

#SERVETHELOOP DUMP (FOR THE RLOOP)

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ABSTRACT. servetheloop notes "dump" - I dump all my notes, including things that I tried but are wrong, here.

Part 1. Eddy Currents, Eddy Current Braking

1. EDDY CURRENTS

Keywords: Eddy currents;
cf. Smythe (1968), Ch. X (his Ch. 10) [2]
Assume Maxwell's "displacement current" is negligible; this is ok if frequencies are such that wavelength λ large compared to dimensions of apparatus L . $\lambda \gg L$ or $\frac{c}{\nu} \gg L$.
I will write down the "vector calculus" formulation of electrodynamics, along side Maxwell's equations, or electrodynamics, over spacetime manifold M . The latter formulation should specialize to the "vector calculus" formulation.
From

$$\text{curl}\mathbf{E} = -\frac{d\mathbf{B}}{dt} (SI) \quad \text{curl}\mathbf{E} = -\frac{1}{c} \frac{\partial \mathbf{B}}{\partial t} (cgs) \text{ or } \frac{\partial B}{\partial t} + \mathbf{d}E = 0$$

Suppose $B = \text{curl}A$ or $B = \mathbf{d}A$ (EY 20170528: is this where the assumption above about $\lambda \gg L$ comes in?), then

$$-\frac{\partial B}{\partial t} = \mathbf{d}E \xrightarrow{f_S} \int_S \mathbf{d}E = \int_{\partial S} E = - \int_S \frac{\partial B}{\partial t} \xrightarrow{B=\mathbf{d}A} - \int_S \frac{\partial}{\partial t} \mathbf{d}A \xrightarrow{\text{flat space}} \int_S \mathbf{d}E = - \int_S \mathbf{d} \frac{\partial A}{\partial t}$$

and so

$$(1) \quad \mathbf{E} = \frac{-\partial \mathbf{A}}{\partial t}$$

up to gauge transformation, if $B = \mathbf{d}\mathbf{A} = \text{curl}\mathbf{A}$

Since this \mathbf{E} field is formed in a conductor, Ohm's law applies. Let's review Ohm's law. Smythe (1968) refers to its 6.02 Ohm's Law - Resistivity section [2]. Indeed, in a lab, the definition of resistance can be defined as this ratio:

$$(2) \quad R_{AB} := \frac{-\int_A^B \mathbf{E}}{I_{AB}} = \frac{V_A - V_B}{I_{AB}} = \frac{\varepsilon_{AB}}{I_{AB}}$$

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Moving along, the right way to think about resistivity ρ is to consider conductivity.
Assume current density is linear to \mathbf{E} field (as \mathbf{E} field pushes charges along). This linear response is reasonable.
Also, assume current density \mathbf{J} is uniform over infinitesimal surface area dA (i.e. surface S).
Define

$$(3) \quad \sigma \equiv \text{conductivity}$$

Then the empirical relation/equation that underpins *Ohm's law* is

$$(4) \quad \mathbf{J} = \sigma \mathbf{E}$$

and define *resistivity* from there:

$$(5) \quad \sigma := \frac{1}{\rho}$$

where ρ is the *resistivity*.
Thus

$$\sigma \int_A^B -\mathbf{E} = \sigma V_{AB} = \int_A^B \mathbf{J} = I_{AB} \frac{l}{A}$$
$$\frac{1}{\rho} R = \frac{l}{A} \text{ or } \boxed{R = \rho \frac{l}{A}}$$

From Maxwell's Equations,

$$(6) \quad \delta(B - 4\pi \mathbf{M}) = \frac{4\pi}{c} J_{\text{free}}$$

If $B = H + 4\pi M = (1 + 4\pi\chi_m)H = \mu H$, then

$$(7) \quad \delta H = \delta \frac{B}{\mu} = \frac{4\pi}{c} J_{\text{free}} \text{ or } \delta B = \mu \frac{4\pi}{c} J_{\text{free}} \iff \text{curl}B = \mu J_{\text{free}} \quad (SI)$$

and if $B = \mathbf{d}A$ and $\mathbf{d}\delta A = 0$.

I build upon the physical setup proposed by Jackson (1998) [3] in Section 5.18 "Quasi-Static Magnetic Fields in Conductors; Eddy Currents; Magnetic Diffusion."

For a system (with characteristic) length L , L being small, compared to electromagnetic wavelength associated with dominant time scale of problem T ,

$$f := \frac{1}{T}; \quad \omega = 2\pi f; \quad \omega\lambda = c \implies \lambda = \frac{c}{\omega} = \frac{c}{2\pi f} = \frac{Tc}{2\pi}$$

$$\frac{L}{\lambda} = \frac{LTc}{2\pi} \gg 1$$

From Maxwell's equations, in particular, Faraday's Law, and in its integral form (over 2-dim. *closed* surface S),

$$(8) \quad \mathbf{d}E + \frac{\partial}{\partial t}B = 0 \text{ or } -\mathbf{d}E = \frac{\partial B}{\partial t} \xrightarrow{f_S} \int_S \frac{\partial B}{\partial t} = - \int_S \mathbf{d}E = - \int_{\partial S} E$$

So on S , changing magnetic flux $\int \frac{\partial B}{\partial t}$ results in E field, circulating around boundary of S , ∂S .

We know that in a conductor, free conducting electrons get pushed around by E fields, result in a current density J . J is related to E , *empirically* (by Ohm's Law)

$$J = \sigma E$$

where σ is the resistivity.

Then use the force law on this induced current J from the B field set up:

$$F_{\text{net}} = \frac{1}{c} \int_S J \times B dA$$

By working through the right-hand rule, F_{net} the force on those currents induced in the conductor due to the B that's there, is in the direction to help oppose changing (increasing or decreasing $\frac{\partial B}{\partial t}$).

To find B , suppose $B = dA$, i.e. $B \in H_{\text{deRham}}^2(M)$, i.e. $B = \text{curl}A$.

For sure,

$$\delta(B - 4\pi c\mathbf{M}) = 4\pi J \iff \text{curl}(B - 4\pi c\mathbf{M}) = \text{curl}H = 4\pi J$$

Be warned now that the relation $B = \mu H$ may not be valid on all domains of interest; μ could even be a tensor! (e.g. $B_{ij} = \mu_{ij}^{kl} H_{kl}$). However, both Jackson (1998) [3] in Sec. 5.18 Quasi-Static Magnetic Fields in Conductors; Eddy Currents; Magnetic Diffusion, pp. 219, and Smythe (1968), Ch. X (his Ch. 10), pp. 368 [2], continues on *as if* this relation is linear: $B = \mu H$.

Nevertheless, as we want to find B by finding its "vector potential" A , we obtain a diffusion equation:

$$(9) \quad \begin{aligned} -\delta B &= *\mathbf{d} * \mathbf{d}A = (-1)\delta\mathbf{d}A = (-1)(\Delta - \mathbf{d}\delta)A \xrightarrow{\mathbf{d}\delta A=0} -\Delta A = \\ &= 4\pi\mu J = 4\pi\mu\sigma E = 4\pi\mu\sigma \left(-\frac{\partial A}{\partial t} \right) \\ &\implies \boxed{\Delta A = 4\pi\mu\sigma \frac{\partial A}{\partial t}} \end{aligned}$$

where in the first 2 steps (equalities), $-\delta B = *\mathbf{d} * \mathbf{d}A = (-1)\delta\mathbf{d}A$ it's interesting to note that the codifferential δ for the 2 form B had to be written out explicitly, and then the codifferential for the 1-form A is *different* from the δ for B by a(n important) factor of (-1) ; where $\mathbf{d}\delta A = 0$ must be satisfied by the form A takes; and where, since $B = \mathbf{d}A$,

$$(10) \quad \mathbf{d}E + \frac{\partial B}{\partial t} = \mathbf{d}E + \frac{\partial}{\partial t}\mathbf{d}A = \mathbf{d} \left(E + \frac{\partial A}{\partial t} \right) = 0 \implies E = -\frac{\partial A}{\partial t} + \text{grad}\Phi \xrightarrow{\Phi = \text{constant}} E = -\frac{\partial A}{\partial t}$$

whereas a choice of gauge for E was chosen so that $\Phi = \text{constant}$ (and so a particular form for E was chosen, amongst those in the *same* equivalence class of $H_{\text{deRham}}^1(M)$).

To ensure that the differential geometry formulation is in agreement with the practical vector calculus formulation, compare Eq. 9 with Eq. (5.160) of Jackson (1998) [3] and Eq. (10) in Sec. 10.00 of Smythe (1968) [2].

To summarize what's going on, I think one should at least understand in one's head how Maxwell's Equations apply, (and I will try to write in SI here)

$$(11) \quad \boxed{\begin{aligned} \int_S \frac{\partial \mathbf{B}}{\partial t} dA &= - \oint \mathbf{E} \cdot d\mathbf{s} \implies \mathbf{J} = \sigma \mathbf{E} \implies \mathbf{F}_{\text{net}} = \int_S \mathbf{J} \times \mathbf{B} dA \\ \text{find } \mathbf{B} &=? \quad \text{using form } \mathbf{B} = \nabla \times \mathbf{A}, \\ \nabla^2 \mathbf{A} &= \mu\sigma \frac{\partial \mathbf{A}}{\partial t} \quad (SI) \end{aligned}}$$

where, a change in magnetic flux over a surface S over the conductor, $\int_S \frac{\partial \mathbf{B}}{\partial t} dA$ induces a circulation of E field around S , $-\oint \mathbf{E} \cdot d\mathbf{s}$, and this E field is pushing around *free conducting charges* according to Ohm's law, $\mathbf{J} = \sigma \mathbf{E}$, with σ being the conductivity of the conducting material, and this current density \mathbf{J} is then acted upon by the prevailing B field, according to the usual force law. To find \mathbf{B} , one can find \mathbf{A} and *try* to find \mathbf{A} analytically.

Keep in mind that for $\nabla^2 \mathbf{A} = \mu\sigma \frac{\partial \mathbf{A}}{\partial t}$, we had used, critically, the Maxwell equation $\nabla \times \mathbf{H} = \mathbf{J}$, with \mathbf{J} being the *induced current of free conducting charges on the conductor*. This \mathbf{H} will contribute (through linear superposition) to the \mathbf{B} that could already be there due to the permanent magnet.

What can we measure quantitatively?

- Can we measure \mathbf{J} inside (on) the conductor?
- Can we separate magnetization \mathbf{M} of material from \mathbf{B} , to obtain the actual \mathbf{B} (and then use linear superposition, $\mathbf{B}_{\text{total}} = \mathbf{B}_{\text{permanent magnet}} + \mathbf{B}_{\text{induced currents}}$?)

Also, keep in mind the context that the conductor at hand is the long, almost semi-infinite rectangle of a conductor, aluminum sub-rail, specified by the SpaceX Hyperloop. Force on that will cause an equal and opposite force on the pod, with its permanent magnets attached, and thus braking the pod.

REFERENCES

[1] Scott B. Hughes. **Magnetic braking: Finding the effective length over which the eddy currents form.** [Magnetic braking: Finding the effective length over which the eddy currents form](#)

[2] William R. Smythe, **Static and Dynamic Electricity**. 3rd ed. (McGraw-Hill, New York, 1968).

[3] J.D. Jackson. **Classical Electrodynamics** Third Edition. Wiley. 1998. ISBN-13: 978-0471309321