

# Maximizing Power Coefficient Output of a Vertical Wind Turbine

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# Agenda



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# Introduction



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- Wind turbine are responsible for:
  - Roughly 5% of the worlds power
  - 8 % of United States power
- Over the past ten years, the Americas' wind energy capacity has tripled
- Goal of a wind turbine is to produce the largest amount of electrical energy possible by extracting as much energy as it can from the wind
- Efficiency is measured by the power coefficient ( $C_p$ )
- The higher  $C_p$  the better energy output
- Average range of  $C_p$  for a 1 m diameter blade is from 0.35 to 0.45.



- Maximize a wind turbine power coefficient ( $C_p$ ) by changing blade geometric parameters (Outside Radius of the Blade, Tip Speed Ratio, Root Chord, Tip Chord, Root Alpha, Tip Alpha, Aerofoil) while satisfying the given constraints.

$$J_1 = \max(C_p)$$

$$\text{Maximize } J(x,p)$$

$$\text{Subject to } g(x,p) \leq 0$$

$$x_{i, LB} \leq x_i \leq x_{i, UB} \quad (i = 1, \dots, 6)$$

# Design Variables



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- The blade profile was kept constant which was the S822 blade
- Additional Design Variables

$x_1$  = Turbine radius ( $R$ )

$x_2$  = Tip chord length ( $tipchord$ )

$x_3$  = Root chord length ( $rootChord$ )

$x_4$  = Desired root angle of attack ( $rootAlpha$ )

$x_5$  = Desired tip angle of attack ( $tipAlpha$ )

$x_6$  = ( $tipSpeedRatio$ )

$x_7$  = Blade profile data (S822)

$$\begin{bmatrix} x_1 \\ x_2 \\ x_3 \\ x_4 \\ x_5 \\ x_6 \end{bmatrix} = \begin{bmatrix} R \\ Tipchord \\ rootChord \\ rootAlpha \\ tipAlpha \\ tipSpeedRatio \end{bmatrix}$$

Design Vector

# Parameters



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## Design Constants:

- Wind speed ;  $p_1 = 3 \text{ m/s}$
- Number of Blades;  $p_2 = 3$
- Inside radius of the blade aka (hubRadius);  $p_3 = 0.12 \text{ m}$
- Number of elements along the blade length (elementsPerBlade);  $p_4 = 30$

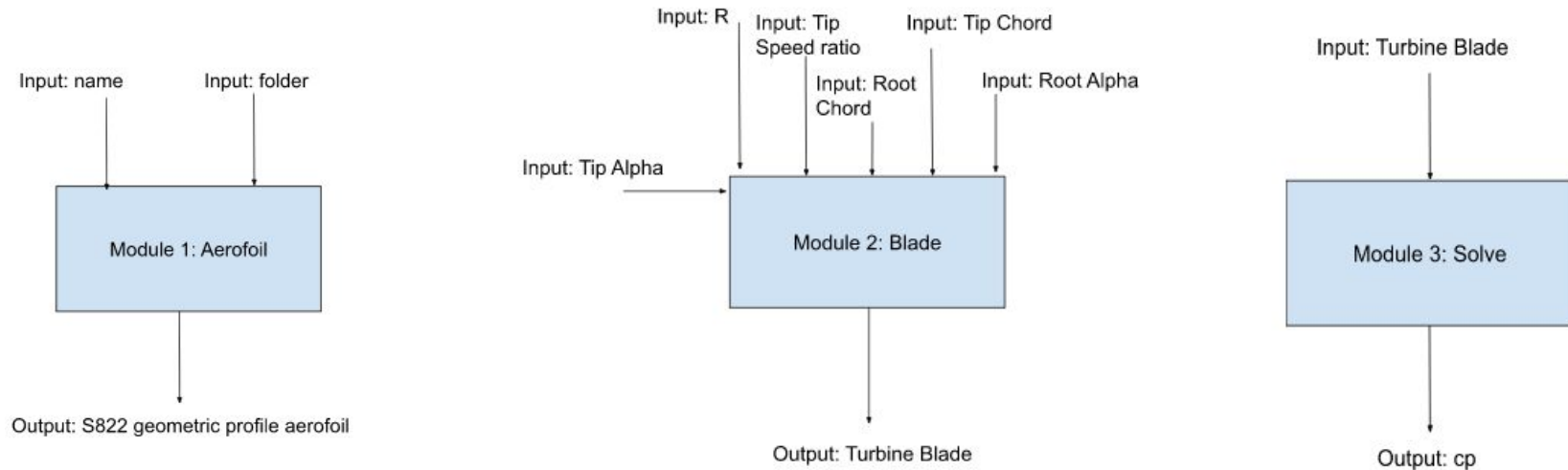
## Physical constants:

- Density of air at  $20^\circ \text{C}$ , 1 bar;  $p_5 = 1.225 \text{ (kg/m}^3\text{)}$
- Dynamic viscosity of air at  $20^\circ \text{C}$ , 1 bar;  $p_6 = 1.82053 \cdot 10^{-5} \text{ Pa}\cdot\text{s}$

# Module Identification



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**Module 1: AEROFOIL** Represents aerofoil profile. **Loads data, lift/drag coefficient lookup & blade geometry. Creates a new aerofoil** with the given name and reads the relevant data from the given folder directory.

**Module 2: BLADE** takes care of the wind turbine blade design. It **acquires all variables necessary** to define the blade geometry and **creates a new turbine blade with the given parameters.**

**Module 3: SOLVE** Solves all **elements** of this blade design for pitch angle. **Calculates the resulting output power coefficient.**

# Equations



$$\text{local speed ratio} = \frac{(\text{tip speed ratio})(r)}{R_o}$$

$$\text{local Blade Solidity} = \frac{(\text{numBlades})(\text{chord})}{2\pi r}$$

$$\text{inflow angle} = \arctan\left(\frac{1 - axInd}{\text{local SpeedRatio}(1 + angInd)}\right)$$

$$V_{rel} = \frac{\text{windspeed}(1 - axInd)}{\sin(\text{inFlowAngle})}$$

$$Re = \frac{(\rho V_{rel})(\text{chord})}{\mu}$$

$$C_x = C_L \cos(\text{inflowAngle}) + C_D \sin(\text{inflowAngle})$$

$$C_\theta = C_L \sin(\text{inflowAngle}) + C_D \cos(\text{inflowAngle})$$

$$axInd = \frac{1}{\frac{4\sin(\text{inflowAngle})^2}{C_x(\text{localBladeSolidity})} + 1}$$

$$angInd = \frac{1}{\frac{4\sin(\text{inflowAngle}) \cos(\text{inflowAngle})}{C_\theta(\text{localBladeSolidity})} - 1}$$

$$\text{pitch} = \text{inflowAngle} - \alpha$$

$$F_\theta = 0.5\rho V_{rel}^2(\text{chord})(r)(C_\theta)$$

$$T = \int F_\theta dr \rightarrow \text{Total torque on blade}$$

$$C_p = \frac{P_{blade}}{P_{wind}} = \frac{(\text{rotation speed})(T)(\# \text{ of blades})}{\frac{1}{2}\rho V_{wind}^3 * \text{Area}}$$



# N-2 Diagram



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In	name, folder	tipAlpha, R , tipSpeedRatio, rootChord, tipchord, rootAlpha		
	<b>Aerofoil</b>	S822 geometric profile aerofoil		
		<b>Blade</b>	Turbine Blade	
			<b>Solve</b>	Cp
				<b>Out</b>

# Feasibility



Our **algorithm** is a **very realistic** one and therefore presents **upper and lower bounds** for every single design variable.

- Turbine radius (R):  $0.3 \leq x_1 \leq 1$  [m]
- Tip chord length (tipchord):  $0.2 \leq x_2 \leq 0.5$  [m]
- Root chord length (rootChord):  $0.2 \leq x_3 \leq 1$  [m]
- Desired root angle of attack (rootAlpha):  $0 \leq x_4 \leq 12$  degrees
- Desired tip angle of attack (tipAlpha):  $5 \leq x_5 \leq 10$  degrees
- (tipSpeedRatio) :  $1 \leq x_6 \leq 10$

Turbine radius (R)	Tip chord length (tipchord)	Root chord length (rootChord)	Desired root angle of attack (rootAlpha)	Desired tip angle of attack (tipAlpha)	(tipSpeedRatio)	Observation (Coefficient of Power)
0.475	0.2	0.8	0.017453293	0.087266463	2	0.353229322

**The simulation returned a coefficient of power of 0.35229.** This is a very positive sign that our algorithm works and that we are getting a realistic output. The average wind turbine falls in the **35-45% range**

# Design of Experiments



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**One-at-a-Time**

Levels (l) = 5

Factors (n) = 6

# Experiments =  $1 + n(l-1) \rightarrow$   
25 experiments

Experiment #	Turbine radius (R)	Tip chord length (tipchord)	Root chord length (rootChord)	Desired root angle of attack (rootAlpha)	Desired tip angle of attack (tipAlpha)	(tipSpeedRatio)	Observation (Coefficient of Power)
1	0.3	0.2	0.2	0.017453293	0.087266463	2	0.038392307
2	0.475	0.2	0.2	0.017453293	0.087266463	2	0.044529733
3	0.65	0.2	0.2	0.017453293	0.087266463	2	0.039306392
4	0.825	0.2	0.2	0.017453293	0.087266463	2	0.035335239
5	1	0.2	0.2	0.017453293	0.087266463	2	0.031430548
6	0.475	0.275	0.2	0.017453293	0.087266463	2	0.143633189
7	0.475	0.35	0.2	0.017453293	0.087266463	2	0
8	0.475	0.425	0.2	0.017453293	0.087266463	2	0
9	0.475	0.5	0.2	0.017453293	0.087266463	2	0
10	0.475	0.2	0.4	0.017453293	0.087266463	2	0.19465744
11	0.475	0.2	0.6	0.017453293	0.087266463	2	0.274269051
12	0.475	0.2	0.8	0.017453293	0.087266463	2	0.353229322
13	0.475	0.2	1	0.017453293	0.087266463	2	0.410049907
14	0.475	0.2	0.2	0.034906585	0.087266463	2	0.075347948
15	0.475	0.2	0.2	0.052359878	0.087266463	2	0.106064441
16	0.475	0.2	1	0.06981317	0.087266463	2	0
17	0.475	0.2	1	0.087266463	0.087266463	2	0
18	0.475	0.2	1	0.017453293	0.109083078	2	0
19	0.475	0.2	1	0.017453293	0.130899694	2	0
20	0.475	0.2	1	0.017453293	0.15271631	2	0
21	0.475	0.2	1	0.017453293	0.174532925	2	0
22	0.475	0.2	1	0.017453293	0.087266463	4	0
23	0.475	0.2	1	0.017453293	0.087266463	6	0
24	0.475	0.2	1	0.017453293	0.087266463	8	0
25	0.475	0.2	1	0.017453293	0.087266463	10	0

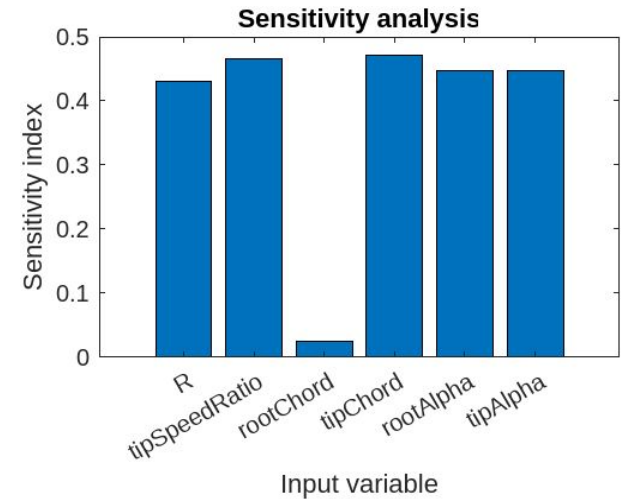
Experiment #	Turbine radius (R)	Tip chord length (tipchord)	Root chord length (rootChord)	Desired root angle of attack (rootAlpha)	Desired tip angle of attack (tipAlpha)	(tipSpeedRatio)	Observation (Coefficient of Power)
13	0.475	0.2	1	0.017453293	0.087266463	2	0.410049907

# Sensitivity Analysis



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Design Variable	Sensitivity Index	Importance
Turbine Radius ( R )	0.4313	More important than Root Chord Length, but less important than other variables
Tip Speed Ratio	0.4660	Important
Root Chord Length	0.0244	Least important
Tip Chord Length	0.4717	Most Important
Root angle of attack	0.4481	Equally Important
Tip angle of attack	0.4481	



# Multi-start SQP



- 10 random design vectors
  - Used as initial guesses for the SQP optimizer.
- Converges at the locally maximum  $C_p$
- SQP was implemented using the 'fmincon' function in Matlab
- Results:
  - All initial design vector inputs converged to the same  $C_p = 0.4809$
- Note
  - First order optimality value from 'fmincon' function were non-zero & in the order of  $10^{-4}$
  - Most likely due to non-smoothness of the objective function
  - We are not absolute certainty that the design vector is a global minimum

SQP Results

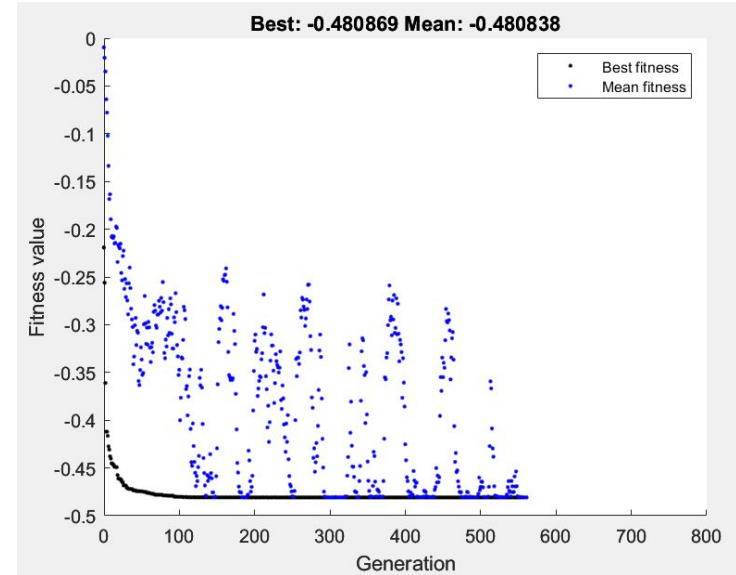
Iteration	$C_p$	Time [s]
1	0.4809	10.4
2	0.4809	4.2
3	0.4809	5.4
4	0.4809	8.2
5	0.4809	6.4
6	0.4809	6
7	0.4809	4.3
8	0.4809	4.4
9	0.4809	7.1
10	0.4809	5.6

# Genetic Algorithm



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- 10 trials of the GA using a population size of 50, with a maximum of 800 generations.
- The crossover rate = 0.5 (balance between retaining good design vectors across future generations while also diversifying the population enough to prevent any convergence to locally minimum objective)
- Results:
  - Approx. 0.4808
  - Average run time for GA is more than SQP
  - Hence, a costly approach



GA Convergence Plot (Population Size = 50;  
Crossover Fraction = 0.5; Runtime = 574 s)

# GA-SQP Hybrid



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- Utilized GA first, then SQP optimizer using result from GA.
- Both multi-start SQP and hybrid GA-SQP converged to the same design vector.
- GA-SQP validates Multi-Start SQP.
- Final design for single objective ( $C_p$ ):
  - $\mathbf{X}^* = [R, \text{tipChord}, \text{rootAlpha}, \text{tipAlpha}, \text{tipSpeedRatio}]^*$
  - = **[0.841, 0.086, 9, 9, 4.14]**

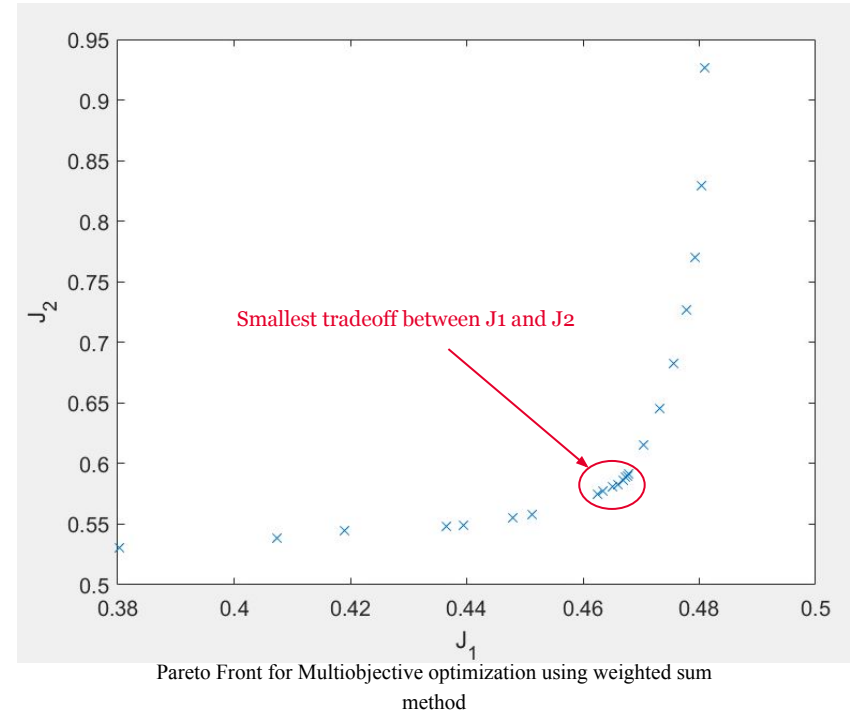
GA-SQP Results

Trial #	$C_p$ (1 <sup>st</sup> pass: GA)	$C_p$ (2 <sup>nd</sup> pass: SQP)
1	0.480858	0.4809
2	0.480843	0.4809
3	0.480839	0.4809
4	0.480869	0.4809
5	0.480854	0.4809

# Multiobjective Optimization



- $J_1 = C_p(X)$ 
  - $X = [R \text{ tipChord rootAlpha tipAlpha tipSpeedRatio}]$
- $J_2 = \text{tip chord length} + R$
- Goal is to maximize  $J_1$  while minimizing  $J_2$  subject to the inequality constraints  $g(X) \leq 0$ .
- $J_1$  and  $J_2$  are normalized appropriately:
  - $J_1^* = J_1 / (-0.4809)$
  - $J_2^* = J_2 / (2.2)$
- New objective function is created using the weighted sum method:
  - $J_3 = \lambda(J_1^*) + (1-\lambda)J_2^*$
  - $g(X) \leq 0$
  - $\lambda \in [0,1]$
- $J_1 \in [0.462, 0.468]$  and  $J_2 \in [0.575, 0.591]$  in the generated pareto front attains small increases in  $J_2$  for the higher  $J_1$





# Future Work



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- Finalize a post optimality analysis.
- Use a different blade profile.
- Maximize the Coefficient of Power ( $C_p$ ) for larger wind turbines.
- Scale blade radius and tip chord length in the multiobjective optimization, corresponding to how much material each dimension provides to the blade.

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- [2] Miller, Tom. “What Is the Future of Wind Energy?” Caltech Science Exchange, <https://scienceexchange.caltech.edu/topics/sustainability/wind-energy-advantages-disadvantages>.
  
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Thank you! Questions?