## ME 488: DESIGN OF EXPERIMENTS

LECTURE 3: FULL FACTORIALS

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### **NUCLEAR POWER SHUT-OFF VALVES**

## Kühme DN 200 Butterfly Reactor Containment Shut-Off Valve



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Kühme DN 200 Butterfly Reactor Containment Shut-Off Valve



## **Optimization Concerns**

Due to its use on a submarine, we want to minimize the acoustic operating characteristics. We have design options of:

- · Nominal Diameter: Either 600 mm or 1200 mm
- Closing Springs: 1000N/m or 2000N/m\*
- · Seal Method: Metal-Metal or Metal-Elastomer\*

### **FULL FACTORIAL DESIGNS**

# **Factorial Designs**

- Two Treatment Variables A and B with a total number of levels
  - of a and b respectively
- $a \times b$  factorial design: levels of both variables are selected in random order
- More general:  $a \times b \times c \times ...$  factorial design
- If the same number of replicates in each cell the design is
   Balanced
- If all possible *combinations* of  $a \times b \times c \times ...$  are included in design, the design is said to be **Full**

# Balanced Full Factorial Design

## $a \times b$ Factorial Design

- · k Treatment Variables
- Main Effects  $\binom{k}{1}$
- Two-Way Interactions  $\binom{k}{2}$
- Three-Way Interactions  $\binom{k}{3}$
- . . .
- ·  $df_{total} = a \times b \times c \times \cdots \times l_k \times (n-1)$

## Most Common Design Setup

- k Factors, each with 2 Levels designated as + and -
- 2<sup>k</sup> refers to the number of unique cells or runs in each replicate of the design
- Easy to Analyze
- Good at the beginning of a study
- · Only valid if effect is unidirectional

#### Sort of Trivial

• Each replicate consists of  $2^1 = 2$  runs

- Model:  $y = \beta_0 + \beta_1 x_1$
- Idea is to see if a factor  $[x_1]$  matters
- · Only checks at two different values of that factor

#### Back to our Valve...

- · We want to see if the Nominal Diameter matters
- Each replicate consists of  $2^1 = 2$  runs
- · Design Matrix

Standard Order	Run Order	<i>X</i> <sub>1</sub>
1	2	_
2	1	+

• Model:  $y = \beta_0 + \beta_1 X_1 + \varepsilon_{error}$ 

#### Back to our Valve..

• Model Matrix [sort of pointless for 2<sup>1</sup> design]

Standard Order	Run Order	<i>X</i> <sub>1</sub>
1	2	_
2	1	+

Planning Matrix

Standard Order	Run Order	Nominal Diameter
1	2	600mm
2	1	1200mm

• We aren't going to fully analyze this, we will look at a more complex example later.

## Very Common Design

• Each replicate consists of  $2^2 = 4$  runs

Run	<i>X</i> <sub>1</sub>	<i>X</i> <sub>2</sub>
1	_	_
2	_	+
3	+	_
4	+	+

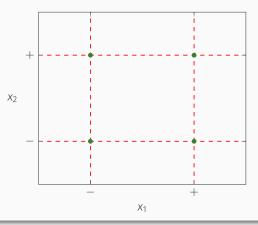
- Model Main Effects Only:  $y = \beta_0 + \beta_1 x_1 + \beta_2 x_2 + \varepsilon_{error}$
- · Interaction Effects:

$$y = \beta_0 + \beta_1 x_1 + \beta_2 x_2 + \beta_{12} x_{12} + \varepsilon_{error}; x_{12} = x_1 x_2$$

- · Still only checks at two different values of that factor
- But allows investigation of interaction effects

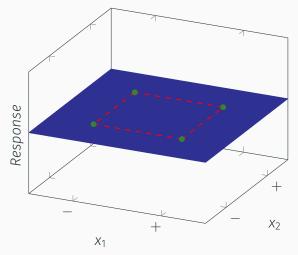
# 2<sup>2</sup> Design Graphic

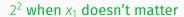
2<sup>2</sup> Designs are visualized as a square

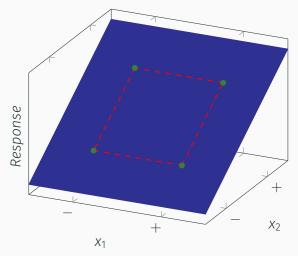


These are four 'test' points seeking the slope of the response

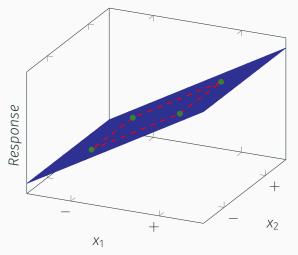




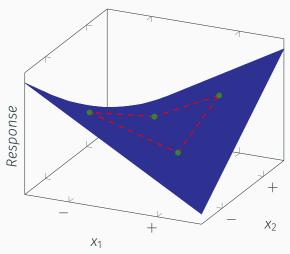












## Degrees of Freedom Run Out...

Everything is good, except when you want to detect interactions...

• 
$$y = \beta_0 + \beta_1 x_1 + \beta_2 x_2 + \beta_{12} x_{12} + \varepsilon_{error}$$

• 
$$df_{x_1} = K_{x_1} - 1 = 2 - 1 = 1$$

• 
$$df_{x_2} = K_{x_2} - 1 = 2 - 1 = 1$$

• 
$$df_{X_{12}} = (K_{X_1} - 1)(K_{X_2} - 1) = (2 - 1)(2 - 1) = 1$$

• 
$$df_{total} = K_{x_1}K_{x_2} - 1 = (2)(2) - 1 = 3$$
; For  $n_i = 1$ 

But that means

$$df_{error} = df_{total} - df_{x_1} - df_{x_2} - df_{x_{12}} = 3 - 1 - 1 - 1 = 0$$

So how do we gain dferror to look at interactions?

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$$y = \beta_0 + \beta_1 x_1 + \beta_2 x_2 + \beta_{12} x_{12} + \varepsilon_{error}$$

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$$df_{x_1} = K_{x_1} - 1 = 2 - 1 = 1$$

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$$df_{x_2} = K_{x_2} - 1 = 2 - 1 = 1$$

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$$df_{X_{12}} = (K_{X_1} - 1)(K_{X_2} - 1) = (2 - 1)(2 - 1) = 1$$

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$$df_{total} = K_{x_1}K_{x_2} - 1 = (2)(2) - 1 = 3$$
; For  $n_i = 1$ 

But that means

$$df_{error} = df_{total} - df_{x_1} - df_{x_2} - df_{x_{12}} = 3 - 1 - 1 - 1 = 0$$

So how do we gain  $df_{error}$  to look at interactions? Increase  $n_i$ , AKA Do more replicates!

### Just to make it clear...

When doing a 2<sup>2</sup> design:

- There are TWO Factors [e.g. Temp, Press, Viscosity, etc]
- There are TWO Levels of Each Factor [e.g. +, and -, but means 'On'/'Off', '24.3mm'/'12mm', etc.]
- Each Replicate needs  $2^2 = 4$  Runs [measurements] taken
- You can model it with or without df<sub>error</sub>
- · You can model it with or without interactions
- If you run only one Replicate, then you have no df<sub>error</sub> for an Interaction Model

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- You can model it with or without interactions
- If you run only one Replicate, then you have no df<sub>error</sub> for an Interaction Model

Now, let's look at a 2<sup>3</sup> design before we get into examples, since this one is a bit less trivial

# Now we are getting somewhere

• Each replicate consists of  $2^3 = 8$  runs

Run	<i>X</i> <sub>1</sub>	<i>X</i> <sub>2</sub>	<i>X</i> <sub>3</sub>
1	_	_	_
2	_	_	+
3	_	+	_
4	_	+	+
5	+	_	_
6	+	_	+
7	+	+	_
8	+	+	+

· Still only checks at TWO different values of each factor

#### Possible Models

· Model Main Effects Only:

$$y = \beta_0 + \beta_1 x_1 + \beta_2 x_2 + \beta_3 x_3 + \varepsilon_{error}$$

· Two Way Interaction Effects:

$$y = \beta_0 + \beta_1 x_1 + \beta_2 x_2 + \beta_3 x_3$$
  
+\beta\_{12} x\_{12} + \beta\_{13} x\_{13} + \beta\_{23} x\_{23} + \varepsilon\_{error}  
; \chi\_{12} = \chi\_1 x\_2; \chi\_{13} = \chi\_1 x\_3; \chi\_{23} = \chi\_2 x\_3

• Three Way Interaction Effects:

$$\begin{aligned} y &= \beta_0 + \beta_1 x_1 + \beta_2 x_2 + \beta_3 x_3 \\ &+ \beta_{12} x_{12} + \beta_{13} x_{13} + \beta_{23} x_{23} \\ &+ \beta_{123} x_{123} + \varepsilon_{error} \\ ; x_{12} &= x_1 x_2; x_{13} = x_1 x_3; x_{23} = x_2 x_3; x_{123} = x_1 x_2 x_3 \end{aligned}$$

**Quick Check** 

Quick check: What does  $\beta_0$  represent?

### **Quick Check**

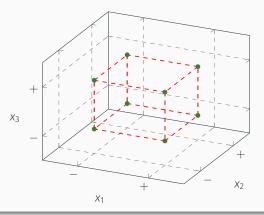
Quick check: What does  $\beta_0$  represent?

$$\beta_0 = \bar{y}$$

Its the 'Average' model [i.e. none of the factors matter]

# 2<sup>3</sup> Design Graphic

2<sup>3</sup> Designs are visualized as a cube



These are eight 'test' points seeking the response surface

Source		df	$df_{n=1}$	$df_{n=2}$	df <sub>n</sub>
А	<i>X</i> <sub>1</sub>	$K_{x_1} - 1$	1	1	1
В	<i>X</i> <sub>2</sub>	$K_{x_2} - 1$	1	1	1
С	<i>X</i> <sub>3</sub>	$K_{x_3} - 1$	1	1	1
AB	X <sub>12</sub>	$(K_{x_1}-1)(K_{x_2}-1)$	1	1	1
AC	X <sub>13</sub>	$(K_{x_1}-1)(K_{x_3}-1)$	1	1	1
ВС	X <sub>23</sub>	$(K_{x_2}-1)(K_{x_3}-1)$	1	1	1
ABC	X <sub>123</sub>	$(K_{x_1}-1)(K_{x_2}-1)(K_{x_3}-1)$	1	1	1
Error	€error	$K_{X_1}K_{X_2}K_{X_3}(n-1)$	0	8	8(n-1)
Total		$K_{x_1}K_{x_2}K_{x_3}n-1$	7	15	8n — 1

So how do we gain dferror to allow us to look at interactions?

• Yes, we can increase  $n_i$ , AKA Do more Replicates

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  - Make no Engineering sense
  - · or are Statistically insignificant

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- We can also get rid of interaction terms that either:
  - · Make no Engineering sense
  - or are Statistically insignificant

#### But we have to be careful and not cut too much!

- · Take out interactions of little value
- · Don't let regression model suffer too much

# Measuring a Model

- Measure of Usefulness of a Regression Model is expressed in a term called Coefficient of Determination
- But most people call it  $r^2 = \frac{SS_{model}}{SS_{total}}$
- The ratio of the variation the model can explain to the amount of total variation in the data.
- · Usually easier to calculate from an ANOVA by:

• 
$$r^2 = 1 - \frac{SS_{error}}{SS_{total}}$$

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### Quick check

- Range of  $r^2$  is?  $\leq r^2 \leq$
- $r^2 = 1$ : Means what? and  $r^2 = 0$ : Means what?

But we are dealing with a bunch of independent factors and interactions so...

- We use an Adjusted Coefficient of Determination
- $\cdot$  But most people call it  $r_{adj}^2$
- $\cdot r_{adj}^2 = 1 \frac{df_{total}}{df_{error}} \frac{SS_{error}}{SS_{total}}$
- $r_{adj}^2 < r^2$
- $\cdot$   $r_{adj}^2$  is safer to use in application

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As for those pesky coefficients...without boring you with the needless details

• We just want to be confident that they are not 0. Why?

# **Use Engineering Sense**

Occam's Razor: Simplest model is 'probably' best

- Throw out terms until  $r_{adi}^2$  doesn't degrade
- Use Engineering Sense and Principles
  - 1. Hierarchical Ordering Principle
    - · Lower order effects are likely more important than higher
    - · Effects of the same order are likely equally important
  - 2. Effect Sparsity Principle
    - Number of important effects in a factorial experiment is small
    - · True model is most often linear.
  - 3. Effect Heredity Principle
    - For an interaction to be significant, usually at least one of its parent factors should be significant.

#### Back to our valve...

Kühme DN 200 Butterfly Reactor Containment Shut-Off Valve



## **Optimization Concerns**

Due to its use on a submarine, we want to minimize the acoustic operating characteristics. We have design options of:

- Nominal Diameter: Either 600 mm or 1200 mm
- Closing Springs: 1000N/m or 2000N/m
- · Seal Manufacture: Metal-Metal or Metal-Elastomer

## Setup

- There are THREE Factors [K = 3]
  - · x<sub>1</sub>: Nominal Diameter
  - x<sub>2</sub>: Closing Springs Constant
  - x<sub>3</sub>: Seal Manufacture
- · There are TWO Levels to each factor
  - *x*<sub>1</sub>: Nominal Diameter [—:600mm; +:1200mm]
  - $x_2$ : Closing Springs Constant [-:1000N/m; +:2000N/m]
  - x<sub>3</sub>: Seal Manufacture [—: M-M; +: M-E]
- So this is a 2<sup>3</sup> Design
- We are going to test all combinations with equal number of samples per combination, so it is a?
- Each replicate consists of  $2^3 = 8$  runs

## Design Matrix

Standard Order	Run Order	<i>X</i> <sub>1</sub>	<i>X</i> <sub>2</sub>	<i>X</i> <sub>3</sub>
1	6	_	_	_
2	8	_	_	+
3	5	_	+	_
4	2	_	+	+
5	4	+	_	_
6	3	+	_	+
7	7	+	+	_
8	1	+	+	+

### **Planning Matrix**

Standard Order	Run Order	Nom. Dia.	Spring Const.	Seal
1	6	600mm	1000N/m	M-M
2	8	600mm	1000N/m	M-E
3	5	600mm	2000N/m	M-M
4	2	600mm	2000N/m	M-E
5	4	1200mm	1000N/m	M-M
6	3	1200mm	1000N/m	M-E
7	7	1200mm	2000N/m	M-M
8	1	1200mm	2000N/m	M-E

#### **Model Matrix**

Standard Order	Run Order	<i>X</i> <sub>1</sub>	<i>X</i> <sub>2</sub>	<i>X</i> <sub>3</sub>	X <sub>12</sub>	X <sub>13</sub>	X <sub>23</sub>	X <sub>123</sub>
1	6	_	_	_	+	+	+	_
2	8	_	_	+	+	_	_	+
3	5	_	+	_	_	+	_	+
4	2	_	+	+	_	_	+	_
5	4	+	_	_	_	_	+	+
6	3	+	_	+	_	+	_	_
7	7	+	+	_	+	_	_	_
8	1	+	+	+	+	+	+	+

# Collecting Data and putting it into Model Matrix

Due to the cost and radiation exposure concerns only one replicate was done

Standard Order	У	<i>X</i> <sub>1</sub> A	<i>х</i> <sub>2</sub> В		<i>X</i> <sub>12</sub> AB		<i>X</i> <sub>23</sub> BC	X <sub>123</sub> ABC
1	68	_	_	_	+	+	+	_
2	87	_	_	+	+	_	_	+
3	64	_	+	_	_	+	_	+
4	57	_	+	+	_	_	+	_
5	91	+	_	_	_	_	+	+
6	131	+	_	+	_	+	_	_
7	85	+	+	_	+	_	_	_
8	123	+	+	+	+	+	+	+

#### Possible Models

· Model Main Effects Only:

$$y = \beta_0 + \beta_1 X_1 + \beta_2 X_2 + \beta_3 X_3 + \varepsilon_{error}$$

· Two Way Interaction Effects:

$$y = \beta_0 + \beta_1 X_1 + \beta_2 X_2 + \beta_3 X_3$$
  
+\beta\_{12} X\_{12} + \beta\_{13} X\_{13} + \beta\_{23} X\_{23} + \varepsilon\_{error}  
; X\_{12} = X\_1 X\_2; X\_{13} = X\_1 X\_3; X\_{23} = X\_2 X\_3

\*\*\*Three Way Interaction Effects\*\*\*:

$$\begin{aligned} y &= \beta_0 + \beta_1 x_1 + \beta_2 x_2 + \beta_3 x_3 \\ &+ \beta_{12} x_{12} + \beta_{13} x_{13} + \beta_{23} x_{23} \\ &+ \beta_{123} x_{123} + \varepsilon_{error} \\ ; x_{12} &= x_1 x_2; x_{13} = x_1 x_3; x_{23} = x_2 x_3; x_{123} = x_1 x_2 x_3 \end{aligned}$$

## Put the data into a CSV File and bring it into R

```
> myData <- read.csv("ME488_Lecture_Week3_DATA.csv")
> myData # Confirm Data is loaded
```

#### Output

```
I Aco_Res A B C

I 1 1 91 1 -1 -1

1 2 2 123 1 1 1

4 3 3 68 -1 -1 -1

5 4 4 131 1 -1 1

6 5 5 85 1 1 -1

7 6 6 87 -1 -1 1

8 7 7 64 -1 1 -1

9 8 8 57 -1 1 1
```

## Run a Regression Model and Look at the Summary

```
1 | > m<-lm(Aco_Res~A*B*C, data=myData)
```

### Output

3

5

6 7

8

9

10

11

12

13

14

15

16

17

18 19

20

```
Call:
lm(formula = Aco Res ~ A * B * C, data = myData)
Residuals:
ALL 8 residuals are 0: no residual degrees of freedom!
Coefficients:
            Estimate Std. Error t value Pr(>|t|)
(Intercept)
               88.25
                             NA
                                     NA
                                               NA
               19 25
                             NΑ
                                     NΑ
                                               NΑ
               -6.00
                             NA
                                     NA
                                               NA
              11.25
                             NA
                                     NA
                                               NA
A \cdot B
              2.50
                             NΑ
                                     NΑ
                                               NΑ
A \cdot C
              8 25
                             NΑ
                                     NΑ
                                               NΑ
B : C
              -3.50
                             NA
                                     NA
                                               NA
A \cdot B \cdot C
              3.00
                             NΑ
                                     NΑ
                                               NΑ
Residual standard error: NaN on O degrees of freedom
Multiple R-squared: 1, Adjusted R-squared:
                                                      NaN
F-statistic: NaN on 7 and 0 DF, p-value: NA
```

### Model at this point

· Three Way Interaction Effects:

$$y = \beta_0 + \beta_1 x_1 + \beta_2 x_2 + \beta_3 x_3$$

$$+\beta_{12} x_{12} + \beta_{13} x_{13} + \beta_{23} x_{23}$$

$$+\beta_{123} x_{123} + \varepsilon_{error}$$

$$; x_{12} = x_1 x_2; x_{13} = x_1 x_3; x_{23} = x_2 x_3; x_{123} = x_1 x_2 x_3$$

$$y = 88.25 + 19.25 x_1 - 6.00 x_2 + 11.25 x_3 + 2.50 x_{12} + 8.25 x_{13} - 3.50 x_{23} + 3.00 x_{123} + \varepsilon_{error}$$

Supposedly everything matters, but no confidence in anything!

### Downgrade the Model

· Drop the Three Way Interaction Effect

$$y = \beta_0 + \beta_1 x_1 + \beta_2 x_2 + \beta_3 x_3 + \beta_{12} x_{12} + \beta_{13} x_{13} + \beta_{23} x_{23} + \varepsilon_{error}$$

· And run it again

```
1 > m<-lm(Aco_Res~A+B+C+A*B+A*C+B*C, data=myData)
2 > summary(m)
```

#### Output

2

5

10

11 12 13

14

15

```
Coefficients:
           Estimate Std. Error t value Pr(>|t|)
(Intercept)
              88.25
                        3.00
                              29.417
                                     0.0216 *
             19.25
                    3.00
                              6.417
                                     0.0984 .
              -6.00
                    3.00
                             -2.000 0.2952
             11.25
                    3.00
                             3.750
                                     0.1659
A : B
             2.50
                        3.00 0.833
                                     0.5577
             8.25
                        3.00 2.750
A : C
                                     0.2220
B \cdot C
              -350
                        3.00 - 1.167
                                       0 4511
Signif. codes: 0 '***' 0.001 '**' 0.05 '.' 0.1 ' ' 1
Residual standard error: 8.485 on 1 degrees of freedom
Multiple R-squared: 0.9857, Adjusted R-squared: 0.8998
F-statistic: 11.48 on 6 and 1 DF, p-value: 0.2222
```

#### Issues

 The F is above 8 but we have to be careful due to low sample size

```
1 F-statistic: 11.48 on 6 and 1 DF, p-value: 0.2222
```

 A few coefficients p-values are horrible, A:B [Nominal Diameter interacting with Spring Constants] is the worst

```
A:B 2.50 3.00 0.833 0.5577
```

• We still have room to move in  $r_{adj}^2$ 

```
Multiple R-squared: 0.9857, Adjusted R-squared: 0.8998
```

9

11 12

13

14

#### So lets get rid of A:B and see what happens

```
Coefficients:
           Estimate Std. Error t value Pr(>|t|)
(Intercept)
            88.250
                   2.761 31.959 0.000978 ***
            19.250 2.761 6.971 0.019963 *
                   2.761 -2.173 0.161884
            -6.000
                   2.761 4.074 0.055297 .
            11.250
A : C
            8.250 2.761 2.988 0.096145
                   2.761 -1.268 0.332576
B \cdot C
            -3500
Signif. codes: 0 '***' 0.001 '**' 0.05 '.' 0.1 ' ' 1
Residual standard error: 7.81 on 2 degrees of freedom
Multiple R-squared: 0.9757, Adjusted R-squared: 0.9151
F-statistic: 16.09 on 5 and 2 DF, p-value: 0.05954
```

# You can keep refining..and will do in homework!

But before we go, remember we are trying to see if the confidence interval on the coefficients contain zero.

We are pretty sure A [Nominal Diameter] matters, and it looks like C [Seal Method] is getting close. Getting a sense that B [Spring Constants] don't really matter.

#### **DUE FOR NEXT TIME**

#### But...

- At the end we started dropping terms, which means we wasting resources by over-collecting data
- Is there a way to capitalize on this, if we know ahead of time that some interactions are not important?
- Yes, Fractional Factorial Designs

### Things to help you succeed

- · Design, Planning, and Model Matrices
- $\cdot$  Relationship between Factors,  $x_i$  and ABC notation
- · Interpreting a summary of a regression in R