

Design of FIR Filters using Frequency Sampling method

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- Let $h(n)$ be the filter coefficients of an FIR filter and $H(k)$ is the DFT of $h(n)$. Then we have,

$$h(n) = \frac{1}{N} \sum_{k=0}^{N-1} H(k) e^{j2\pi kn/N} \quad ; \quad n = 0, 1, \dots, N-1 \quad \dots\dots\dots(1)$$

and

$$H(k) = \sum_{n=0}^{N-1} h(n) e^{-j2\pi kn/N} \quad ; \quad k = 0, 1, \dots, N-1 \quad \dots\dots\dots(2)$$

- The DFT samples $H(k)$ for an FIR sequence can be regarded as samples of the filter z - transform evaluated at N points equally spaced around the unit circle.

i.e.,
$$H(k) = H(z) \Big|_{z=e^{j2\pi k/N}} \dots\dots\dots(3)$$

- The transfer function $H(z)$ of an FIR filter with impulse response is given by,

$$H(z) = \sum_{n=0}^{N-1} h(n) z^{-n} \dots\dots\dots(4)$$

➤ Substituting (1) in (4) we get,

$$\begin{aligned} H(z) &= \sum_{n=0}^{N-1} \left[\frac{1}{N} \sum_{k=0}^{N-1} H(k) e^{j2\pi kn/N} \right] z^{-n} \\ &= \sum_{k=0}^{N-1} \frac{H(k)}{N} \sum_{n=0}^{N-1} \left(e^{j2\pi k/N} z^{-1} \right)^n \\ &= \sum_{k=0}^{N-1} \frac{H(k)}{N} \left(\frac{1 - \left(e^{j2\pi k/N} z^{-1} \right)^N}{1 - e^{j2\pi k/N} z^{-1}} \right) \\ &= \frac{1 - z^{-N}}{N} \sum_{k=0}^{N-1} \frac{H(k)}{1 - e^{j2\pi k/N} z^{-1}} \end{aligned} \dots\dots\dots(5)$$

➤ We know,

$$H(e^{j\omega}) \Big|_{\omega=\frac{2\pi k}{N}} = H(e^{j2\pi k / N}) = H(k) \quad \text{.....(6)}$$

i.e., $H(k)$ is the k^{th} DFT component obtained by sampling the frequency response $H(e^{j\omega})$.

Frequency response of FIR filter:

- The frequency response of the FIR filter can be obtained by setting $z=e^{j\omega}$ in (5), we get,

$$\begin{aligned} H(e^{j\omega}) &= \frac{1-e^{-j\omega N}}{N} \sum_{k=0}^{N-1} \frac{H(k)}{1-e^{j2\pi k/N} e^{-j\omega}} \\ &= \frac{e^{-j\omega N/2} (e^{j\omega N/2} - e^{-j\omega N/2})}{N} \sum_{k=0}^{N-1} \frac{H(k)}{1-e^{-j(\omega-2\pi k/N)}} \\ &= \frac{e^{-j\omega N/2}}{N} \sum_{k=0}^{N-1} \frac{H(k)(e^{j\omega N/2} - e^{-j\omega N/2})}{e^{-j(\omega-2\pi k/N)/2} (e^{j(\omega-2\pi k/N)/2} - e^{-j(\omega-2\pi k/N)/2})} \\ &= \frac{e^{-j\omega N/2}}{N} \sum_{k=0}^{N-1} \frac{H(k) \sin(\omega N/2)}{e^{-j\omega/2} e^{j\pi k/N} \sin((\omega/2) - \pi k/N)} \\ &= \frac{e^{-j\omega \frac{N-1}{2}}}{N} \sum_{k=0}^{N-1} \frac{H(k) e^{-j\pi k/N} \sin(\omega N/2)}{\sin((\omega/2) - \pi k/N)} \end{aligned}$$

$$\sin ce, \quad \sin\left(\frac{\omega N}{2} - k\pi\right) = (-1)^k \sin\left(\frac{\omega N}{2}\right)$$

$$H(e^{j\omega}) = \frac{e^{-j\omega\frac{N-1}{2}}}{N} \sum_{k=0}^{N-1} \frac{H(k)(-1)^k e^{-j\pi k/N} \sin N\left(\frac{\omega}{2} - \frac{\pi k}{N}\right)}{\sin\left(\frac{\omega}{2} - \frac{\pi k}{N}\right)} \dots\dots\dots(7)$$

Design:

- Based on the set of samples that we choose from the frequency response, there are two types of design.

Type 1 design:

- The frequency samples of the desired response $H_d(e^{j\omega})$ are determined using the relation,

$$H(k) = H_d(e^{j\omega}) \Big|_{\omega = \frac{2\pi}{N}k} ; k = 0, 1, \dots, N-1 \quad \dots\dots\dots(8)$$

- The frequency samples can be expressed in the form,

$$H(k) = |H(k)| e^{j\theta(k)} \quad \dots\dots\dots(9)$$

➤ For linear phase,

$$\theta(k) = \begin{cases} -\alpha\omega \Big|_{\omega=\frac{2\pi}{N}k} & ; \quad k = 0,1,\dots,N-1 \\ -\left(\frac{N-1}{2}\right)\frac{2\pi}{N}k & \dots\dots\dots(10) \\ -\left(\frac{N-1}{N}\right)\pi k & ; \quad k = 0,1,\dots,N-1 \end{cases}$$

➤ The filter coefficients $h(n)$ can be obtained by finding IDFT of $H(k)$, i.e.,

$$h(n) = \frac{1}{N} \sum_{k=0}^{N-1} H(k) e^{j2\pi kn/N} \quad ; \quad n = 0,1,\dots,N-1 \quad \dots\dots(11)$$

- If $h(n)$, the impulse response of the filter is to be a real valued signal, the frequency samples $H(k)$ must satisfy the symmetry requirement.

for N odd or even,

$$H(N-k) = H^*(k) \quad ; \quad k=0,1,\dots,N-1 \quad \dots\dots(12)$$

and also for N even, $H(N/2)=0$

- With the frequency response $H(k)$, the magnitude response is an even function,

$$|H(k)| = |H(N-k)| \quad k=0,1,\dots,N-1 \quad \dots\dots(13)$$

and the phase is an odd function

$$\theta(k) = -\theta(N-k) \quad k=0,1,\dots,N-1 \quad \dots\dots(14)$$

➤ Replacing k by $(N-k)$ in (10), we get

$$\begin{aligned}\theta(N-k) &= -\left(\frac{N-1}{N}\right)\pi(N-k) \\ &= -(N-1)\pi + \left(\frac{N-1}{N}\right)\pi k\end{aligned}$$

➤ To satisfy the requirements of (14), $\theta(k)$ for N odd is given by

$$\theta(k) = \begin{cases} -\left(\frac{N-1}{N}\right)\pi k & ; \quad k = 0, 1, \dots, \frac{N-1}{2} \\ (N-1)\pi - \left(\frac{N-1}{N}\right)\pi k & ; \quad k = \frac{N+1}{2}, \dots, N-1 \end{cases} \quad \dots\dots(15)$$

➤ Similarly for N even,

$$\theta(k) = \begin{cases} -\left(\frac{N-1}{N}\right)\pi k & ; \quad k = 0, 1, \dots, \frac{N}{2} - 1 \\ (N-1)\pi - \left(\frac{N-1}{N}\right)\pi k & ; \quad k = \frac{N}{2} + 1, \dots, N-1 \\ 0 & ; \quad k = \frac{N}{2} \end{cases} \dots (16)$$

➤ Substituting (15) in (9), we get for N odd,

$$H(k) = \begin{cases} |H(k)| e^{-j(N-1)\pi k / N} & ; \quad k = 0, 1, \dots, \frac{N-1}{2} \\ |H(k)| e^{j\left[(N-1)\pi - \left(\frac{N-1}{N}\right)\pi k\right]} & ; \quad k = \frac{N+1}{2}, \dots, N-1 \end{cases} \dots (17)$$

➤ Substituting (16) in (9), we get for N even,

$$H(k) = \begin{cases} |H(k)| e^{-j(N-1)\pi k / N} & ; \quad k = 0, 1, \dots, \frac{N}{2} - 1 \\ |H(k)| e^{j\left[(N-1)\pi - \left(\frac{N-1}{N}\right)\pi k\right]} & ; \quad k = \frac{N}{2} + 1, \dots, N - 1 \\ 0 & ; \quad k = \frac{N}{2} \end{cases} \quad \dots(18)$$

➤ If the filter is to be linear phase, then $h(n)$ must satisfy the symmetry condition,
 $h(n) = h(N-1-n)$ (19)

➤ Using this symmetry condition and symmetry condition of $H(k)$ the filter coefficients can be written as,

for N odd

$$h(n) = \frac{1}{N} \left\{ H(0) + 2 \sum_{k=1}^{\frac{N-1}{2}} \operatorname{Re} \left[H(k) e^{j2\pi kn/N} \right] \right\} \quad \dots(20)$$

for N even

$$h(n) = \frac{1}{N} \left\{ H(0) + 2 \sum_{k=1}^{\frac{N}{2}-1} \operatorname{Re} \left[H(k) e^{j2\pi kn/N} \right] \right\} \quad \dots(21)$$

The system function of the filter is given by,

$$H(z) = \sum_{n=0}^{N-1} h(n) z^{-n} \quad \dots(22)$$

Type 2 design

- The frequency samples of the desired response $H_d(e^{j\omega})$ are determined using the relation,

$$H(k) = H_d(e^{j\omega}) \Big|_{\omega = \frac{2\pi}{N} \left(k + \frac{1}{2}\right)} ; k = 0, 1, \dots, N-1 \quad \dots\dots(23)$$

- The filter coefficients $h(n)$ can be obtained by finding IDFT of $H(k)$, i.e.,

$$h(n) = \frac{1}{N} \sum_{k=0}^{N-1} H(k) e^{j2\pi kn/N} ; n = 0, 1, \dots, N-1 \quad (24)$$

- If $h(n)$, the impulse response of the filter is to be a real valued signal, the frequency samples $H(k)$ must satisfy the symmetry requirement.

for N odd,

$$H(N - k - 1) = H^*(k)$$

$$k = 0, 1, \dots, \frac{N-1}{2} - 1$$

$$H\left(\frac{N-1}{2}\right) = 0$$

for N even

$$H(N - k - 1) = H^*(k)$$

$$k = 0, 1, \dots, \frac{N}{2} - 1$$

- Using this symmetry condition and symmetry condition of $H(k)$ the filter coefficients can be written as,

for N odd

$$h(n) = \frac{2}{N} \sum_{k=1}^{\frac{N-3}{2}} \operatorname{Re} \left[H(k) e^{j\pi n(2k+1)/N} \right]$$

for N even

$$h(n) = \frac{2}{N} \sum_{k=1}^{\frac{N-2}{2}} \operatorname{Re} \left[H(k) e^{j\pi n(2k+1)/N} \right]$$