

TCET Formula Sheet

Decibel Formulas

Relative Power Gain

$$A_P = \frac{P_O}{P_I}$$

where P_O and P_I are defined as the following:

$$P_I = \frac{V_I^2}{R_I}$$

$$P_O = \frac{V_O^2}{R_O}$$

Relative Voltage Gain

$$A_V = \frac{V_O}{V_I}$$

Relative Power Gain in dB

$$A_P(\text{db}) = 10 \log_{10} A_P$$

$$\text{Given that } R_O = R_I$$

If $R_O \neq R_I$ then the general form is given by the following:

$$A_P(\text{db}) = 10 \log_{10} \left(\frac{V_O^2}{R_O} \cdot \frac{R_I}{V_I^2} \right)$$

Relative Voltage Gain in dB

$$A_V(\text{db}) = 20 \log_{10} \left(\frac{V_O}{V_I} \right) = 20 \log_{10} A_V$$

If $R_O \neq R_I$ then the general form is given by the following:

$$A_V(\text{db}) = 20 \log_{10} \left(\frac{V_O}{V_I} \right) - 10 \log_{10} \left(\frac{R_O}{R_I} \right)$$

Absolute Power Gain dBm

$$A_P(\text{dBm}) = 10 \log_{10} \left(\frac{P}{1 \text{ mW}} \right), \text{ dBm}$$

Absolute Power Gain dBw

$$A_P(\text{dBw}) = 10 \log_{10} \left(\frac{P}{1 \text{ W}} \right), \text{ dBw}$$

Signal-to-Noise Ratio

$$\text{SNR} = 10 \log_{10} \left(\frac{\text{Signal Power}}{\text{Noise Power}} \right)$$

$$\text{And given that } R_O = R_I,$$

$$\text{SNR} = 10 \log_{10} \left(\frac{V_S^2}{V_N^2} \right)$$

$$\text{SNR} = 20 \log_{10} \left(\frac{V_S}{V_N} \right) \text{dB}$$

Impulse Noise

$$\text{dB}_S = 20 \log_{10} \left(\frac{P}{0.0002 \bar{\mu}} \right), \text{ where } P \text{ is sound pressure in } \bar{\mu}$$

$$\bar{\mu} = 1 \frac{\text{dyne}}{\text{cm}^2} = 10^{-6} \text{ of atmospheric pressure at sea level}$$

Convert Parallel to Series Resonant Circuits

$$R_s = \frac{R_p * X_p^2}{R_p^2 + X_p^2} = \frac{R_p}{Q^2 + 1}$$

$$X_s = \frac{R_p^2 * X_p}{R_p^2 + X_p^2} = \frac{X_p * Q^2}{Q^2 + 1}$$

Convert Series to Parallel Resonant Circuits

$$R_p = \frac{R_s^2 + X_s^2}{R_s}$$

$$X_p = \frac{R_s^2 + X_s^2}{X_s}$$

Impedance Matching

$$R_{src} = R_L, \text{ for DC sources.}$$

$$Z_{src} = Z_L, \text{ for AC sources.}$$

$$\text{Source Resistance} = \text{Load Resistance}$$

$$P_I = P_O$$

Key Points L-Pad Networks

1. The primary applications of L-networks involve impedance matching in RF circuits, transmitters, and receivers.
2. L-networks are useful in matching one amplifier output to the input of a following stage.
3. Any RF circuit application covering a narrow frequency range is a candidate for an L-network.
4. There are four basic versions of the L-network, with two low-pass versions and two high-pass versions.
5. Most widely used since they attenuate harmonics, noise, and other undesired signals.
- 6. The impedances that are being matched determine the Q (quality factor) of the circuit, which cannot be specified or controlled.****
- 7. There are limits to the range of impedances that it can match.****

Key Points Pi-Pad Networks

1. The π -networks primary application is to match a high impedance source to lower value load impedance
2. It can also be used in reverse to match a low impedance to a higher impedance.
3. The π -network also can be considered two back-to-back L-networks with a virtual impedance between them.
4. To use the L-network procedures, you need to assume an intermediate virtual load/source resistance $R_V = \frac{R_H}{Q^2 + 1}$
5. R_H is the higher of the two design impedances R_{src} and R_L
- 6. The resulting R_V will be lower than either R_{src} or R_L depending on the desired Q .**
- 7. Typical Q values are usually in the 5 to 20 range.**

Key Points T-Pad Networks

1. The primary applications of L-networks involve impedance matching in RF circuits, transmitters, and receivers.
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4. There are four basic versions of the L-network, with two low-pass versions and two high-pass versions.
5. Most widely used since they attenuate harmonics, noise, and other undesired signals.
- 6. The impedances that are being matched determine the Q (quality factor) of the circuit, which cannot be specified or controlled.****
- 7. There are limits to the range of impedances that it can match.****

L-Pad Formulas (Low Pass 1)

$$Q = \sqrt{\frac{R_L}{R_{src}} - 1}$$

$$X_L = Q R_{src}$$

$$L = \frac{X_L}{2\pi f}$$

$$X_C = \frac{R_L}{Q}$$

$$C = \frac{1}{2\pi f X_C}$$

$$BW = \frac{f}{Q}$$

L-Pad Formulas (Conversion Series-Parallel)

$$R_s = \text{series resistance} = \frac{R_p}{Q^2 + 1}$$

$$R_p = \text{parallel resistance} = R_s(Q^2 + 1)$$

$$X_s = \text{series reactance} = \frac{X_p Q^2}{Q^2 + 1}$$

$$X_p = \text{parallel reactance} = \frac{X_s(Q^2 + 1)}{Q^2}$$

$$Q = \sqrt{\frac{R_p}{R_{s1}}} = \frac{X_L}{R_s} = \frac{R_p}{X_C}$$

If $Q > 5$, you can use the simplified approximations:

$$R_p = Q^2 R_s$$

$$X_p = X_s$$

L-Pad Formulas (Low Pass 2)

$$Q = \sqrt{\frac{R_{src}}{R_L} - 1}$$

$$X_L = Q R_L$$

$$L = \frac{X_L}{2\pi f}$$

$$X_C = \frac{R_{src}}{Q}$$

$$C = \frac{1}{2\pi f X_C}$$

$$BW = \frac{f}{Q}$$

$$R_R = \frac{L}{CR} = R(Q^2 + 1) = \text{resonant equivalent resistance}$$

Pi-Pad Formulas (Low Pass)

$BW = \frac{f}{Q}$

$R_V = \frac{R_H}{Q^2 + 1}$

$X_L = QR_L$; use this formula for X_{L_1} and X_{L_2}

$L = \frac{X_L}{2\pi f}$; use this formula for L_1 and L_2

$X_{C_1} = \frac{R_{src}}{Q}$

$X_{C_2} = \frac{R_L}{Q}$

$C = \frac{1}{2\pi fX_C}$; use this formula for C_1 and C_2

$Q = \sqrt{\frac{R_{src}}{R_L} - 1}; R_{src} = R_V$

Add $L_1 + L_2$ to get total inductance.

Resonance

Etc.

Telecommunications (Chapter 11)

Etc.
