

**1. Problem 2.64 on Sedra & Smith 8<sup>th</sup> ed.**

Using the difference amplifier configuration of Fig. 2.16 and assuming an ideal op amp, design the circuit to provide the following differential gains. In each case, the differential input resistance should be  $10\text{ k}\Omega$ .

(a)  $1\text{ V/V}$  (b)  $5\text{ V/V}$  (c)  $10\text{ V/V}$  (d)  $25\text{ V/V}$

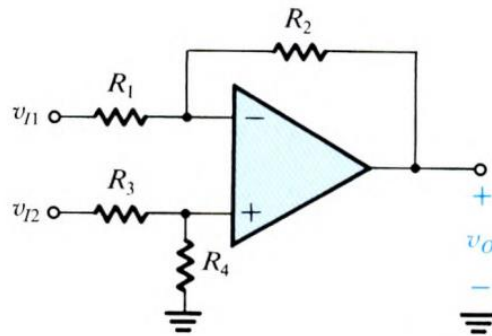


Figure 2.16

**2. Problem 2.65 on Sedra & Smith 8<sup>th</sup> ed.**

For the circuit shown in Fig. P2.65, express  $v_O$  as a function of  $v_1$  and  $v_2$ . What is the input resistance seen by  $v_1$  alone? By  $v_2$  alone? By a source connected between the two input terminals? By a source connected to both input terminals simultaneously?

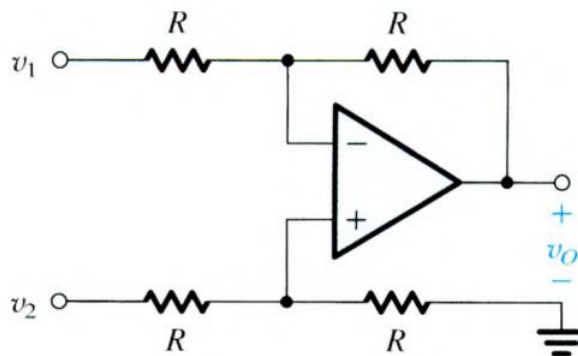


Figure P2.65

### 3. Problem 2.69 on Sedra & Smith 8<sup>th</sup> ed.

To obtain a high-gain, high-input-resistance difference amplifier, the circuit in Fig. P2.69 employs positive feedback, in addition to the negative feedback provided by the resistor  $R$  connected from the output to the negative input of the op amp. Specifically, a voltage divider ( $R_5$ ,  $R_6$ ) connected across the output feeds a fraction  $\beta$  of the output, that is, a voltage  $\beta v_O$ , back to the positive-input terminal of the op amp through a resistor  $R$ . Assume that  $R_5$  and  $R_6$  are much smaller than  $R$  so that the current through  $R$  is much lower than the current in the voltage divider, with the result that  $\beta \cong R_6/(R_5 + R_6)$ . Show that the differential gain is given by

$$A_d \equiv \frac{v_O}{v_{Id}} = \frac{1}{1 - \beta}$$

(Hint: Use superposition.)

Design the circuit to obtain a differential gain of 10 V/V and differential input resistance of 2 M $\Omega$ . Select values for  $R$ ,  $R_5$ , and  $R_6$ , such that  $(R_5 + R_6) \leq R/100$ .

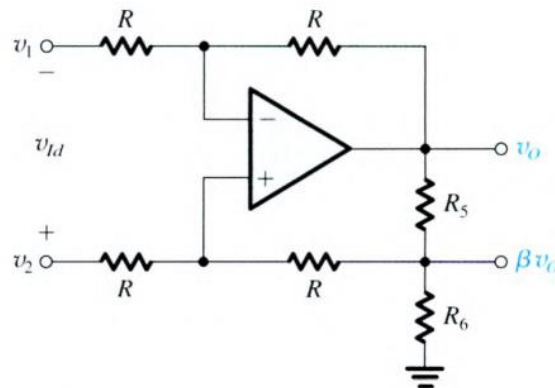


Figure P2.69

4. For a p-type silicon in which the dopant concentration  $N_A = 5 \times 10^{18}/\text{cm}^3$ , find the

hole and electron concentrations at  $T=300\text{K}$ . (Use the parameter given below)

$$n_i = BT^{3/2} e^{-E_g/2kT} \quad (3.2)$$

where  $B$  is a material-dependent parameter that is  $7.3 \times 10^{15} \text{ cm}^{-3} \text{ K}^{-3/2}$  for silicon;  $T$  is the temperature in  $K$ ;  $E_g$ , a parameter known as the **bandgap energy**, is 1.12 electron volt (eV) for silicon<sup>2</sup>; and  $k$  is Boltzmann's constant ( $8.62 \times 10^{-5} \text{ eV/K}$ ).

5. Assuming that the temperature dependence of  $I_s$  arises mostly because  $I_s$  is proportional to  $n_i^2$ , use the expression for  $n_i$  in Eq3.2 (given in problem 4.) to determine the factor by which  $n_i^2$  changes as T changes from 300K to 305K. This will be approximately the same factor by which  $I_s$  changes for a 5°C rise in temperature. What is the factor?
6. Calculate  $I_s$  and the current  $I$  for  $V = 750\text{mV}$  for a pn junction for which  $N_A = 10^{17}/\text{cm}^3$ ,  $N_D = 10^{16}/\text{cm}^3$ ,  $A = 100\mu\text{m}^2$ ,  $n_i = 1.5 \times 10^{10}/\text{cm}^3$ ,  $L_p = 5\mu\text{m}$ ,  $L_n = 10\mu\text{m}$ ,  $D_p = 10\text{cm}^2/\text{s}$ , and  $D_n = 18\text{cm}^2/\text{s}$ .

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