Cheat Sheet for EE464

Performance Parameters

$$TruePowerFactor = \frac{P}{S} = DPF \frac{I_{1,RMS}}{I_{RMS}}$$

$$THD = \sqrt{(\frac{I_{rms}}{I_{1rms}})^2 - 1}$$

Symmetry	Condition Required	a_h and b_h		
Even	f(-t) = f(t)	$b_h = 0$ $a_h = \frac{2}{\pi} \int_0^{\pi} f(t) \cos(h\omega t) d(\omega t)$		
Odd	f(-t) = -f(t)	$a_h = 0$ $b_h = \frac{2}{\pi} \int_0^{\pi} f(t) \sin(h\omega t) d(\omega t)$		
Half-wave	$f(t) = -f(t + \frac{1}{2}T)$	$a_h = b_h = 0$ for even h $a_h = \frac{2}{\pi} \int_0^{\pi} f(t) \cos(h\omega t) d(\omega t)$ for odd h $b_h = \frac{2}{\pi} \int_0^{\pi} f(t) \sin(h\omega t) d(\omega t)$ for odd h		

Figure 1: Fourier Transform Table

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Peak Switch Current

$$\hat{I}_{sw} = rac{1}{(1-D)} rac{N_2}{N_1} I_o + rac{N_1}{N_2} rac{(1-D)T_s}{2L_m} V_o$$

Peak Switch Voltage

$$\hat{V}_{sw} = V_d + rac{N_1}{N_2} V_o = rac{V_d}{(1-D)}$$

Figure 2: Flyback switch considerations

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ν _{BN}		$T_a = \frac{1}{T_a}$	-	1	
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Figure 3: Bipolar Switching

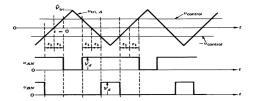


Figure 4: Unipolar switching

$$\begin{split} V_o &= V_s \bigg(\frac{D}{1-D}\bigg) \bigg(\frac{N_2}{N_1}\bigg) \\ &= \frac{D}{V_o} = \frac{D}{RCf} \\ I_{L_{m,\max}} &= I_{L_m} + \frac{\Delta i_{L_m}}{2} \\ &= \frac{V_s D}{(1-D)^2 R} \bigg(\frac{N_2}{N_1}\bigg)^2 + \frac{V_s DT}{2L_m} \\ I_{L_{m,\min}} &= I_{L_m} - \frac{\Delta i_{L_m}}{2} \quad \text{equate this to zero for dem boundary} \\ &= \frac{V_s D}{(1-D)^2 R} \bigg(\frac{N_2}{N_1}\bigg)^2 - \frac{V_s DT}{2L_m} \\ \Delta V_{o, \text{ESR}} &= \Delta i_C r_C = I_{L_{m,\max}} \bigg(\frac{N_1}{N_2}\bigg) r_C \end{split}$$

Figure 5: Flyback Formulas

$$SwitchUtilization = \frac{Po}{Psw} = \frac{Io.Vo}{q.Vswmax.Iswmax} \qquad (1)$$

$$\begin{bmatrix} V_o = V_s D \left(\frac{N_2}{N_1} \right) \end{bmatrix} \begin{bmatrix} \frac{\Delta V_o}{V_o} = \frac{1 - D}{8L_x C f^2} \end{bmatrix}$$

$$\Delta V_{o, \text{ESR}} = \Delta i_C r_C = \Delta i_{L_x} r_C = \left[\frac{V_o (1 - D)}{L_x f} \right] r_C$$

$$\Delta i_{L_m} = \frac{V_s DT}{L_m}$$

Figure 6: Forward (single switched) Converter Formulas

$$\boxed{ V_o = 2V_s \bigg(\frac{N_S}{N_P} \bigg) D \left[\frac{\Delta V_o}{V_o} = \frac{1 - 2D}{32L_x C f^2} \right] }$$

$$\Delta V_{o,ESR} = \Delta i_{L_x} r_C = \left[\frac{V_o \bigg(\frac{1}{2} - D \bigg)}{L_x f} \right] r_C$$

Figure 7: Push Pull Formulas

$$V_o = V_s \left(\frac{D}{1-D}\right) \qquad \Delta V_{C_1} = \frac{I_o DT}{C} = \frac{V_o D}{RC_1 f}$$

$$\Delta i_{L_1} = \frac{V_s DT}{L_1} = \frac{V_s D}{L_1 f} \qquad \Delta V_o = \Delta V_{C_2} = \frac{V_o D}{RC_2 f}$$

$$\Delta i_{L_2} = \frac{V_s DT}{L_2} = \frac{V_s D}{L_2 f} \qquad C_1 = \frac{D}{R(\Delta V_{C_1}/V_o) f}$$

$$C_2 = \frac{D}{R(\Delta V_o/V_o) f}$$

Figure 8: Sepic Converter Formulas

$$\begin{split} V_o &= -V_s \bigg(\frac{D}{1-D} \bigg) \, \Bigg| \, \frac{\Delta V_o}{V_o} &= \frac{1-D}{8L_2C_2f^2} \\ \Delta v_{C_1} &\approx \frac{1}{C_1} \int_{DT}^T I_{L_1} d(t) = \frac{I_{L_1}}{C_1} (1-D)T = \frac{V_s}{RC_1f} \bigg(\frac{D^2}{1-D} \bigg) \\ & \qquad \qquad \Delta v_{C_1} \approx \frac{V_oD}{RC_1f} \\ \\ \Delta i_{L1} &= \frac{V_sDT}{L_1} = \frac{V_sD}{L_1f} \, \Bigg| \, \Delta i_{L2} &= \frac{V_sDT}{L_2} = \frac{V_sD}{L_2f} \\ \\ L_{1,\,\text{min}} &= \frac{(1-D)^2R}{2Df} \quad L_{2,\,\text{min}} = \frac{(1-D)R}{2f} \end{split}$$

Figure 9: Cuk Converter Formulas