Cheat Sheet for EE464

Performance Parameters

$$TruePowerFactor = \frac{P}{S} = DPF \frac{I_{1,RMS}}{I_{RMS}}$$

$$THD = \sqrt{(\frac{I_{rms}}{I_{1rms}})^2 - 1}$$

| Symmetry | Condition Required | a_h and b_h |
|-----------|-------------------------------|---|
| Even | f(-t) = f(t) | $b_h = 0$ $a_h = \frac{2}{\pi} \int_0^{\pi} f(t) \cos(h\omega t) d(\omega t)$ |
| Odd | f(-t) = -f(t) | $a_h = 0$ $b_h = \frac{2}{\pi} \int_0^{\pi} f(t) \sin(h\omega t) d(\omega t)$ |
| Half-wave | $f(t) = -f(t + \frac{1}{2}T)$ | $a_h = b_h = 0 \text{ for even } h$ $a_h = \frac{2}{\pi} \int_0^{\pi} f(t) \cos(h\omega t) d(\omega t) \text{ for odd } h$ $b_h = \frac{2}{\pi} \int_0^{\pi} f(t) \sin(h\omega t) d(\omega t) \text{ for odd } h$ |

Figure 1: Fourier Transform Table

| $V_o = V_s D\left(\frac{N_2}{N_1}\right)$ | $\frac{\Delta V_o}{V_o} = \frac{1 - D}{8L_x C f^2}$ |
|---|--|
| $\Delta V_{o, ESR} = \Delta i_C r_C =$ | $\Delta i_{L_x} r_C = \left[\frac{V_o(1-D)}{L_x f} \right] r_C$ |
| $\Delta i_{L_m} = \frac{V_s DT}{L_m}$ | |

Figure 6: Forward (single switched) Converter Formulas

Switch Selection

Peak Switch Current

$$\hat{I}_{sw} = rac{1}{(1-D)} rac{N_2}{N_1} I_o + rac{N_1}{N_2} rac{(1-D)T_s}{2L_m} V_o$$

Peak Switch Voltage

$$\hat{V}_{sw} = V_d + rac{N_1}{N_2} V_o = rac{V_d}{(1-D)}$$

Figure 2: Flyback switch considerations

| $V_o = 2V_s \left(\frac{N_S}{N_P}\right) D$ | $\frac{\Delta V_o}{V_o} = \frac{1 - 2D}{32L_x C f^2}$ |
|---|---|
| $\Delta V_{o,ESR} = \Delta i_{L_x} r_o$ | $C = \left[\frac{V_o(\frac{1}{2} - D)}{L_x f}\right] r_C$ |

Figure 7: Push Pull Formulas

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Figure 3: Bipolar Switching



Figure 4: Unipolar switching

$$\begin{bmatrix} V_o = V_s \left(\frac{D}{1 - D} \right) \end{bmatrix} \Delta V_{C_1} = \frac{I_o DT}{C} = \frac{V_o D}{RC_1 f}$$

$$\Delta i_{L_1} = \frac{V_s DT}{L_1} = \frac{V_s D}{L_1 f} \begin{bmatrix} \Delta V_o = \Delta V_{C_2} = \frac{V_o D}{RC_2 f} \end{bmatrix}$$

$$\Delta i_{L_2} = \frac{V_s DT}{L_2} = \frac{V_s D}{L_2 f} \begin{bmatrix} C_1 = \frac{D}{R(\Delta V_{C_1}/V_o)f} \end{bmatrix}$$

$$C_2 = \frac{D}{R(\Delta V_o/V_o)f}$$

Figure 8: Sepic Converter Formulas

$$\begin{split} \boxed{V_o = V_s \bigg(\frac{D}{1-D}\bigg) \bigg(\frac{N_2}{N_1}\bigg)} & \boxed{\frac{\Delta V_o}{V_o} = \frac{D}{RCf}} & (L_m)_{\min} = \frac{(1-D)^2 R}{2f} \bigg(\frac{N_1}{N_2}\bigg)^2 \\ I_{L_{m,\max}} = I_{L_m} + \frac{\Delta i_{L_m}}{2} & L_m = \frac{V_s DT}{\Delta i_{L_m}} = \frac{V_s D}{\Delta i_{L_m} f} \\ & = \frac{V_s D}{(1-D)^2 R} \bigg(\frac{N_2}{N_1}\bigg)^2 + \frac{V_s DT}{2L_m} & \sum_{\substack{k = 1 \\ k \neq j \\ m \neq j}} & \sum_{\substack{k = 1 \\ k \neq j}} & \sum_{\substack{k = 1 \\$$

Figure 5: Flyback Formulas

$$\begin{split} V_o &= -V_s \bigg(\frac{D}{1-D}\bigg) \, \Bigg[\, \frac{\Delta V_o}{V_o} &= \frac{1-D}{8L_2C_2f^2} \\ \\ \Delta v_{C1} &\approx \frac{1}{C_1} \int\limits_{DT}^T I_{L1} d(t) = \frac{I_{L1}}{C_1} (1-D)T = \frac{V_s}{RC_1f} \bigg(\frac{D^2}{1-D}\bigg) \\ \\ & \qquad \qquad \bigg(\Delta v_{C1} \approx \frac{V_oD}{RC_1f} \bigg) \\ \\ \Delta i_{L1} &= \frac{V_sDT}{L_1} = \frac{V_sD}{L_1f} \, \Bigg[\, \Delta i_{L2} = \frac{V_sDT}{L_2} = \frac{V_sD}{L_2f} \\ \\ \\ L_{1,\,\text{min}} &= \frac{(1-D)^2R}{2Df} \quad L_{2,\,\text{min}} = \frac{(1-D)R}{2f} \end{split}$$

(1)

Figure 9: Cuk Converter Formulas

$$SwitchUtilization = \frac{Po}{Psw} = \frac{Io.Vo}{q.Vswmax.Iswmax}$$