TCET Formula Sheet

Decibel Formulas Relative Power Gain

$$A_P = \frac{P_O}{P_I}$$

where P_O and P_I are defined as the following:

$$P_I = \frac{V_I^2}{R_I}$$

$$P_O = \frac{V_O^2}{R_O}$$

Relative Voltage Gain

$$A_V = \frac{V_O}{V_I}$$

Relative Power Gain in dB

$$A_P(db) = 10 \log_{10} A_P$$

Given that $R_O = R_I$

If $R_O \neq R_I$ then the general form is given by the following:

$$A_P(db) = 10 \log_{10} \left(\frac{V_O^2}{N_O} \right)^{\frac{1}{2}}$$

Relative Voltage Gain in dB

$$A_V(db) = 20 \log_{10} \left(\frac{V_O}{V_I}\right) = 20 \log_{10} A_V$$

If $R_O \neq R_I$ then the general form is given by the following:

$$A_V(db) = 20 \log_{10} \left(\frac{V_O}{V_I}\right) - 10 \log_{10} \left(\frac{R_O}{R_I}\right)$$

Absolute Power Gain dBm

$$A_{P(dBm)} = 10 \log_{10} \left(\frac{P}{1 \text{ mW}} \right), \text{ dBm}$$

Absolute Power Gain dBw

$$A_{P(dBw)} = 10 \log_{10} \left(\frac{P}{1 \text{ W}}\right), \text{ dBw}$$

Signal-to-Noise Ratio

$$\begin{aligned} \text{SNR} &= 10 \log_{10} \left(\frac{\text{Signal Power}}{\text{Noise Power}} \right) \\ \text{And given that } R_O &= R_I, \\ \text{SNR} &= 10 \log_{10} \left(\frac{V_S^2}{V_N^2} \right) \\ \text{SNR} &= 20 \log_{10} \left(\frac{V_S}{V_S} \right) \text{dB} \end{aligned}$$

Impulse Noise

$$dB_S = 20 \log_{10} \left(\frac{P}{0.0002\bar{\mu}} \right)$$
, where P is sound pressure in $\bar{\mu}$

$$\bar{\mu} = 1 \frac{\text{dyne}}{\text{cm}^2} = 10^{-6}$$
 of atmospheric pressure at sea level

Convert Parallel to Series Resonant Circuits

$$R_{s} = \frac{R_{p} * X_{p}^{2}}{R_{p}^{2} + X_{p}^{2}} = \frac{R_{p}}{Q^{2} + 1}$$
$$X_{s} = \frac{R_{p}^{2} * X_{p}}{R_{p}^{2} + X_{p}^{2}} = \frac{X_{p} * Q^{2}}{Q^{2} + 1}$$

Convert Series to Parallel Resonant Circuits

$$R_p = \frac{R_s^2 + X_s^2}{R_s}$$
$$X_p = \frac{R_s^2 + X_s^2}{X_s}$$

Impedance Matching

 $R_{src} = R_L$, for DC sources. $Z_{src} = Z_L$, for AC sources. Source Resistance = Load Resistance $P_I = P_O$

Key Points L-Pad Networks

- 1. The primary applications of L-networks involve impedance matching in RF circuits, transmitters, and receivers.
- 2. L-networks are useful in matching one amplifier output to the input of a following stage.
- 3. Any RF circuit application covering a narrow frequency range is a candidate for an L-network.
- 4. There are four basic versions of the L-network, with two low-pass versions and two high-pass versions.
- 5. Most widely used since they attenuate harmonics, noise, and other undesired signals.
- 6. The impedances that are being matched determine the Q (quality factor) of the circuit, which cannot be specified or controlled.**
- 7. There are limits to the range of impedances that it can match.**

Key Points Pi-Pad Networks

- 1. The π -networks primary application is to match a high impedance source to lower value load impedance
- 2. It can also be used in reverse to match a low impedance to a higher impedance.
- 3. The π -network also can be considered two backto-back L-networks with a virtual impedance between them.
- 4. To use the L-network procedures, you need to assume an intermediate virtual load/source resistance $R_V = \frac{R_H}{O^2 + 1}$
- 5. R_H is the higher of the two design impedances R_{src} and R_L
- 6. The resulting R_V will be lower than either R_{src} or R_L depending on the desired Q.
- 7. Typical Q values are usually in the 5 to 20 range.

Key Points T-Pad Networks

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- 2. L-networks are useful in matching one amplifier output to the input of a following stage.
- 3. Any RF circuit application covering a narrow frequency range is a candidate for an L-network.
- 4. There are four basic versions of the L-network, with two low-pass versions and two high-pass versions.
- 5. Most widely used since they attenuate harmonics, noise, and other undesired signals.
- 6. The impedances that are being matched determine the Q (quality factor) of the circuit, which cannot be specified or controlled.**
- 7. There are limits to the range of impedances that it can match.**

L-Pad Formulas (Low Pass 1)

$$Q = \sqrt{\frac{R_L}{R_{src}} - 1}$$

$$X_L = QR_{src}$$

$$L = \frac{X_L}{2\pi f}$$

$$X_C = \frac{R_L}{Q}$$

$$C = \frac{1}{2\pi f X_C}$$

$$BW = \frac{f}{Q}$$

L-Pad Formulas (Conversion Series-Parallel)

$$R_s = \text{ series resistance} = \frac{R_p}{Q^2 + 1}$$

$$R_p = \text{ parallel resistance} = R_s(Q^2 + 1)$$

$$X_s = \text{ series reactance} = \frac{X_p Q^2}{Q^2 + 1}$$

$$X_p = \text{ parallel reactance} = \frac{X_s(Q^2 + 1)}{Q^2}$$

$$Q = \sqrt{\frac{R_p}{R_s 1}} = \frac{X_L}{R_s} = \frac{R_p}{X_C}$$

If Q > 5, y you can use the simplified approximations:

$$R_p = Q^2 R_s$$
$$X_p = X_s$$

L-Pad Formulas (Low Pass 2)

$$Q = \sqrt{\frac{R_{src}}{R_L} - 1}$$

$$X_L = QR_L$$

$$L = \frac{X_L}{2\pi f}$$

$$X_C = \frac{R_{src}}{Q}$$

$$C = \frac{1}{2\pi f X_C}$$

$$BW = \frac{f}{Q}$$

$$R_R = \frac{L}{CR} = R(Q^2 + 1) = \text{ resonant equivalent resistance}$$

Resonance

Etc.

Telecommunications (Chapter 11)

Etc.