γ δ σ β γ δ	$ \begin{array}{c} 1.531 \\ 6.67 - 1 \\ 9.71 - 4 \end{array} $ $ \begin{array}{c} \mathbf{5f_{7/2}^2 6d_{3/2}^1 7s_{1/2}^2} \\ \underline{k \text{ (eV)}} \\ 1500 \\ 1.085 + 2 \\ 0.294 \\ 9.10 - 2 \\ 1.58 - 1 \end{array} $ $ \begin{array}{c} 1.610 + 2 \\ 0.313 \\ 1.76 - 1 \\ 1.14 - 1 \end{array} $	1.582 6.58-1 -6.54-4 2000 7.715+1 0.919 4.20-1 5.61-2 1.130+2 0.770 1.12-1 2.29-2	1.636 5.73-1 -3.02-3 3000 4.277+1 1.325 2.83-1 4.48-3 5.658+1 1.153 -6.35-2 1.30-2	1.666 4.60-1 -4.75-3 4000 2.652+1 1.502 9.46-2 -1.43-3 3.122+1 1.301 -3.18-2 3.22-2	1.689 3.46-1 -6.08-3 5000 1.777+1 1.600 -1.57-2 2.39-3 1.876+1 1.365 1.00-1 5.07-2	1.707 2.42-1 -7.14-3 6000 1.258+1 1.661 -5.77-2 8.26-3 1.203+1 1.390 2.71-1 6.63-2	1.721 1.50-1 -8.02-3 7000 9.278+0 1.702 -5.01-2 1.41-2 8.106+0 1.393 4.51-1 7.93-2	1.733 6.97-2 -8.84-3 8000 7.062+0 1.730 -7.91-3 1.93-2 5.685+0 1.383 6.28-1 9.06-2	1.743 1.04-3 -9.56-3 9000 5.511+0 1.748 5.76-2 2.38-2 4.118+0 1.366 7.98-1 1.01-1	1.753 -5.69-2 -1.02-2 10000 4.392+0 1.760 1.38-1 2.76-2 3.064+0 1.343 9.59-1 1.11-1

Table 1 (contin	ued)										
$4f_{5/2}$	σ	3.691+2	1.660+2	4.819+1	1.869+1	8.629+0	4.478+0	2.530+0	1.526+0	9.689-1	6.414-1
$E_b =$	β	0.849	0.984	1.054	1.034	0.985	0.929	0.872	0.818	0.766	0.716
514.4 eV	δ	-2.38-2 $3.89-2$	8.26-2 $6.68-2$	3.46-1 1.11-1	5.93-1 1.48-1	8.01-1 $1.80-1$	9.74 - 1 $2.10 - 1$	1.12+0 2.39-1	1.24+0 2.67-1	1.35+0 2.94-1	1.43+0 3.20-1
$-4f_{7/2}$	σ	4.657+2	2.075+2	5.965+1	2.297+1	1.053+1	5.433+0	3.054+0	1.833+0	1.158+0	7.634-1
$E_b =$	β	0.884	1.002	1.051	1.019	0.966	0.907	0.851	0.798	0.749	0.702
498.5 eV	δ	-1.91-2 $4.12-2$	9.91-2 6.85-2	3.76-1 1.11-1	6.27 - 1 $1.48 - 1$	8.36-1 1.80-1	1.01+0 2.11-1	1.15+0 2.41-1	1.27+0 2.71-1	1.37+0 3.00-1	1.46+0 3.27-1
$-5s_{1/2}$	σ	1.008+1	6.650+0	3.574+0	2.257+0	1.564+0	1.152+0	8.848-1	7.011-1	5.691-1	4.710-1
$E_b =$	β	1.446	1.520	1.595	1.633	1.658	1.677	1.694	1.708	1.721	1.733
405.0 eV	$\gamma \\ \delta$	7.40-1 $2.94-3$	7.44-1 6.38-4	6.62 - 1 $-2.41 - 3$	5.46-1 -4.45-3	4.27 - 1 $-6.01 - 3$	3.16-1 $-7.28-3$	2.15-1 -8.34-3	1.26-1 $-9.23-3$	4.93-2 $-9.99-3$	-1.50-2 $-1.07-2$
$-5p_{1/2}$	σ	8.619+0	6.323+0	3.846+0	2.590+0	1.860+0	1.396+0	1.083+0	8.608-1	6.983-1	5.759-1
$E_b =$	β	1.126	1.371	1.572	1.648	1.682	1.697	1.702	1.701	1.696	1.687
326.8 eV	$_{\delta}^{\gamma}$	7.08-1 -3.76-3	6.52 - 1 $-1.68 - 2$	3.92 - 1 $-2.06 - 2$	1.91-1 $-1.90-2$	7.18-2 $-1.74-2$	1.62-2 $-1.61-2$	5.91-3 -1.49-2	2.70-2 $-1.38-2$	6.94-2 $-1.26-2$	1.26-1 $-1.12-2$
$-5p_{3/2}$	σ	3.383+1	2.169+1	1.104+1	6.610+0	4.355+0	3.056+0	2.241+0	1.700+0	1.324+0	1.053+0
$E_b =$	β	1.147	1.324	1.513	1.613	1.675	1.716	1.744	1.762	1.774	1.780
245.9 eV	$_{\delta}^{\gamma}$	3.65-1 8.97-3	2.96-1 $-2.62-3$	1.22 - 1 $-6.41 - 3$	5.90-3 $-1.98-3$	-4.71-2 $4.09-3$	-5.07-2 $1.00-2$	-1.84-2 $1.53-2$	3.88-2 1.98-2	1.13-1 2.36-2	1.99-1 2.69-2
5d _{3/2}	σ	3.622+1	2.311+1	1.093+1	5.972+0	3.594+0	2.315+0	1.569+0	1.106+0	8.048-1	6.013-1
$E_b =$	β	0.949	1.144	1.327	1.401	1.429	1.433	1.423	1.405	1.382	1.355
130.4 eV	δ	1.17-1 -4.88-4	9.12-3 -4.62-4	-4.03-2 $1.66-2$	4.62-2 $3.47-2$	1.93-1 5.04-2	3.62-1 6.37-2	5.35-1 7.52-2	7.04-1 $8.58-2$	8.67 - 1 $9.60 - 2$	1.02+0 1.06-1
5d _{5/2}	σ	5.411+1	3.347+1	1.523+1	8.115+0	4.794+0	3.042+0	2.035+0	1.419+0	1.022+0	7.569-1
$E_b =$	β	1.243	1.357	1.430	1.432	1.408	1.373	1.333	1.292	1.250	1.209
115.1 eV	$\gamma \\ \delta$	7.23-2 2.99-4	-2.29-2 $2.15-3$	-1.57-2 1.47-2	1.17-1 2.89-2	2.92-1 $4.32-2$	4.74-1 5.71-2	6.49 - 1 $7.08 - 2$	8.13-1 $8.46-2$	9.67 - 1 $9.86 - 2$	1.11+0 1.13-1
$-5f_{5/2}$	σ	3.152+1	1.510+1	4.741+0	1.929+0	9.201-1	4.888-1	2.810-1	1.717-1	1.101-1	7.346-2
$E_b =$	β	1.063	1.112	1.104	1.053	0.991	0.929	0.870	0.814	0.761	0.711
6.0 eV	$\frac{\gamma}{\delta}$	4.75-2 $4.18-2$	1.62 - 1 $6.48 - 2$	4.09 - 1 $1.05 - 1$	6.34 - 1 $1.41 - 1$	8.25-1 1.74-1	9.88 - 1 $2.04 - 1$	1.13+0 2.34-1	1.25+0 2.63-1	1.35+0 2.90-1	1.44+0 3.16-1
5f _{7/2}	σ	3.879+1	1.842+1	5.716+0	2.305+0	1.090+0	5.752-1	3.287-1	1.997-1	1.274-1	8.460-2
$E_b = 6.0 \text{ eV}$	β	1.081 5.32-2	1.116 1.77-1	1.092 4.36-1	1.033 6.66-1	0.968 8.59-1	0.905 1.02+0	0.847 1.16+0	0.793 1.28+0	0.743 1.38+0	0.696 1.46+0
0.0 6	$\frac{\gamma}{\delta}$	4.38-2	6.60-2	1.05-1	1.41-1	1.74-1	2.06-1	2.37-1	2.67-1	2.96-1	3.24-1
6s _{1/2}	σ	2.240+0	1.441+0	7.536-1	4.691-1	3.224-1	2.361-1	1.807-1	1.428-1	1.157-1	9.556-2
$E_b = 55.7 \text{ eV}$	β γ	1.491 6.80-1	1.550 6.78-1	1.611 6.00-1	1.644 4.92-1	1.666 3.81-1	1.684 2.77-1	1.699 1.82-1	1.712 9.86-2	1.725 2.69-2	1.736 -3.35-2
55,7 61	δ	1.40-3	-3.99-4	-2.98 - 3	-4.81-3	-6.25 - 3	-7.44 - 3	-8.45 - 3	-9.31-3	-1.01-2	-1.07-2
$6p_{1/2}$	σ	1.710+0	1.211+0	7.118-1	4.715-1	3.355-1	2.505-1	1.936-1	1.535-1	1.243-1	1.024-1
$E_b = 34.0 \text{ eV}$	β γ	1.257 6.70-1	1.449 5.81-1	1.610 3.34-1	1.672 1.55-1	1.698 5.33-2	1.709 9.17-3	1.711 6.41-3	1.708 3.26-2	1.701 7.86-2	1.691 1.38-1
3 1.0 0 1	δ	-1.68-2	-2.19-2	-2.13-2	-1.89-2	-1.71-2	-1.59-2	-1.48-2	-1.38-2	-1.26-2	-1.13-2
$6p_{3/2}$	σ	5.243+0	3.312+0	1.661+0	9.875-1	6.481-1	4.537-1	3.323-1	2.518-1	1.960-1	1.558-1
$E_b = 18.3 \text{ eV}$	$eta \ \gamma$	1.230 3.38-1	1.378 2.61-1	1.543 9.81-2	1.633 -5.65-3	1.690 -4.92-2	1.727 -4.68-2	1.752 1.062	1.769 4.94-2	1.779 1.26-1	1.784 2.13-1
10.5 01	δ	4.12-4	-6.41-3	-6.88 - 3	-1.65 - 3	4.51-3	1.03-2	1.55-2	1.99-2	2.37-2	2.68-2
6d _{3/2}	σ	2.276+0	1.439+0	6.754-1	3.680-1	2.213-1	1.425-1	9.663-2	6.814-2	4.958-2	3.704-2
$E_b = 6.0 \text{ eV}$	$eta \ \gamma$	1.010 1.06-1	1.182 3.90-3	1.347 -3.52-2	1.414 5.50-2	1.438 2.01-1	1.440 3.70-1	1.428 5.47-1	1.409 7.19-1	1.384 8.81-1	1.356 1.03+0
	δ	-4.13-3	-1.22 - 3	1.68-2	3.45-2	4.96-2	6.29-2	7.50-2	8.58-2	9.56-2	1.05-1
7s _{1/2}	σ	1.820-1	1.164-1	6.059-2	3.760-2	2.578-2	1.886-2	1.442-2	1.139-2	9.226-3	7.622-3
$E_b = 6.0 \text{ eV}$	β γ	1.494 6.79-1	1.551 6.76-1	1.610 5.98-1	1.643 4.90-1	1.667 3.77-1	1.686 2.72-1	1.702 1.78-1	1.715 9.65-2	1.726 2.58-2	1.736 -3.46-2
	δ	1.29-3	-4.70-4	-3.02-3	-4.87-3	-6.31-3	-7.46-3	-8.40-3	-9.27-3	-1.00-2	-1.08-2
Z= 98, Cf: [R	n]5f ⁶ _{5/2} 5	5f _{7/2} 7s _{1/2}									
		k (eV)									
Shell		1500	2000	3000	4000	5000	6000	7000	8000	9000	10000
$\begin{array}{l} 4p_{3/2} \\ E_b = \end{array}$	$\frac{\sigma}{eta}$	1.095+2 0.166	7.847+1 0.854	4.373+1 1.296	2.720+1 1.480	1.827+1 1.584	1.296+1 1.649	9.571+0 1.692	7.296+0 1.722	5.702+0 1.742	4.549+0 1.755
1291.5 eV	γ	-4.06-4	4.13 - 1	3.05 - 1	1.14 - 1	-4.38 - 3	-5.44 - 2	-5.46 - 2	-1.94-2	4.07 - 2	1.18 - 1
	δ	1.79-1	6.49-2	5.92-3	-1.75-3	1.61-3	7.45-3	1.34-2	1.90-2	2.38-2	2.79-2
$4d_{3/2} E_b =$	$\frac{\sigma}{eta}$	1.624+2 0.243	1.154+2 0.722	5.842+1 1.129	3.244+1 1.287	1.957+1 1.357	1.259+1 1.387	8.513+0 1.393	5.984+0 1.386	4.343+0 1.371	3.236+0 1.350
993.7 eV	γ	1.59 - 1	1.30 - 1	-5.89 - 2	-4.31-2	7.71 - 2	2.41 - 1	4.20 - 1	5.99 - 1	7.68 - 1	9.28 - 1
4.1	δ	1.35-1	2.85-2	1.19-2	3.06-2	4.92-2	6.51-2	7.88-2	9.06-2	1.01-1	1.10-1
$4d_{5/2}$ $E_b =$	$\frac{\sigma}{eta}$	2.550+2 0.659	1.722+2 1.046	8.260+1 1.307	4.448+1 1.374	2.628+1 1.382	1.663+1 1.365	1.109+1 1.335	7.708+0 1.300	5.536+0 1.261	4.088+0 1.222
-	,										

able 1 (contin	ued)										
933.1 eV	$\gamma \\ \delta$	2.39-1 8.51-2	8.83-2 1.77-2	-6.65-2 1.19-2	1.27-2 2.63-2	1.76-1 4.16-2	3.64-1 5.67-2	5.53-1 7.16-2	7.31-1 8.58-2	8.93-1 9.94-2	1.04+0 1.13-1
$4f_{5/2}$	σ	3.934+2	1.778+2 0.973	5.188+1	2.021+1	9.365+0	4.874+0	2.760+0 0.880	1.668+0	1.060+0	7.030-1
$E_b = 541.1 \text{ eV}$	$eta \gamma$	0.827 $-3.54-2$	6.51-2	1.053 3.24-1	1.038 5.71-1	0.993 7.84-1	0.938 9.62-1	0.880 1.11+0	0.825 1.23+0	0.773 1.34+0	0.725 1.43+0
	δ	3.54 - 2	6.37 - 2	1.08 - 1	1.45 - 1	1.78 - 1	2.09 - 1	2.37 - 1	2.63 - 1	2.89 - 1	3.15 - 1
4f _{7/2}	σ	4.969+2	2.223+2	6.423+1	2.484+1	1.143+1	5.916+0	3.332+0	2.003+0	1.268+0	8.369-1
$E_b = 523.3 \text{ eV}$	β	0.866	0.994	1.051	1.024	0.973	0.916	0.858	0.804	0.755	0.709
323.3 EV	$\gamma \\ \delta$	-3.20-2 $3.77-2$	8.08-2 $6.55-2$	3.55-1 1.08-1	6.07 - 1 $1.45 - 1$	8.21-1 1.78-1	9.98-1 $2.10-1$	1.14+0 2.39-1	1.26+0 2.67-1	1.37+0 2.94-1	1.45+0 3.22-1
5s _{1/2}	σ	1.021+1	6.757+0	3.641+0	2.303+0	1.598+0	1.179+0	9.064-1	7.191-1	5.843-1	4.839-1
$E_b =$	β	1.397	1.483	1.566	1.608	1.636	1.657	1.673	1.687	1.700	1.712
423.6 eV	δ	7.52-1 3.62-3	7.64-1 1.03-3	6.91-1 $-2.30-3$	5.79-1 -4.51-3	4.61-1 $-6.17-3$	3.50-1 -7.52-3	2.49-1 -8.67-3	1.58 - 1 $-9.66 - 3$	7.91-2 $-1.05-2$	1.10-2 $-1.13-2$
5p _{1/2}	σ	8.567+0	6.327+0	3.884+0	2.631+0	1.898+0	1.431+0	1.113+0	8.875-1	7.217-1	5.965-1
$E_b =$	β	1.072	1.340	1.557	1.639	1.677	1.694	1.701	1.701	1.697	1.690
341.9 eV	$\gamma \\ \delta$	7.29-1 -3.13-3	6.89 - 1 $-1.79 - 2$	4.31-1 $-2.22-2$	2.20-1 $-2.05-2$	9.06-2 $-1.86-2$	2.56-2 $-1.71-2$	6.60 - 3 $-1.59 - 2$	2.05-2 $-1.48-2$	5.75-2 $-1.36-2$	1.10-1 $-1.22-2$
5n	$\frac{\sigma}{\sigma}$	3.478+1	2.234+1	1.139+1	6.834+0	4.509+0	3.168+0	2.328+0	1.768+0	1.378+0	1.098+0
$5p_{3/2}$ $E_b =$	β	1.118	1.303	1.139+1	1.600	1.665	1.708	1.737	1.757	1.576+0	1.777
248.8 eV	γ	3.70-1	3.08-1	1.36-1	1.54-2	-4.27 - 2	-5.23-2	-2.61-2	2.61-2	9.66-2	1.79-1
	δ	1.02-2	-2.26-3	-6.89-3	-2.72-3	3.37-3	9.42-3	1.49-2	1.97-2	2.39-2	2.73-2
$5d_{3/2}$ $E_b =$	$\frac{\sigma}{eta}$	3.742+1 0.922	2.401+1 1.125	1.143+1 1.315	6.271+0 1.395	3.788+0 1.426	2.448+0 1.434	1.663+0 1.427	1.175+0 1.410	8.566-1 1.389	6.409-1 1.364
136.0 eV	γ	1.31 - 1	1.90 - 2	-4.31-2	3.24 - 2	1.71 - 1	3.37-1	5.10-1	6.79-1	8.40-1	9.92-1
	δ	2.88 - 4	-1.10-3	1.53-2	3.35-2	4.93-2	6.31-2	7.51-2	8.57-2	9.54-2	1.05-1
$5d_{5/2}$	σ	5.591+1	3.474+1	1.589+1	8.497+0	5.036+0	3.204+0	2.149+0	1.501+0	1.083+0	8.030-1
$E_b = 124.5 \text{ eV}$	β γ	1.232 8.67-2	1.351 -1.63-2	1.430 -2.22-2	1.435 1.02-1	1.413 2.71-1	1.380 4.52-1	1.342 6.29-1	1.300 7.95-1	1.259 9.47-1	1.218 1.09+0
	δ	5.72-4	1.62-3	1.38-2	2.76-2	4.17-2	5.59-2	6.99-2	8.35-2	9.68-2	1.10-1
5f _{5/2}	σ	3.289+1	1.586+1	5.022+0	2.056+0	9.852-1	5.255-1	3.030-1	1.856-1	1.193-1	7.974-2
$E_b = 6.0 \text{ eV}$	β γ	1.058 3.78-2	1.112 1.48-1	1.108 3.92-1	1.060 6.17-1	1.000 8.12-1	0.938 9.79-1	0.878 1.12+0	0.821 1.24+0	0.769 1.34+0	0.720 1.43+0
0.0 C V	δ	3.96-2	6.25-2	1.02-1	1.38-1	1.72-1	2.03-1	2.31-1	2.58-1	2.85-1	3.11-1
5f _{7/2}	σ	3.978+1	1.900+1	5.944+0	2.411+0	1.146+0	6.071-1	3.479-1	2.119-1	1.355-1	9.013-2
$E_b = 6.0 \text{ eV}$	β	1.078 4.26-2	1.117	1.097 4.20-1	1.040 6.50-1	0.976 8.48-1	0.914 1.01+0	0.854 1.15+0	0.799 1.27+0	0.749 1.37+0	0.703 1.46+0
0.0 6 V	$\frac{\gamma}{\delta}$	4.20-2	1.63-1 $6.38-2$	1.02-1	1.38-1	1.72-1	2.04-1	2.34-1	2.63-1	2.91-1	3.18-1
6s _{1/2}	σ	2.232+0	1.438+0	7.539-1	4.698-1	3.232-1	2.369-1	1.815-1	1.436-1	1.164-1	9.628-2
$E_b =$	β	1.451	1.516	1.583	1.620	1.646	1.664	1.680	1.693	1.705	1.716
58.1 eV	δ	6.91-1 $1.80-3$	6.96 - 1 $-1.71 - 4$	6.28 - 1 $-2.96 - 3$	5.22-1 -4.93-3	4.12-1 $-6.44-3$	3.08-1 $-7.71-3$	2.13-1 $-8.80-3$	1.29-1 -9.74-3	5.46-2 $-1.06-2$	-9.28-3 -1.13-2
6p _{1/2}	σ	1.662+0	1.183+0	7.000-1	4.659-1	3.329-1	2.494-1	1.933-1	1.537-1	1.248-1	1.030-1
$E_b =$	β	1.220	1.426	1.597	1.664	1.694	1.707	1.710	1.708	1.703	1.694
34.9 eV	$\gamma \\ \delta$	6.97-1	6.16-1 $-2.36-2$	3.68-1 $-2.30-2$	1.80-1 $-2.03-2$	6.90-2	1.64-2	5.70-3 -1.57-2	2.49-2	6.55-2	1.21-1
6n		-1.81-2 5.108+0	3.231+0	1.623+0	9.662-1	-1.82-2 $6.348-1$	-1.68-2 4.449-1	3.263-1	-1.47-2 $2.476-1$	-1.36-2 1.929-1	-1.23-2 1.536-1
$6p_{3/2}$ $E_b =$	$\frac{\sigma}{eta}$	1.206	1.357	1.525	1.619	1.679	1.719	1.746	1.764	1.775	1.782
19.4 eV	γ	3.47 - 1	2.74 - 1	1.11 - 1	2.86 - 3	-4.60-2	-4.92-2	-1.90-2	3.56-2	1.08 - 1	1.92 - 1
	δ	1.09-3	-6.33-3	-7.52-3	-2.47-3	3.78-3	9.76-3	1.51-2	1.97-2	2.38-2	2.72-2
$7s_{1/2} E_b =$	$\frac{\sigma}{eta}$	1.518-1 1.455	9.738-2 1.519	5.081-2 1.584	3.158-2 1.620	2.168-2 1.644	1.587-2 1.663	1.215-2 1.679	9.602-3 1.694	7.783—3 1.708	6.435-3 1.719
6.0 eV	γ	6.88-1	6.92 - 1	6.23-1	5.18-1	4.10-1	3.05-1	2.10 - 1	1.25-1	5.23-2	-1.00-2
	δ	1.65-3	-2.81-4	-3.01-3	-4.97 - 3	-6.52 - 3	-7.79-3	-8.83-3	-9.74-3	-1.05-2	-1.12-2
Z= 99, Es: [Ri	n]5f ⁶ _{5/2} 5	5f _{7/2} 7s _{1/2}									
		k (eV)									
Shell		1500	2000	3000	4000	5000	6000	7000	8000	9000	10000
$4p_{3/2}$	σ	1.102+2	7.968+1	4.465+1	2.786+1	1.875+1	1.333+1	9.860+0	7.526+0	5.890+0	4.704+0
$E_b = 1335.5 \text{ eV}$	$eta \gamma$	0.013 -1.06-1	0.789 4.01-1	1.262 3.26-1	1.456 1.33-1	1.565 7.65-3	1.634 -5.01-2	1.681 -5.77-2	1.713 -2.92-2	1.735 2.51-2	1.750 9.73-2
	δ	2.01-1	7.44-2	7.67-3	-1.96 - 3	8.36-4	6.64-3	1.28-2	1.85-2	2.36-2	2.79-2
4d _{3/2}	σ	1.635+2	1.176+2	6.022+1	3.365+1	2.039+1	1.316+1	8.923+0	6.288+0	4.572+0	3.413+0
$E_b =$	β	0.167	0.673	1.103	1.271	1.348	1.382	1.393	1.389	1.376	1.357
1032.4 eV	$\gamma \\ \delta$	1.32-1 1.57-1	1.47-1 3.52-2	-5.28-2 $1.10-2$	-5.27-2 $2.91-2$	5.69-2 4.79-2	2.14-1 $6.40-2$	3.89-1 7.81-2	5.66-1 $9.01-2$	7.36-1 1.01-1	8.96-1 1.10-1
4d _{5/2}	σ	2.586+2	1.763+2	8.532+1	4.619+1	2.739+1	1.738+1	1.162+1	8.093+0	5.824+0	4.306+0
$E_b =$	β	0.607	1.018	1.298	1.372	1.384	1.369	1.342	1.308	1.270	1.232
968.4 eV	γ	2.42 - 1	1.09-1 2.11-2	-6.63 - 2	-3.18-4 2.51-2	1.56-1 4.02-2	3.40 - 1	5.27-1 6.98-2	7.05 - 1	8.69-1 9.79-2	1.02+0
•	δ	1.00 - 1		1.12 - 2			5.51-2		8.42 - 2		1.11 - 1

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Table 1 (contin	,										
$4f_{5/2}$	σ	4.160+2	1.891+2	5.555+1	2.175+1	1.011+1	5.282+0	2.999+0	1.816+0	1.157+0	7.679 - 1
$E_b =$	β	0.806	0.962	1.051	1.041	0.999	0.945	0.889	0.834	0.782	0.734
567.5 eV	γ	-4.57 - 2	4.93 - 2	3.05 - 1	5.52 - 1	7.66 - 1	9.47 - 1	1.10+0	1.22+0	1.33+0	1.42+0
	δ	3.19-2	6.08 - 2	1.06 - 1	1.42 - 1	1.75 - 1	2.06 - 1	2.35 - 1	2.60 - 1	2.86 - 1	3.11 - 1
$4f_{7/2}$	σ	5.275+2	2.371+2	6.889+1	2.676+1	1.236+1	6.416+0	3.623+0	2.182+0	1.384+0	9.146 - 1
$E_b =$	β	0.848	0.985	1.051	1.028	0.979	0.924	0.867	0.813	0.763	0.717
551.0 eV	γ	-4.39-2	6.36 - 2	3.36 - 1	5.89 - 1	8.05 - 1	9.85 - 1	1.13+0	1.26+0	1.36+0	1.45+0
	δ	3.42-2	6.27 - 2	1.06 - 1	1.42 - 1	1.76 - 1	2.07 - 1	2.37 - 1	2.64 - 1	2.91 - 1	3.17 - 1
$5s_{1/2}$	σ	1.033+1	6.855+0	3.705+0	2.348+0	1.632+0	1.205+0	9.276 - 1	7.368 - 1	5.993 - 1	4.968 - 1
$E_b =$	β	1.346	1.442	1.533	1.580	1.611	1.634	1.651	1.666	1.679	1.691
442.7 eV	γ	7.60-1	7.82-1	7.21-1	6.13-1	4.97-1	3.85-1	2.84-1	1.92-1	1.10-1	3.95-2
	δ	4.35-3	1.49-3	-2.14 - 3	-4.54-3	-6.34 - 3	-7.78-3	-9.01-3	-1.01-2	-1.10-2	-1.18-2
$5p_{1/2}$	σ	8.499+0	6.317+0	3.914+0	2.668+0	1.934+0	1.463+0	1.142+0	9.133 - 1	7.446 - 1	6.168 - 1
$E_b =$	β	1.017	1.305	1.538	1.628	1.670	1.690	1.699	1.700	1.698	1.692
357.4 eV	$\gamma \\ \delta$	7.45-1 -2.53-3	7.25 - 1 $-1.90 - 2$	4.70-1 $-2.40-2$	2.50-1	1.11-1 $-2.00-2$	3.70-2	9.65-3	1.61-2	4.69-2 $-1.46-2$	9.45-2
					-2.21-2		-1.83-2	-1.69-2	-1.58-2		-1.32-2
$5p_{3/2}$	σ	3.584+1	2.307+1	1.179+1	7.084+0	4.680+0	3.293+0	2.422+0	1.842+0	1.437+0	1.146+0
$E_b =$	β	1.087	1.277	1.475	1.583	1.652	1.697	1.729	1.750	1.765	1.774
258.7 eV	$\gamma \\ \delta$	3.76-1 1.17-2	3.20-1 $-1.69-3$	1.50-1 -7.37-3	2.58-2 $-3.52-3$	-3.78-2 2.59-3	-5.32-2 8.79-3	-3.28-2 $1.45-2$	1.42-2 1.95-2	8.01-2 $2.39-2$	1.59-1 2.76-2
$5d_{3/2}$	σ	3.873+1	2.499+1	1.197+1	6.599+0	4.000+0	2.593+0	1.766+0	1.251+0	9.137-1	6.849-1
$E_b = 141.7 \text{ eV}$	β	0.896 1.43-1	1.104 2.87-2	1.302 -4.48-2	1.387 2.07-2	1.423	1.433 3.12-1	1.429 4.82-1	1.415 6.51-1	1.395 8.12-1	1.372 9.64-1
141.7 ev	$\gamma \\ \delta$	1.43-1	-1.61-3	-4.46-2 1.41-2	3.24-2	1.52-1 4.84-2	6.23-2	7.46-2	8.54-2	9.50-2	1.04-1
$5d_{5/2}$	σ	5.797+1	3.619+1	1.664+1 1.429	8.931+0	5.308+0	3.386+0	2.277+0	1.594+0 1.309	1.152+0	8.553-1
$E_b = 133.1 \text{ eV}$	$eta \ \gamma$	1.221 9.99-2	1.344 -9.39-3	-2.75-2	1.438 8.85-2	1.418 2.53-1	1.387 4.31-1	1.349 6.07-1	7.74–1	1.268 9.27-1	1.228 1.07+0
155.1 CV	δ	9.12-4	1.18-3	1.29-2	2.66-2	4.03-2	5.43-2	6.83-2	8.19-2	9.51-2	1.08-1
F.f.	σ	3.572+1	1.736+1	5.543+0	2.283+0	1.100+0	5.890-1	3.408-1	2.093-1	1.349-1	9.033-2
$5f_{5/2}$ $E_b =$	β	1.054	1.730+1	1.113	1.066	1.100+0	0.947	0.887	0.830	0.778	9.033-2 0.729
6.0 eV	γ	2.95-2	1.37-1	3.79-1	6.02-1	7.99-1	9.67-1	1.11+0	1.23+0	1.34+0	1.43+0
	δ	3.75-2	6.04-2	9.99-2	1.36-1	1.69-1	2.00-1	2.29-1	2.55-1	2.81-1	3.07-1
5f _{7/2}	σ	4.336+1	2.086+1	6.582+0	2.686+0	1.283+0	6.824-1	3.924-1	2.396-1	1.536-1	1.024-1
$E_b =$	β	1.076	1.118	1.101	1.046	0.984	0.922	0.863	0.807	0.757	0.711
6.0 eV	γ	3.34-2	1.51 - 1	4.06 - 1	6.37 - 1	8.35 - 1	1.00+0	1.15+0	1.26+0	1.37+0	1.45+0
	δ	3.97 - 2	6.19 - 2	1.00 - 1	1.35 - 1	1.69 - 1	2.02 - 1	2.31 - 1	2.60 - 1	2.87 - 1	3.14 - 1
6s _{1/2}	σ	2.273+0	1.468+0	7.714-1	4.813-1	3.314-1	2.432-1	1.865-1	1.476-1	1.198-1	9.918-2
$E_b =$	β	1.407	1.479	1.553	1.594	1.621	1.642	1.658	1.672	1.684	1.696
60.4 eV	γ	7.01 - 1	7.14 - 1	6.55 - 1	5.53 - 1	4.45 - 1	3.41 - 1	2.45 - 1	1.60 - 1	8.35 - 2	1.72 - 2
	δ	2.23-3	1.11-4	-2.89-3	-5.02-3	-6.66-3	-8.01-3	-9.17-3	-1.02-2	-1.11-2	-1.19-2
$6p_{1/2}$	σ	1.659+0	1.186+0	7.072 - 1	4.732 - 1	3.394 - 1	2.551 - 1	1.983 - 1	1.581 - 1	1.287 - 1	1.064 - 1
$E_b =$	β	1.179	1.397	1.581	1.655	1.689	1.704	1.709	1.708	1.704	1.697
37.7 eV	γ	7.22-1	6.51-1	4.03-1	2.06-1	8.63-2	2.54-2	7.12-3	1.95-2	5.42-2	1.05-1
	δ	-1.92-2	-2.54-2	-2.49-2	-2.20-2	-1.96-2	-1.79-2	-1.67-2	-1.56-2	-1.45-2	-1.32-2
$6p_{3/2}$	σ	5.247+0	3.324+0	1.673+0	9.971-1	6.558-1	4.600-1	3.377-1	2.565-1	2.001-1	1.594-1
$E_b =$	β	1.179	1.333	1.504	1.603	1.666	1.709	1.738	1.758	1.771	1.779
22.2 eV	$_{\delta}^{\gamma}$	3.54-1 1.87-3	2.86-1 $-6.21-3$	1.24-1 -8.16-3	1.20-2 -3.30-3	-4.22-2 3.02-3	-5.09-2 $9.17-3$	-2.61-2 $1.47-2$	2.34-2 $1.96-2$	9.10-2 $2.38-2$	1.72-1 2.75-2
$7s_{1/2}$	σ	1.513-1 1.412	9.721-2 1.482	5.084-2 1.555	3.164-2 1.594	2.175-2	1.594-2 1.639	1.220-2 1.657	9.656-3	7.833-3 1.687	6.482-3
$E_b = 6.0 \text{ eV}$	$eta \ \gamma$	6.98-1	7.10-1	6.49–1	5.49-1	1.620 4.42-1	3.38-1	2.42-1	1.673 1.56-1	8.03-2	1.699 1.57-2
0.0 C V	δ	2.06-3	-1.71-5	-2.96-3	-5.07-3	-6.73-3	-8.09-3	-9.22 - 3	-1.02-2	-1.10-2	-1.18-2
7 400 5 1				2.00	0.07	0,73 3	0.00	0,22 3	1,02 2	2	2
Z=100, Fm: [Kn J515/2										
		k (eV)									
Shell		1500	2000	3000	4000	5000	6000	7000	8000	9000	10000
4p _{3/2}	σ	1.106+2	8.083+1	4.556+1	2.852+1	1.924+1	1.370+1	1.015+1	7.759+0	6.080+0	4.861+0
$E_b =$	β		0.720	1.227	1.430	1.545	1.618	1.668	1.703	1.727	1.744
1379.9 eV	γ	-2.28-1	3.84 - 1	3.45 - 1	1.53 - 1	2.09 - 2	-4.46-2	-5.93 - 2	-3.76 - 2	1.07 - 2	7.79 - 2
	δ	2.21 - 1	8.51 - 2	9.74 - 3	-2.07 - 3	5.70-5	5.77 - 3	1.20 - 2	1.80 - 2	2.33-2	2.79 - 2
4d _{3/2}	σ	1.645+2	1.197+2	6.200+1	3.487+1	2.122+1	1.374+1	9.341+0	6.598+0	4.808+0	3.595+0
$E_b =$	β	0.091	0.623	1.075	1.254	1.338	1.377	1.391	1.390	1.380	1.363
1071.0 eV	γ	9.57 - 2	1.61 - 1	-4.52 - 2	-6.08 - 2	3.81 - 2	1.87 - 1	3.57 - 1	5.33 - 1	7.03 - 1	8.63 - 1
	δ	1.79-1	4.31-2	1.02-2	2.76-2	4.66-2	6.30-2	7.72-2	8.96-2	1.00 - 1	1.10-1
4d _{5/2}	σ	2.618+2	1.802+2	8.805+1	4.792+1	2.851+1	1.815+1	1.216+1	8.488+0	6.119+0	4.532+0
$E_b =$	β	0.553	0.989	1.287	1.370	1.386	1.373	1.348	1.316	1.279	1.241
1003.8 eV	γ	2.38-1	1.30-1	-6.46-2	-1.23-2	1.37-1	3.16-1	5.01-1	6.79-1	8.45-1	9.96-1
	δ	1.16-1	2.51-2	1.05-2	2.38-2	3.88-2	5.34-2	6.80-2	8.24-2	9.61-2	1.09-1
$4f_{5/2}$	σ	4.396+2	2.010+2	5.943+1	2.337+1	1.091+1	5.715+0	3.254+0	1.974+0	1.260+0	8.375-1

 $5f_{7/2}$

 $E_b = 7.0 \text{ eV}$

 $6s_{1/2}$

 $E_b =$

 $6p_{1/2}$

 $6p_{3/2}$

 $7s_{1/2}$

62.7 eV

39.1 eV

22.9 eV

6.0 eV

4.702+1

1.073

2.44 - 2

3.77 - 2

2.310+0

1.360

7.10 - 1

2.72 - 3

1.652+0

1.133

7.46 - 1

5.374+0

1.152

3.61 - 1

2.68 - 3

1.506 - 1

1.365

7.07 - 1

2.53-3

-2.05 - 2

 $_{eta}^{\sigma}$

 $_{\delta}^{\gamma}$

σ

β

δ

 β

 $_{\delta}^{\gamma}$

β

 $_{\delta}^{\gamma}$

 σ

β

2.278+1

1.119

1.39 - 1

6.00 - 2

1.495+0

1.439

7.32 - 1

4.44 - 4

1.186+0

1.366

6.87 - 1

3.411+0

1.308

2.98 - 1

-6.02 - 3

9.697 - 2

1.442

7.28 - 1

3.01 - 4

-2.73 - 2

7.248+0

1.106

3.93 - 1

9.80 - 2

7.879 - 1

1.520

6.83 - 1

-2.79 - 3

7.126 - 1

1.564

4.39 - 1

1.720+0

1.484

1.37 - 1

-8.77 - 3

5.084-2

1.522

6.77 - 1

-2.87 - 3

-2.69 - 2

2.974+0

1.052

6.23 - 1

1.33 - 1

4.923-1

1.564

5.86 - 1

-5.09 - 3

4.793 - 1

1.644

2.35 - 1

-2.38 - 2

1.027+0

1.586

2.17 - 2

-4.15 - 3

3.168 - 2

1.566

5.80 - 1

-5.15 - 3

1.428+0

0.991

8.22 - 1

1.66 - 1

3.393-1

1.595

4.79 - 1

-6.86 - 3

3.451 - 1

1.682

1.06 - 1

6.759 - 1

1.653

-2.11-2

-3.76 - 2

2.21 - 3

2.180 - 2

1.594

4.75 - 1

-6.93 - 3

7.624 - 1

0.930

9.93 - 1

1.99 - 1

2.492 - 1

3.75 - 1

-8.32 - 3

2.603 - 1

1.700

3.63 - 2

-1.92 - 2

4.746 - 1

-5.17 - 2

8.54-3

1.599 - 2

1.615

3.73 - 1

-8.39 - 3

1.698

1.617

4.399 - 1

0.872

1.14+0

2.29 - 1

1.635

2.79 - 1

-9.55 - 3

2.029 - 1

1.707

1.03-2

-1.77 - 2

3.488 - 1

-3.21-2

1.43 - 2

1.633

2.76 - 1

-9.62 - 3

1.226 - 2

1.729

1.912-1

2.694 - 1

0.816

1.26+0

2.57 - 1

1.516-1

1.650

1.92 - 1

-1.06-2

1.623 - 1

1.708

1.58 - 2

-1.66-2

2.652 - 1

1.23 - 2

1.94 - 2

9.705 - 3

1.649

1.88 - 1

-1.07 - 2

1.751

1.730 - 1

0.765

1.36+0

2.84 - 1

1.663

1.14 - 1

-1.16-2

1.324 - 1

1.705

4.44-2

-1.54-2

2.071 - 1

1.766

7.52 - 2

2.38 - 2

7.878 - 3

1.665

1.11 - 1

-1.16-2

1.231-1

1.156 - 1

0.718

1.45+0

3.10 - 1

1.020-1

1.675

4.58 - 2

-1.25-2

1.097 - 1

1.699

8.96-2

-1.42 - 2

1.652 - 1

1.775

1.52 - 1

2.77-2

6.524-3

1.678

4.32-2

-1.24-2

Table 1 (contin	nued)										
$E_b =$	β	0.784	0.950	1.049	1.044	1.004	0.953	0.898	0.843	0.791	0.742
594.9 eV	$\gamma \\ \delta$	-5.53-2 $2.82-2$	3.37-2 5.78-2	2.86-1 1.03-1	5.33-1 1.40-1	7.48-1 1.73-1	9.32-1 2.04-1	1.08+0 2.32-1	1.21+0 2.58-1	1.32+0 2.83-1	1.41+0 3.07-1
4f _{7/2}	σ	5.582+2	2.522+2	7.370+1	2.875+1	1.333+1	6.941+0	3.930+0	2.372+0	1.506+0	9.972-1
$E_b =$	β	0.829	0.976	1.051	1.031	0.985	0.931	0.875	0.821	0.770	0.724
577.4 eV	γ	-5.49 - 2	4.69 - 2	3.17 - 1	5.71 - 1	7.88 - 1	9.72 - 1	1.12+0	1.25+0	1.35+0	1.44+0
	δ	3.06-2	5.98-2	1.04 - 1	1.39-1	1.72 - 1	2.04 - 1	2.34 - 1	2.61 - 1	2.88 - 1	3.13-1
$5s_{1/2}$	σ	1.043+1	6.943+0	3.765+0	2.390+0	1.664+0	1.230+0	9.479 - 1	7.537 - 1	6.137 - 1	5.093 - 1
$E_b =$	β	1.290	1.397	1.498	1.549	1.583	1.608	1.628	1.643	1.657	1.670
461.4 eV	γ	7.66 - 1	7.99 - 1	7.51 - 1	6.48 - 1	5.33 - 1	4.22 - 1	3.20 - 1	2.27 - 1	1.44 - 1	7.05 - 2
	δ	5.18-3	2.02-3	-1.92 - 3	-4.54 - 3	-6.49 - 3	-8.05 - 3	-9.36 - 3	-1.05-2	-1.15-2	-1.24-2
$5p_{1/2}$	σ	8.409+0	6.287+0	3.932+0	2.698+0	1.965+0	1.492+0	1.169+0	9.373 - 1	7.662 - 1	6.361 - 1
$E_b =$	β	0.962	1.269	1.517	1.616	1.662	1.685	1.696	1.699	1.698	1.693
367.0 eV	γ	7.58 - 1	7.58 - 1	5.09 - 1	2.82 - 1	1.33 - 1	5.01 - 2	1.46 - 2	1.38 - 2	3.81 - 2	8.04 - 2
	δ	-2.25 - 3	-2.01-2	-2.58-2	-2.39-2	-2.15-2	-1.95-2	-1.81-2	-1.68-2	-1.56-2	-1.42-2
$5p_{3/2}$	σ	3.688+1	2.379+1	1.219+1	7.335+0	4.852+0	3.418+0	2.517+0	1.916+0	1.497+0	1.195+0
$E_b =$	β	1.055	1.249	1.453	1.566	1.638	1.686	1.719	1.743	1.759	1.770
268.5 eV	γ	3.80 - 1	3.31 - 1	1.64 - 1	3.69 - 2	-3.20-2	-5.31-2	-3.83 - 2	3.27 - 3	6.45 - 2	1.39 - 1
	δ	1.34-2	-1.01-3	-7.81-3	-4.34-3	1.75-3	8.10-3	1.40-2	1.93-2	2.39-2	2.78-2
$5d_{3/2}$	σ	4.001+1	2.595+1	1.252+1	6.930+0	4.215+0	2.740+0	1.872+0	1.329+0	9.725 - 1	7.302 - 1
$E_b =$	β	0.867	1.081	1.287	1.378	1.419	1.432	1.431	1.419	1.402	1.380
147.1 eV	γ	1.55 - 1	3.89 - 2	-4.56-2	1.01 - 2	1.33 - 1	2.88 - 1	4.55 - 1	6.22 - 1	7.83 - 1	9.35 - 1
	δ	2.29-3	-2.04-3	1.30-2	3.14-2	4.75 - 2	6.16-2	7.40-2	8.50-2	9.48 - 2	1.04 - 1
$5d_{5/2}$	σ	5.997+1	3.760+1	1.739+1	9.367+0	5.583+0	3.571+0	2.406+0	1.688+0	1.222+0	9.090 - 1
$E_b =$	β	1.210	1.338	1.428	1.440	1.423	1.393	1.357	1.318	1.278	1.237
139.4 eV	γ	1.13 - 1	-2.08 - 3	-3.19 - 2	7.65 - 2	2.35 - 1	4.10 - 1	5.85 - 1	7.52 - 1	9.07 - 1	1.05+0
	δ	1.32-3	7.79-4	1.20-2	2.55 - 2	3.91 - 2	5.29 - 2	6.67 - 2	8.04 - 2	9.36 - 2	1.06 - 1
5f _{5/2}	σ	3.861+1	1.890+1	6.089+0	2.523+0	1.221+0	6.566-1	3.812-1	2.348-1	1.516-1	1.018-1
$E_b =$	β	1.049	1.111	1.116	1.072	1.015	0.956	0.896	0.839	0.786	0.738
7.0 eV	γ	2.15 - 2	1.25 - 1	3.65 - 1	5.88 - 1	7.84 - 1	9.54 - 1	1.10+0	1.22+0	1.33+0	1.42+0
	δ	3.54 - 2	5.84 - 2	9.78 - 2	1.33 - 1	1.66 - 1	1.97 - 1	2.26 - 1	2.53 - 1	2.78 - 1	3.03 - 1