

Manufactured Solution for 3D Navier-Stokes equation using Maple*

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Abstract

This document presents the source terms generated by the application of the Method of Manufactured Solutions (MMS) on the the 3D Navier-Stokes equations using the analytical manufactured solutions for ρ, u, v, w and p presented by Roy et al. (2002).

1 3D Navier-Stokes Equations

The 3D Navier-Stokes equations in conservation form are:

$$\frac{\partial(\rho)}{\partial t} + \frac{\partial(\rho u)}{\partial x} + \frac{\partial(\rho v)}{\partial y} + \frac{\partial(\rho w)}{\partial z} = 0 \quad (1)$$

$$\frac{\partial(\rho u)}{\partial t} + \frac{\partial(\rho u^2 + p - \tau_{xx})}{\partial x} + \frac{\partial(\rho uv - \tau_{xy})}{\partial y} + \frac{\partial(\rho uw - \tau_{xz})}{\partial z} = 0 \quad (2)$$

$$\frac{\partial(\rho v)}{\partial t} + \frac{\partial(\rho vu - \tau_{yx})}{\partial x} + \frac{\partial(\rho v^2 + p - \tau_{yy})}{\partial y} + \frac{\partial(\rho vw - \tau_{yz})}{\partial z} = 0 \quad (3)$$

$$\frac{\partial(\rho w)}{\partial t} + \frac{\partial(\rho wu - \tau_{zx})}{\partial x} + \frac{\partial(\rho wv - \tau_{zy})}{\partial y} + \frac{\partial(\rho w^2 + p - \tau_{zz})}{\partial z} = 0 \quad (4)$$

$$\frac{\partial(\rho e_t)}{\partial t} + \frac{\partial(\rho u e_t + pu - u\tau_{xx} - v\tau_{xy} - w\tau_{xz} + q_x)}{\partial x} + \frac{\partial(\rho v e_t + pv - u\tau_{yx} - v\tau_{yy} - w\tau_{yz} + q_y)}{\partial y} + \frac{\partial(\rho w e_t + pw - u\tau_{zx} - v\tau_{zy} - w\tau_{zz} + q_z)}{\partial z} = 0 \quad (5)$$

where the Equation (1) is mass conservation, Equations (2) – (4) are momentum, and Equation (5) is the energy. Notice that Equations (2)–(4) include viscous effects.

For a calorically perfect gas, the Navier-Stokes equations are closed with two auxiliary relations for energy:

$$e_t = e + \frac{u^2 + v^2 + w^2}{2} \quad \text{and} \quad e = \frac{1}{\gamma - 1} RT, \quad (6)$$

*The manufactured solution has been presented by Roy, Smith, and Ober (2002).

where γ is the ratio of specific heats, and with the ideal gas equation of state:

$$p = \rho RT. \quad (7)$$

The shear stress tensor is:

$$\begin{aligned} \tau_{xx} &= \frac{2}{3}\mu \left(2\frac{\partial u}{\partial x} - \frac{\partial v}{\partial y} - \frac{\partial w}{\partial z} \right), & \tau_{xy} &= \tau_{yx} = \mu \left(\frac{\partial u}{\partial y} + \frac{\partial v}{\partial x} \right), \\ \tau_{yy} &= \frac{2}{3}\mu \left(2\frac{\partial v}{\partial y} - \frac{\partial u}{\partial x} - \frac{\partial w}{\partial z} \right), & \tau_{yz} &= \tau_{zy} = \mu \left(\frac{\partial v}{\partial z} + \frac{\partial w}{\partial y} \right), \\ \tau_{zz} &= \frac{2}{3}\mu \left(2\frac{\partial w}{\partial z} - \frac{\partial u}{\partial x} - \frac{\partial v}{\partial y} \right), & \tau_{xz} &= \tau_{zx} = \mu \left(\frac{\partial u}{\partial z} + \frac{\partial w}{\partial x} \right), \end{aligned} \quad (8)$$

where μ is the absolute viscosity. The heat flux vector is given by:

$$q_x = -k \frac{\partial T}{\partial x}, \quad q_y = -k \frac{\partial T}{\partial y}, \quad \text{and} \quad q_z = -k \frac{\partial T}{\partial z} \quad (9)$$

where k is the thermal conductivity, which can be determined by choosing the Prandtl number:

$$k = \frac{\gamma R \mu}{(\gamma - 1) Pr}.$$

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2 Manufactured Solution

Roy et al. (2002) introduce the general form of the primitive solution variables to be a function of sines and cosines:

$$\phi(x, y) = \phi_0 + \phi_x f_s \left(\frac{a_{\phi x} \pi x}{L} \right) + \phi_y f_s \left(\frac{a_{\phi y} \pi y}{L} \right) + \phi_z f_s \left(\frac{a_{\phi z} \pi z}{L} \right), \quad (10)$$

where $\phi = \rho, u, v, w$ or p , and $f_s(\cdot)$ functions denote either sine or cosine function. Note that in this case, ϕ_x, ϕ_y and ϕ_z are constants and the subscripts do not denote differentiation.

Therefore, the manufactured analytical solution for each one of the variables in Navier-Stokes equations are:

$$\begin{aligned} \rho(x, y, z) &= \rho_0 + \rho_x \sin \left(\frac{a_{\rho x} \pi x}{L} \right) + \rho_y \cos \left(\frac{a_{\rho y} \pi y}{L} \right) + \rho_z \sin \left(\frac{a_{\rho z} \pi z}{L} \right), \\ u(x, y, z) &= u_0 + u_x \sin \left(\frac{a_{ux} \pi x}{L} \right) + u_y \cos \left(\frac{a_{uy} \pi y}{L} \right) + u_z \cos \left(\frac{a_{uz} \pi z}{L} \right), \\ v(x, y, z) &= v_0 + v_x \cos \left(\frac{a_{vx} \pi x}{L} \right) + v_y \sin \left(\frac{a_{vy} \pi y}{L} \right) + v_z \sin \left(\frac{a_{vz} \pi z}{L} \right), \\ w(x, y, z) &= w_0 + w_x \sin \left(\frac{a_{wx} \pi x}{L} \right) + w_y \sin \left(\frac{a_{wy} \pi y}{L} \right) + w_z \cos \left(\frac{a_{wz} \pi z}{L} \right), \\ p(x, y, z) &= p_0 + p_x \cos \left(\frac{a_{px} \pi x}{L} \right) + p_y \sin \left(\frac{a_{py} \pi y}{L} \right) + p_z \cos \left(\frac{a_{pz} \pi z}{L} \right). \end{aligned} \quad (11)$$

The MMS applied to Navier-Stokes equations consists in modifying Equations (1) – (5) by adding a source term to the right-hand side of each equation:

$$\begin{aligned}
\frac{\partial(\rho)}{\partial t} + \frac{\partial(\rho u)}{\partial x} + \frac{\partial(\rho v)}{\partial y} + \frac{\partial(\rho w)}{\partial z} &= Q_\rho \\
\frac{\partial(\rho u)}{\partial t} + \frac{\partial(\rho u^2 + p - \tau_{xx})}{\partial x} + \frac{\partial(\rho uv - \tau_{xy})}{\partial y} + \frac{\partial(\rho uw - \tau_{xz})}{\partial z} &= Q_u, \\
\frac{\partial(\rho v)}{\partial t} + \frac{\partial(\rho vu - \tau_{yx})}{\partial x} + \frac{\partial(\rho v^2 + p - \tau_{yy})}{\partial y} + \frac{\partial(\rho vw - \tau_{yz})}{\partial z} &= Q_v, \\
\frac{\partial(\rho w)}{\partial t} + \frac{\partial(\rho wu - \tau_{zx})}{\partial x} + \frac{\partial(\rho wv - \tau_{zy})}{\partial y} + \frac{\partial(\rho w^2 + p - \tau_{zz})}{\partial z} &= Q_w, \\
\frac{\partial(\rho e_t)}{\partial t} + \frac{\partial(\rho ue_t + pu - u\tau_{xx} - v\tau_{xy} - w\tau_{xz} + q_x)}{\partial x} + \frac{\partial(\rho ve_t + pv - u\tau_{yx} - v\tau_{yy} - w\tau_{yz} + q_y)}{\partial y} + \frac{\partial(\rho we_t + pw - u\tau_{zx} - v\tau_{zy} - w\tau_{zz} + q_z)}{\partial z} &= Q_{e_t},
\end{aligned} \tag{12}$$

so the modified set of equations has known, analytical solution.

In the case of Q_ρ , Q_u , Q_v , Q_w and Q_{e_t} are conveniently obtained by analytical differentiation of Equation (11) using Equations (1) – (5) as differential operators, the solution of Equation (12) is Equation (11).

Such terms are obtained by symbolic manipulations of equations above using Maple and are presented in the following sections.

3 Source term for Navier-Stokes mass conservation equation

$$\begin{aligned}
Q_\rho &= \frac{a_{\rho x}\pi\rho_x}{L} \cos\left(\frac{a_{\rho x}\pi x}{L}\right) \left[u_0 + u_x \sin\left(\frac{a_{ux}\pi x}{L}\right) + u_y \cos\left(\frac{a_{uy}\pi y}{L}\right) + u_z \cos\left(\frac{a_{uz}\pi z}{L}\right) \right] + \\
&\quad - \frac{a_{\rho y}\pi\rho_y}{L} \sin\left(\frac{a_{\rho y}\pi y}{L}\right) \left[v_0 + v_x \cos\left(\frac{a_{vx}\pi x}{L}\right) + v_y \sin\left(\frac{a_{vy}\pi y}{L}\right) + v_z \sin\left(\frac{a_{vz}\pi z}{L}\right) \right] + \\
&\quad + \frac{a_{\rho z}\pi\rho_z}{L} \cos\left(\frac{a_{\rho z}\pi z}{L}\right) \left[w_0 + w_x \sin\left(\frac{a_{wx}\pi x}{L}\right) + w_y \sin\left(\frac{a_{wy}\pi y}{L}\right) + w_z \cos\left(\frac{a_{wz}\pi z}{L}\right) \right] + \\
&\quad + \frac{a_{ux}\pi u_x}{L} \cos\left(\frac{a_{ux}\pi x}{L}\right) \left[\rho_0 + \rho_x \sin\left(\frac{a_{\rho x}\pi x}{L}\right) + \rho_y \cos\left(\frac{a_{\rho y}\pi y}{L}\right) + \rho_z \sin\left(\frac{a_{\rho z}\pi z}{L}\right) \right] + \\
&\quad + \frac{a_{vy}\pi v_y}{L} \cos\left(\frac{a_{vy}\pi y}{L}\right) \left[\rho_0 + \rho_x \sin\left(\frac{a_{\rho x}\pi x}{L}\right) + \rho_y \cos\left(\frac{a_{\rho y}\pi y}{L}\right) + \rho_z \sin\left(\frac{a_{\rho z}\pi z}{L}\right) \right] + \\
&\quad - \frac{a_{wz}\pi w_z}{L} \sin\left(\frac{a_{wz}\pi z}{L}\right) \left[\rho_0 + \rho_x \sin\left(\frac{a_{\rho x}\pi x}{L}\right) + \rho_y \cos\left(\frac{a_{\rho y}\pi y}{L}\right) + \rho_z \sin\left(\frac{a_{\rho z}\pi z}{L}\right) \right]
\end{aligned} \tag{13}$$

4 Source term for Navier-Stokes momentum equation

$$\begin{aligned}
Q_u = & -\frac{a_{px}\pi p_x}{L} \sin\left(\frac{a_{px}\pi x}{L}\right) + \\
& + \frac{a_{\rho x}\pi \rho_x}{L} \cos\left(\frac{a_{\rho x}\pi x}{L}\right) \left[u_0 + u_x \sin\left(\frac{a_{ux}\pi x}{L}\right) + u_y \cos\left(\frac{a_{uy}\pi y}{L}\right) + u_z \cos\left(\frac{a_{uz}\pi z}{L}\right)\right]^2 + \\
& - \frac{a_{\rho y}\pi \rho_y}{L} \sin\left(\frac{a_{\rho y}\pi y}{L}\right) \left[v_0 + v_x \cos\left(\frac{a_{vx}\pi x}{L}\right) + v_y \sin\left(\frac{a_{vy}\pi y}{L}\right) + v_z \sin\left(\frac{a_{vz}\pi z}{L}\right)\right] \left[u_0 + u_x \sin\left(\frac{a_{ux}\pi x}{L}\right) + u_y \cos\left(\frac{a_{uy}\pi y}{L}\right) + u_z \cos\left(\frac{a_{uz}\pi z}{L}\right)\right] + \\
& + \frac{a_{\rho z}\pi \rho_z}{L} \cos\left(\frac{a_{\rho z}\pi z}{L}\right) \left[w_0 + w_x \sin\left(\frac{a_{wx}\pi x}{L}\right) + w_y \sin\left(\frac{a_{wy}\pi y}{L}\right) + w_z \cos\left(\frac{a_{wz}\pi z}{L}\right)\right] \left[u_0 + u_x \sin\left(\frac{a_{ux}\pi x}{L}\right) + u_y \cos\left(\frac{a_{uy}\pi y}{L}\right) + u_z \cos\left(\frac{a_{uz}\pi z}{L}\right)\right] + \\
& + \frac{2a_{ux}\pi u_x}{L} \cos\left(\frac{a_{ux}\pi x}{L}\right) \left[\rho_0 + \rho_x \sin\left(\frac{a_{\rho x}\pi x}{L}\right) + \rho_y \cos\left(\frac{a_{\rho y}\pi y}{L}\right) + \rho_z \sin\left(\frac{a_{\rho z}\pi z}{L}\right)\right] \left[u_0 + u_x \sin\left(\frac{a_{ux}\pi x}{L}\right) + u_y \cos\left(\frac{a_{uy}\pi y}{L}\right) + u_z \cos\left(\frac{a_{uz}\pi z}{L}\right)\right] + \\
& - \frac{a_{uy}\pi u_y}{L} \sin\left(\frac{a_{uy}\pi y}{L}\right) \left[\rho_0 + \rho_x \sin\left(\frac{a_{\rho x}\pi x}{L}\right) + \rho_y \cos\left(\frac{a_{\rho y}\pi y}{L}\right) + \rho_z \sin\left(\frac{a_{\rho z}\pi z}{L}\right)\right] \left[v_0 + v_x \cos\left(\frac{a_{vx}\pi x}{L}\right) + v_y \sin\left(\frac{a_{vy}\pi y}{L}\right) + v_z \sin\left(\frac{a_{vz}\pi z}{L}\right)\right] + \\
& - \frac{a_{uz}\pi u_z}{L} \sin\left(\frac{a_{uz}\pi z}{L}\right) \left[\rho_0 + \rho_x \sin\left(\frac{a_{\rho x}\pi x}{L}\right) + \rho_y \cos\left(\frac{a_{\rho y}\pi y}{L}\right) + \rho_z \sin\left(\frac{a_{\rho z}\pi z}{L}\right)\right] \left[w_0 + w_x \sin\left(\frac{a_{wx}\pi x}{L}\right) + w_y \sin\left(\frac{a_{wy}\pi y}{L}\right) + w_z \cos\left(\frac{a_{wz}\pi z}{L}\right)\right] + \\
& + \frac{a_{vy}\pi v_y}{L} \cos\left(\frac{a_{vy}\pi y}{L}\right) \left[\rho_0 + \rho_x \sin\left(\frac{a_{\rho x}\pi x}{L}\right) + \rho_y \cos\left(\frac{a_{\rho y}\pi y}{L}\right) + \rho_z \sin\left(\frac{a_{\rho z}\pi z}{L}\right)\right] \left[u_0 + u_x \sin\left(\frac{a_{ux}\pi x}{L}\right) + u_y \cos\left(\frac{a_{uy}\pi y}{L}\right) + u_z \cos\left(\frac{a_{uz}\pi z}{L}\right)\right] + \\
& - \frac{a_{wz}\pi w_z}{L} \sin\left(\frac{a_{wz}\pi z}{L}\right) \left[\rho_0 + \rho_x \sin\left(\frac{a_{\rho x}\pi x}{L}\right) + \rho_y \cos\left(\frac{a_{\rho y}\pi y}{L}\right) + \rho_z \sin\left(\frac{a_{\rho z}\pi z}{L}\right)\right] \left[u_0 + u_x \sin\left(\frac{a_{ux}\pi x}{L}\right) + u_y \cos\left(\frac{a_{uy}\pi y}{L}\right) + u_z \cos\left(\frac{a_{uz}\pi z}{L}\right)\right] + \\
& + \frac{4a_{ux}^2\pi^2\mu u_x}{3L^2} \sin\left(\frac{a_{ux}\pi x}{L}\right) + \frac{a_{uy}^2\pi^2\mu u_y}{L^2} \cos\left(\frac{a_{uy}\pi y}{L}\right) + \frac{a_{uz}^2\pi^2\mu u_z}{L^2} \cos\left(\frac{a_{uz}\pi z}{L}\right)
\end{aligned} \tag{14}$$

5 Source term for Navier-Stokes energy equation

$$\begin{aligned}
Qe = & -\frac{a_{px}\pi p_x}{L} \frac{\gamma}{\gamma-1} \sin\left(\frac{a_{px}\pi x}{L}\right) \left[u_0 + u_x \sin\left(\frac{a_{ux}\pi x}{L}\right) + u_y \cos\left(\frac{a_{uy}\pi y}{L}\right) + u_z \cos\left(\frac{a_{uz}\pi z}{L}\right)\right] + \\
& + \frac{a_{py}\pi p_y}{L} \frac{\gamma}{\gamma-1} \cos\left(\frac{a_{py}\pi y}{L}\right) \left[v_0 + v_x \cos\left(\frac{a_{vx}\pi x}{L}\right) + v_y \sin\left(\frac{a_{vy}\pi y}{L}\right) + v_z \sin\left(\frac{a_{vz}\pi z}{L}\right)\right] + \\
& - \frac{a_{pz}\pi p_z}{L} \frac{\gamma}{\gamma-1} \sin\left(\frac{a_{pz}\pi z}{L}\right) \left[w_0 + w_x \sin\left(\frac{a_{wx}\pi x}{L}\right) + w_y \sin\left(\frac{a_{wy}\pi y}{L}\right) + w_z \cos\left(\frac{a_{wz}\pi z}{L}\right)\right] + \\
& + \frac{a_{\rho x}\pi \rho_x}{2L} \cos\left(\frac{a_{\rho x}\pi x}{L}\right) \left[u_0 + u_x \sin\left(\frac{a_{ux}\pi x}{L}\right) + u_y \cos\left(\frac{a_{uy}\pi y}{L}\right) + u_z \cos\left(\frac{a_{uz}\pi z}{L}\right)\right] \left(\left[u_0 + u_x \sin\left(\frac{a_{ux}\pi x}{L}\right) + u_y \cos\left(\frac{a_{uy}\pi y}{L}\right) + u_z \cos\left(\frac{a_{uz}\pi z}{L}\right)\right]^2 + \right. \\
& \quad \left. + \left[w_0 + w_x \sin\left(\frac{a_{wx}\pi x}{L}\right) + w_y \sin\left(\frac{a_{wy}\pi y}{L}\right) + w_z \cos\left(\frac{a_{wz}\pi z}{L}\right)\right]^2 + \left[v_0 + v_x \cos\left(\frac{a_{vx}\pi x}{L}\right) + v_y \sin\left(\frac{a_{vy}\pi y}{L}\right) + v_z \sin\left(\frac{a_{vz}\pi z}{L}\right)\right]^2\right) + \\
& - \frac{a_{\rho y}\pi \rho_y}{2L} \sin\left(\frac{a_{\rho y}\pi y}{L}\right) \left[v_0 + v_x \cos\left(\frac{a_{vx}\pi x}{L}\right) + v_y \sin\left(\frac{a_{vy}\pi y}{L}\right) + v_z \sin\left(\frac{a_{vz}\pi z}{L}\right)\right] \left(\left[u_0 + u_x \sin\left(\frac{a_{ux}\pi x}{L}\right) + u_y \cos\left(\frac{a_{uy}\pi y}{L}\right) + u_z \cos\left(\frac{a_{uz}\pi z}{L}\right)\right]^2 + \right. \\
& \quad \left. + \left[w_0 + w_x \sin\left(\frac{a_{wx}\pi x}{L}\right) + w_y \sin\left(\frac{a_{wy}\pi y}{L}\right) + w_z \cos\left(\frac{a_{wz}\pi z}{L}\right)\right]^2 + \left[v_0 + v_x \cos\left(\frac{a_{vx}\pi x}{L}\right) + v_y \sin\left(\frac{a_{vy}\pi y}{L}\right) + v_z \sin\left(\frac{a_{vz}\pi z}{L}\right)\right]^2\right) + \\
& + \frac{a_{\rho z}\pi \rho_z}{2L} \cos\left(\frac{a_{\rho z}\pi z}{L}\right) \left[w_0 + w_x \sin\left(\frac{a_{wx}\pi x}{L}\right) + w_y \sin\left(\frac{a_{wy}\pi y}{L}\right) + w_z \cos\left(\frac{a_{wz}\pi z}{L}\right)\right] \left(\left[u_0 + u_x \sin\left(\frac{a_{ux}\pi x}{L}\right) + u_y \cos\left(\frac{a_{uy}\pi y}{L}\right) + u_z \cos\left(\frac{a_{uz}\pi z}{L}\right)\right]^2 + \right. \\
& \quad \left. + \left[w_0 + w_x \sin\left(\frac{a_{wx}\pi x}{L}\right) + w_y \sin\left(\frac{a_{wy}\pi y}{L}\right) + w_z \cos\left(\frac{a_{wz}\pi z}{L}\right)\right]^2 + \left[v_0 + v_x \cos\left(\frac{a_{vx}\pi x}{L}\right) + v_y \sin\left(\frac{a_{vy}\pi y}{L}\right) + v_z \sin\left(\frac{a_{vz}\pi z}{L}\right)\right]^2\right) + \\
& + \frac{a_{ux}\pi u_x}{2L} \cos\left(\frac{a_{ux}\pi x}{L}\right) \left\{ \left(\left[w_0 + w_x \sin\left(\frac{a_{wx}\pi x}{L}\right) + w_y \sin\left(\frac{a_{wy}\pi y}{L}\right) + w_z \cos\left(\frac{a_{wz}\pi z}{L}\right)\right]^2 + \left[v_0 + v_x \cos\left(\frac{a_{vx}\pi x}{L}\right) + v_y \sin\left(\frac{a_{vy}\pi y}{L}\right) + v_z \sin\left(\frac{a_{vz}\pi z}{L}\right)\right]^2\right) + \right. \\
& \quad \left. + 3 \left[u_0 + u_x \sin\left(\frac{a_{ux}\pi x}{L}\right) + u_y \cos\left(\frac{a_{uy}\pi y}{L}\right) + u_z \cos\left(\frac{a_{uz}\pi z}{L}\right)\right]^2 \left[\rho_0 + \rho_x \sin\left(\frac{a_{\rho x}\pi x}{L}\right) + \rho_y \cos\left(\frac{a_{\rho y}\pi y}{L}\right) + \rho_z \sin\left(\frac{a_{\rho z}\pi z}{L}\right)\right] + \right. \\
& \quad \left. + \left[p_0 + p_x \cos\left(\frac{a_{px}\pi x}{L}\right) + p_y \sin\left(\frac{a_{py}\pi y}{L}\right) + p_z \cos\left(\frac{a_{pz}\pi z}{L}\right)\right] \frac{2\gamma}{(\gamma-1)} \right\} + \\
& - \frac{a_{uy}\pi u_y}{L} \sin\left(\frac{a_{uy}\pi y}{L}\right) \left[v_0 + v_x \cos\left(\frac{a_{vx}\pi x}{L}\right) + v_y \sin\left(\frac{a_{vy}\pi y}{L}\right) + v_z \sin\left(\frac{a_{vz}\pi z}{L}\right)\right] \left[\rho_0 + \rho_x \sin\left(\frac{a_{\rho x}\pi x}{L}\right) + \rho_y \cos\left(\frac{a_{\rho y}\pi y}{L}\right) + \rho_z \sin\left(\frac{a_{\rho z}\pi z}{L}\right)\right] \cdot \\
& \quad \cdot \left[u_0 + u_x \sin\left(\frac{a_{ux}\pi x}{L}\right) + u_y \cos\left(\frac{a_{uy}\pi y}{L}\right) + u_z \cos\left(\frac{a_{uz}\pi z}{L}\right)\right] + \\
& - \frac{a_{uz}\pi u_z}{L} \sin\left(\frac{a_{uz}\pi z}{L}\right) \left[w_0 + w_x \sin\left(\frac{a_{wx}\pi x}{L}\right) + w_y \sin\left(\frac{a_{wy}\pi y}{L}\right) + w_z \cos\left(\frac{a_{wz}\pi z}{L}\right)\right] \left[\rho_0 + \rho_x \sin\left(\frac{a_{\rho x}\pi x}{L}\right) + \rho_y \cos\left(\frac{a_{\rho y}\pi y}{L}\right) + \rho_z \sin\left(\frac{a_{\rho z}\pi z}{L}\right)\right] \cdot \\
& \quad \cdot \left[u_0 + u_x \sin\left(\frac{a_{ux}\pi x}{L}\right) + u_y \cos\left(\frac{a_{uy}\pi y}{L}\right) + u_z \cos\left(\frac{a_{uz}\pi z}{L}\right)\right] +
\end{aligned}
\tag{17}$$

[illegible]

[illegible]

$$\begin{aligned}
& - \frac{2a_{px}a_{\rho x}\pi^2kp_x\rho_x \cos\left(\frac{a_{\rho x}\pi x}{L}\right) \sin\left(\frac{a_{px}\pi x}{L}\right)}{L^2R\left[\rho_0 + \rho_x \sin\left(\frac{a_{\rho x}\pi x}{L}\right) + \rho_y \cos\left(\frac{a_{\rho y}\pi y}{L}\right) + \rho_z \sin\left(\frac{a_{\rho z}\pi z}{L}\right)\right]^2} + \\
& - \frac{2a_{py}a_{\rho y}\pi^2kp_y\rho_y \sin\left(\frac{a_{\rho y}\pi y}{L}\right) \cos\left(\frac{a_{py}\pi y}{L}\right)}{L^2R\left[\rho_0 + \rho_x \sin\left(\frac{a_{\rho x}\pi x}{L}\right) + \rho_y \cos\left(\frac{a_{\rho y}\pi y}{L}\right) + \rho_z \sin\left(\frac{a_{\rho z}\pi z}{L}\right)\right]^2} + \\
& - \frac{2a_{pz}a_{\rho z}\pi^2kp_z\rho_z \cos\left(\frac{a_{\rho z}\pi z}{L}\right) \sin\left(\frac{a_{pz}\pi z}{L}\right)}{L^2R\left[\rho_0 + \rho_x \sin\left(\frac{a_{\rho x}\pi x}{L}\right) + \rho_y \cos\left(\frac{a_{\rho y}\pi y}{L}\right) + \rho_z \sin\left(\frac{a_{\rho z}\pi z}{L}\right)\right]^2} + \\
& + \frac{4}{3} \frac{a_{ux}a_{vy}\pi^2\mu u_x v_y}{L^2} \cos\left(\frac{a_{ux}\pi x}{L}\right) \cos\left(\frac{a_{vy}\pi y}{L}\right) + \\
& - \frac{4}{3} \frac{a_{ux}a_{wz}\pi^2\mu u_x w_z}{L^2} \cos\left(\frac{a_{ux}\pi x}{L}\right) \sin\left(\frac{a_{wz}\pi z}{L}\right) + \\
& - \frac{2a_{uy}a_{vx}\pi^2\mu u_y v_x}{L^2} \sin\left(\frac{a_{uy}\pi y}{L}\right) \sin\left(\frac{a_{vx}\pi x}{L}\right) + \\
& + \frac{2a_{uz}a_{wx}\pi^2\mu u_z w_x}{L^2} \cos\left(\frac{a_{wx}\pi x}{L}\right) \sin\left(\frac{a_{uz}\pi z}{L}\right) + \\
& - \frac{4}{3} \frac{a_{vy}a_{wz}\pi^2\mu v_y w_z}{L^2} \cos\left(\frac{a_{vy}\pi y}{L}\right) \sin\left(\frac{a_{wz}\pi z}{L}\right) + \\
& - \frac{2a_{vz}a_{wy}\pi^2\mu v_z w_y}{L^2} \cos\left(\frac{a_{vz}\pi z}{L}\right) \cos\left(\frac{a_{wy}\pi y}{L}\right).
\end{aligned}$$

6

6 Comments

Source terms Q_ρ , Q_u , Q_v and Q_w have been generated automatically by replacing the analytical expressions (11) into respective operators, followed by the usage of Maple commands for collecting, sorting and factorizing the terms. Yet, to achieve the final form of source term Q_{e_t} , due to its higher complexity, a slightly different procedure has been applied. First, Q_{e_t} has manually been split into several subterms, to facilitate and improve the symbolic manipulation; then Maple commands for collecting, sorting and factorizing have been employed. Finally, the resulting source term has been compared to its original form to ensure correctness. As result, the initially 41-page long expression for Q_{e_t} has been reduced to Equation (17). Please see file `NavierStokes_equation_3d_e_Maple.pdf` for the original expression of Q_{e_t} .

Files containing C codes for the source terms have also been generated. They are: `NavierStokes_3d_e_code.C`, `NavierStokes_3d_rho_code.C`, `NavierStokes_3d_u_code.C`, `NavierStokes_3d_v_code.C` and `NavierStokes_3d_w_code.C`.

An example of the automatically generated C file from the source term for mass conservation equation is:

```
double SourceQ_rho ( double x, double y, double z, double u_0, double u_x, double u_y, double u_z, double v_0,
double v_x, double v_y, double v_z, double rho_0, double rho_x, double rho_y, double rho_z,
double p_0, double p_x, double p_y, double p_z, double a_px, double a_py, double a_pz,
double a_rhox, double a_rho_y, double a_rhoz, double a_ux, double a_uy, double a_uz, double a_vx,
double a_vy, double a_vz, double a_wx, double a_wy, double a_wz, double mu, double L)
{
double Q_rho;
Q_rho = rho_x * cos(a_rhox * PI * x / L) * (u_0 + u_x * sin(a_ux * PI * x / L) + u_y * cos(a_uy * PI * y / L) +
u_z * cos(a_uz * PI * z / L)) * a_rhox * PI / L - rho_y * sin(a_rho_y * PI * y / L) * (v_0 +
v_x * cos(a_vx * PI * x / L) + v_y * sin(a_vy * PI * y / L) + v_z * sin(a_vz * PI * z / L)) * a_rho_y * PI / L +
rho_z * cos(a_rhoz * PI * z / L) * (w_0 + w_x * sin(a_wx * PI * x / L) + w_y * sin(a_wy * PI * y / L) +
w_z * cos(a_wz * PI * z / L)) * a_rhoz * PI / L + u_x * cos(a_ux * PI * x / L) * (rho_0 +
rho_x * sin(a_rhox * PI * x / L) + rho_y * cos(a_rho_y * PI * y / L) + rho_z * sin(a_rhoz * PI * z / L)) * a_ux * PI / L +
v_y * cos(a_vy * PI * y / L) * (rho_0 + rho_x * sin(a_rhox * PI * x / L) + rho_y * cos(a_rho_y * PI * y / L) +
rho_z * sin(a_rhoz * PI * z / L)) * a_vy * PI / L - w_z * sin(a_wz * PI * z / L) * (rho_0 +
rho_x * sin(a_rhox * PI * x / L) + rho_y * cos(a_rho_y * PI * y / L) + rho_z * sin(a_rhoz * PI * z / L)) * a_wz * PI / L;
return(Q_rho);
}
```

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Finally the gradients of the analytical solutions (11) have also been computed and their respective C codes are presented in NavierStokes_manuf_solutions_grad_and.code.3d.C. Therefore,

$$\nabla \rho = \begin{bmatrix} \frac{a_{\rho x} \pi \rho_x}{L} \cos\left(\frac{a_{\rho x} \pi x}{L}\right) \\ -\frac{a_{\rho y} \pi \rho_y}{L} \sin\left(\frac{a_{\rho y} \pi y}{L}\right) \\ \frac{a_{\rho z} \pi \rho_z}{L} \cos\left(\frac{a_{\rho z} \pi z}{L}\right) \end{bmatrix}, \quad \nabla p = \begin{bmatrix} -\frac{a_{p x} \pi p_x}{L} \sin\left(\frac{a_{p x} \pi x}{L}\right) \\ \frac{a_{p y} \pi p_y}{L} \cos\left(\frac{a_{p y} \pi y}{L}\right) \\ -\frac{a_{p z} \pi p_z}{L} \sin\left(\frac{a_{p z} \pi z}{L}\right) \end{bmatrix}, \quad \nabla u = \begin{bmatrix} \frac{a_{u x} \pi u_x}{L} \cos\left(\frac{a_{u x} \pi x}{L}\right) \\ -\frac{a_{u y} \pi u_y}{L} \sin\left(\frac{a_{u y} \pi y}{L}\right) \\ -\frac{a_{u z} \pi u_z}{L} \sin\left(\frac{a_{u z} \pi z}{L}\right) \end{bmatrix}, \quad (18)$$

$$\nabla v = \begin{bmatrix} -\frac{a_{v x} \pi v_x}{L} \sin\left(\frac{a_{v x} \pi x}{L}\right) \\ \frac{a_{v y} \pi v_y}{L} \cos\left(\frac{a_{v y} \pi y}{L}\right) \\ \frac{a_{v z} \pi v_z}{L} \cos\left(\frac{a_{v z} \pi z}{L}\right) \end{bmatrix} \quad \text{and} \quad \nabla w = \begin{bmatrix} \frac{a_{w x} \pi w_x}{L} \cos\left(\frac{a_{w x} \pi x}{L}\right) \\ \frac{a_{w y} \pi w_y}{L} \cos\left(\frac{a_{w y} \pi y}{L}\right) \\ -\frac{a_{w z} \pi w_z}{L} \sin\left(\frac{a_{w z} \pi z}{L}\right) \end{bmatrix} \quad (19)$$

are written in C language as:

```
grad_rho_an[0] = rho_x * cos(a_rhox * pi * x / L) * a_rhox * pi / L;
grad_rho_an[1] = -rho_y * sin(a_rho_y * pi * y / L) * a_rho_y * pi / L;
grad_rho_an[2] = rho_z * cos(a_rhoz * pi * z / L) * a_rhoz * pi / L;
grad_p_an[0] = -p_x * sin(a_px * pi * x / L) * a_px * pi / L;
grad_p_an[1] = p_y * cos(a_py * pi * y / L) * a_py * pi / L;
```

```

grad_p_an[2] = -p_z * sin(a_pz * pi * z / L) * a_pz * pi / L;
grad_u_an[0] = u_x * cos(a_ux * pi * x / L) * a_ux * pi / L;
grad_u_an[1] = -u_y * sin(a_uy * pi * y / L) * a_uy * pi / L;
grad_u_an[2] = -u_z * sin(a_uz * pi * z / L) * a_uz * pi / L;
grad_v_an[0] = -v_x * sin(a_vx * pi * x / L) * a_vx * pi / L;
grad_v_an[1] = v_y * cos(a_vy * pi * y / L) * a_vy * pi / L;
grad_v_an[2] = v_z * cos(a_vz * pi * z / L) * a_vz * pi / L;
grad_w_an[0] = w_x * cos(a_wx * pi * x / L) * a_wx * pi / L;
grad_w_an[1] = w_y * cos(a_wy * pi * y / L) * a_wy * pi / L;
grad_w_an[2] = -w_z * sin(a_wz * pi * z / L) * a_wz * pi / L;

```

References

Roy, C., T. Smith, and C. Ober (2002). Verification of a compressible cfd code using the method of manufactured solutions. In *AIAA FLuid Dynamics Conference and Exhibit*, Number AIAA 2002-3110.