## Cheat Sheet for EE464

$$\begin{aligned} \text{Form Factor} &= \frac{V_{rms}}{V_{avg}} &\quad \text{Crest Factor} &= \frac{V_{peak}}{V_{rms}} \\ &\quad \text{Distortion Factor} &= \frac{I_{1rms}}{I} \end{aligned}$$

 $\begin{array}{c} \text{Distortion Factor}{=}\frac{I_{1rms}}{I_{rms}}\\ \phi: \text{ phase difference between fundamentals of current and voltage}\\ \text{Displacement Power Factor}{=}\cos(\phi) \end{array}$ 

True Power Factor=
$$\frac{P}{S}$$
=DPF  $\frac{I_{1,RMS}}{I_{RMS}}$   
 $THD = \sqrt{(\frac{I_{rms}}{I_{1rms}})^2 - 1}$ 

Magnetic Circuits

Flux Linkage = 
$$\lambda = N\phi$$
 |  $\mathcal{F} = \Phi R = NI$  |  $B = \mu H$   
 $B = \frac{\Phi}{A}$  |  $L = \frac{N\phi}{I} = N^2/\mathcal{R}$  |  $L = \frac{\lambda}{I}$   
 $NBA = \Phi N = \lambda$  |  $\mathcal{R} = \frac{l}{\mu A}$  |  $E = \frac{1}{2}\frac{B^2}{\mu} = \frac{1}{2}LI^2$   
 $\Delta Q = It$  |  $\Delta V = \frac{\Delta Q}{C}$  |  $\int Hdl = NI$ 

$$\begin{array}{|c|c|c|c|c|} \hline \textbf{Converters} \\ \hline & \frac{V_o}{V_s} = \frac{D}{1-D} \frac{N_2}{N_1} & \frac{\Delta V_o}{V_o} = \frac{D}{RCf} & L_{m,min} = \frac{(1-D)^2 R}{2f} (\frac{N_1}{N_2})^2 \\ \hline & I_C = I_{L_M} \frac{N_1}{N_2} - \frac{V_o}{R} & L_m = \frac{V_s DT}{\Delta i_{L_m}} & \Delta V_o = \Delta i_c r_c = I_{L_m,max} \frac{N_1}{N_2} r_c \\ \hline & \hat{V}_{sw} = V_s + \frac{N_1}{N_2} V_o = \frac{V_s}{(1-D)} & I_{L_m} = \frac{V_s D}{(1-D)^2 R} \frac{N_2}{N_1}^2 \pm \frac{V_s DT}{2L_m} \\ \hline & \hat{I}_{sw} = \frac{1}{(1-D)} \frac{N_2}{N_1} I_o + \frac{N_1}{N_2} \frac{(1-DT_s)}{2L_m} V_o \\ \hline \end{array}$$

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$$\begin{vmatrix} \frac{\mathbf{To}}{\mathbf{Vo}} & \frac{V_o}{V_s} = 2\frac{N_2}{N_1}D & \frac{\Delta V_o}{V_o} = \frac{1-2D}{32L_xCf^2} & I_{L_x} = \frac{V_o}{R} \\ \Delta V_o = \Delta i_{L_x}r_c = r_c\frac{V_o(\frac{1}{2}-D)}{L_xf} \\ \end{vmatrix}$$

$$\begin{array}{c|c} & \frac{V_o}{V_s} = \frac{D}{1-D} & \left| \frac{\Delta V_o}{V_o} = \frac{1-D}{8L_2C_2f^2} \right| \Delta V_{C_1} \approx \frac{V_oD}{RC_1f} \\ & \Delta I_{L_1} = \frac{V_sDT}{L_1} & \Delta I_{L_2} = \frac{V_sDT}{L_2} \\ & L_{1,min} = \frac{(1-D)^2R}{2Df} & L_{2,min} = \frac{(1-D)R}{2f} \\ & \Delta V_{C_1} \approx \frac{1}{C_1} \int_{DT}^T I_{L_1} dt = \frac{I_{L_1}}{C_1} (1-D)T = \frac{V_s}{RC_1f} \frac{D^2}{1-D} \\ \end{array}$$

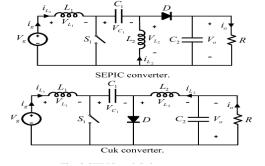


Figure 1: Sepic and Cuk Converter Schematics

| Topology  | $V_{sw}$     | $I_{sw}$                       | $V_{01,max}$  | q |
|-----------|--------------|--------------------------------|---|---|
| Push Pull | $2V_{d,max}$ | $\sqrt{2} \frac{I_{o,max}}{n}$ | $\frac{4}{\pi\sqrt{2}}\frac{V_{d,max}}{n}$            | 2 |
| Half B.   | $V_{d,max}$  | $\sqrt{2}I_{o,max}$            | $\frac{\pi\sqrt{2}}{\pi\sqrt{2}} \frac{n}{V_{d,max}}$ | 2 |
| Full B.   | $V_{d,max}$  | $\sqrt{2}I_{o,max}$            | $\frac{4}{\pi\sqrt{2}}V_{d,max}$                      | 4 |

Table 1: Swith Utilization doesnt change  $(1/2\pi)$  for n:1 trans. ratio and in linear region scaled by  $(m_a\pi)/4$ 

$$\begin{aligned} V_o &= V_s \bigg( \frac{D}{1 - D} \bigg) \\ \Delta V_{C1} &= \frac{I_o DT}{C} = \frac{V_o D}{R C_1 f} \\ \Delta i_{L1} &= \frac{V_s DT}{L_1} = \frac{V_s D}{L_1 f} \\ \Delta V_o &= \Delta V_{C2} = \frac{V_o D}{R C_2 f} \\ \Delta i_{L2} &= \frac{V_s DT}{L_2} = \frac{V_s D}{L_2 f} \\ C_1 &= \frac{D}{R (\Delta V_{C1} / V_o) f} \\ I_{L1} &= I_s = \frac{V_o I_o}{V_s} = \frac{V_o^2}{V_s R} \\ I_{L2} &= I_o \end{aligned}$$

Figure 2: Sepic Converter Formulas

Switch Selection

Peak Switch Current 
$$\hat{I}_{sw}=\frac{1}{(1-D)}\frac{N_2}{N_1}I_o+\frac{N_1}{N_2}\frac{(1-D)T_s}{2L_m}V_o$$
 Peak Switch Voltage 
$$\hat{V}_{sw}=V_d+\frac{N_1}{N_2}V_o=\frac{V_d}{(1-D)}$$

$$\hat{V}_{sw} = V_d + rac{N_1}{N_2} V_o = rac{V_d}{(1-D)^2}$$

Figure 3: Flyback switch considerations

Figure 4: Full and Half Bridge Relations

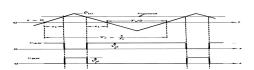


Figure 5: Bipolar Switching



Figure 6: Unipolar switching