Cheat Sheet for EE464

$$FormFactor = \frac{V_{rms}}{V_{avg}}CrestFactor = \frac{V_{peak}}{V_{rms}}$$

$$DistortionFactor = \frac{I_{1rms}}{I_{rms}}$$

$$\phi: phase \ difference \ between \ fundamentals \ of \ current \ and \ voltage$$

$$DisplacementPowerFactor = \cos(\phi)$$

$$TruePowerFactor = \frac{P}{S} = DPF \frac{I_{1,RMS}}{I_{RMS}}$$

$$THD = \sqrt{(\frac{I_{rms}}{I_{1rms}})^2 - 1}$$

$$\begin{split} V_o &= V_s \bigg(\frac{D}{1-D}\bigg) \bigg(\frac{N_2}{N_1}\bigg) \\ & \left[\frac{\Delta V_o}{V_o} = \frac{D}{RCf} \right] \\ I_{L_{m,\max}} &= I_{L_m} + \frac{\Delta i_{L_m}}{2} \\ & = \frac{V_s D}{(1-D)^2 R} \bigg(\frac{N_2}{N_1}\bigg)^2 + \frac{V_s D T}{2L_m} \\ & = \frac{V_s D}{\left(1-D\right)^2 R} \bigg(\frac{N_2}{N_1}\bigg)^2 + \frac{V_s D T}{2L_m} \\ & = \frac{V_s D}{\left(1-D\right)^2 R} \bigg(\frac{N_2}{N_1}\bigg)^2 - \frac{V_s D T}{2L_m} \\ & = \frac{V_s D}{\left(1-D\right)^2 R} \bigg(\frac{N_2}{N_1}\bigg)^2 - \frac{V_s D T}{2L_m} \\ & = \frac{V_s D}{\left(1-D\right)^2 R} \bigg(\frac{N_2}{N_1}\bigg)^2 - \frac{V_s D T}{2L_m} \\ & = \frac{V_s D}{\left(1-D\right)^2 R} \bigg(\frac{N_2}{N_1}\bigg)^2 - \frac{V_s D T}{2L_m} \\ & = \frac{V_s D}{\left(1-D\right)^2 R} \bigg(\frac{N_2}{N_1}\bigg)^2 - \frac{V_s D T}{2L_m} \\ & = \frac{V_s D}{\left(1-D\right)^2 R} \bigg(\frac{N_2}{N_1}\bigg)^2 - \frac{V_s D T}{2L_m} \\ & = \frac{V_s D}{\left(1-D\right)^2 R} \bigg(\frac{N_2}{N_1}\bigg)^2 - \frac{V_s D T}{2L_m} \\ & = \frac{V_s D}{\left(1-D\right)^2 R} \bigg(\frac{N_2}{N_1}\bigg)^2 - \frac{V_s D T}{2L_m} \\ & = \frac{V_s D}{\left(1-D\right)^2 R} \bigg(\frac{N_2}{N_1}\bigg)^2 - \frac{V_s D T}{2L_m} \\ & = \frac{V_s D}{\left(1-D\right)^2 R} \bigg(\frac{N_2}{N_1}\bigg)^2 - \frac{V_s D T}{2L_m} \\ & = \frac{V_s D}{\left(1-D\right)^2 R} \bigg(\frac{N_1}{N_1}\bigg)^2 - \frac{V_s D T}{2L_m} \\ & = \frac{V_s D}{\left(1-D\right)^2 R} \bigg(\frac{N_1}{N_1}\bigg)^2 - \frac{V_s D T}{2L_m} \\ & = \frac{V_s D}{\left(1-D\right)^2 R} \bigg(\frac{N_1}{N_1}\bigg)^2 - \frac{V_s D T}{2L_m} \\ & = \frac{V_s D}{\left(1-D\right)^2 R} \bigg(\frac{N_1}{N_1}\bigg)^2 - \frac{V_s D T}{2L_m} \\ & = \frac{V_s D}{\left(1-D\right)^2 R} \bigg(\frac{N_1}{N_1}\bigg)^2 - \frac{V_s D T}{2L_m} \\ & = \frac{V_s D}{\left(1-D\right)^2 R} \bigg(\frac{N_1}{N_1}\bigg)^2 - \frac{V_s D T}{2L_m} \\ & = \frac{V_s D}{\left(1-D\right)^2 R} \bigg(\frac{N_1}{N_1}\bigg)^2 - \frac{V_s D T}{N_1} \\ & = \frac{V_s D}{\left(1-D\right)^2 R} \bigg(\frac{N_1}{N_1}\bigg)^2 - \frac{V_s D T}{N_1} \\ & = \frac{V_s D}{N_1} \bigg(\frac{N_1}{N_1}\bigg)^2 - \frac{V_s D T}{N_1} \bigg(\frac{N_1}{N_1}\bigg)^2 - \frac{V_s D T}{N_1} \bigg(\frac{N_1}{N_1}\bigg)^2 - \frac{V_s D T}{N_1} \bigg(\frac{N_1}{N_1}\bigg)^2 \bigg(\frac{N_1}{N_1}\bigg)^2 - \frac{V_s D T}{N_1}\bigg(\frac{N_1}{N_1}\bigg)^2 \bigg(\frac{N_1}{N_1}\bigg)^2 \bigg(\frac{N_1}{N_1}$$

Figure 1: Flyback Formulas

$$\begin{bmatrix} V_o = V_s D \bigg(\frac{N_2}{N_1} \bigg) & \boxed{ \frac{\Delta V_o}{V_o} = \frac{1-D}{8L_x C f^2} } \\ \Delta V_{o, \rm ESR} = \Delta i_C r_C = \Delta i_{L_x} r_C = \bigg[\frac{V_o (1-D)}{L_x f} \bigg] r_C \\ \Delta i_{L_m} = \frac{V_s D T}{L_m} \end{bmatrix}$$

Figure 2: Forward (single switched) Converter Formulas

$$\begin{bmatrix} V_o = 2V_s \left(\frac{N_S}{N_P}\right) D \end{bmatrix} \begin{bmatrix} \frac{\Delta V_o}{V_o} = \frac{1 - 2D}{32L_x C f^2} \end{bmatrix}$$

$$\Delta V_{o,ESR} = \Delta i_{L_x} r_C = \begin{bmatrix} \frac{V_o(\frac{1}{2} - D)}{L_x f} \end{bmatrix} r_C$$

Figure 3: Push Pull Formulas

$$V_o = V_s \left(\frac{D}{1-D}\right) \qquad \Delta V_{C_1} = \frac{I_o DT}{C} = \frac{V_o D}{RC_1 f}$$

$$\Delta i_{L_1} = \frac{V_s DT}{L_1} = \frac{V_s D}{L_1 f} \qquad \Delta V_o = \Delta V_{C_2} = \frac{V_o D}{RC_2 f}$$

$$\Delta i_{L_2} = \frac{V_s DT}{L_2} = \frac{V_s D}{L_2 f} \qquad C_1 = \frac{D}{R(\Delta V_{C_1}/V_o) f}$$

$$C_2 = \frac{D}{R(\Delta V_o/V_o) f}$$

Figure 4: Sepic Converter Formulas

$$SwitchUtilization = \frac{Po}{Psw} = \frac{Io.Vo}{q.Vswmax.Iswmax} \tag{1}$$

$$m_f = \frac{f_s}{f_1}, m_a = \frac{V_{control}}{V_{triangle}}$$

$$m_a < 1: linear, m_a > 1: overmodulation$$

$$\begin{split} V_o &= -V_s \bigg(\frac{D}{1-D} \bigg) \, \Bigg| \, \frac{\Delta V_o}{V_o} &= \frac{1-D}{8L_2C_2f^2} \\ \Delta v_{C_1} &\approx \frac{1}{C_1} \int\limits_{DT}^{T} I_{L_1} d(t) = \frac{I_{L_1}}{C_1} (1-D)T = \frac{V_s}{RC_1f} \bigg(\frac{D^2}{1-D} \bigg) \\ & \qquad \qquad \Delta v_{C_1} \approx \frac{V_oD}{RC_1f} \\ \\ \Delta i_{L1} &= \frac{V_sDT}{L_1} = \frac{V_sD}{L_1f} \, \Bigg| \, \Delta i_{L2} = \frac{V_sDT}{L_2} = \frac{V_sD}{L_2f} \\ \\ L_{1, \min} &= \frac{(1-D)^2R}{2Df} \quad L_{2, \min} = \frac{(1-D)R}{2f} \end{split}$$

Figure 5: Cuk Converter Formulas

Switch Selection

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$$\hat{I}_{sw} = rac{1}{(1-D)}rac{N_2}{N_1}I_o + rac{N_1}{N_2}rac{(1-D)T_s}{2L_m}V_o$$

Peak Switch Voltage

$$\hat{V_{sw}} = V_d + rac{N_1}{N_2} V_o = rac{V_d}{(1-D)}$$

Figure 6: Flyback switch considerations

$$\boxed{ V_o = 2 V_{\rm S} \! \bigg(\frac{N_S}{V_P} \bigg) D } \boxed{ V_o = V_{\rm S} \! \bigg(\frac{N_S}{N_P} \bigg) D}$$
 Full Bridge

Figure 7: Full and Half Bridge Relations

$$(V_o)_h = \frac{1}{\sqrt{2}} \cdot 2 \cdot \frac{V_d}{2} \frac{(\hat{V}_{Ao})_h}{V_{d'}2} = \frac{V_d}{\sqrt{2}} \frac{(\hat{V}_{Ao})_h}{V_{d'}2}$$

Figure 8: Rms Voltage of Harmonics Full Bridge Inverter

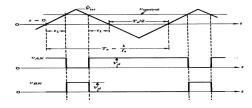


Figure 9: Bipolar Switching

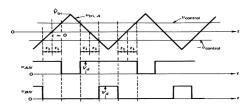


Figure 10: Unipolar switching

Cuk Converter

$$Vc1 = Vo + Vd \tag{2}$$

Transformer Analysis

$$V_{rms} = \frac{2\pi}{\sqrt{2}} . N_2 . f. B_{max} . A \tag{3}$$