Lab 2. Simulation components of dynamic systems

1. My name and HDU ID

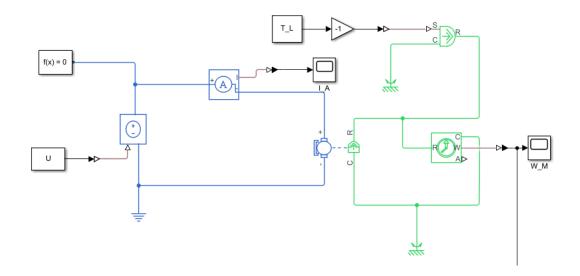
Name:Li Xin

HDU ID:22320404

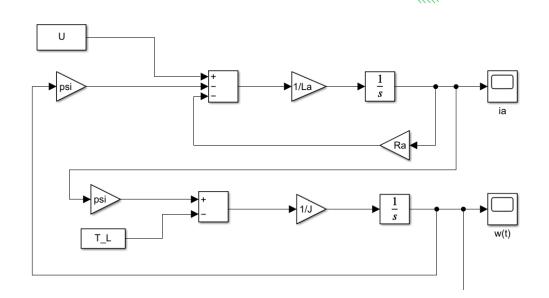
2. My variant and initial data

| No. I | n ITMO | | | Surname, First name in English | Surname, First name in Chinese | Gender | Variant | U | psi | R | L | J1 | J2 | T_load |
|-------|--------|---------|----------|-----------------------------------|--------------------------------------|--------|---------|----|---------|------|---------|---------|---------|---------|
| 3 | 375334 | Ли Синь | 22320404 | LI XIN | 李馨 | Female | 6 | 12 | 0.28648 | 0.35 | 0.00035 | 0.00035 | 0.00234 | 0.68755 |

3. Simscape model of DC-motor



4. Block diagram model of DC-motor



5. Transfer functions of DC-motor

$$L_{a}sI_{a}(s) = U(s) - R_{a}I_{a}(s) - \Psi w(s)$$

$$Jsw(s) = \Psi I_{a}(s) - T_{L}(s)$$

$$I_{a}(s) = \frac{U(s) - \Psi w(s)}{L_{a}s + R_{a}}$$

$$Jsw(s) = \Psi \frac{U(s) - \Psi w(s)}{L_{a}s + R_{a}} - T_{L}(s)$$

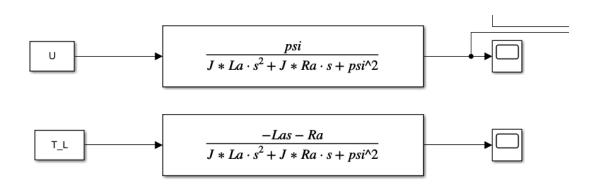
$$Let T_{L} = 0$$

$$W_{1}(s) = \frac{w(s)}{U(s)} = \frac{\Psi}{JL_{a}s^{2} + JR_{a}s + \Psi^{2}}$$

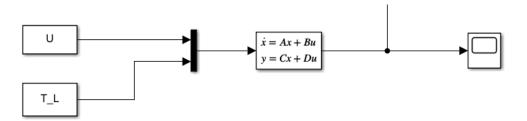
$$Let U(s) = 0$$

$$\Omega(s) = \frac{-(L_a s + R_a)}{Js(L_a s + R_a) + \Psi^2} T_L(s)$$

$$W_2(s) = \frac{-(L_a s + R_a)}{Js(L_a s + R_a) + \Psi^2}$$



6. State space model of DC-motor



$$L_{a}\frac{di_{a}(t)}{dt} = U - R_{a}i_{a}(t) - \Psi\omega(t)$$

$$J\frac{d\omega(t)}{dt} = \Psi i_{a}(t) - T_{L}$$

$$x_{1} = i_{a}, \quad x_{2} = \omega$$

$$\dot{x}_{1} = \frac{di_{a}}{dt}, \quad \dot{x}_{2} = \frac{d\omega}{dt}$$

$$\dot{x}_{1} = \frac{1}{L_{a}}(U - R_{a}x_{1} - \Psi x_{2})$$

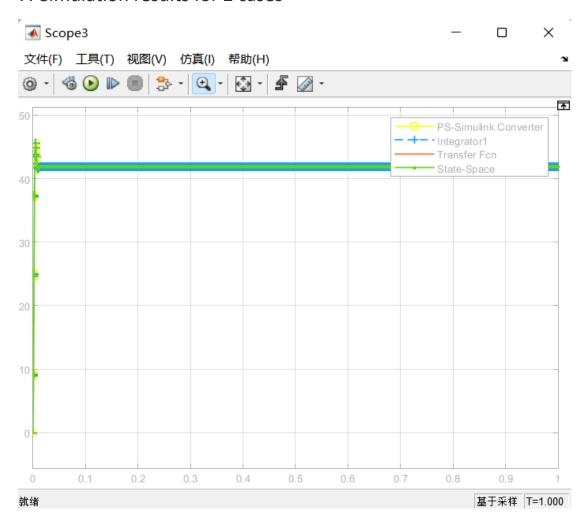
$$\dot{x}_{2} = \frac{1}{J}(\Psi x_{1} - T_{L})$$

$$\begin{bmatrix} \dot{x}_{1} \\ \dot{x}_{2} \end{bmatrix} = \begin{bmatrix} -\frac{R_{a}}{L_{a}} & -\frac{\Psi}{L_{a}} \\ \frac{\Psi}{J} & 0 \end{bmatrix} \begin{bmatrix} x_{1} \\ x_{2} \end{bmatrix} + \begin{bmatrix} \frac{1}{L_{a}} & 0 \\ 0 & -\frac{1}{J} \end{bmatrix} \begin{bmatrix} U \\ T_{L} \end{bmatrix}$$

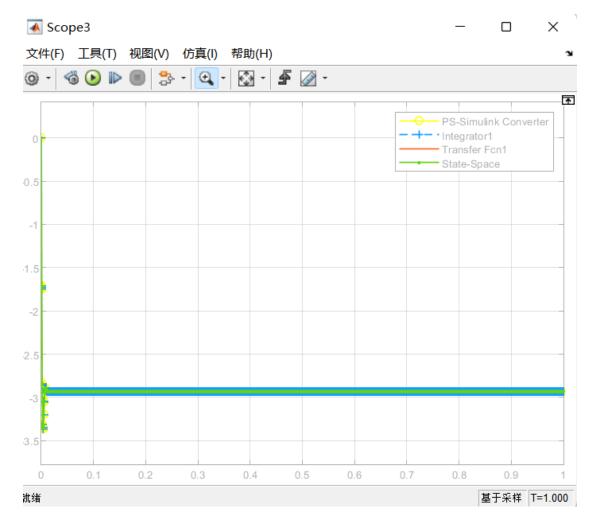
$$y = egin{bmatrix} 0 & 1 \end{bmatrix} egin{bmatrix} x_1 \ x_2 \end{bmatrix} + egin{bmatrix} 0 & 0 \end{bmatrix} egin{bmatrix} U \ T_L \end{bmatrix}$$

$$A = egin{bmatrix} -rac{R_a}{L_a} & -rac{\Psi}{L_a} \ rac{\Psi}{J} & 0 \end{bmatrix}, \quad B = egin{bmatrix} rac{1}{L_a} & 0 \ 0 & -rac{1}{J} \end{bmatrix}, \quad C = egin{bmatrix} 0 & 1 \end{bmatrix}, \quad D = egin{bmatrix} 0 & 0 \end{bmatrix}$$

7. Simulation results for 2 cases



With rated voltage and zero load torque



With zero voltage and rated load torque

8. Calculation of transient response function based on transfer function of DC-motor for two values of inertia

$$JL_{a}s^{2} + JR_{a}s + \Psi^{2} = 0$$

$$s^{2} + 2\zeta\omega_{n}s + \omega_{n}^{2} = 0$$

$$\omega_{n}^{2} = \frac{\Psi^{2}}{JL_{a}}$$

$$2\zeta\omega_{n} = \frac{JR_{a}}{JL_{a}} = \frac{R_{a}}{L_{a}}$$

$$\omega_{n} = \sqrt{\frac{\Psi^{2}}{JL_{a}}}$$

$$\zeta = \frac{R_{a}}{2} \sqrt{\frac{J}{\Psi^{2}L_{a}}}$$

$$\zeta = 0.6109 < 1$$

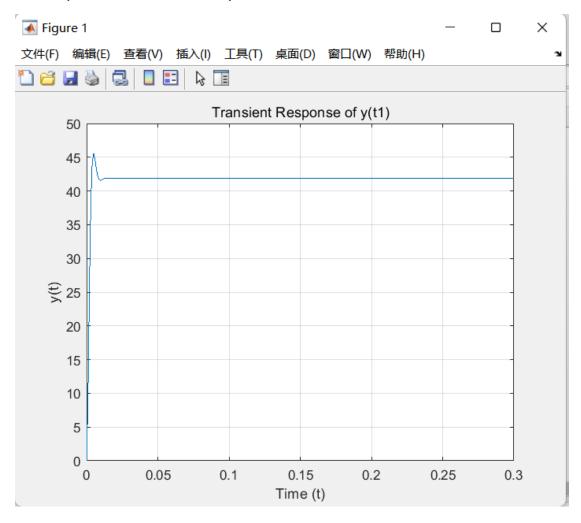
$$\zeta = 1.5795 > 1$$

So the transient response function $\omega(t)$ for $U(t)=U_{-}$ rated , J=J1 is underdamped.

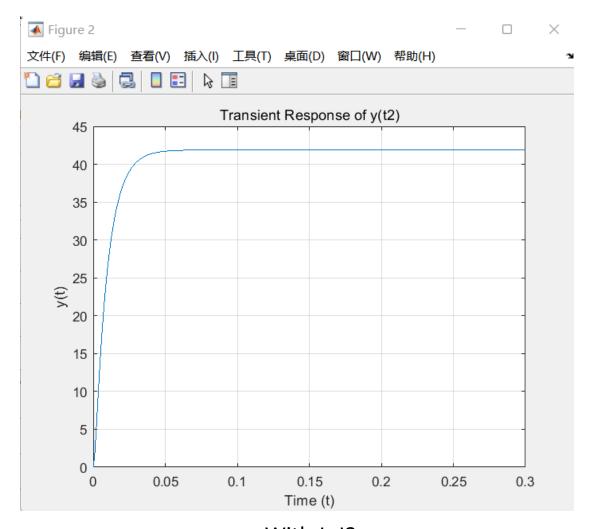
After inverse Laplace transform,

$$\omega(t) = \frac{U_{rated}}{\varphi} \left(1 - e^{-\zeta \omega_n t} \left(\cos(\omega_d t) + \frac{\zeta}{\sqrt{1 - \zeta}} \sin(\omega_d t) \right) \right)$$

9. Graphs of transient responses



With J=J1



With J=J2

10. Values of rise time, maximum overshoot and settling time

For J1

Rise Time (10% to 90%): 0.003 s

Max Overshoot: 8.85%

Settling Time (5% tolerance): 0.008 s

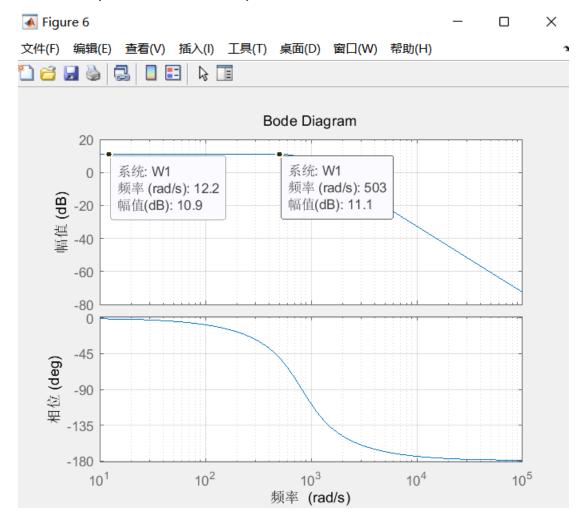
For J2:

Rise Time (10% to 90%): 0.0197 s

Max Overshoot: 0.00%

Settling Time (5% tolerance): 0.0358 s

11. Bode plot of underdamped model of DC-motor



12. Values of the static gain and damped natural frequency calculated from Bode plots

Static Gain K =
$$\frac{10.9}{20}$$
 = $10^{0.545}$ = 3.50

Damped Natural Frequency wd = 503 rad/s

13.conclusion

Model Validation

The derived transfer function and state-space model of the DC motor align with the physical principles of electromechanical systems. The transfer function and state-space matrices were successfully validated through Simulink simulations, confirming their accuracy in describing the motor's dynamics under both no-load and rated load conditions.

Impact of Inertia (J) on Transient Response

For J=J1: The system exhibited **underdamped behavior** (ζ 1 =0.61), resulting in a fast rise time (0.003s) but with an overshoot of 8.85%.

For J=J2: The system became **overdamped** (ζ 2=1.58), eliminating overshoot at the cost of slower response (rise time 0.0197s).

Frequency Domain Analysis

The Bode plot of the underdamped model (J=J1) revealed a static gain K=3.50 and damped natural frequency $\omega d=503$ rad/s. These values align with theoretical predictions, confirming the system's bandwidth and resonance characteristics.