



Numerical Simulation of Turbulent Combustion Using the Turbulent Flamelet Model

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INTRODUCTION

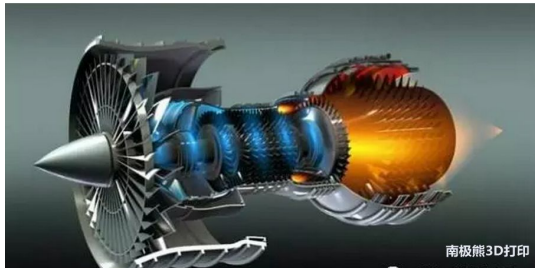
part1.1

part1.3

part1.4

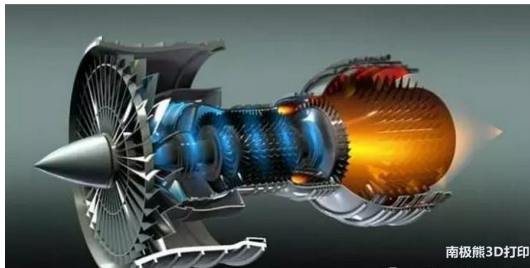
Background

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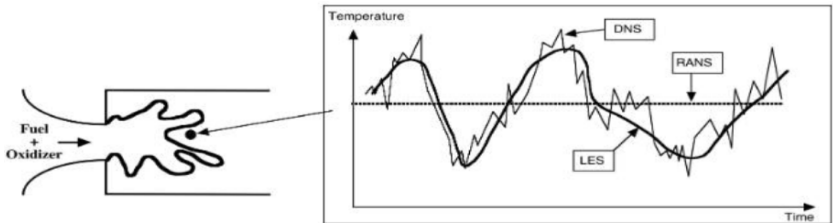
Meaningful to practical systems:

- (a) Improve efficiency, meet demanding standards[1].
- (b) Reduce pollution, environment friendly.

Numerical simulation of flowfield

Based on CFD, there're 3 possible approaches:

- (a) Direct Numerical Simulation(DNS)
 - Precise, but costly(Tremendous memory and CPU).
- (b) Large Eddy Simulation(LES)
 - Compromise between accuracy and computational cost.
- (c) Reynolds Averaged Navier-Stokes(RANS)
 - Inaccurate for combustion phenomenon.



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These drawbacks are overcome by the turbulent flamelet model to be introduced:

- Designed especially for LES, with fewer approximation.
- Relations are provided through scaling law, which is based on DNS database[2].

TURBULENT FLAMELET MODEL

part2.1

part2.2

part2.3

part2.4

Theory

Original G.E. in the context of LES:

$$\frac{\partial \bar{\rho} \tilde{Z}}{\partial t} + \nabla \cdot (\bar{\rho} \tilde{Z} \tilde{\mathbf{u}}) = \nabla \cdot [\bar{\rho} (D + D_T) \nabla \tilde{Z}] \quad (1)$$

$$\frac{\partial \bar{\rho} \tilde{Y}_i}{\partial t} + \nabla \cdot (\bar{\rho} \tilde{Y}_i \tilde{\mathbf{u}}) = \nabla \cdot [\bar{\rho} (D + D_T) \nabla \tilde{Y}_i] + \bar{\omega}_i \quad (2)$$

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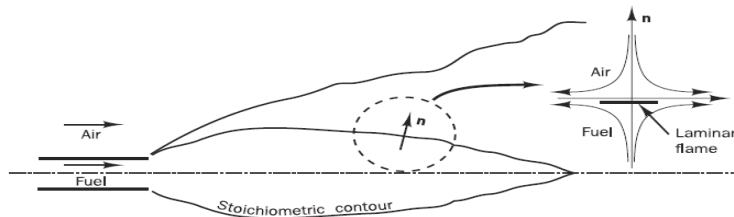
After coordinate transformation $(x_1, x_2, x_3, t) \rightarrow (Z, Z_2, Z_3, \tau)$:

$$\begin{aligned} \bar{\rho} \frac{\partial \tilde{Y}_i}{\partial \tau} + \bar{\rho} \left(\tilde{\mathbf{u}} \cdot \nabla_{\perp} \tilde{Y}_i + \frac{\partial \tilde{Y}_i}{\partial Z_2} \frac{\partial Z_2}{\partial t} + \frac{\partial \tilde{Y}_i}{\partial Z_3} \frac{\partial Z_3}{\partial t} \right) &= \frac{\bar{\rho} \chi}{2Le_T} \frac{\partial^2 \tilde{Y}_i}{\partial^2 \tilde{Z}} \\ &+ \frac{\partial \tilde{Y}_i}{\partial \tilde{Z}} \nabla \cdot \left[\bar{\rho} (\mathcal{D}_{T,i} - \mathcal{D}_T) \vec{n} \cdot \frac{\partial \tilde{Z}}{\partial \vec{n}} \right] + \nabla \cdot (\bar{\rho} \mathcal{D}_{T,i} \nabla_{\perp} \tilde{Y}_i) + \bar{\omega}_i \end{aligned} \quad (3)$$

Laminar Flamelet assumption

Locally, the characteristic timescale of chemical reaction is much smaller than that of flow ($t_c \ll t_f$).

Thus, local flame structure can be described by the diffusion flame under counterflow configuration.

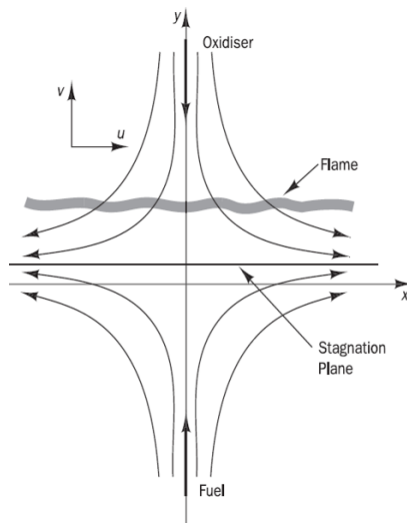


Each micro flamelet can be described by Z and χ :

- Z describes chemical reaction.
- χ indicates turbulence stretching effect.

Thus, a database can be pre-computed for later looking-up.

Turbulent Flamelet



Unlike the laminar flamelet introduced above, G.E. of the counterflow flame is slightly modified by our turbulent flamelet model from

$$\rho \frac{DY_i}{Dt} = \mathcal{D}_i \frac{\partial^2 Y_i}{\partial^2 x} + \omega_i(T, \vec{Y}) \quad (4)$$

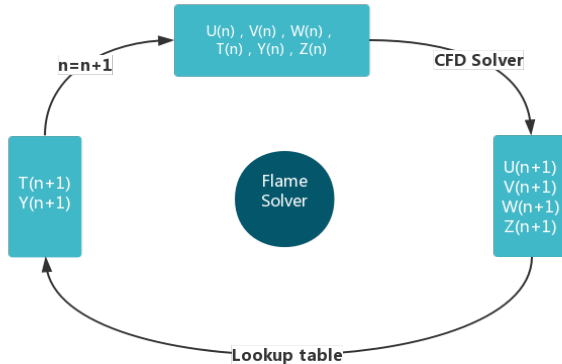
to

$$\bar{\rho} \frac{D\tilde{Y}_i}{Dt} = \mathcal{D}_i \frac{\partial^2 \tilde{Y}_i}{\partial^2 x} + \tilde{\omega}_i(\tilde{T}, \tilde{\vec{Y}}) \quad (5)$$

The two equations share similar form, but have totally different meanings.

Solution procedure

Based on the filtered turbulent flamelet database generated in the way described above, the full solution procedure that incorporates a CFD solver can be described as follows:



NUMERICAL RESULTS

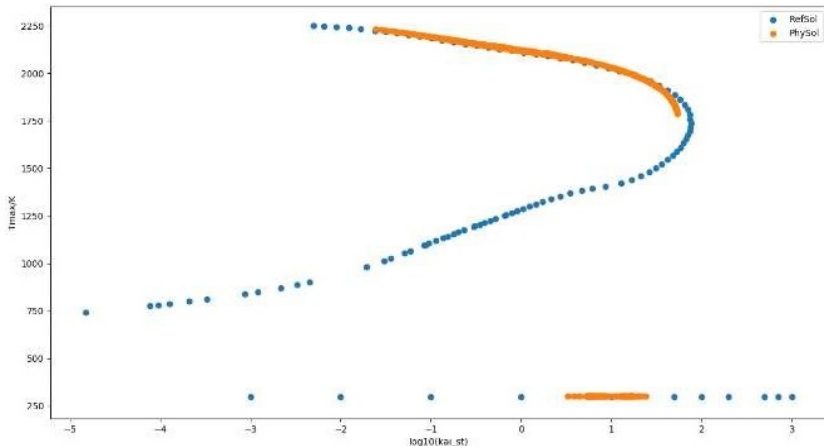
part3.1

part3.2

Comparison of “S” curve

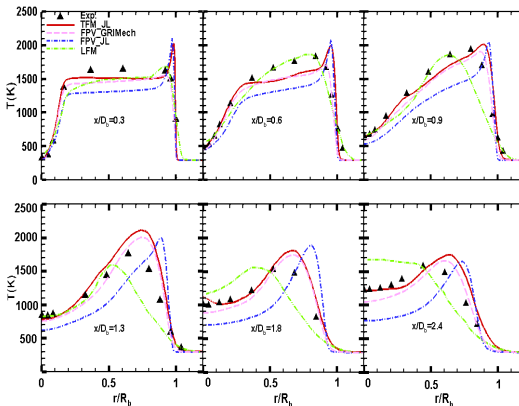
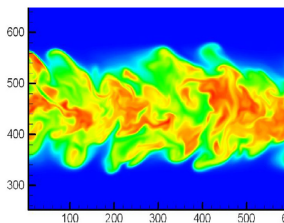
The T_{\max} plot:

- One of the most convincing testing cases.
- Difference and transition position are clearly revealed[3].



Standard case

Comparison between experimental data, which is widely used as benchmark[4].



CONCLUSIONS

part4.1

part4.2

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- Numerical simulation based on Large Eddy Simulation(LES) shows better resolution of flame structures.
- Flamelet modeling based on the filtered G.E. is physically effective for combustion problem.

Reference

- [1] Charles David Pierce and Parviz Moin. “Progress-variable approach for large-eddy simulation of turbulent combustion”. Thesis. 2001 (cit. on pp. 3, 4).
- [2] Wang Lipo. “Analysis of the filtered non-premixed turbulent flame”. In: Combustion and Flame 175 (2017), pp. 259–269 (cit. on pp. 6, 7).
- [3] Joseph F Grcar. “The Twopnt program for boundary value problems”. In: Sandia National Laboratories Report SAND91-8230 (1992) (cit. on p. 15).
- [4] P. E. Dimotakis. “The mixing transition in turbulent flows”. In: Journal of Fluid Mechanics 409 (2000), pp. 69–98. ISSN: 0022-1120. DOI: 10.1017/s0022112099007946 (cit. on p. 16).