

# Com. Elec. Formula Sheet

## Decibel Formulas

### Relative Power Gain

$$A_P = \frac{P_O}{P_I}$$

where  $P_O$  and  $P_I$  are defined as the following:

$$P_I = \frac{V_I^2}{R_I}$$

$$P_O = \frac{V_O^2}{R_O}$$

### Relative Voltage Gain

$$A_V = \frac{V_O}{V_I}$$

### Relative Power Gain in dB

$$A_P(db) = 10 \log_{10} A_P$$

$$\text{Given that } R_O = R_I$$

If  $R_O \neq R_I$  then the general form is given by the following:

$$A_P(db) = 10 \log_{10} \left( \frac{V_O^2}{V_I^2} \frac{R_I}{R_O} \right)$$

### Relative Voltage Gain in dB

$$A_V(db) = 20 \log_{10} \left( \frac{V_O}{V_I} \right) = 20 \log_{10} A_V$$

If  $R_O \neq R_I$  then the general form is given by the following:

$$A_V(db) = 20 \log_{10} \left( \frac{V_O}{V_I} \right) - 10 \log_{10} \left( \frac{R_O}{R_I} \right)$$

### Special Case

If  $R_O \neq R_I$  then the general form is given by the following:

$$\begin{aligned} A_V(db) &= 10 \log_{10} \left( \frac{V_O^2}{V_I^2} \right) - 10 \log_{10} \left( \frac{R_O}{R_I} \right) \\ &= 20 \log_{10} \left( \frac{V_O}{V_I} \right) - 10 \log_{10} \left( \frac{R_O}{R_I} \right) \end{aligned}$$

### Absolute Power Gain dBm

$$A_{P(dbm)} = 10 \log_{10} \left( \frac{P}{1 \text{ mW}} \right), \text{ dBm}$$

### Absolute Power Gain dBw

$$A_{P(dbw)} = 10 \log_{10} \left( \frac{P}{1 \text{ W}} \right), \text{ dBw}$$

### Signal-to-Noise Ratio

$$\text{SNR} = 10 \log_{10} \left( \frac{\text{Signal Power}}{\text{Noise Power}} \right)$$

$$\text{And given that } R_O = R_I,$$

$$\text{SNR} = 10 \log_{10} \left( \frac{V_S^2}{V_N^2} \right)$$

$$\text{SNR} = 20 \log_{10} \left( \frac{V_S}{V_N} \right) \text{dB}$$

### Impulse Noise

$$dB_S = 20 \log_{10} \left( \frac{P}{0.0002 \bar{\mu}} \right), \text{ where } P \text{ is sound pressure in } \bar{\mu}$$

$$\bar{\mu} = 1 \frac{\text{dyne}}{\text{cm}^2} = 10^{-6} \text{ of atmospheric pressure at sea level}$$

### Gaussian (White) Noise

$$P_n = kT\Delta f$$

$$k = \text{Boltzmann's Constant } (1.38 * 10^{-23}) \text{ J/K}$$

$$T = \text{resistor temperature in Kelvin } (K)$$

$$\Delta f = \text{system bandwidth.}$$

### Gaussian (White) Noise Formulas

Using the above proportionality we can relate bandwidth to noise, shown below:

Given the noise can be represented as  $e_n$

then we can say the following:

$$P_n = \frac{V_n^2}{R} = kT\Delta f, \text{ where } V_n = \frac{e_n}{2}$$

This is true by Ohm's law. By solving in terms of  $e_n$  we get the following:

$$\frac{V_n^2}{R} = kT\Delta f \text{ where } V_n = \frac{e_n}{2}$$

$$\left( \frac{e_n}{2} \right)^2 = \left( \frac{e_n^2}{4} \right) = kT\Delta f$$

$$\left( \frac{e_n^2}{4} \right) = kT\Delta f$$

$$e_n = \sqrt{4kT\Delta f R}$$

### Noise Ratio

$$NF = 10 \log_{10} \frac{\frac{S_i}{N_i}}{\frac{S_o}{N_o}} = 10 \log_{10} NR$$

$$NR = \frac{\frac{S_i}{N_i}}{\frac{S_o}{N_o}} \text{ is the Noise Ratio}$$

$$\frac{S_i}{N_i} = \text{input SNR}$$

$$\frac{S_o}{N_o} = \text{output SNR}$$

### Reactance Noise Effects

$$\Delta f_{eq} = \frac{\pi}{2} BW$$

$$BW = 3 \text{ dB; bandwidth for } RC, LC, \text{ or } RLC \text{ circuits.}$$

### Noise Created by Amplifiers in Cascade

$$NR = NR_1 + \frac{NR_2 - 1}{P_{G_1}} + \dots + \frac{NR_n - 1}{P_{G_1} * P_{G_2} * P_{G_{(n-1)}}}$$

$$NR = \text{overall noise ratio of } n \text{ stages.}$$

$$P_G = \text{power gain ratio}$$

### Equivalent Noise Temperature

$$T_{eq} = T_0(NR - 1)$$

where  $T_0 = 290 \text{ K}$ , a reference temperature in Kelvin.

### Equivalent Noise Resistance

Sometimes used by Manufacturers to represent the noise generated by a device with a fictitious resistance. The following represents this:

$$R_{eq} = \sqrt{4kT\Delta f R}$$

### Modulation Index

$$m = \frac{E_i}{E_c}$$

$$\%m = \frac{E_i}{E_c} * 100\%$$

$$\%m = \frac{B - A}{B + A} * 100\%$$

$$B = \text{AM Waveform}$$

$$A = \text{The Minimum Peak-to-Peak value}$$

### Overmodulation

$$\%m = \frac{B - O}{B + O} * 100\%$$

$$B = \text{AM Waveform}$$

$$O = \text{The Minimum Peak-to-Peak value} \leq 0$$

### Amplitude Modulation/Mixing in Frequency Domain

#### Carrier Signal

$$e_c = E_C \sin \omega_c t$$

where  $e_i =$  is the instantaneous value of the carrier

$E_C =$  is the maximum peak value of the carrier when unmodulated

$$\omega = 2\pi f \text{ ("f" is the carrier frequency)}$$

$$t = \text{is a unit of measure}$$

#### Information Signal

$$e_i = E_I \sin \omega_i t$$

where  $e_i =$  is the instantaneous value of the information

$E_i =$  is the maximum peak value of the intelligence

when unmodulated

$$\omega = 2\pi f \text{ ("f" is the carrier frequency)}$$

$$t = \text{is a unit of measure}$$

### AM Modulated Waveform

$$e = E_c \sin \omega_c t + \frac{mE_c}{2} \cos(\omega_c - \omega_i)t - \frac{mE_c}{2} \cos(\omega_c + \omega_i)t$$

1.  $E_c \sin \omega_c t$  relates to the carrier (1)

2.  $\frac{mE_c}{2} \cos(\omega_c - \omega_i)t$  relates to the the lower sideband at  $f_c - f_i$  (2)

3.  $\frac{mE_c}{2} \cos(\omega_c + \omega_i)t$  relates to the the upper sideband at  $f_c + f_i$  (3)

### Power Distribution in Carriers and Sidebands

$$E_{SF} = \frac{mE_C}{2}$$

$$E_{SF} = \text{side frequency amplitude}$$

$$m = \text{modulation index}$$

$$E_C = \text{carrier amplitude}$$

**Total Transmitted Power**

$$P_t = P_c \left(1 + \frac{m^2}{2}\right)$$

$P_t$  = Total Transmitted Power (sidebands and carrier)  
 $m$  = modulation index  
 $P_c$  = carrier power

**Total Transmitted Current**

$I_t$  = Total Transmitted Current (sidebands and carrier)  
 $I$  = modulation index  
 $I_c$  = carrier current

**Frequency Modulation**

**How FM Generator Works? ”The Concept of Deviation”**

$f_{OUT} = f_C + k e_i$   
 $f_{OUT}$  = instantaneous output frequency  
 $f_C$  = output carrier frequency  
 $k$  = deviation constant [kHz/V]  
 $e_i$  = modulating (intelligence) input

**Quick Facts**

- 1. Deviation constant defines how much carrier frequency will deviate for input voltage level.
- 2. Deviation constant dependent on system design.
- 3. Knowing deviation on either side of carrier is essential for determining occupied bandwidth of modulated signal.

**Direct FM**

Direct FM involves messing w/ the frequency component of a sinusoidal wave:

$$f \text{ in } \omega(A_P \sin(\omega t + \theta) = A_P \sin(2\pi f t + \theta))$$

**Indirect FM**

Indirect FM involves messing w/ the phase angle component of a sinusoidal wave:

$$\theta \text{ in the sinusoid } (A_P \sin(\omega t + \theta) = A_P \sin(2\pi f t + \theta))$$

**FM IN THE FREQUENCY DOMAIN**

$e = A \sin(\omega_c t + m_f \sin \omega_i t)$   
 $e$  = instantaneous voltage  
 $A$  = peak value of original carrier wave  
 $\omega_c$  = carrier carrier angular velocity ( $2\pi f_c$ )  
 $\omega_i$  = modulating intelligence signal angular velocity ( $2\pi f_i$ )

**Modulation Index**

$m_f$  = FM Modulation Index =  $\frac{\delta}{f_i}$   
 $\delta$  = maximum frequency shift caused by the intelligence signal (deviation)  
either above or below the carrier; therefore, deviation written as 3 kHz, for example, has  
 $\delta$  = 3 kHz (not 6 kHz) in the above.  
 $f_i$  = of the intelligence (modulating) signal

**FM Spectrum Analyzer**

Remember that each Bessel table entry represents the ratio  $\frac{V_2}{V_1}$  for its respective carrier  $J_0$  or sideband  $J_1$  and above signal component, for a given modulation index.

$$P_{dB} = 20 \log_{10} \frac{V_2}{V_1}$$

**Power Distribution**

**Carson’s Rule Approximation**

$$BW \cong 2(\delta_{max} + f_{i_{max}})$$

**Percent of Modulation and Deviation Ratio**

$$DR = \frac{\text{max possible freq deviation}}{\text{max input freq}} = \frac{f_{dev(max)}}{f_{i(max)}}$$

**Fourier Series**

$$a_0 = \frac{1}{2\pi} \int_{-\pi}^{\pi} f(x) dx$$
  
$$a_n = \frac{1}{\pi} \int_{-\pi}^{\pi} \cos(nx) dx$$
  
$$b_n = \frac{1}{\pi} \int_{-\pi}^{\pi} \sin(nx) dx$$

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