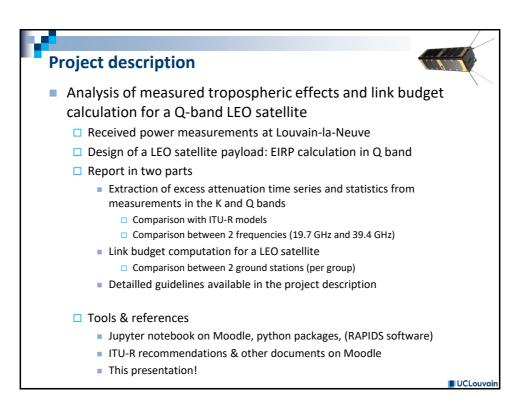
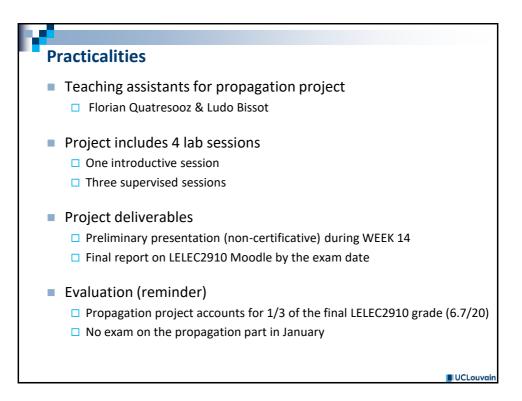
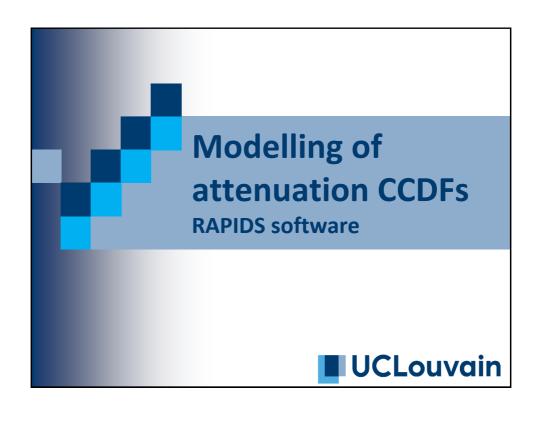


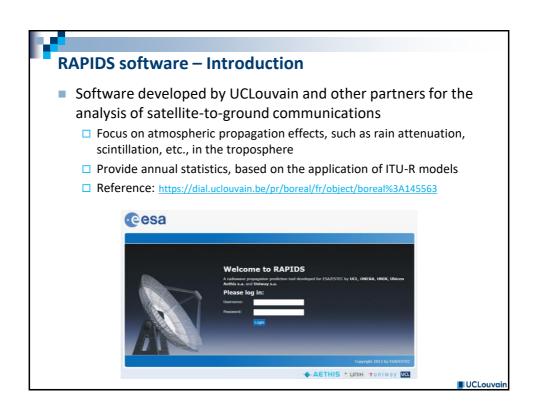
Context From received power time series, obtain statistics and develop models for various attenuation components Using Complementary Cumulative Distribution Functions (CCDF) of total attenuation and various components PREDICTION OF ATMOSPHERIC EFFECTS - BERGEN PREDICTION OF ATMOSPHERIC EFFECTS - BERGEN OUTAGE TIME (%)

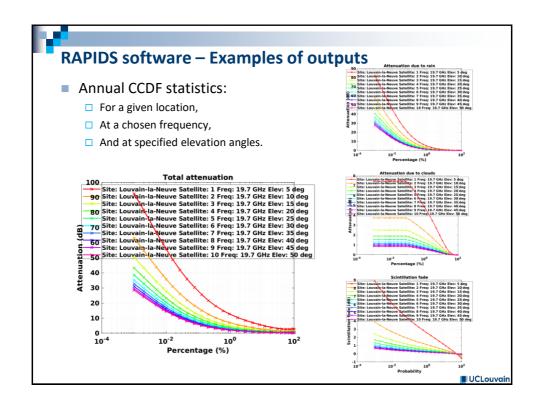


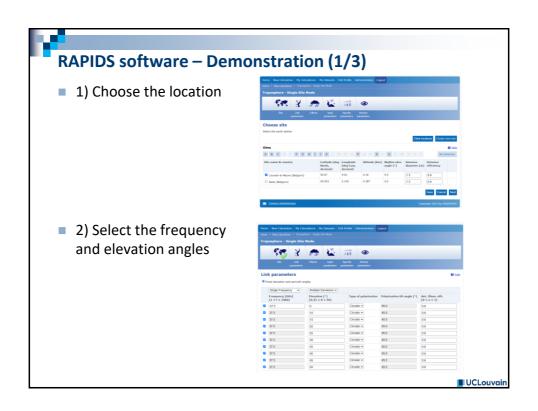
Content and organisation				
November	Mon 11	3-4	Armistice	
			Atmospheric Propagation and Satellite Systems: Introduction	
	Thu 14	7-8	Gaseous Absorption	
	Mon 18	3-4	Extinction and Depolarization by Hydrometeors	
	Thu 21	7-8	Project: introduction and organization	
	Mon 25	3-4	Transport Theory and Tropospheric Radiometry	
	Thu 28	7-8	Project: supervized session	
December	Mon 2	3-4	Tropospheric Scintillation, Refraction and Multipaths	
	Thu 5	7-8	Project: supervized session	
	Mon 9	3-4	Ionospheric Propagation – Remote Sensing, SatCom and GNSS	
	Thu 12	7-8	Project: supervized session	
	Mon 16	3-4	Project: preliminary presentation	
	Thu 19	7-8	Project: preliminary presentation	

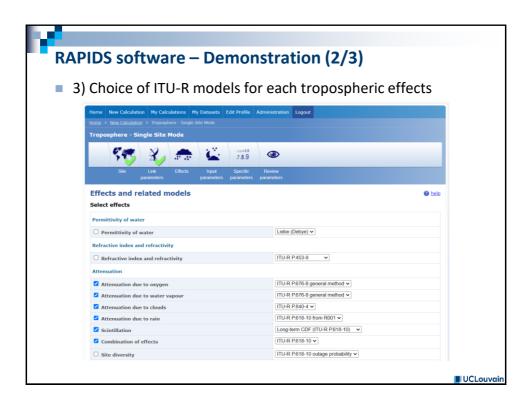


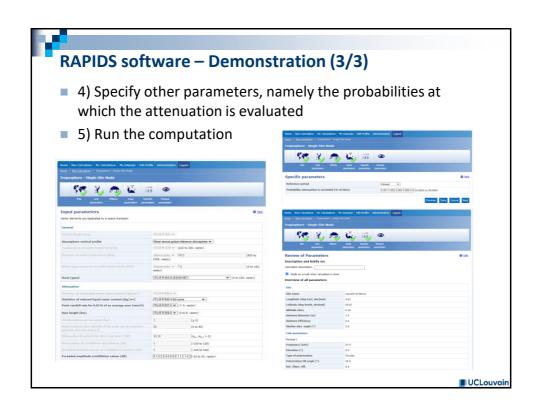






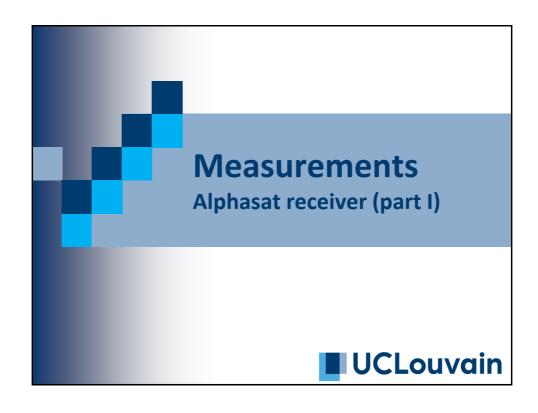






RAPIDS software – Summary

- This year: no need for you to run RAPIDS computations, as the outputs will be directly given to you
 - ☐ For all groups: access to attenuation statistics at LLN, for elevation angles between 5° and 90°, and at
 - 19.7 GHz
 - 39.4 GHz
 - 37.5 GHz
 - □ Per group, individually: access to attenuation statistics at another station, for elevation angles between 5° and 90°, and at
 - 37.5 GHz
- All data will be accessible on Moodle, after you have registered in a group



Motivations

- Goal: evaluate and predict propagation effects on space systems
- Available tools:
 - ☐ Beacon receiver → accurate but costly, need long-term measurements
 - □ Radiometer → useful to measure gaseous attenuation
 - □ Ground meteorological instruments → only provides meteorological quantities at the ground
 - □ Radiosondes → access to vertical profiles of meteorological quantities
 - ...





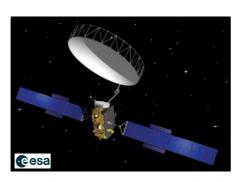




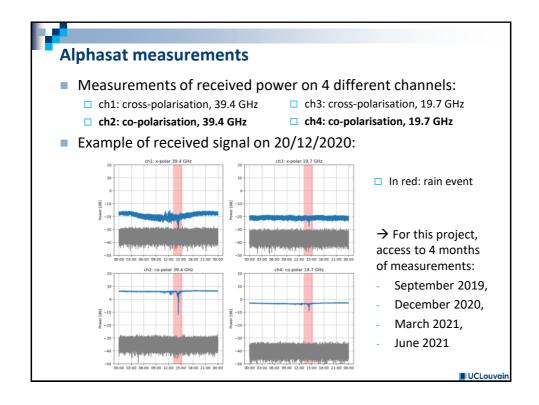
■ UCLouvair

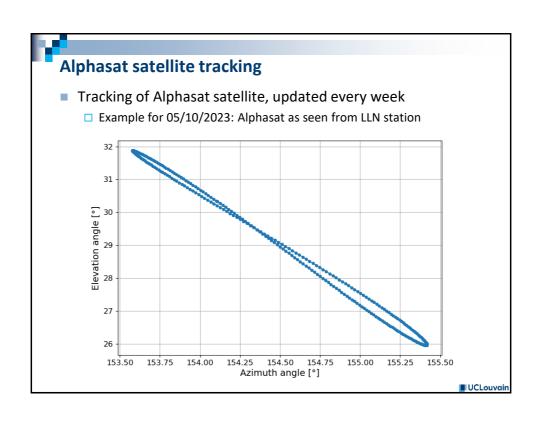
Alphasat

- Alphasat is a geostationary communication satellite, launched in 2013
 - □ It is also equipped with beacons emitting at 19.7 GHz and 39.4 GHz
 - ☐ Since 2017, UCLouvain has a receiver on the roof of the Maxwell building

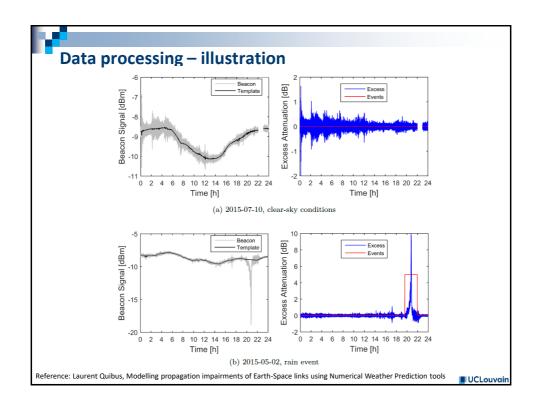








Data processing ■ The absolute 0dB attenuation level is not directly available ☐ Receiver non-idealities (gain variations, pointing inaccuracies, temperature effects) ☐ Gaseous attenuation unknown in the absence of radiometer → Not possible to extract the total attenuation Instead, extract the excess attenuation □ Corresponds to the attenuation due to rain and scintillation -50 □ Requires the use of a template to recover the OdB level -60 ☐ Requires the detection of rain -65 events (here, by inspection) time [s] ■ UCLouvair

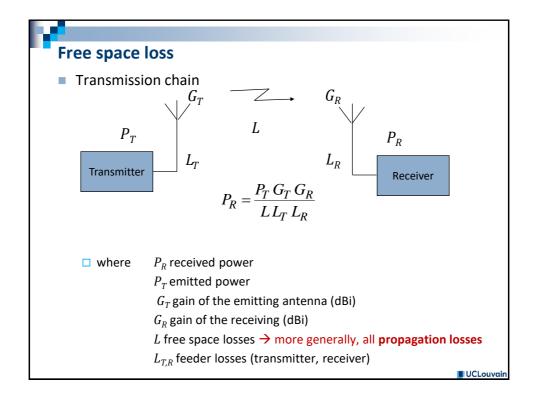


Data processing – step by step

- 0) Load Alphasat measurements (received beacon signal), P_r
- 1) Add rain event detections
- 2) Evaluate the template level P_{temp}, either by low-pass filtering with FFT (keeping a given number of harmonics) or using polynomial fits. Rain events should not be used for the template definition, e.g., by replacing them with linear interpolation between the start and the end of the rain event.
 - → There is no unique solution, justify your choices!
- \blacksquare 3) Extract the excess attenuation, defined as $A_{\rm exc} = P_{\rm temp} P_r$
- 4) Compute relevant statistics, compare with the models, explain, discuss, ...

→ Steps 0 and 1 already completed, can be found in the Jupyter notebook **project_part_!.ipynb**





Free space loss

Effective isotropic radiated power (EIRP)

$$EIRP = \frac{P_T G_T}{L_T} = P_{TI}$$

■ Effective isotropic received power

$$P_{RI} = \frac{P_R L_R}{G_R}$$

Free space losses

$$L_{dB} = 10 \log \left(\frac{P_{TI}}{P_{RI}} \right)$$

Free space loss

Example: identical EIRP produced by two different systems



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Free space loss: from Tx to Rx

Assuming two antennas with matched polarizations, the power density arriving at the receiving antenna is (taking L_T = 1)

$$S = \frac{P_T G_T}{4\pi r^2} \quad (W/m^2)$$

■ Power received by Rx antenna (taking L_R = 1)

$$P_R = \frac{P_T G_T A_{eR}}{4\pi r^2} \quad (W)$$

 $\hfill\Box$ where $A_{\it eR}$ is the effective area of the receiving antenna

$$G_R = \frac{4\pi}{\lambda^2} A_{eR}$$



Free space loss: receive antenna

■ Effective antenna area = surface multiplied by the efficiency

$$A_{eR} = \eta \left(\frac{\pi D^2}{4} \right)$$

- where η is the efficiency (typically 0.55 for a parabolic antenna and 0.75 for a horn) and D is the antenna diameter
- For a directive antenna, the gain and the received power depend on the direction $(\theta, \varphi) \rightarrow$ directivity

$$D(\vartheta,\varphi) = \frac{P(\vartheta,\varphi)}{P_t/4\pi}$$

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Free space loss vs. frequency

$$P_R = \frac{P_T G_T A_{eR}}{4\pi r^2}$$

$$P_R = \frac{P_T A_{eT} A_{eR}}{\lambda^2 r^2}$$

$$P_R = \frac{P_T A_{eT} G_R}{4\pi r^2}$$

$$P_R = \frac{P_T G_T G_R \lambda^2}{\left(4\pi r\right)^2}$$

- \blacksquare Assuming that the diameters of the antennas are fixed, A_{eT} and A_{eR} are the fixed variables
 - □ In that case, the second equation is used → the power increases as the square of frequency

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Free space loss

Path-loss

$$L = \left(\frac{P_{TI}}{P_{RI}}\right) = \frac{P_T G_T}{\left(\frac{P_R}{G_R}\right)} = \frac{P_T G_T G_R}{P_R}$$

$$P_R = \frac{EIRP G_R \lambda^2}{(4\pi r)^2} = \frac{EIRP G_R}{L}$$

$$L = \left(\frac{4\pi r}{\lambda}\right)^2$$

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Link budget

- System design
 - ☐ For performance evaluation the signal-to-noise ratio (SNR) is one of the most important metric

$$SNR = \frac{P_R}{N} = \frac{EIRP G_R}{NL}$$

- Evaluation of signal level
 - Should account for all system gain/loss (antennas, amplifiers, cables, etc.)
 - Should include tropospheric degradations
 - EIRP is the design target parameter
- Evaluation of noise power
 - Thermal noise (AWGN)

$$N = kTB \quad (W)$$



$$\frac{P_R}{N} = \frac{EIRP G_R}{BN_0 L} = \frac{EIRP G_R/T}{BkL_{TOT}}$$

$$\frac{P_R}{N_0} = \frac{EIRP G_R/T}{kL_{TOT}}$$



Link budget: reminder about noise

Thermal noise

$$N = kTB$$
 (W)

- Noise figure and temperature
 - ☐ Measures the SNR degradation by a quadripole

$$F = \frac{(S/N)_{1}}{(S/N)_{2}}$$

$$F - 1 = \frac{T}{T_{0}} ; \quad T = T_{0}(F - 1)$$

Cascaded quadripoles

$$F_{12} = F_1 + \frac{F_2 - 1}{G_1}$$

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Link budget: SNR margin and service availability

 A security margin is generally added at link level in order to enable some degradation to occur before the link cuts off

$$\frac{P_R}{N_0} = M \left(\frac{P_R}{N_0}\right)_{req}$$

$$M(dB) = \left(\frac{P_R}{N_0}\right) - \left(\frac{P_R}{N_0}\right)_{req}$$

$$M = \frac{EIRP G_R/T}{(P_R/N_0)_{req} kL_{TOT}}$$

- Tropospheric degradations are random
 - □ Need to define the service availability to estimate the attenuation

Ty nower	20	dBW
Tx power Tx circuit loss	20	dBvv dB
Antenna gain	51.6	
EIRP (P_TG_T)	69.6	dBW
Free space loss	202.7	dB
Tropospheric loss (depending on availability)	4	dB
Micellaneous loss	6	dB
Received isotropic power	-143.1	dBW
Rx antenna gain	35.1	dB
Misalignment loss (antenna lobe)	2	dB
Received power P_R	-110	dBW
Rx noise factor F	11.5	dB
Rx noise temperature = 3806 K	35.8	dBK
Antenna temp. (sky noise) = 300K	24.8	dBK
System noise temp. = 4106K	36.1	dBK
Rx sensitivity G/T	-1	dB/K
$N_0 = kT$	-192.5	
$SNR = P_R/N_0$	82.5	dB (Hz)

W

From GEO to LEO attenuation statistics

- 0) Load GEO statistics from RAPIDS simulations (at the location of interest and the chosen frequency)
- 1) Choice of a LEO satellite and computation of its trajectory
- **2**) Determination of the probability occurrence of the LEO satellite at an elevation angle θ , denoted $p(\theta)$
- 3) Conversion of GEO to LEO statistics using a conditional probability

$$p(A > A_0) = \sum_{\theta} p(A > A_0 | \theta) \ p(\theta),$$

where $p(A > A_0 | \theta)$ is the probability of exceeded attenuation for an elevation angle θ .

4) Link budget computation

→ Step 0 already completed, can be found in the Jupyter notebook **project_part_II.ipynb**