#### **FOR TWO CELLS (numerics)**

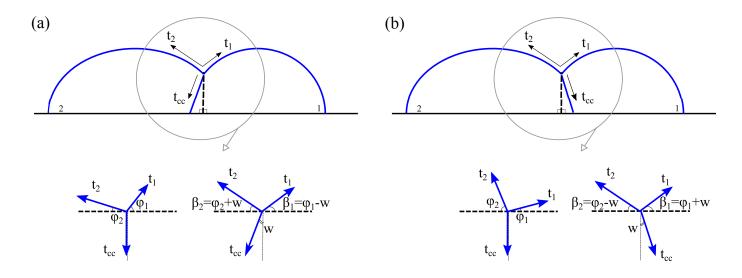
#### Let index 1 denote leader cell while index 2 denotes trailer cell.

An inverse approach where the morphological measurements are known, and the forces (tensions) and velocity are unknown.

Symbol		Meaning (non-dimensional quantities)
f	$\frac{\Delta F}{F}$	Maximal adhesion/protrusion
$t_1$	$\frac{T_1}{F}$	Leader membrane tension
$t_2$	$\frac{T_2}{F}$	Trailer membrane tension
$t_{cc}$	$\frac{T_{cc}}{F}$	Cell-cell adhesive forces
$t_0$	$\frac{T_0}{F}$	Characteristic tension that breaks cell-substrate adhesion
τ	$\frac{T}{F}$	Ratio of membrane tension to adhesion/protrusion
ζ	Effective viscous drag	Effective viscous drag

<sup>\*\*</sup> Start with a guess for tensions. Set  $t_1=1$ , and guesses for  $t_2\in[0.5,2]$  and  $t_{cc}\in[0.01,0.5]$ .

<sup>\*\*</sup> Choose arbitrary values for w and h.



**Figure 1**. Side-view of the two cells. Two possibilities are considered including (a) negative *w* angle and (b) positive *w* angle.

## 1) FORCE BALANCE AT THE TOP OF CELL-CELL INTERACTION REGION given $t_1, t_2$ and $t_{cc}$ (plus a choice of w) to obtain $\phi_1, \phi_2$ then $\beta_1, \beta_2$

(1.a') 
$$t_1 \cos \phi_1 - t_2 \cos \phi_2 = 0$$
 (x-direction)  
(1.b')  $t_1 \sin \phi_1 + t_2 \sin \phi_2 - t_{cc} = 0$  (y-direction)

and

(1.a) 
$$t_1 \cos \beta_1 - t_2 \cos \beta_2 + \frac{w}{|w|} t_{cc} \sin|w| = 0$$
 (x-direction)

(1.b) 
$$t_1 \sin \beta_1 + t_2 \sin \beta_2 - t_{cc} \cos |w| = 0$$
 (y-direction)

Reduce to:

(1.a) 
$$\beta_1 = \cos^{-1}\left(\frac{t_2}{t_1}\cos\beta_2 - \frac{w}{|w|}\frac{t_{cc}}{t_1}\sin|w|\right)$$

$$\text{(1.b)} \quad t_1 \sin \left[ \cos^{-1} \! \left( \frac{t_2}{t_1} \cos \beta_2 - \frac{w}{|w|} \, \frac{t_{cc}}{t_1} \, \sin |w| \, \right) \right] + t_2 \sin \beta_2 - t_{cc} \cos |w| = 0$$

Solve 1.b with fzero in Matlab for  $\beta_2$ . Then use equation 1.a to solve for  $\beta_1$ .

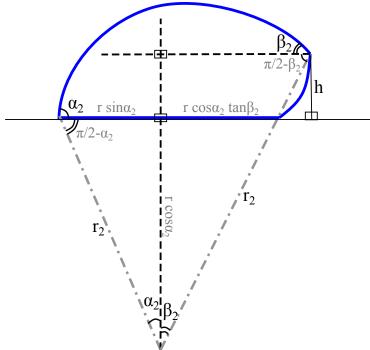
Alternative: eqs. (1.a') and (1.b') reduce to:

(1.a') 
$$\phi_1 = \cos^{-1}\left(\frac{t_2}{t_1}\cos\phi_2\right)$$
  
(1.b')  $t_1 \sin\left[\cos^{-1}\left(\frac{t_2}{t_1}\cos\phi_2\right)\right] + t_2 \sin\phi_2 - t_{cc} = 0$ 

Solve 1.b' with zero in Matlab for  $\phi_2$ . Then use 1.a' to solve for  $\phi_1$ . Finally,  $\beta_1 = \phi_1 \pm w$  and  $\beta_2 = \phi_2 \pm w$  depending on sign of w.

### 2) USE AREAS AND TRIGONOMETRY given $\beta_1, \beta_2, h$ to find $r_1, r_2, \alpha_1$ and $\alpha_2$

From Fig. 2 the **shaded** area of the second cell (trailer) is



$$A_2 = \frac{\pi r_2^2}{2} \frac{(\alpha_2 + \beta_2)}{\pi} - \frac{1}{2} r_2^2 \sin \alpha_2 \cos \alpha_2 - \frac{1}{2} r_2^2 \cos^2 \alpha_2 \tan \beta_2 \equiv 1$$

which yields the following expressions for the radii:

(2.a) 
$$r_1 = \left[ \frac{(\alpha_1 + \beta_1)}{2} - \frac{1}{2} \sin \alpha_1 \cos \beta_1 - \frac{1}{2} \cos^2 \alpha_1 \tan \beta_1 \right]^{-1/2}$$
(2.b) 
$$r_1 = \left[ \frac{(\alpha_2 + \beta_2)}{2} - \frac{1}{2} \sin \alpha_1 \cos \beta_1 - \frac{1}{2} \cos^2 \alpha_1 \tan \beta_1 \right]^{-1/2}$$

(2.b) 
$$r_2 = \left[ \frac{(\alpha_2 + \beta_2)}{2} - \frac{1}{2} \sin \alpha_2 \cos \beta_2 - \frac{1}{2} \cos^2 \alpha_2 \tan \beta_2 \right]^{-1/2}$$

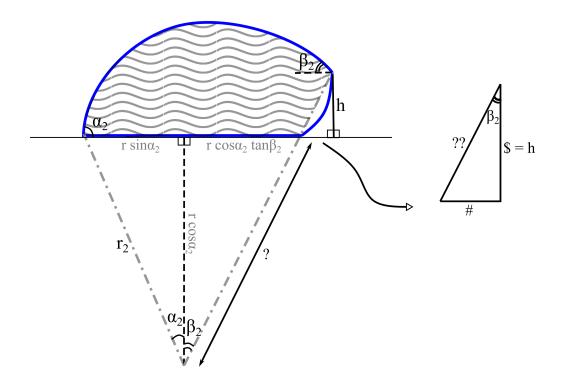


Figure 3. Zoom in of trailer cell to illustrate area computation for (2.a) and (2.b)

We can improve our area calculation slightly; including the small triangle on the right-side (not the arc section) in the area calculation produces

$$A_2 = \frac{\pi r_2^2}{2} \frac{(\alpha_2 + \beta_2)}{\pi} - \frac{1}{2} r_2^2 \sin \alpha_2 \cos \alpha_2 - \frac{1}{2} r_2^2 \cos^2 \alpha_2 \tan \beta_2 + \frac{1}{2} r_2^2 \Big(\cos \beta_2 - \cos \alpha_2 \tan \beta_2\Big) \Big(\sin \beta_2 - \cos \alpha_2 \tan^2 \beta_2\Big) \equiv 1$$

The resulting radii are

(2.a) 
$$r_{1} = \left[ \frac{(\alpha_{1} + \beta_{1})}{2} - \frac{1}{2} \sin \alpha_{1} \cos \beta_{1} - \frac{1}{2} \cos^{2} \alpha_{1} \tan \beta_{1} + \frac{1}{2} \left( \cos \beta_{1} - \cos \alpha_{1} \tan \beta_{1} \right) \left( \sin \beta_{1} - \cos \alpha_{1} \tan^{2} \beta_{1} \right) \right]^{-1/2}$$
(2.b) 
$$r_{2} = \left[ \frac{(\alpha_{2} + \beta_{2})}{2} - \frac{1}{2} \sin \alpha_{2} \cos \beta_{2} - \frac{1}{2} \cos^{2} \alpha_{2} \tan \beta_{2} + \frac{1}{2} \left( \cos \beta_{2} - \cos \alpha_{2} \tan \beta_{2} \right) \left( \sin \beta_{2} - \cos \alpha_{2} \tan^{2} \beta_{2} \right) \right]^{-1/2}$$

From trigonometry we also know that

$$(2.c) \quad h = r_1 \left( \cos \beta_1 - \cos \alpha_1 \right)$$

$$(2.d) \quad h = r_2 \left(\cos \beta_2 - \cos \alpha_2\right)$$

#### 3) FROM LAPLACE'S LAW the intracellular pressure is:

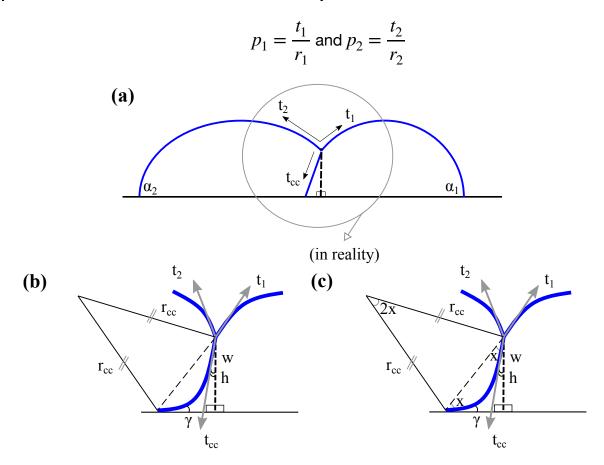


Figure 3. Zoom in of the cell-cell interface and the resulting angles in the wedge

#### 4) FROM LAPLACE'S LAW find the radius of curvature for the cell-cell junction

$$p_2 - p_1 = \frac{t_{cc}}{r_{cc}} \rightarrow r_{cc} = \frac{t_{cc}}{t_2/r_2 - t_1/r_1}$$

# 5) USE TRIGONOMETRY AT CELL-CELL INTERFACE given $h,w,r_{cc}$ , to find the angle $\gamma$ at the ventral end of the cell-cell boundary

(1) 
$$\cos(|x| + |w|) = \frac{h}{s}$$

$$(2) \sin(|x| + \gamma) = \frac{h}{s}$$

 $(3) s^2 = 2r_{cc}^2 (1 - \cos(2|w|))$  (where s is the third side in the isosceles triangle with sides  $r_{cc}$ )

Combining (1) and (3), to obtain:

$$\frac{h^2}{\cos^2(|x| + |w|)} = 2r_{cc}^2 \left(1 - \cos(2|x|)\right) \text{ fzero for } x \in [0, \pi/4].$$

Then: 
$$\gamma = \frac{\pi}{2} - |w| - 2|x|$$
.

#### 6) LASTLY, USE THE FORCE BALANCE AT THE VENTRAL POINTS:

Force balance at the front endpoint of the leader cell:

(6.a) 
$$(1+f)\left(1-\frac{t_1}{t_0+\tau}\right)-\zeta_1 v = t_1 \cos \alpha_1$$

Force balance at the rear endpoint of the trailer cell:

(6.b) 
$$(1-f)\left(1-\frac{t_2}{t_0-\tau}\right) + \zeta_2 v = t_2 \cos \alpha_2$$

Force balance at the cell-cell interaction zone:

(6.c) 
$$t_{cc}\cos(\gamma) = \zeta_{cc}v$$

Obtain velocity. (Each equation represents a plane in 3D space)