

Part 2

Simple network, complex
function

Synthetic switch: more complex
network with bistability

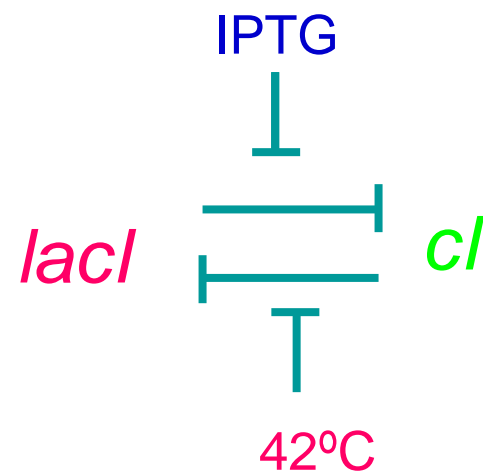
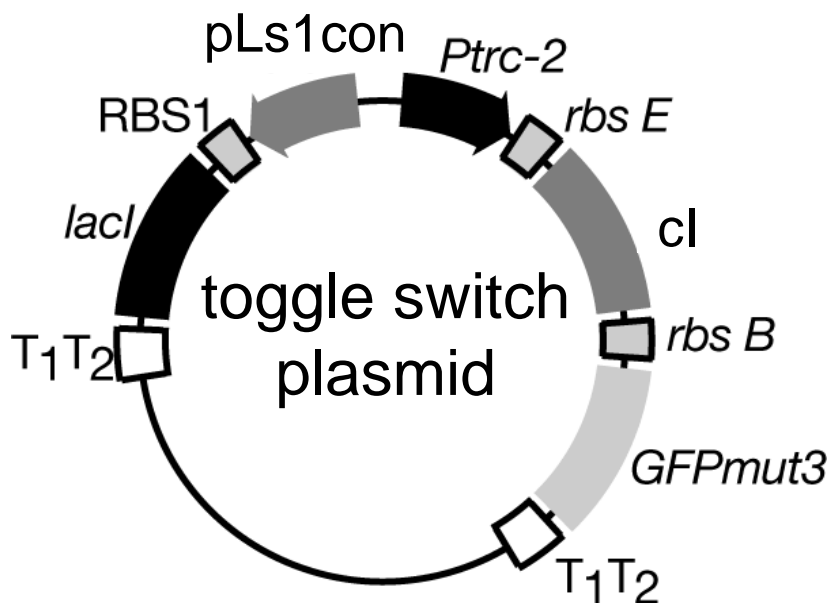
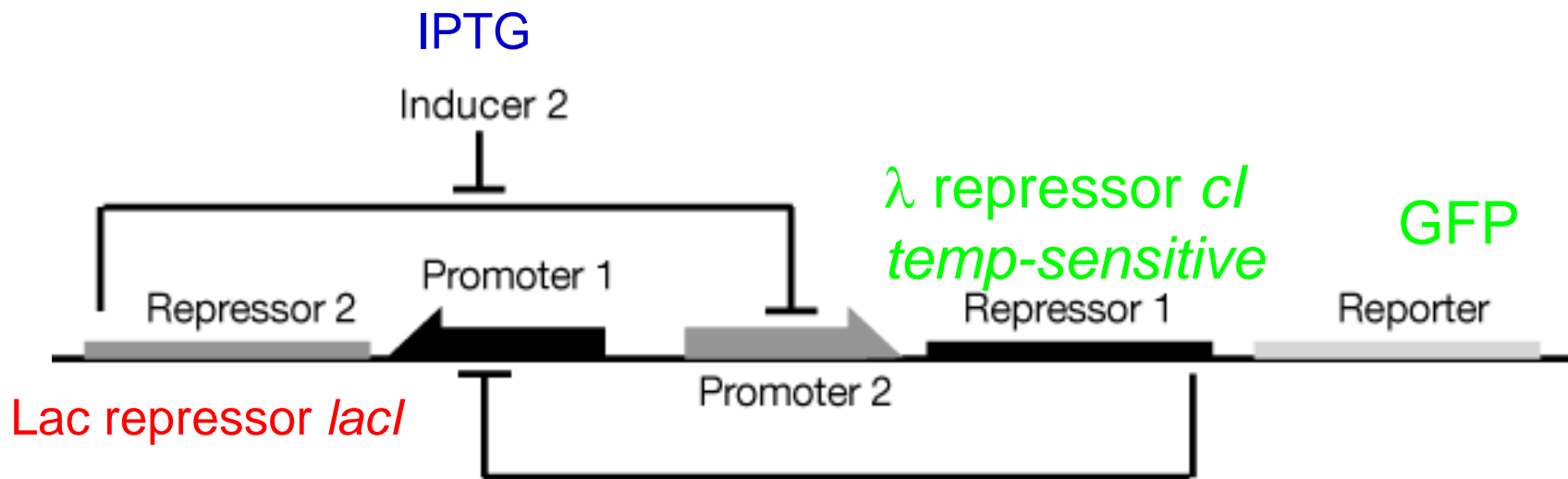
Week 3, 3/5-7/2019

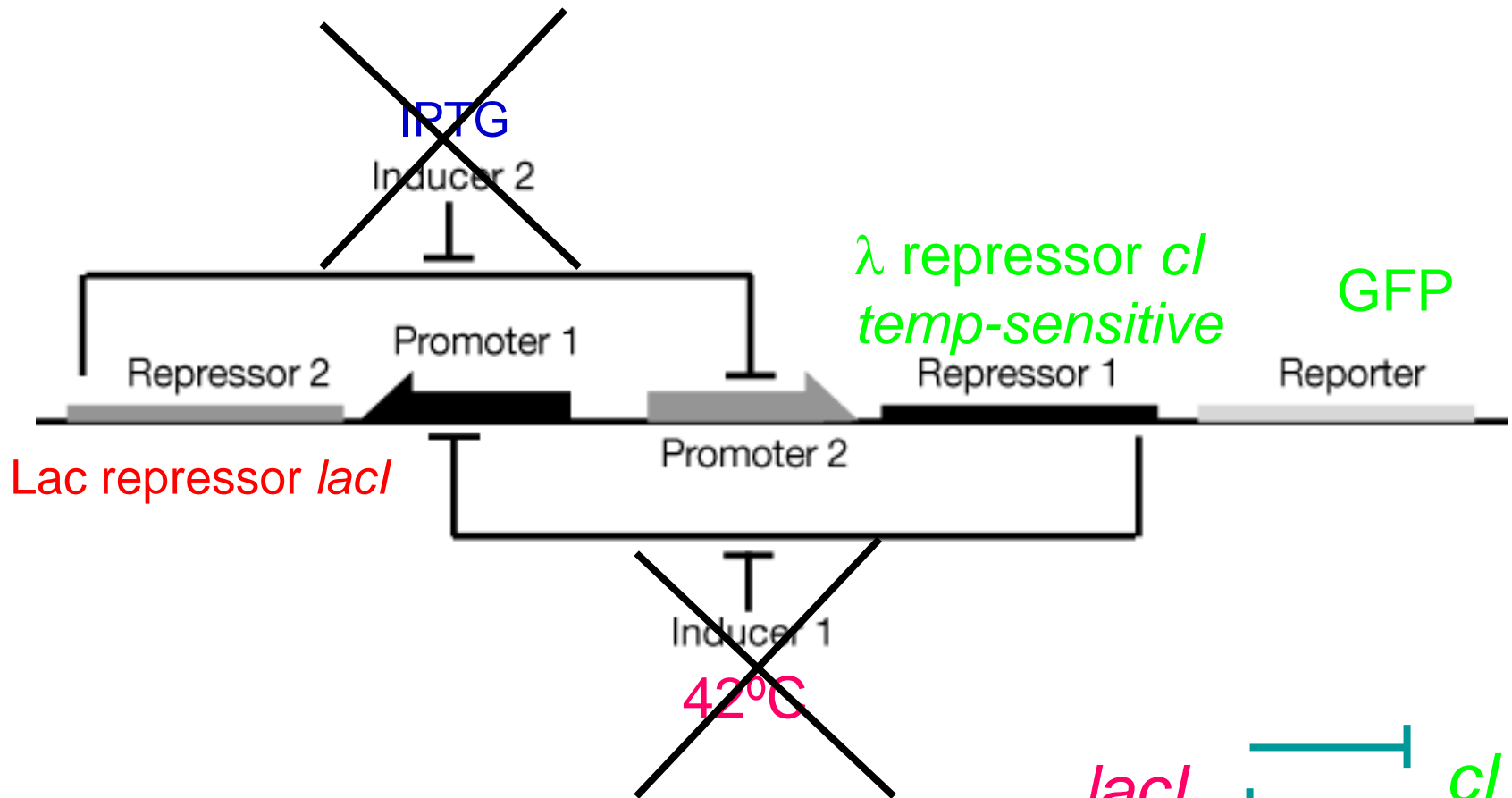
Synthetic bistability: a more complex network

T. S. Gardner, C. R. Cantor, and J. J. Collins. Construction of a genetic toggle switch in *Escherichia coli*. *Nature* **403**, 339-342 (2000).

- why did they do this?

- they are engineers, who want to create new things from known
- toggle switch (拨动开关) is simple, but possibly useful
- know the mathematic principles
- have the tools and bioparts
- results might be as predicted, or might not, let's take a look!

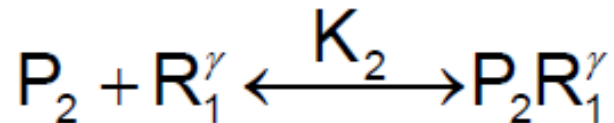
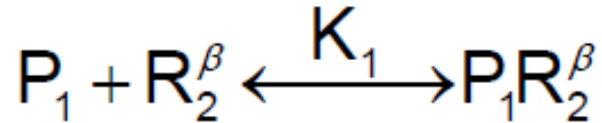




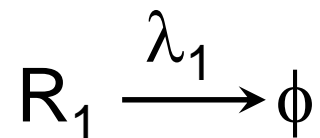
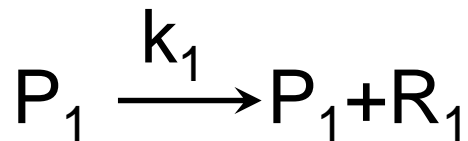
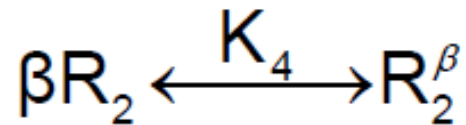
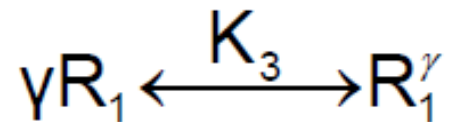
IPTG	42°C	<i>lacI</i>	<i>cl</i>	GFP
Off	Off	Off	On	On
Off	Off	ON	Off	Off

Bistability
History dependent

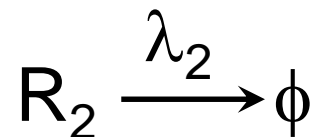
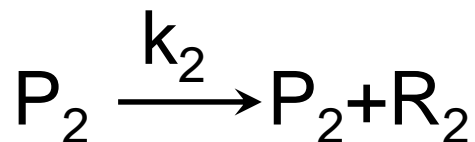
Derivation of the mathematic model



Fast events



slow events



$$[P^T] = [P_1^T] = [P_1] + [P_1 R_2^\beta] = [P_2^T] = [P_2] + [P_2 R_1^\gamma]$$

Derivation of the mathematic model

Now the rate of synthesis of repressor 1 and 2 can be written as:

$$R_{\text{gen1}} = k_1[P^T] \frac{[P_1]}{[P_1] + [P_1 R_2^\beta]} = k_1[P^T] \frac{1}{1 + K_1[R_2^\beta]} = \frac{k_1[P^T]}{1 + K_1 K_4 [R_2]^\beta}$$

$$R_{\text{gen2}} = k_2[P^T] \frac{[P_2]}{[P_2] + [P_2 R_1^\gamma]} = k_2[P^T] \frac{1}{1 + K_2[R_1^\gamma]} = \frac{k_2[P^T]}{1 + K_2 K_3 [R_1]^\gamma}$$

The rates k_1 and k_2 are the effective synthesis rates

Derivation of the mathematic model

Assuming a first order decay process, the kinetic equations are

$$\frac{d[R_1]}{dt} = \frac{k_1[P^T]}{1 + K_1 K_4 [R_2]^\beta} - \lambda_1 [R_1]$$

$$\frac{d[R_2]}{dt} = \frac{k_2[P^T]}{1 + K_2 K_3 [R_1]^\gamma} - \lambda_2 [R_2]$$

The equations can be eventually simplified as

$$\begin{aligned} \frac{dU}{dt} &= \frac{\alpha_1}{1 + V^\beta} - \lambda_1 U \\ \frac{dV}{dt} &= \frac{\alpha_2}{1 + U^\gamma} - \lambda_2 V \end{aligned}$$



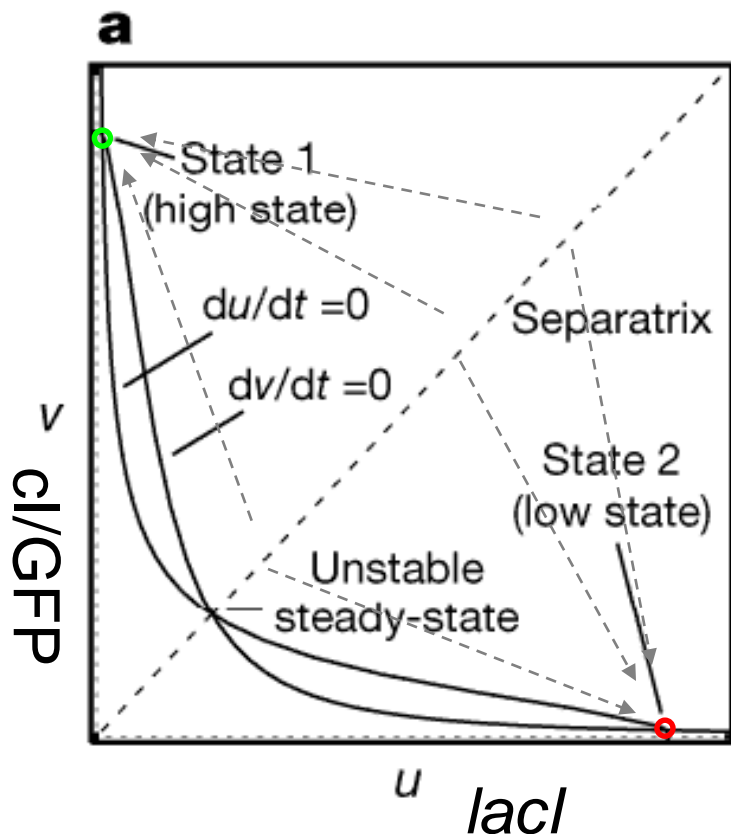
Bistability 双稳态

$$\begin{aligned}\frac{dU}{dt} &= \frac{\alpha_1}{1+V^\beta} - \lambda_1 U \\ \frac{dV}{dt} &= \frac{\alpha_2}{1+U^\gamma} - \lambda_2 V\end{aligned}$$

稳态解:

$$\frac{dU}{dt} = \frac{\alpha_1}{1+V^\beta} - \lambda_1 U \equiv 0$$

$$\frac{dV}{dt} = \frac{\alpha_2}{1+U^\gamma} - \lambda_2 V \equiv 0$$



$dU/dt=0$ represent a line $U = \frac{\alpha_1}{\lambda_1(1+V^\beta)}$

$dV/dt=0$ represent a line $V = \frac{\alpha_2}{\lambda_2(1+U^\gamma)}$

The two lines are called nullclines, the intersections are called fixed point, or steady states.

What does this mean?

Analysis of this type of diagram without solving the ODE is called stability analysis.

Let's use the Matlab for graphical illustration of stability analysis. To simplify the equations, we set λ_1 and λ_2 to 1.

```
% function gardnerfunc.m define ODE equation
function dydt = f(t,y,flag,a1,a2,beta,gamma)
% [u] = y(1) [v]=y(2)
dydt = [a1/(1+y(2)^beta)-y(1); a2/(1+y(1)^gamma)-y(2)];
```

```
% function gardner1.m stability analysis for bistability
```

```
clear;hold off;options=[];
```

```
a1=10;b=2;
```

```
a2=10;g=2;
```

```
% draw nullcline
```

```
y1=0:0.01:30;x2=0:0.01:30;
```

```
x1=a1./(1+y1.^b); y2=a2./(1+x2.^g);
```

```
figure(1); plot(x1,y1);hold on; plot(x2,y2,'r-');plot([0 30],[0 30],'k--');
```

```
legend('dU/dt=0','dV/dt=0');
```

```
axis([-0.5 12 -0.5 12]);xlabel('U, cl');ylabel('V, LacI');title('IPTG off, 42°C off');
```

```
% calculate the dynamic process from any initial value
```

```
button =0;
```

```
while button~=3 % right click stop the program
```

```
[x1,y1,button]=ginput(1); % get the initial value from mouse left click
```

```
x0=x1;y0=y1;
```

```
[t1 yt]=ode45('gardnerfunc',[0 10],[x0 y0],options,a1,a2,b,g);
```

```
if x0>y0
```

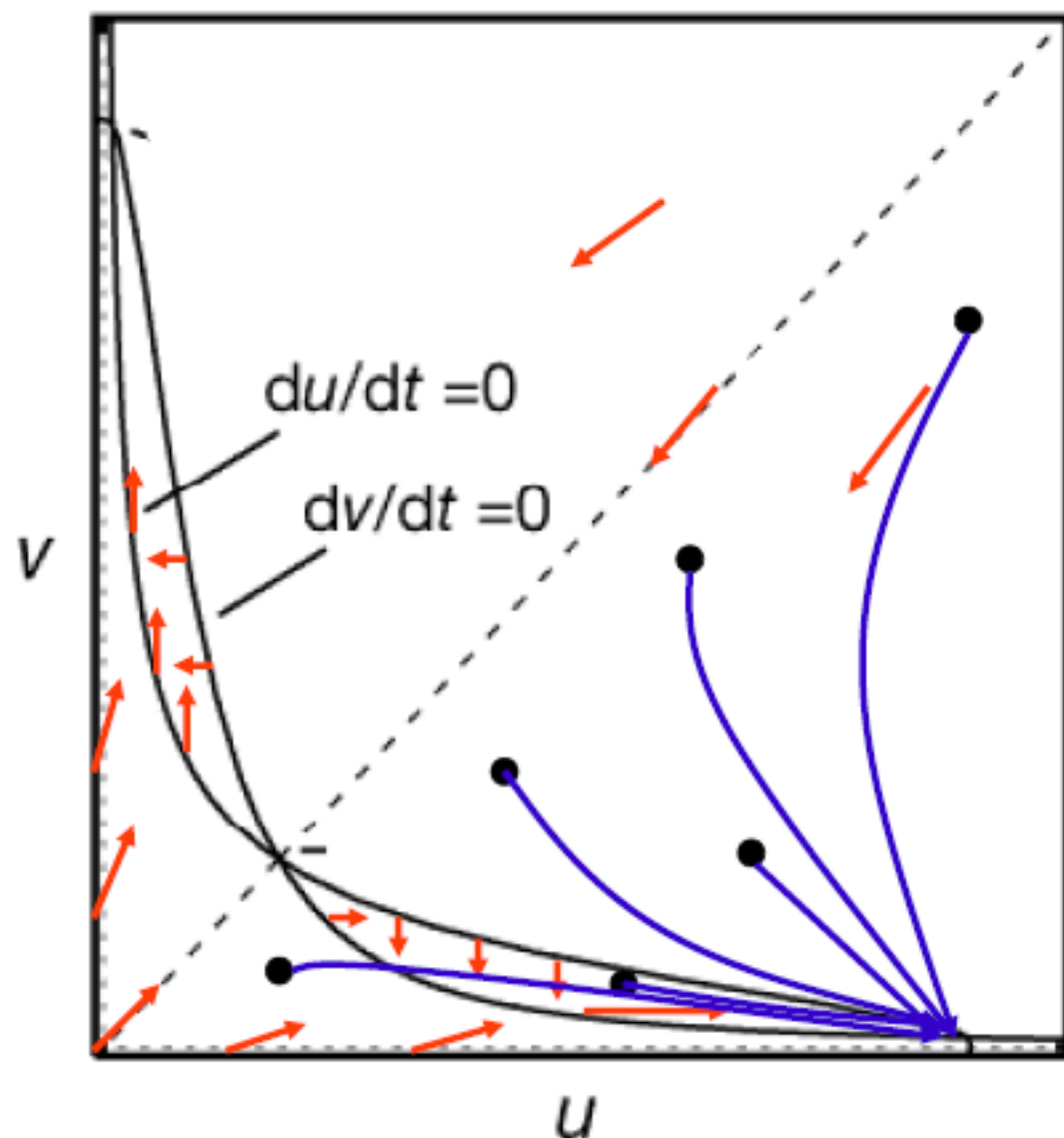
```
    plot(yt(:,1),yt(:,2),'m.-');% lower half
```

```
else
```

```
    plot(yt(:,1),yt(:,2),'c.-'); % upper half
```

```
end
```

```
end
```



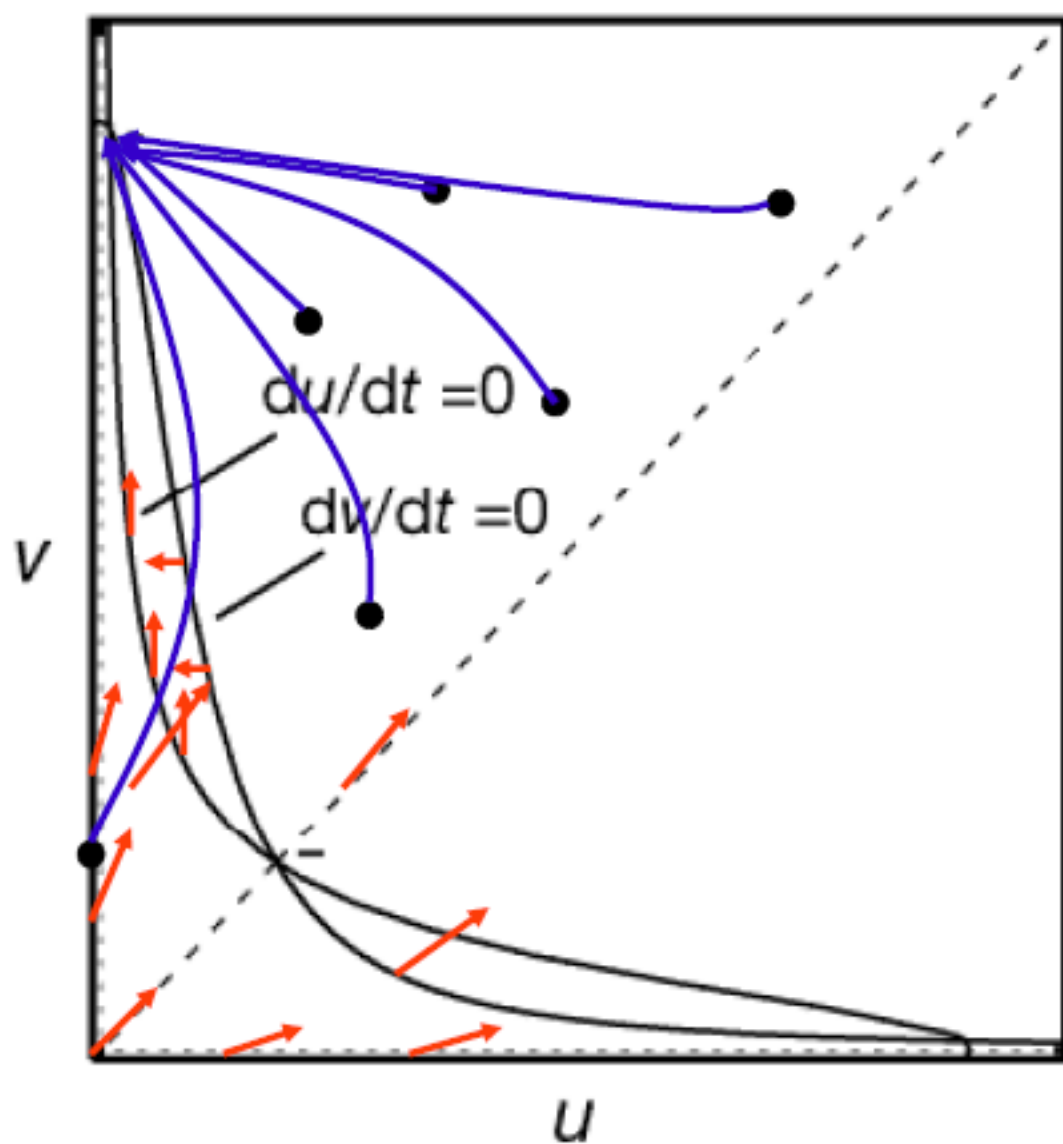
nullclines:

$$u = \frac{\alpha_1}{1+v^\beta}$$

$$v = \frac{\alpha_2}{1+u^\gamma}$$

$$\frac{du}{dt} = \frac{\alpha_1}{1+v^\beta} - u$$

$$\frac{dv}{dt} = \frac{\alpha_2}{1+u^\gamma} - v$$



nullclines:

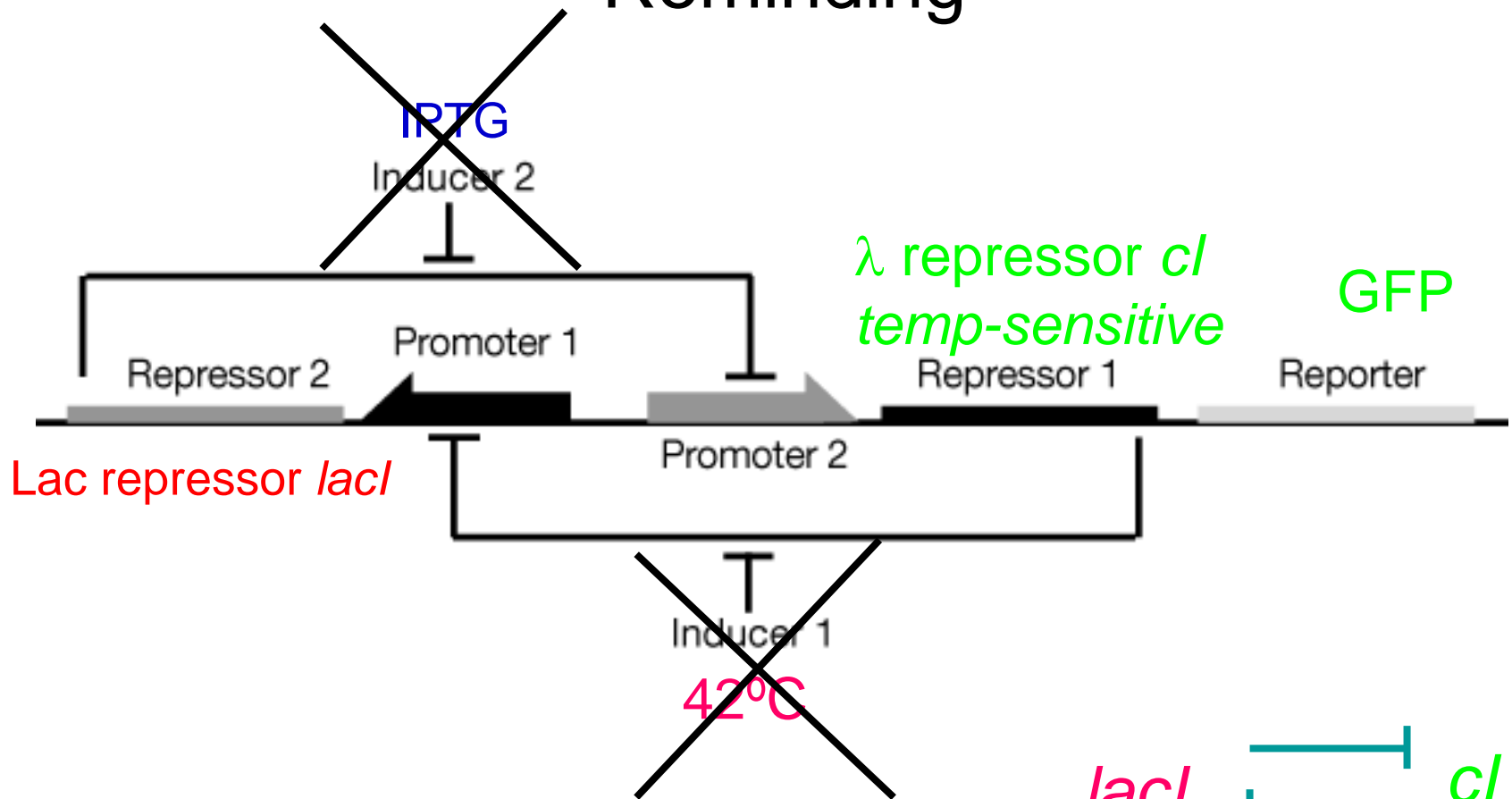
$$u = \frac{\alpha_1}{1+v^\beta}$$

$$v = \frac{\alpha_2}{1+u^\gamma}$$

$$\frac{du}{dt} = \frac{\alpha_1}{1+v^\beta} - u$$

$$\frac{dv}{dt} = \frac{\alpha_2}{1+u^\gamma} - v$$

Reminding



lacI  *cl*

IPTG	42°C	<i>lacI</i>	<i>cl</i>	GFP
Off	Off	Off	On	On
Off	Off	ON	Off	Off

Bistability
History dependent



Bistability 双稳态

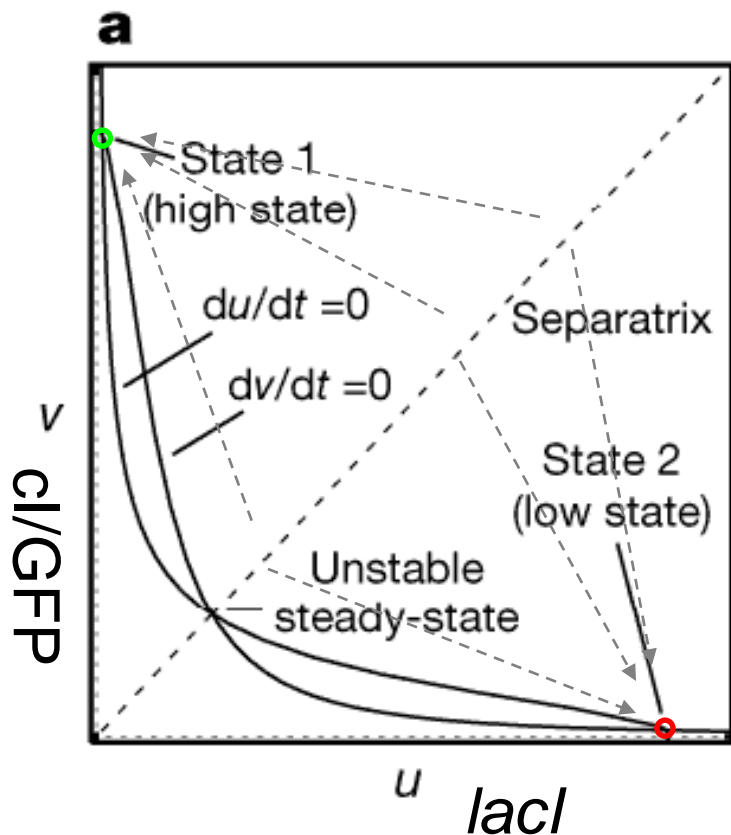
$$\frac{dU}{dt} = \frac{\alpha_1}{1+V^\beta} - \lambda_1 U$$

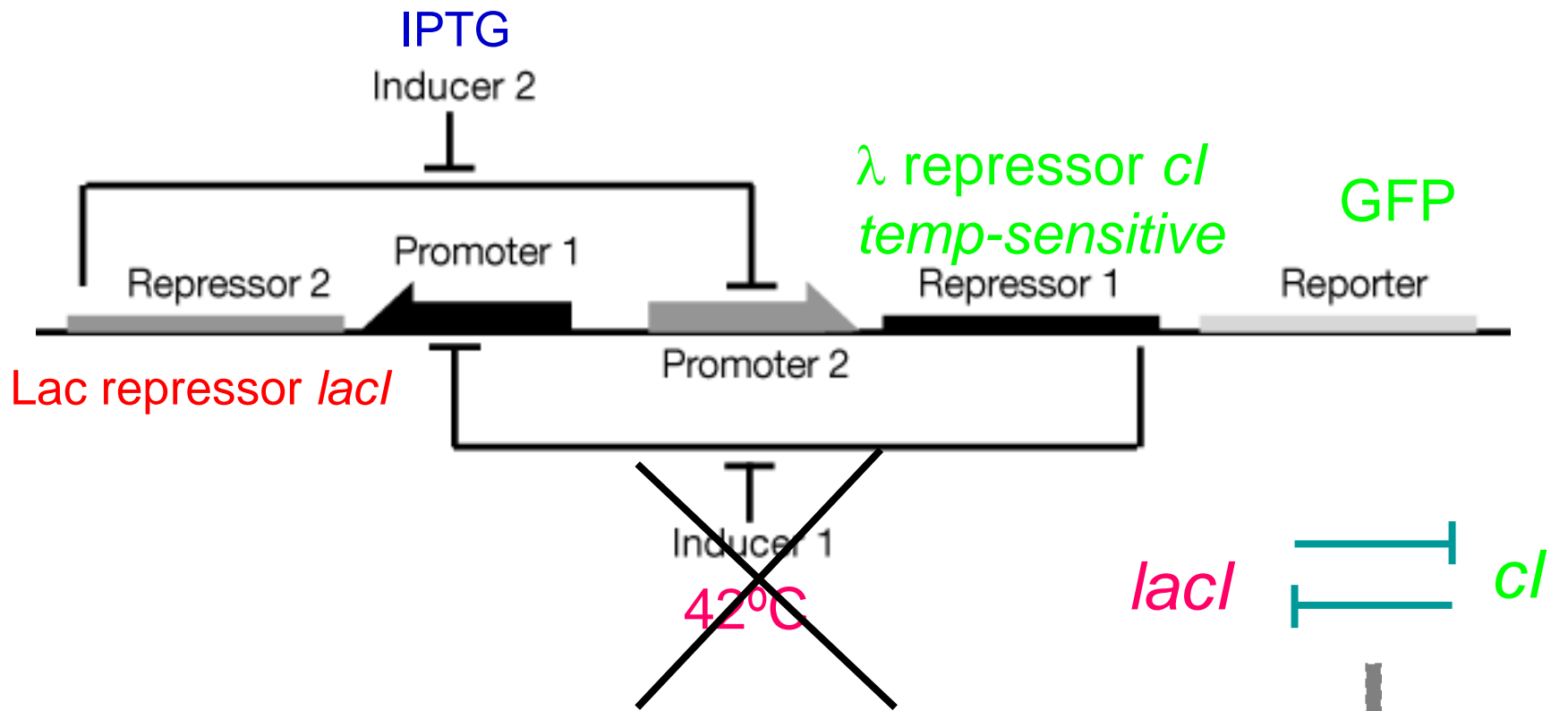
$$\frac{dV}{dt} = \frac{\alpha_2}{1+U^\gamma} - \lambda_2 V$$

稳态解:

$$\frac{dU}{dt} = \frac{\alpha_1}{1+V^\beta} - \lambda_1 U \equiv 0$$

$$\frac{dV}{dt} = \frac{\alpha_2}{1+U^\gamma} - \lambda_2 V \equiv 0$$





IPTG	42°C	<i>lacI</i>	<i>cl</i>	GFP
off > on	Off	Off	On	On

GFP turned on



Bistability 双稳态

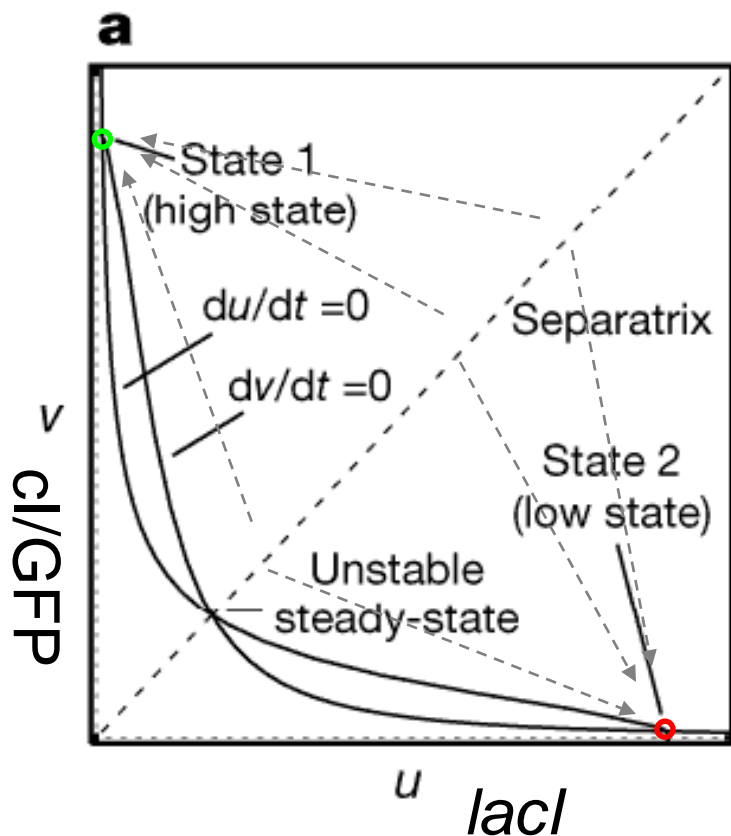
$$\frac{dU}{dt} = \frac{\alpha_1}{1+V^\beta} - \lambda_1 U$$

$$\frac{dV}{dt} = \frac{\alpha_2}{1+U^\gamma} - \lambda_2 V$$

稳态解:

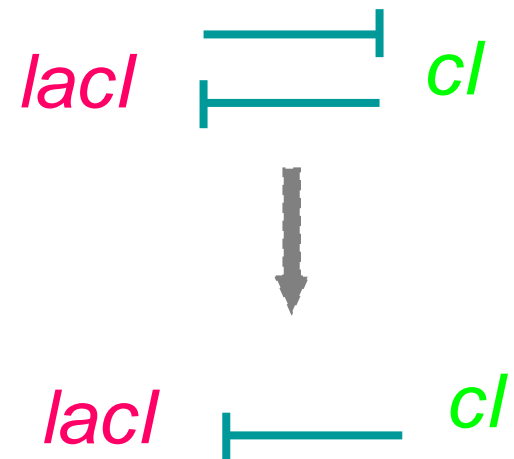
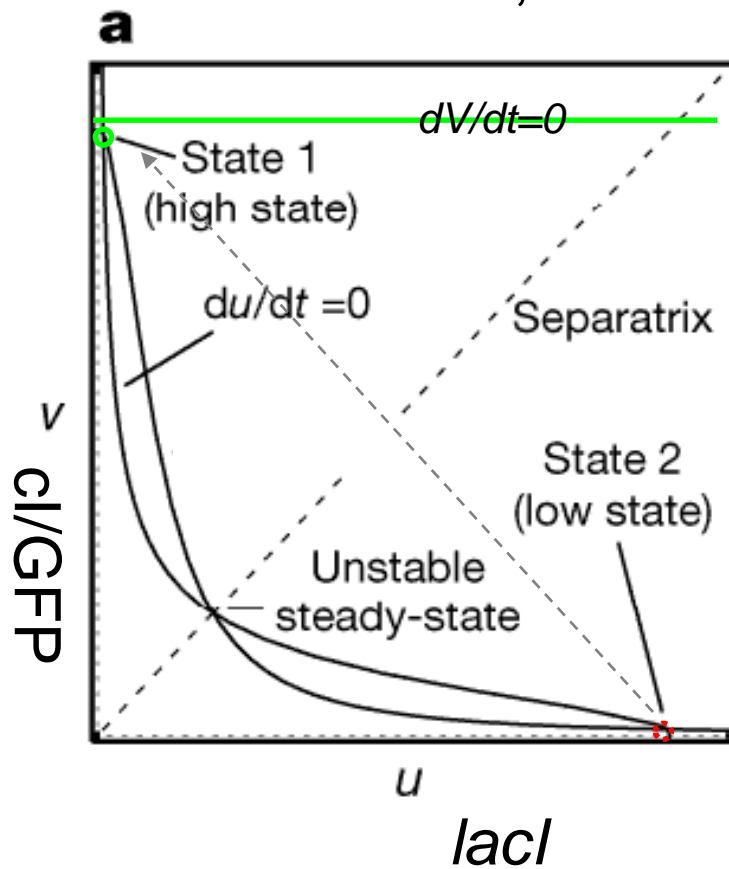
$$\frac{dU}{dt} = \frac{\alpha_1}{1+V^\beta} - \lambda_1 U \equiv 0$$

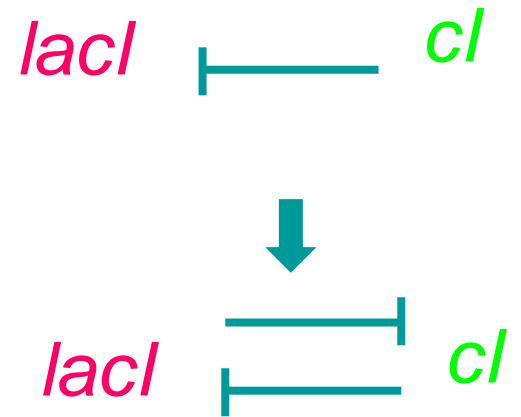
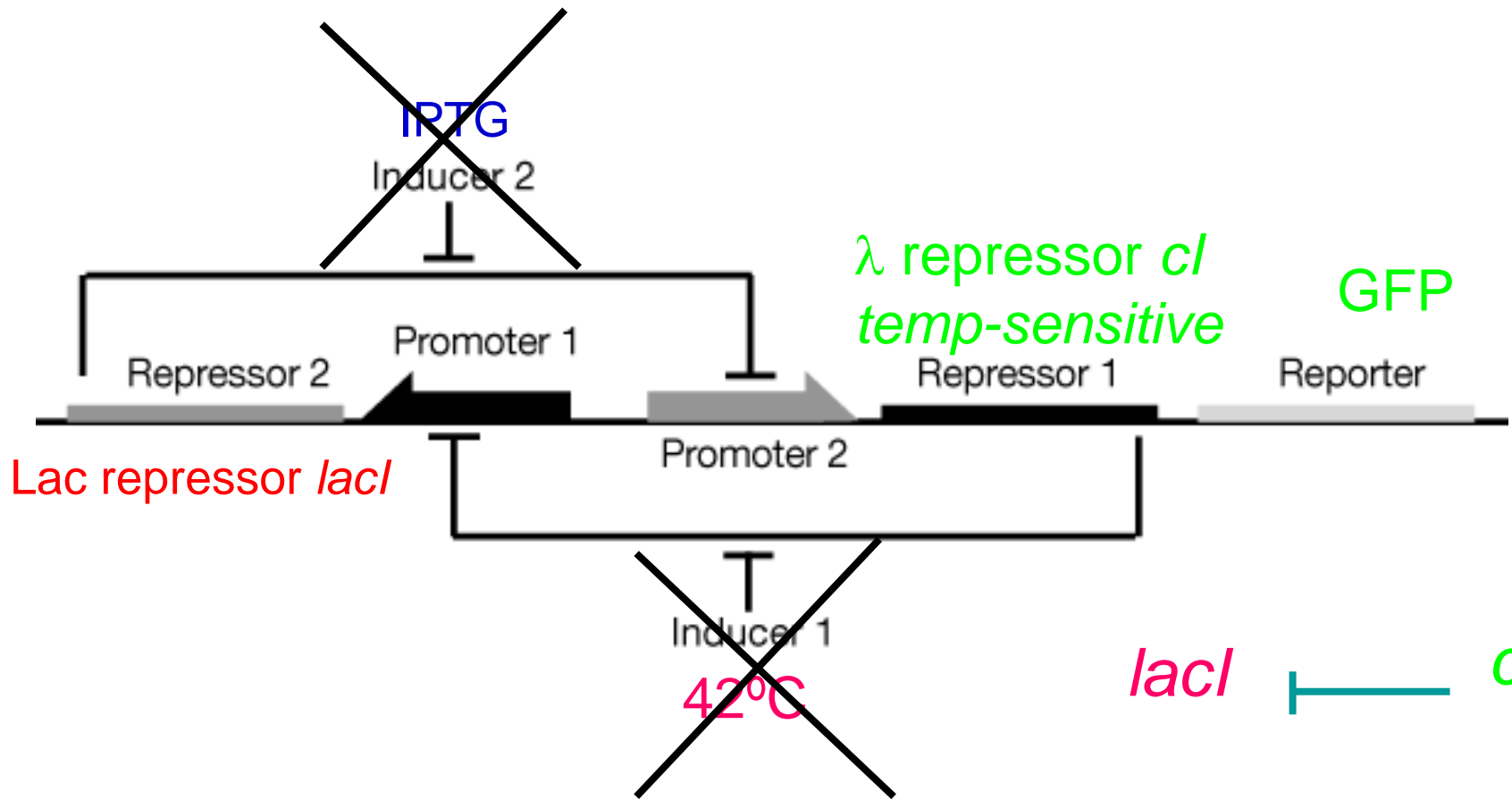
$$\frac{dV}{dt} = \frac{\alpha_2}{1+U^\gamma} - \lambda_2 V \equiv 0$$



IPTG off>on

new null cline, one state:GFP on



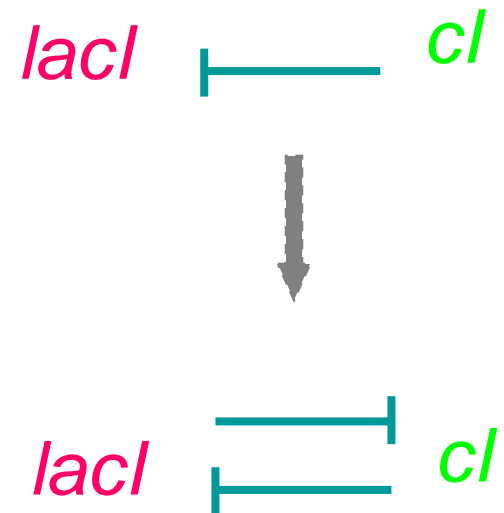
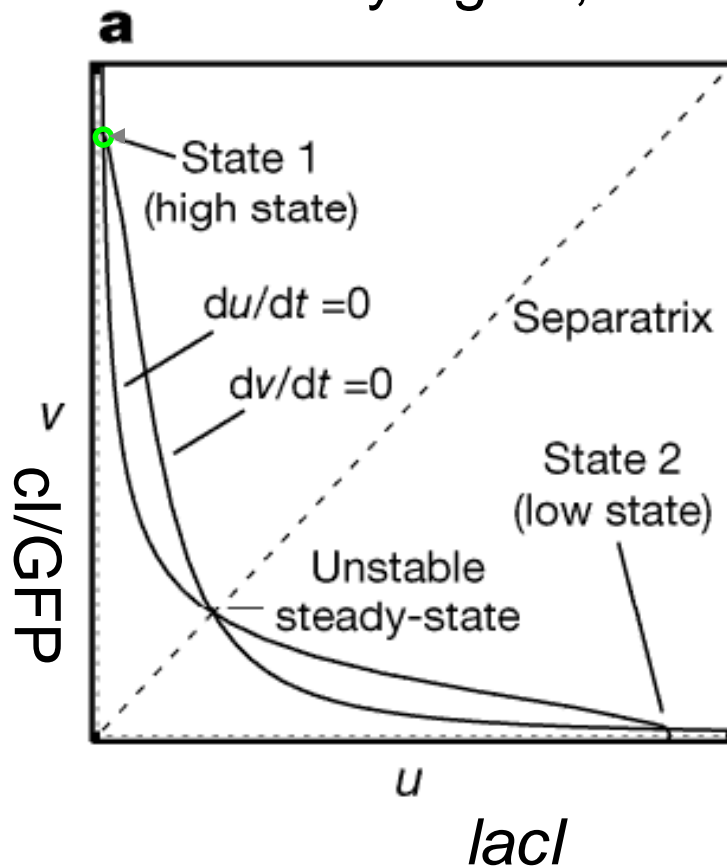


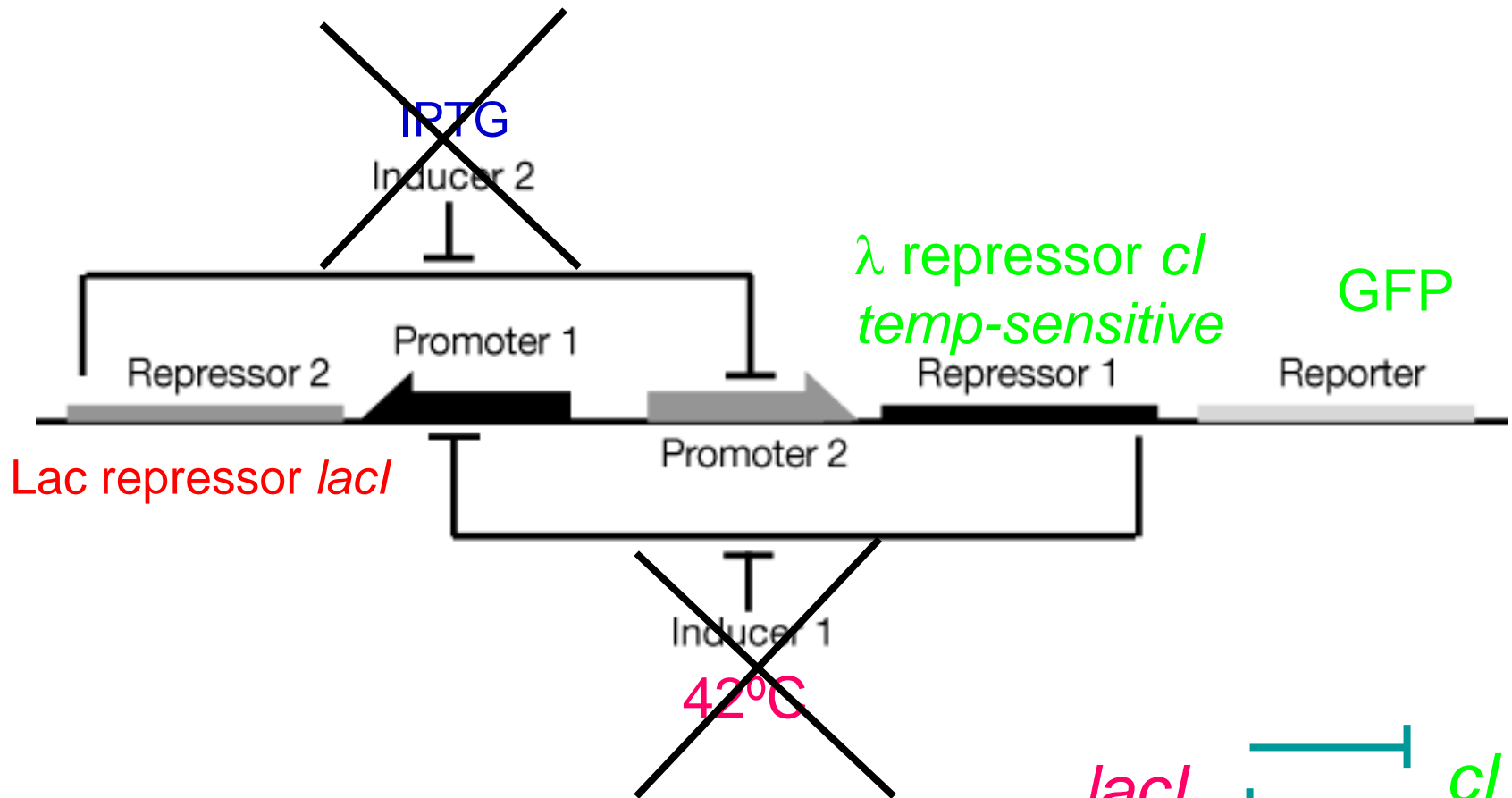
IPTG	42°C	<i>lacI</i>	<i>cl</i>	GFP
On > off	Off	Off	On	On

GFP kept on

IPTG on>off

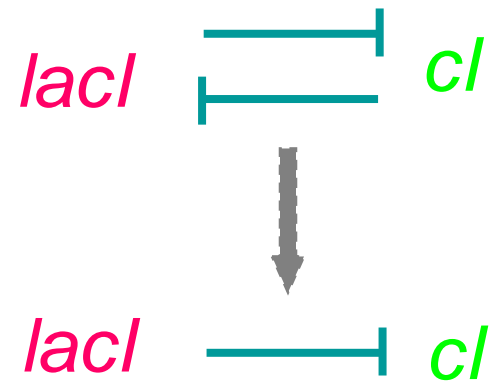
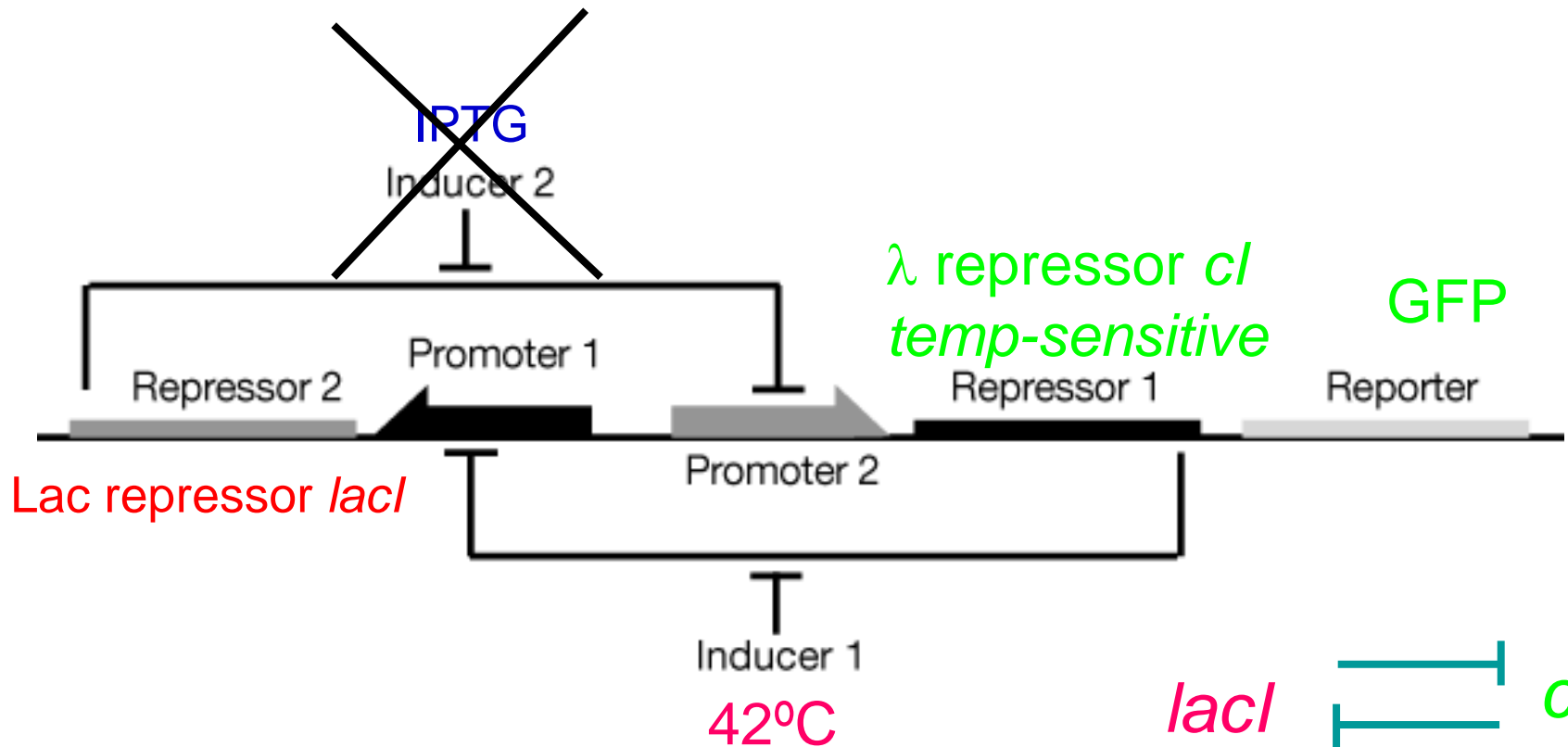
Bistability again, but GFP on state is reachable





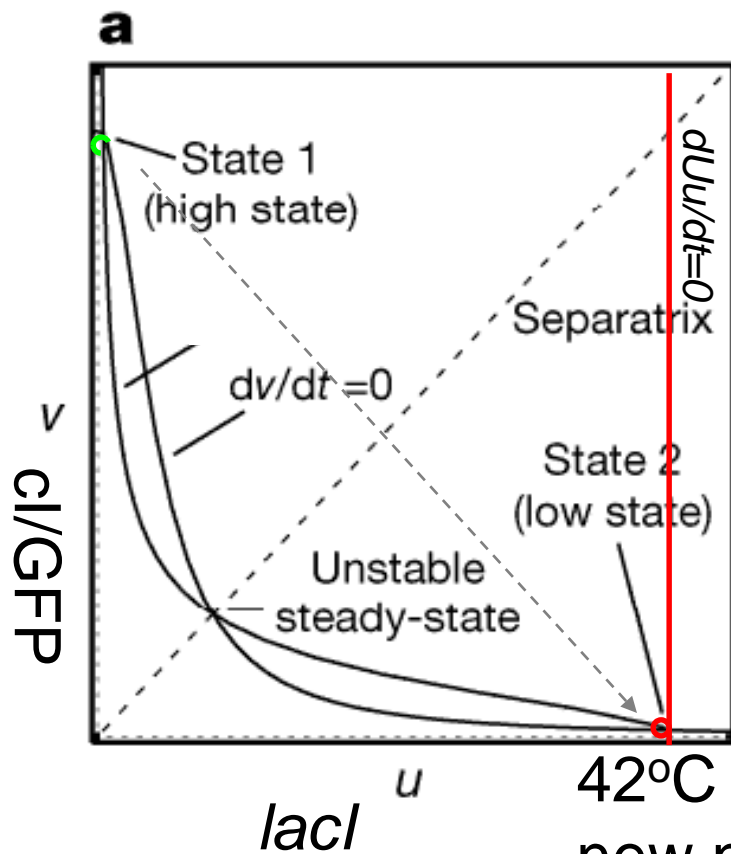
IPTG	42°C	<i>lacI</i>	<i>cl</i>	GFP
Off	Off	Off	On	On
On	On	On	Off	Off

Bistability
History dependent



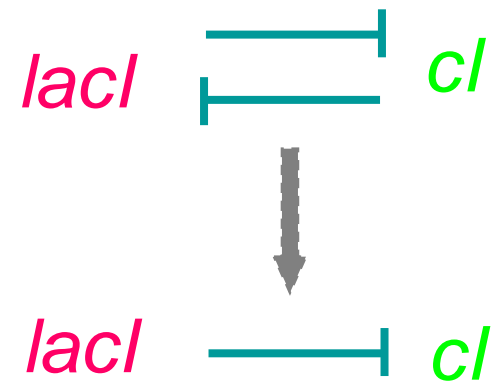
IPTG	42°C	<i>lacI</i>	<i>cl</i>	GFP
Off	off>on	On	Off	Off

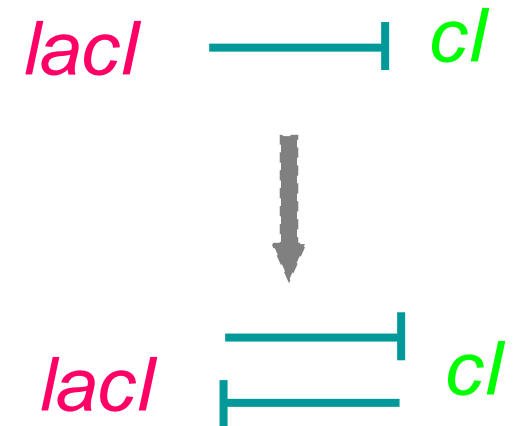
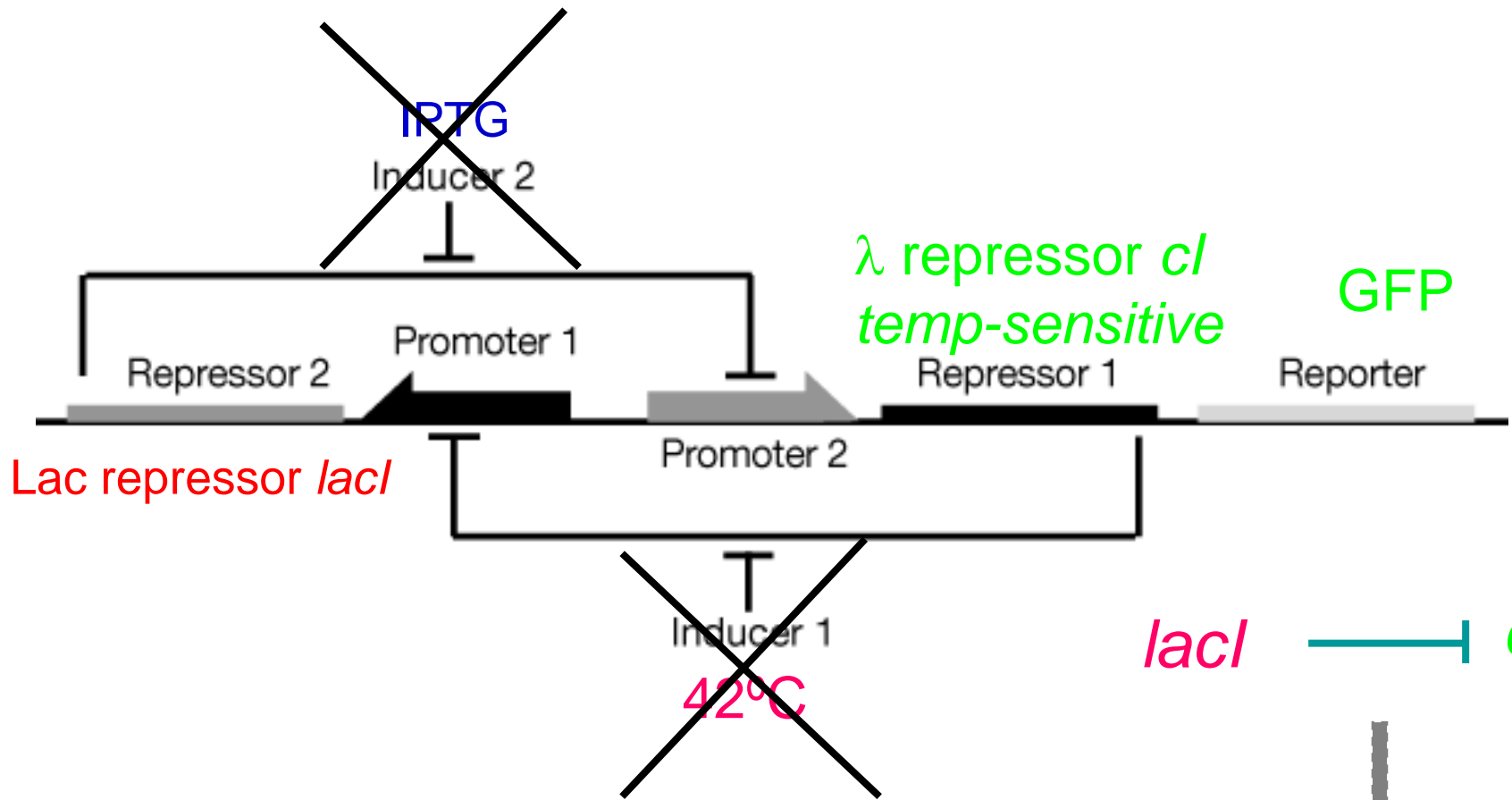
GFP turned off



$42^\circ C$ off \rightarrow on

new null cline, one state: GFP off



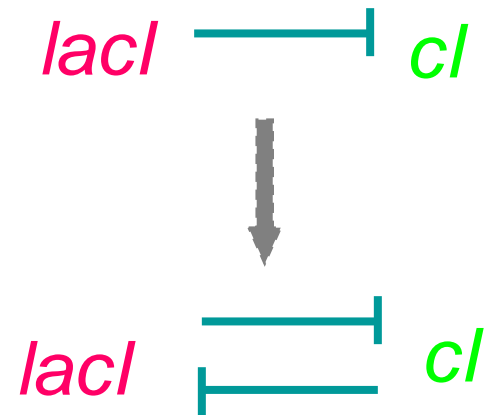
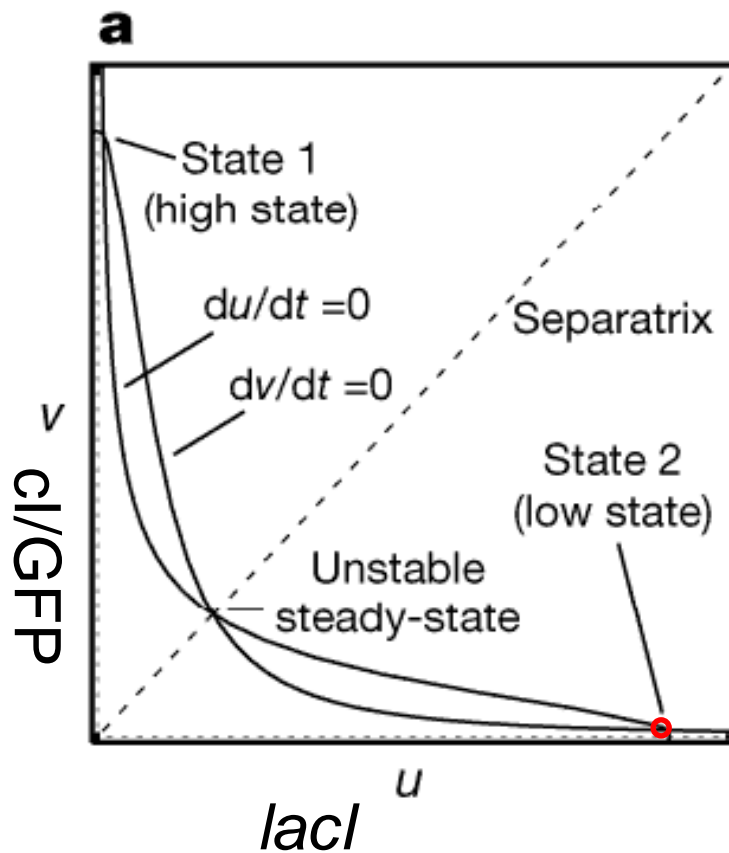


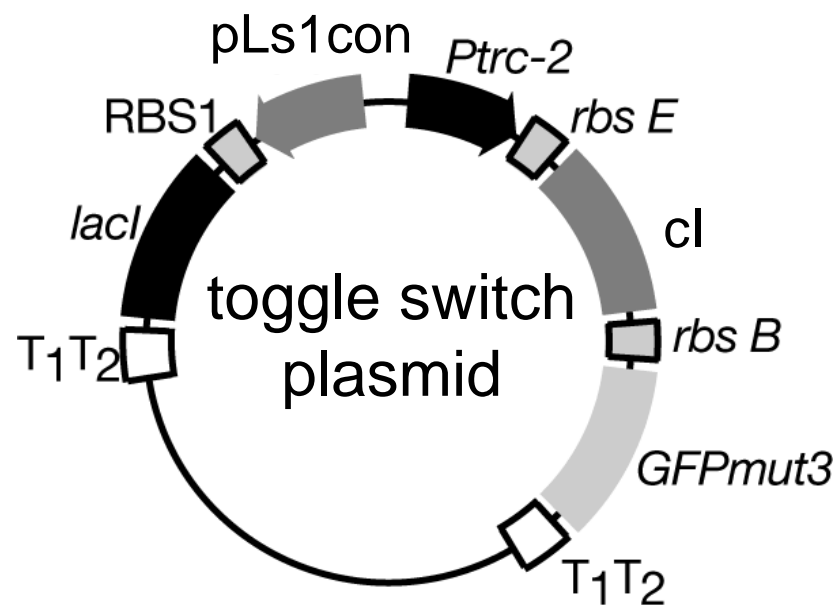
GFP kept off

IPTG	42°C	<i>lacI</i>	<i>cl</i>	GFP
Off	on>off	On	Off	Off

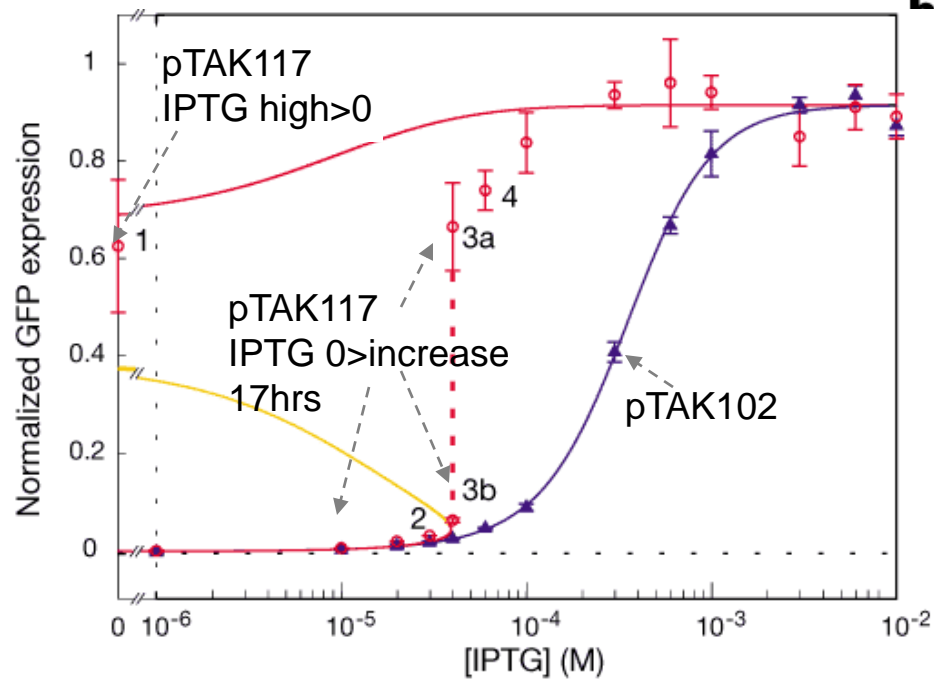
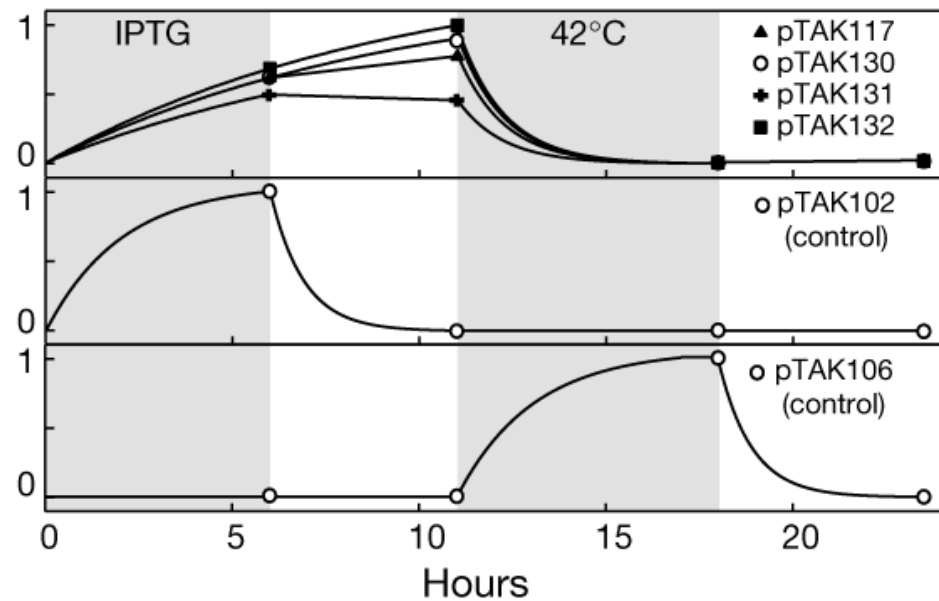
42°C on>off

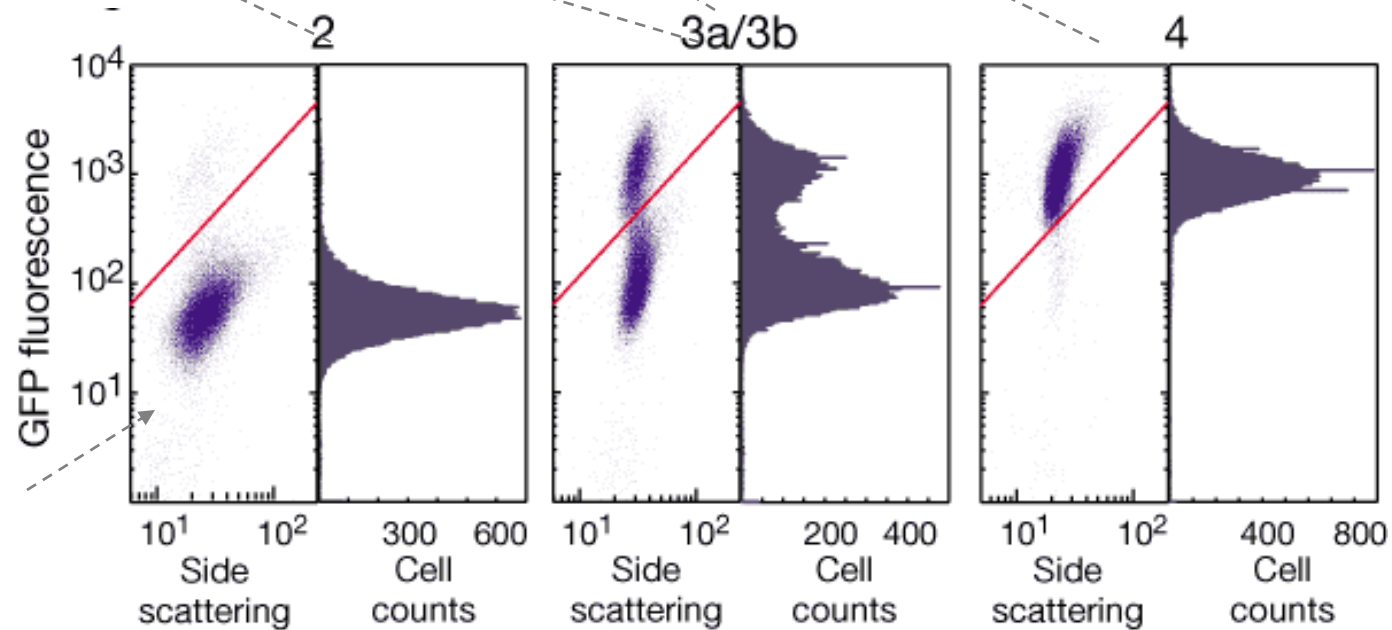
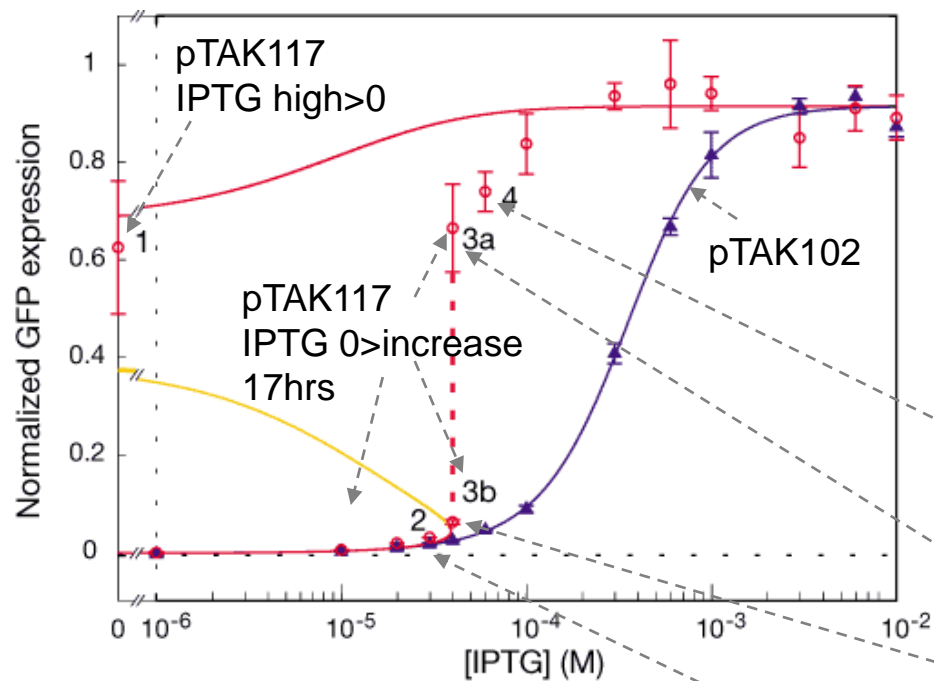
Bistability again, but only GFP off state is reachable





a Normalized GFP expression

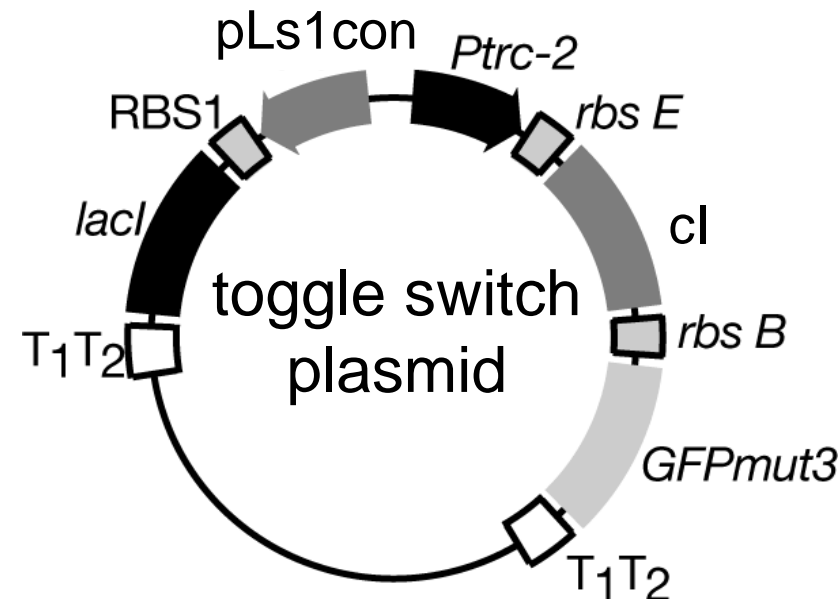




每个点代表一个细胞

Lessons:

1. Quantitation is critical: they used a number of repressor, promoter and rbs, some don't work.
2. Coopertivity of repressor is critical, know from mathematics.
3. Mathematics mostly works
4. Single cell data is different from their mathematics
5. Noises in gene expressions



Analytic stability analysis (not required)

Considering the following two coupled differential equations:

$$\dot{x} = f(x, y)$$

$$\dot{y} = g(x, y)$$

The nullclines are defined as:

$$\dot{x} = 0 \rightarrow f(x_o, y_o) = 0$$

$$\dot{y} = 0 \rightarrow g(x_o, y_o) = 0$$

In order to solve the above eq. we linearize around the fixed points (x_0, y_0) :

$$\tilde{x} \equiv x - x_o$$

$$\tilde{y} \equiv y - y_o$$

Analytic stability analysis (not required)

If $f(x,y)$ and $g(x,y)$ are approximated by a first order Taylor expansion, The previous eq. can be written as:

$$\begin{aligned}\vec{\dot{X}} &= A\vec{X} & \vec{\dot{X}} &= \begin{bmatrix} \dot{x} \\ \dot{y} \end{bmatrix} \\ A &= \begin{bmatrix} a & b \\ c & d \end{bmatrix} & \vec{X} &= \begin{bmatrix} \tilde{x} \\ \tilde{y} \end{bmatrix}\end{aligned}$$

The matrix A is characterized by its trace and the determinant

$$\tau = \text{trace}(A) = a + d$$

$$\Delta = \det(A) = ad - bc$$

Analytic stability analysis (not required)

Let's try to find a solution of the convenient form:

$$\dot{\vec{v}} = \lambda \vec{v} = A \vec{v}$$

This vector is called the eigenvector, λ is the corresponding eigenvalue. The eq. about can be solved by:

$$\det \begin{bmatrix} a - \lambda & b \\ c & d - \lambda \end{bmatrix} = 0$$

Leading to:

$$\lambda_1 = \frac{\tau + \sqrt{\tau^2 - 4\Delta}}{2}$$

$$\lambda_2 = \frac{\tau - \sqrt{\tau^2 - 4\Delta}}{2}$$

$$\Delta = \lambda_1 \lambda_2$$

$$\tau = \lambda_1 + \lambda_2$$

Analytic stability analysis (not required)

For a stable fixed point both λ_1 and λ_2 should be negative.
Therefore a stable fixed point:

$$\Delta > 0$$

$$\tau < 0$$

Analytic stability analysis (not required)

Now let's evaluate the stability of the toggle switch

$$\dot{u} = f(u, v) = \frac{\alpha_1}{1 + v^\beta} - u$$

$$\dot{v} = g(u, v) = \frac{\alpha_2}{1 + u^\gamma} - v$$

The fixed points are:

$$u = \frac{\alpha_1}{1 + v^\beta}$$

$$v = \frac{\alpha_2}{1 + u^\gamma}$$

Analytic stability analysis (not required)

The matrix A is given by:

$$A = \begin{bmatrix} -1 & \frac{-\alpha_1 \beta v^{\beta-1}}{(1+v^\beta)^2} \\ \frac{-\alpha_2 \gamma u^{\gamma-1}}{(1+u^\gamma)^2} & -1 \end{bmatrix}$$

The trace is always negative. The only requirement for stability is $\Delta > 0$. let's focus on $\Delta = 0$, which define the boundary in parameter space that separate bistable from monostable region, which is

$$\frac{\alpha_1 \beta v^{\beta-1}}{(1+v^\beta)^2} \frac{\alpha_2 \gamma u^{\gamma-1}}{(1+u^\gamma)^2} = 1$$

Analytic stability analysis (not required)

Assuming the ratio between ON and Off states is large, the phase diagram can be estimated

