# Exercise 7 - TTK4130 Modeling and Simulation

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# 1 Problem 1

$$\begin{split} \frac{\partial p(x,t)}{\partial t} &= -cZ_0 \frac{\partial q(x,t)}{\partial x} \\ \frac{\partial q(x,t)}{\partial t} &= -\frac{c}{Z_0} \frac{\partial p(x,t)}{\partial x} - \frac{F(q(x,t))}{\rho_0} \\ c &= \sqrt{\frac{\beta}{\rho_0}} \\ Z_0 &= \frac{\rho_0 c}{A} = \frac{\sqrt{\rho_0 \beta}}{A} \\ F &= \rho_0 B q \\ B &= \frac{8\nu_0}{r_0^2} \end{split}$$

Helmholtz mass balance

$$\frac{V}{\beta}\dot{p} = q \tag{1}$$

Helmholtz moment balance

$$h\rho_0 \dot{q} = -Ap \tag{2}$$

#### 1.1 a

Using Equation 1, the mass balance for each volume can be set up as

$$\frac{V}{\beta}\dot{p}_i = q_{i-1} - q_i \Rightarrow \dot{p}_i = \frac{c^2\rho_0}{Ah}(q_{i-1} - q_i).$$

Using Equation 2, the moment balance for each volume can be set up as

$$h\rho_0\dot{q}_i = -A(p_{i-1} - p_i) - Fh \Rightarrow \dot{q}_{i-1} = \frac{A}{h\rho_0}(p_{i-1} - p_i) - Bq_{i-1}.$$

#### 1.2 b

$$\begin{split} \dot{\mathbf{x}} &= \mathbf{A}\mathbf{x} + \mathbf{B}\mathbf{u} \\ \mathbf{y} &= \mathbf{C}\mathbf{x} + \mathbf{D}\mathbf{u} \\ \mathbf{u} &= \begin{bmatrix} q_0 \\ q_N \end{bmatrix} \text{ and } \mathbf{y} = \begin{bmatrix} p_1 \\ p_N \end{bmatrix} \\ \mathbf{x}^T &= \begin{bmatrix} p_1 & q_1 & p_2 & q_2 & \dots & q_{N-1} & p_N \end{bmatrix} \end{split}$$

$$\mathbf{A} = \begin{bmatrix} 0 & -\frac{c^2 \rho_0}{Ah} & 0 & \dots & & & & 0 \\ \frac{A}{h\rho_0} & -B & -\frac{A}{h\rho_0} & 0 & \dots & & & 0 \\ 0 & \frac{c^2 \rho_0}{Ah} & 0 & -\frac{c^2 \rho_0}{Ah} & 0 & \dots & & 0 \\ 0 & 0 & \frac{A}{h\rho_0} & -B & -\frac{A}{h\rho_0} & 0 & \dots & & 0 \\ \vdots & \vdots & \ddots & \ddots & \ddots & \ddots & \ddots & \vdots \\ 0 & 0 & \dots & 0 & \frac{c^2 \rho_0}{Ah} & 0 & -\frac{c^2 \rho_0}{Ah} & 0 \\ 0 & 0 & \dots & 0 & \frac{c^2 \rho_0}{Ah} & 0 & -\frac{A}{h\rho_0} \\ 0 & 0 & \dots & \dots & 0 & \frac{c^2 \rho_0}{Ah} & 0 \end{bmatrix}$$

$$\mathbf{B} = \begin{bmatrix} \frac{c^2 \rho_0}{Ah} & 0\\ 0 & \vdots\\ \vdots & \vdots\\ \vdots & 0\\ 0 & -\frac{c^2 \rho_0}{Ah} \end{bmatrix}$$
$$\mathbf{C} = \begin{bmatrix} 1 & 0 & \cdots & \cdots & 0\\ 0 & \cdots & \cdots & 0 & 1 \end{bmatrix}$$
$$\mathbf{D} = 0$$

The diagonal and the 1st and -1st superdiagonal of A alternate between two values. This makes it easy to implement in MATLAB.

#### 1.3 d

The response is quite similar for the three values of N, as seen in Figure 1. When consulting the bode plots in figures 2 and 3, it is clear that the system is more oscillating for large values of N. The code for generating these plots can be seen in listings 1 and 2

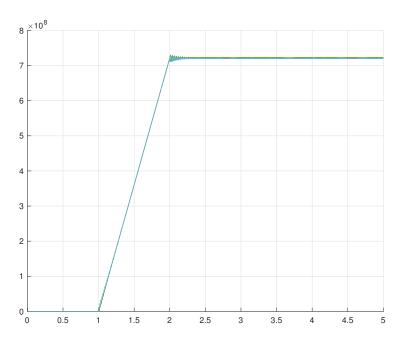


Figure 1:  $p_1$  and  $p_N$  plotted for all values of N.

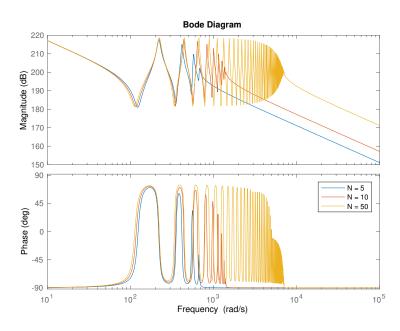


Figure 2: Bode plot of the response from  $q_0$  to  $p_1$  for all values of N.

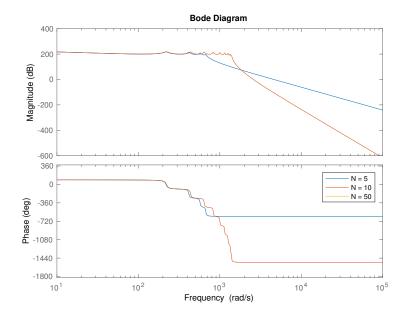


Figure 3: Bode plot of the response from  $q_0$  to  $p_N$  for all values of N.

# 2 Problem 2

$$\frac{\partial q}{\partial t} = -\frac{A}{\rho_0} \frac{\partial p}{\partial x} + \nu_0 \left( \frac{\partial^2 q}{\partial x^2} - \frac{8}{r_0^2} q \right). \tag{3}$$

### 2.1 a

Using that  $\frac{\partial q_i}{\partial x} \simeq \frac{1}{h}(q_i - q_{i-1})$  for small h, twice, yields

$$\begin{split} \frac{\partial^2 q_i}{\partial x^2} &\simeq \frac{1}{h} (\frac{\partial q_i}{\partial x} - \frac{\partial q_{i-1}}{\partial x}) \simeq \frac{1}{h} (\frac{1}{h} (q_i - q_{i-1}) - \frac{1}{h} (q_{i-1} - q_{i-2})) \\ &\qquad \qquad \underbrace{\frac{\partial^2 q_i}{\partial x^2} = \frac{q_{i-2} - 2q_i + q_i}{h^2}}_{\end{split}$$

#### 2.2 b

Discretizing in a similar manner as in Problem 1

$$\underline{q_{i-1} = \frac{A}{h\rho_0}(p_{i-1} - p_i) - (\frac{2\nu_0}{h^2} + \frac{8}{r_0^2})q_{i-1} + \frac{\nu_0}{h^2}(q_{i-2} + q_i)}$$

$$\mathbf{A} = \begin{bmatrix} 0 & -\frac{c^2 \rho_0}{Ah} & 0 & \dots & 0 \\ \frac{A}{h\rho_0} & -(\frac{2\nu_0}{h^2} + \frac{8}{r_0^2}) & -\frac{A}{h\rho_0} & \frac{\nu_0}{h^2} & 0 & \dots & 0 \\ 0 & \frac{c^2 \rho_0}{Ah} & 0 & -\frac{c^2 \rho_0}{Ah} & 0 & \dots & 0 \\ 0 & \frac{\nu_0}{h^2} & \frac{A}{h\rho_0} & -(\frac{2\nu_0}{h^2} + \frac{8}{r_0^2}) & -\frac{A}{h\rho_0} & \frac{\nu_0}{h^2} & \dots & 0 \\ \vdots & \vdots & \ddots & \ddots & \ddots & \ddots & \ddots & \vdots \\ 0 & 0 & \dots & 0 & \frac{c^2 \rho_0}{Ah} & 0 & -\frac{c^2 \rho_0}{Ah} & 0 \\ 0 & 0 & \dots & 0 & \frac{\nu_0}{h^2} & \frac{A}{h\rho_0} & -(\frac{2\nu_0}{h^2} + \frac{8}{r_0^2}) & -\frac{A}{h\rho_0} \\ 0 & 0 & \dots & 0 & \frac{c^2 \rho_0}{Ah} & 0 \end{bmatrix}$$

$$\mathbf{B} = \begin{bmatrix} \frac{c^2 \rho_0}{Ah} & 0 \\ \frac{\nu_0}{h^2} & 0 \\ 0 & 0 \\ \vdots & \vdots \\ 0 & 0 \\ 0 & \frac{\nu_0}{h^2} \\ 0 & -\frac{c^2 \rho_0}{Ah} \end{bmatrix}$$
$$\mathbf{C} = \begin{bmatrix} 1 & 0 & \cdots & \cdots & 0 \\ 0 & \cdots & \cdots & 0 & 1 \end{bmatrix}$$
$$\mathbf{D} = 0$$

# 3 Problem 3

#### 3.1 a

Since  $x_1$  and  $x_2$  appear as time derivatives in the DAE, they are differential variables.  $x_3$  is an algebraic variable, as its derivative does not appear.

#### 3.2 b

 $x_1$  is dependent on  $x_3$  (or the other way around), and  $x_2$  s dependent on  $x_1$ . This means that there is only one independent variable in the system, and therefore the system has 1 degree of freedom.

#### 3.3 c

To transform the DAE to an ODE we have to differentiate twice:

$$\frac{d}{dt}(x_1 - u) = \dot{x}_1 - \dot{u}$$

$$x_3 = \dot{u}$$

$$\frac{d^2}{dt^2}(x_1 - u) = \dot{x}_3 - \ddot{u}$$

$$\dot{x}_3 = \ddot{u}$$

Therefore, the system is of index 2.

#### 3.4 d

$$0 = x_3 - \dot{u}$$
$$\dot{x}_2 = x_1$$
$$0 = x_1 - u$$

Listing 1: Code for initialising a system with N volumes.

```
L = 19.76;
  beta = 1.7052*10^9;
  rho = 870;
  r = 6.17*10^{(-3)};
  nu = 8*10^{-}(-5);
  area = pi*r^2;
  c = sqrt(beta/rho);
  h = L/N;
  Z_0 = rho*c/area;
  b = 8*nu/r^2;
  x_0 = zeros(N+N-1,1);
13
  tsim = 5;
14
  A = zeros(N+N-1,N+N-1);
  B = zeros(N+N-1,2);
  C = zeros(2,N+N-1);
  D = zeros(2,2);
19
  C(1,1) = 1;
  C(2,N+N-1) = 1;
23
B(1,1) = c^2*rho/(area*h);
B(N+N-1,2) = -c^2*rho/(area*h);
```

```
27
   v = repmat([0 -b], 1, N-1);
  v(1,N + N - 1) = 0;
   A = diag(v);
31
32
   v = repmat([-c^2*rho/(area*h) - area/(rho*h)], 1,N-1);
33
34
   A = A + diag(v,1);
35
36
   v = repmat([area/(rho*h) c^2*rho/(area*h)], 1,N-1);
37
38
  A = A + diag(v,-1);
39
```

Listing 2: Code for running and plotting a system with N volumes.

```
clear; clc;
  N = 5;
3
  ModSim_ex7_1c_init;
   sim('ModSim_ex7_1c_model')
   figure(1)
   hold on; grid on;
  plot(p_1.Time, p_1.Data, p_N.Time, p_N.Data);
   sys5 = ss(A,B,C,D);
13
14
  N = 10;
15
16
   ModSim_ex7_1c_init;
17
18
   sim('ModSim_ex7_1c_model')
19
20
   figure(1)
   plot(p_1.Time, p_1.Data, p_N.Time, p_N.Data);
   sys10 = ss(A,B,C,D);
24
25
26
  N = 50;
28
30 | ModSim_ex7_1c_init;
```

```
31
  sim('ModSim_ex7_1c_model')
33
  figure(1)
  \verb|plot(p_1.Time, p_1.Data, p_N.Time, p_N.Data)|;
  print -depsc ex7_1c
  sys50 = ss(A,B,C,D);
38
  figure(2)
  bode(sys5(1,1),sys10(1,1),sys50(1,1))
  legend('N = 5','N = 10','N = 50')
  print -depsc ex7_1c_bode_p1
  figure(3)
  bode(sys5(1,2),sys10(1,2),sys50(1,2))
legend('N = 5','N = 10','N = 50')
  print -depsc ex7_1c_bode_pN
```