

# Complete-Mix Tanks-in-Series Approach to Modeling Hydraulics of Oxidation Ponds

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# 1 Introduction

The complete-mix tanks-in-series (CMTS) approach can be used to model the hydraulics of oxidation ponds. The CMTS approach is a conceptual model that is often more accurate than complex models such as advection-dispersion. The CMTS assumes that the total volume of a pond can be approximated by  $n$  completely mixed tanks linked in series (Figure 1). The approach can be improved by including a backwards (“recycle”) flow rate between tanks which is assumed to be a fraction of the overall flow rate (Finney 2006).

Assuming a first-order reaction rate, an  $n$  tank system can be represented by (Finney 2006)

$$\begin{aligned}
 -\left(\frac{Q+Q_r}{V} + k\right) c_1 + \frac{Q_r}{V} c_2 &= -\frac{Q c_{in}}{V} \text{ for tank 1} \\
 \left(\frac{Q+Q_r}{V}\right) c_{i-1} - \left[\left(\frac{Q+2Q_r}{V}\right) + k\right] c_i &= 0 \text{ for tanks } 2, 3, \dots, n-1 \\
 \left(\frac{Q+Q_r}{V}\right) c_{n-1} - \left[\left(\frac{Q+Q_r}{V}\right) + k\right] c_n &= 0 \text{ for tank } n
 \end{aligned} \tag{1}$$

where

- $Q$  = influent flow rate ( $\text{m}^3/\text{day}$ )
- $Q_r$  = recycle flow rate ( $\text{m}^3$ )
- $V$  = tank or compartment volume ( $\text{m}^3$ )
- $k$  = first order reaction rate constant ( $\text{day}^{-1}$ )
- $c_{in}$  = influent pollutant concentration ( $\text{mg/l}$ )
- $c_i$  = pollutant concentration in conceptual tank  $i$  ( $\text{mg/l}$ )

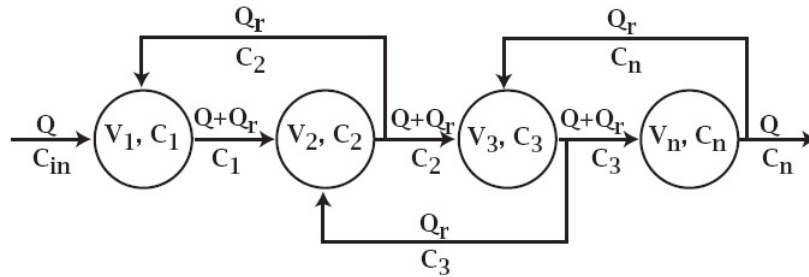


Figure 1:  $n$  tanks in series (Finney 2006)

## 2 Methodology

When expanded to fit  $n$  tanks, system (1) becomes a tridiagonal system of the general form

$$\begin{bmatrix} f_1 & g_1 & & & & & \\ e_1 & f_2 & g_2 & & & & \\ & e_2 & f_3 & g_3 & & & \\ & & \cdot & \cdot & \cdot & & \\ & & & \cdot & \cdot & \cdot & \\ & & & & \cdot & \cdot & \cdot \\ & & & & & e_{n-1} & f_{n-1} & g_{n-1} \\ & & & & & & e_n & f_n \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \\ x_3 \\ \cdot \\ \cdot \\ \cdot \\ x_{n-1} \\ x_n \end{bmatrix} = \begin{bmatrix} r_1 \\ r_2 \\ r_3 \\ \cdot \\ \cdot \\ \cdot \\ r_{n-1} \\ r_n \end{bmatrix}$$

This type of  $Ax=\underline{b}$  linear system can be solved using the technique of Gauss elimination. Gauss elimination would involve storing a large amount of empty space and carrying out many useless computations. This problem is ideal for use with the Gauss-Seidell (G-S) method. The G-S method is efficient in terms of speed and memory when systems involve large numbers of zero terms. In cases like these each equation as well as the G-S algorithm can be hard-wired into the program for increased efficiency (Chapra et al. 286-289).

The general algorithm for the G-S method with relaxation is

$$x_i^{(k+1)} = x_i^{(k)} + \omega \left[ \left( b_i - \sum_{j=1}^{i-1} a_{ij}x_j^{(k+1)} - \sum_{j=i}^n a_{ij}x_j^{(k)} \right) / a_{ii} \right] \quad (2)$$

Where  $x^{(k)}$  denotes the solution at the  $k^{th}$  iteration and  $\omega$  is the relaxation factor ( $0 < \omega < 2$ ) that affects the convergence of the rate of the solution. If  $\omega < 1$  then the convergence rate is underrelaxed. If  $\omega > 1$  then the convergence rate is overrelaxed. There exists a value of  $\omega$  for which the solution will converge the fastest.

A sufficient condition to ensure convergence is diagonal dominance

$$|a_{ii}| > \sum_{\substack{j=1 \\ j \neq i}}^n |a_{ij}| \quad (3)$$

Equation (3) states that for each row the absolute value of the diagonal element must be greater than the sum of the absolute value of the off diagonal elements to ensure convergence (Figure 2). The convergence speed of the solution is directly related to the degree of diagonal dominance, however, the solution may still converge if this criterion is not satisfied (Finney 2006).

```

do i=1,ntanks
  offdiagsum=0
  offdiagsum=sum(abs(A(i,1:ntanks)))-abs(A(i,i))
  if(offdiagsum>abs(A(i,i)))then
    write(*,*)"Answer may not converge."
  end if
end do

```

Figure 2: Test for diagonal dominance

Program CMTS (Appendix A) does not utilize the full benefits of the G-S method. Program CMTS uses the coefficient matrix  $A$  augmented with the right hand side vector  $\underline{b}$  as  $[A|\underline{b}]$ . Storing a whole coefficient matrix is inefficient but the calculations for this lab are not computationally intensive. In this case the speed of the procedure is not noticeably slowed. The G-S method is carried out within the main program (Figure 3).

```

do
  itr=itr+1
  done=0
  do i=1,ntanks
    check=0
    check=x(i)
    x(i)=x(i)+w*((AB(i,ntanks+1)-sum(AB(i,1:i-1)*x(1:i-1))&
      -sum(AB(i,i:ntanks)*x(i:ntanks)))/AB(i,i))
    if(abs(check-x(i))<eps)then
      done=done+1
    end if
  end do
  if(stopping criteria met)then
    exit
  end if
end do

```

Figure 3: Gauss-Seidell algorithm

The first stopping criterion for this method is a max iteration test. A high relaxation factor can cause the number of iterations to be very high. The second stopping criterion is and a solution found test

$$|x_i^{(k)} - x_i^{(k+1)}| < \varepsilon \quad (4)$$

This method tests the solution element by element for increased accuracy (Figure 4).

```

if(abs(check-x(i))<eps)then
  done=done+1
end if
if(done==ntanks)then
  write(*,*)"Solution found"
  exit
end if

```

Figure 4: Solution found test

### 3 Application

The concentration in each “tank” is determined from various parameters which are known in the problem (Table 1).

Table 1: Parameters associated with determining concentration values

Parameter	Variable	Value
Influent flow rate	$Q$	10000
Recycle flow rate	$Q_r$	$.2Q$
Tank or compartment volume	$V$	50000 m <sup>3</sup>
First order reaction rate constant	$k$	0.093/day
Influent pollutant concentration	$c_{in}$	30 mg/l
Stopping tolerance	$\varepsilon$	0.00001
Relaxation factor	$\omega$	1.0

Each parameter can be varied to determine the sensitivity of the solution

Table 2: Variation of parameters

Run #	Variable	Initial value	New value	Variation
1	$Q$	10000	11000	10%
2			9000	-10%
3	$Q_r$	$.2Q$	$.22Q$	10%
4			$.18Q$	-10%
5	$V$	50000 m <sup>3</sup>	55000	10%
6			45000	-10%
7	$k$	0.093/day	0.1023	10%
8			0.0837	-10%
9	$c_{in}$	30 mg/l	30	10%
10			27	-10%
11	$\varepsilon$	0.00001	0.000011	10%
12			0.000009	-10%

## 4 Results

Using the suggested value of 5 tanks, program CMTS gives

$$c = \begin{bmatrix} 27.03 & 24.77 & 22.70 & 20.83 & 19.34 \end{bmatrix}^T \text{ (mg/l)}$$

The final value of the concentration ( $c_n$ ) is higher than the observed value of 19 mg/l. A higher number of tanks must be tried using trial and error to find a  $c_n$  that matches the observed value (Table 3). 18 iterations gives the closest  $c_n$  to the observed value 19 mg/l.

Table 3: Determining optimal number of tanks

# of Tanks	$c_n$
5	19.34
10	19.11
15	19.03
16	19.01
17	19.01
18	19.00

The sensitivity analysis reveals how  $c_n$  changes with the variation of parameters (all values found using  $c_{initial}=30$ ,  $n=18$  tanks,  $\omega=1$ ) (Table 4). The most influential parameter,  $c_{in}$ , causes a direct variation in  $c_n$ .  $Q_r$  and  $\varepsilon$  cause the least variation in  $c_n$ .

Table 4: Sensitivity analysis

Run #	Variable	New value	Variation	$c_n$	$\Delta c_n$	# iterations
1	$Q$	11000	10%	19.79	4.16%	22
2		9000	-10%	18.08	-4.84%	22
3	$Q_r$	.22 $Q$	10%	19.00	0.00%	24
4		.18 $Q$	-10%	18.99	-0.05%	21
5	$V$	55000	10%	18.16	-4.42%	22
6		45000	-10%	19.87	4.58%	22
7	$k$	0.1023	10%	18.17	-4.37%	22
8		0.0837	-10%	19.87	4.58%	22
9	$c_{in}$	30	10%	20.90	10.00%	20
10		27	-10%	17.10	-10.00%	23
11	$\varepsilon$	0.000011	10%	19.00	0.00%	22
12		0.000009	-10%	19.00	0.00%	22

When all other parameters are held constant and  $\omega$  is allowed to vary the only effect is a change in the number of iterations to find the solution (Table 5). The number of iterations vary widely but the most acceptable range for the relaxation coefficient is  $.9 < \omega < 1.5$ . Within that range,  $\omega=1.2$  yields the least iterations. A graph of the relaxation factor shows the associated trend (Figure 5). The minimum value on the graph is the best choice for  $\omega$ .

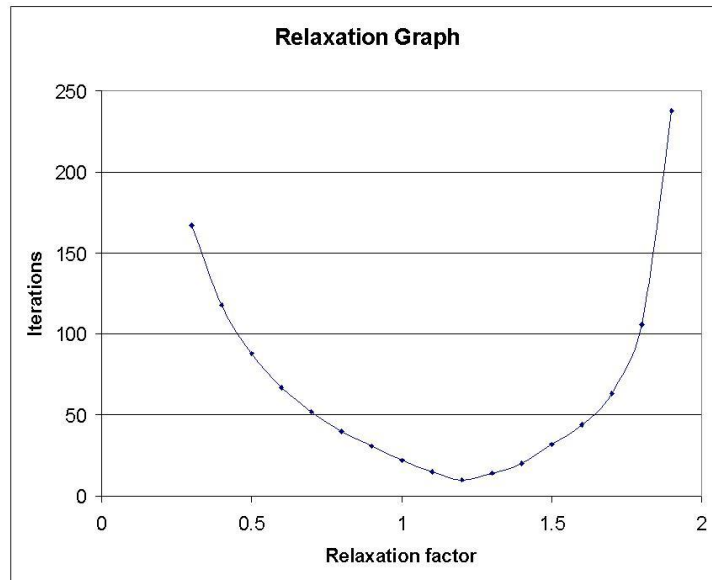


Figure 5: Relaxation factor vs. iteration count



Table 5: Relaxation factor variation

Run #	$\omega$	Iterations
13	0.1	539
14	0.2	263
15	0.3	167
16	0.4	118
17	0.5	88
18	0.6	67
19	0.7	52
20	0.8	40
21	0.9	31
22	1	22
23	1.1	15
24	1.2	10
25	1.3	14
26	1.4	20
27	1.5	32
28	1.6	44
29	1.7	63
30	1.8	106
31	1.9	238
32	2	>5000

## 5 Conclusion

The following can be concluded from the analysis:

- The concentration values that 5 tanks will yield are 27.03, 24.77, 22.70, 20.83 and 19.34 mg/l respectively.
- 18 tanks will most closely match the observed  $c_n$  value of 19 mg/l
- A relaxation factor of  $\omega=1.2$  will yield the least iterations
- The most influential parameter is  $c_{in}$ .
- Least influential parameters are  $Q_r$  and  $\varepsilon$ .

## 6 References

Chapra, Steven, and Raymond Canale. Numerical Methods for Engineers. 5th ed. New York: McGraw Hill, 2006.

Finney,Brad. Lab 9 handout, Humboldt State University, Spring 2006.

## Appendix A

### Source Code and Program Output

```
Script started on Tue 18 Apr 2006 08:54:30 PM PDT
cwb12@ere-server:~/engr325/lab9> cat lab9.2.f90

program cmts
  implicit none
  integer::ntanks,itr,maxit,i,j
  double precision::Q,Qr,V,k,cin,w,offdiagsum,eps,check,done
  double precision,allocatable,dimension(:,:)::A,AB
  double precision,allocatable,dimension(:)::b,x
  logical::diagdom,singular
  character(len=1)::ans

  interface
    subroutine gsswap(a,neqn,diagdom,singular)
      implicit none
      integer, intent(in)::neqn
      double precision, dimension(:,:), intent(inout)::a
      logical, intent(out)::diagdom, singular
    end subroutine gsswap
  end interface

  !This program will compute the effluent concentration values of
  !a pond using the complete-mix tank-in series approach using
  !the Gauss-Seidell method to solve for the concentration values.
  !~~variable list~~
  !--input variables--
  !ntanks      =number of tanks to use as an estimate
  !Q           =influent flowrate (m^3/day)
  !Qr          =recycle flow rate (m^3/day)
  !V           =tank or compartment volume
  !k           =first order reaction rate constant (day^-1)
```

```
!cin      =influent polution concentration
!w        =relaxation coefficent
!eps      =solution found tolerance
!maxit    =maximum number of iterations
!x        =solution vector needs initial guess
!--output variables--
!x        =solution vector of final concentration values
!itr      =number of iteration carried out
!--internal variables--
!i,j      =loop vaiables
!A        =holds initial coefficient matrix
!b        =initial right hand side vector
!ans      =answer to "do you want to continue?"

write(*,*)"This program will compute the effluent concentration values"
write(*,*)"of a pond using the complete-mix tank-in series approach using"
write(*,*)"the Gauss-Seidell method to solve for the concentration values."
write(*,*)" "
write(*,*)"How many tanks?"
read(*,*)ntanks
if(ntanks<=0)then
    write(*,"(a21,i2,a6)")"Can't do operation on",ntanks," tanks"
    stop
end if
allocate(A(ntanks,ntanks),x(ntanks),b(ntanks),AB(ntanks,ntanks+1))
A=0
b=0
Q=10000
Qr=.2*Q
V=50000/ntanks
k=.093
cin=30
write(*,*)"Enter the relaxation coefficient 0<w<2"
read(*,*)w
eps=.00001
maxit=4999
do i=1,ntanks
    write(*,"(a28,i3)")"Enter concentration for tank",i
    read(*,*)x(i)
end do
A(1,1)=-((Q+Qr)/V+k)
A(1,2)=Qr/V
b(1)=(-Q*cin)/V
if(ntanks>1)then
    do i=2,ntanks-1
```

```

        A(i,i-1)=(Q+Qr)/V
        A(i,i)=-((Q+2*Qr)/V+k)
        A(i,i+1)=Qr/V
    end do
    A(ntanks,ntanks-1)=(Q+Qr)/V
    A(ntanks,ntanks)=-((Q+Qr)/V+k)
end if
AB=A                !create augmented matrix instead of modifying originals
AB(1:ntanks,ntanks+1)=b(1:ntanks)    !augment A with b
write(*,*)" [A|b] ="
do i=1,ntanks
    write(*,"(a)",advance="no")"|"
    write(*,"(1000f8.3)",advance="no")(AB(i,j),j=1,ntanks+1)
    write(*,"(a)")"|"
end do

do i=1,ntanks
    offdiagsum=0
    offdiagsum=sum(abs(A(i,1:ntanks)))-abs(A(i,i))
    if(offdiagsum>abs(A(i,i)))then
        write(*,*)"Answer may not converge."
        write(*,*)"Continue? (y,n)"
        read(*,*)ans
        do
            if(ans=="n")then
                stop
            else if(ans/="y")then
                write(*,*)"not an option"
            else if(ans=="y")then
                exit
            end if
        end do
    end if
end do

call gsswap(AB,ntanks,diagdom,singular)
!do i=1,ntanks
!  write(*,"(a)",advance="no")"|"
!  write(*,"(1000f8.3)",advance="no")(AB(i,j),j=1,ntanks+1)
!  write(*,"(a)")"|"
!end do
if(singular)then
    write(*,*)"The coefficient matrix is singular."
    stop
end if

```

```
if(.not.diagdom)then
  write(*,*)"The augmented matrix is not diagonally dominant, &
    may not converge."
  write(*,*)"Continue? (y,n)"
  read(*,*)ans
  do
    if(ans=="n")then
      stop
    else if(ans/="y")then
      write(*,*)"not an option"
    else if(ans=="y")then
      exit
    end if
  end do
end if

!write(*,"(a11,f8.5)")"offdiagsum=",offdiagsum
itr=0
do
  itr=itr+1
  done=0
  do i=1,ntanks
    check=0
    check=x(i)
    x(i)=x(i)+w*((AB(i,ntanks+1)-sum(AB(i,1:i-1)*x(1:i-1))&
      -sum(AB(i,i:ntanks)*x(i:ntanks)))/AB(i,i))
    if(abs(check-x(i))<eps)then
      done=done+1
    end if
  end do
  !write(*,*)"x="
  !do i=1,ntanks
    ! write(*,"(f10.5)")x(i)
  !end do
  if(done==ntanks)then
    write(*,*)" "
    write(*,*)"Solution found"
    write(*,*)"x="
    do i=1,ntanks
      write(*,"(f10.5)")x(i)
    end do
    exit
  else if(itr>maxit)then
    write(*,*)"No solution,max iterations exceeded"
    exit
  end if
end do
```

```

        end if
    end do
    write(*,*)" "
    write(*,"(a12,i2,a9,f9.5)")"average for ",ntanks," tanks = "&
                                   ,sum(x(1:ntanks))/ntanks
    write(*,"(a5,i4,a12)")"took ",itr," iterations."
    write(*,*)" "
    stop
end program

cwb12@ere-server:~/enr325/lab9> ifort lab9.2.f90 gsswap.o
cwb12@ere-server:~/enr325/lab9> lab9 < values.dat
This program will compute the effluent concentration values
of a pond using the complete-mix tank-in series approach using
the Gauss-Seidell method to solve for the concentration values.

How many tanks?
Enter the relaxation coefficient 0<w<2
Enter concentration for tank 1 Enter concentration for tank 2
Enter concentration for tank 3 Enter concentration for tank 4
Enter concentration for tank 5
[A|b]=
| -1.293  0.200  0.000  0.000  0.000 -30.000| | 1.200 -1.493
0.200  0.000  0.000  0.000| | 0.000  1.200 -1.493  0.200
0.000  0.000| | 0.000  0.000  1.200 -1.493  0.200  0.000| |
0.000  0.000  0.000  1.200 -1.293  0.000|

Solution found
x=
27.03302
24.76849
22.69861
20.83421
19.33569

average for 5 tanks = 22.93400 took 14 iterations.

cwb12@ere-server:~/enr325/lab9> cat values.dat 5 1 30 30 30 30 30
cwb12@ere-server:~/enr325/lab9> exit

Script done on Tue 18 Apr 2006 08:55:45 PM PDT

```