Cheat Sheet for EE464

$$FormFactor = \frac{V_{rms}}{V_{avg}}$$

$$CrestFactor = \frac{V_{peak}}{V_{rms}}$$

$$DistortionFactor = \frac{I_{1rms}}{I_{rms}}$$

ϕ : *phase difference between fundamentals of current and voltage*

$$DisplacementPowerFactor = \cos(\phi)$$

$$TruePowerFactor = \frac{P}{S} = DPF\frac{I_{1,RMS}}{I_{RMS}}$$

$$THD = \sqrt{(\frac{I_{rms}}{I_{1rms}})^2 - 1}$$

Converters

$$\boxed{V_o = V_s\left(\frac{D}{1-D}\right)\left(\frac{N_2}{N_1}\right)} \quad \boxed{\frac{\Delta V_o}{V_o} = \frac{D}{RCf}} \quad \boxed{(L_m)_{\min} = \frac{(1-D)^2 R}{2f}\left(\frac{N_1}{N_2}\right)^2}$$

$$I_{L_{m,\max}} = I_{L_m} + \frac{\Delta i_{L_m}}{2} = \frac{V_s D}{(1-D)^2 R}\left(\frac{N_2}{N_1}\right)^2 + \frac{V_s DT}{2L_m}$$

$$L_m = \frac{V_s DT}{\Delta i_{L_m}} = \frac{V_s D}{\Delta i_{L_m} f}$$

$$I_{L_{m,\min}} = I_{L_m} - \frac{\Delta i_{L_m}}{2} = \frac{V_s D}{(1-D)^2 R}\left(\frac{N_2}{N_1}\right)^2 - \frac{V_s DT}{2L_m}$$

equate this to zero for dcm boundary

$$(\Delta i_{L_m})_{\text{open}} = \frac{-V_o(1-D)T}{L_m}\left(\frac{N_1}{N_2}\right) \qquad (\Delta i_{L_m})_{\text{closed}} = \frac{V_s DT}{L_m}$$

$$\Delta V_{o,\text{ESR}} = \Delta i_C r_C = I_{L_{m,\max}}\left(\frac{N_1}{N_2}\right) r_C$$

Figure 1: Flyback Formulas

$$\boxed{V_o = V_s D\left(\frac{N_2}{N_1}\right)} \quad \boxed{\frac{\Delta V_o}{V_o} = \frac{1-D}{8L_x C f^2}}$$

$$\Delta V_{o,\text{ESR}} = \Delta i_C r_C = \Delta i_{L_x} r_C = \left[\frac{V_o(1-D)}{L_x f}\right] r_C$$

$$\Delta i_{L_m} = \frac{V_s DT}{L_m}$$

Figure 2: Forward (single switched) Converter Formulas

$$\boxed{V_o = 2V_s\left(\frac{N_S}{N_P}\right)D} \quad \boxed{\frac{\Delta V_o}{V_o} = \frac{1-2D}{32 L_x C f^2}}$$

$$\Delta V_{o,ESR} = \Delta i_{L_x} r_C = \left[\frac{V_o(\frac{1}{2} - D)}{L_x f}\right] r_C$$

Figure 3: Push Pull Formulas

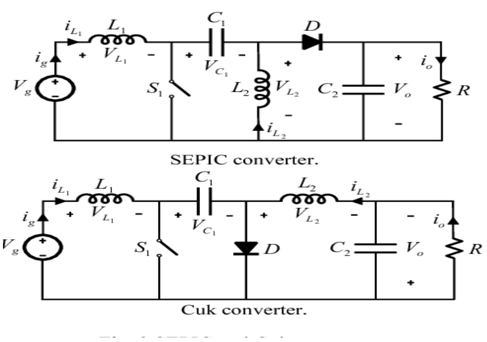

Figure 4: Sepic and Cuk Converter Schematics

$$SwitchUtilization = \frac{Po}{Psw} = \frac{Io.Vo}{q.Vswmax.Iswmax} \tag{1}$$

Inverters

$$m_f = \frac{f_s}{f_1}, m_a = \frac{V_{control}}{V_{triangle}}$$

$$\boxed{V_o = V_s\left(\frac{D}{1-D}\right)} \quad \Delta V_{C_1} = \frac{I_o DT}{C} = \frac{V_o D}{RC_1 f}$$

$$\Delta i_{L_1} = \frac{V_s DT}{L_1} = \frac{V_s D}{L_1 f} \quad \boxed{\Delta V_o = \Delta V_{C_2} = \frac{V_o D}{RC_2 f}}$$

$$\Delta i_{L_2} = \frac{V_s DT}{L_2} = \frac{V_s D}{L_2 f} \quad \boxed{C_1 = \frac{D}{R(\Delta V_{C_1}/V_o)f}}$$

$$\boxed{C_2 = \frac{D}{R(\Delta V_o/V_o)f}}$$

Figure 5: Sepic Converter Formulas

$$\boxed{V_o = -V_s\left(\frac{D}{1-D}\right)} \quad \boxed{\frac{\Delta V_o}{V_o} = \frac{1-D}{8L_2C_2f^2}}$$

$$\Delta v_{C_1} \approx \frac{1}{C_1}\int_{DT}^{T} I_{L_1} d(t) = \frac{I_{L1}}{C_1}(1-D)T = \frac{V_s}{RC_1 f}\left(\frac{D^2}{1-D}\right)$$

$$\boxed{\Delta v_{C_1} \approx \frac{V_o D}{RC_1 f}}$$

$$\boxed{\Delta i_{L1} = \frac{V_s DT}{L_1} = \frac{V_s D}{L_1 f}} \quad \boxed{\Delta i_{L2} = \frac{V_s DT}{L_2} = \frac{V_s D}{L_2 f}}$$

$$L_{1,\min} = \frac{(1-D)^2 R}{2Df} \qquad L_{2,\min} = \frac{(1-D)R}{2f}$$

Figure 6: Cuk Converter Formulas

Switch Selection

Peak Switch Current

$$\hat{I}_{sw} = \frac{1}{(1-D)}\frac{N_2}{N_1}I_o + \frac{N_1}{N_2}\frac{(1-D)T_s}{2L_m}V_o$$

Peak Switch Voltage

$$\hat{V}_{sw} = V_d + \frac{N_1}{N_2}V_o = \frac{V_d}{(1-D)}$$

Figure 7: Flyback switch considerations

$$\boxed{V_o = 2V_s\left(\frac{N_S}{N_P}\right)D} \quad \boxed{V_o = V_s\left(\frac{N_S}{N_P}\right)D}$$

Full Bridge   Half Bridge

Figure 8: Full and Half Bridge Relations

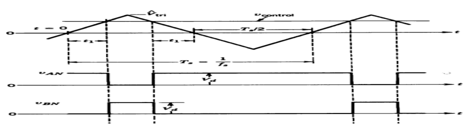

Figure 9: Bipolar Switching

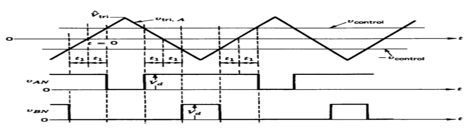

Figure 10: Unipolar switching

$$m_a < 1 : linear, m_a > 1 : overmodulation$$

$$(V_o)_h = \frac{1}{\sqrt{2}} \cdot 2 \cdot \frac{V_d}{2}\frac{(\hat{V}_{Ao})_h}{V_d/2} = \frac{V_d}{\sqrt{2}}\frac{(\hat{V}_{Ao})_h}{V_d/2}$$

Figure 11: Rms Voltage of Harmonics Full Bridge Inverter

Cuk Converter

$$Vc1 = Vo + Vd \tag{2}$$

Transformer Analysis

$$V_{rms} = \frac{2\pi}{\sqrt{2}}.N_2.f.B_{max}.A \tag{3}$$

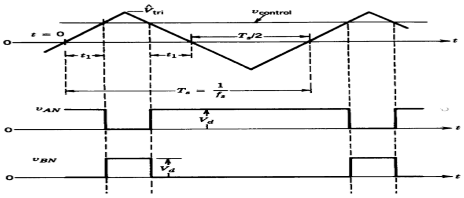

Figure 12: Bipolar Switching

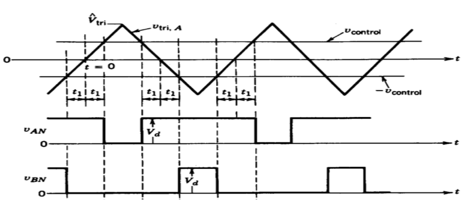

Figure 13: Unipolar switching