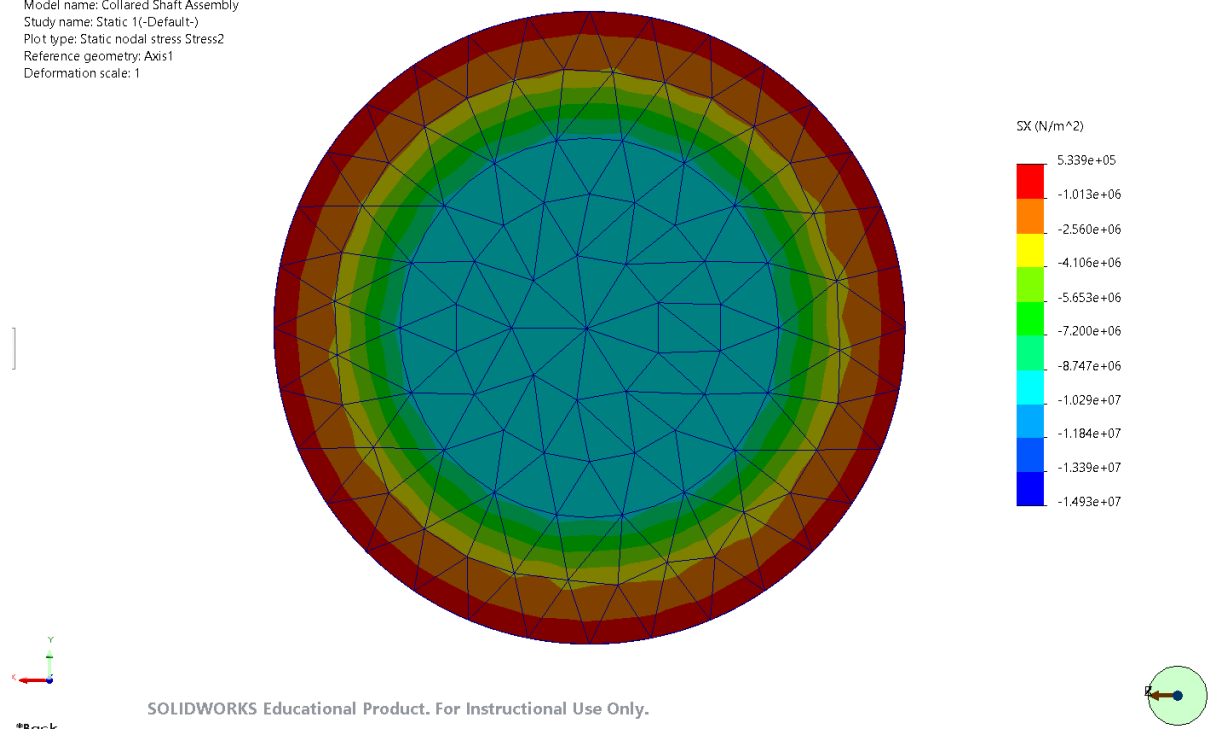


Problem: Shaft with shaft cover Thermal stresses:

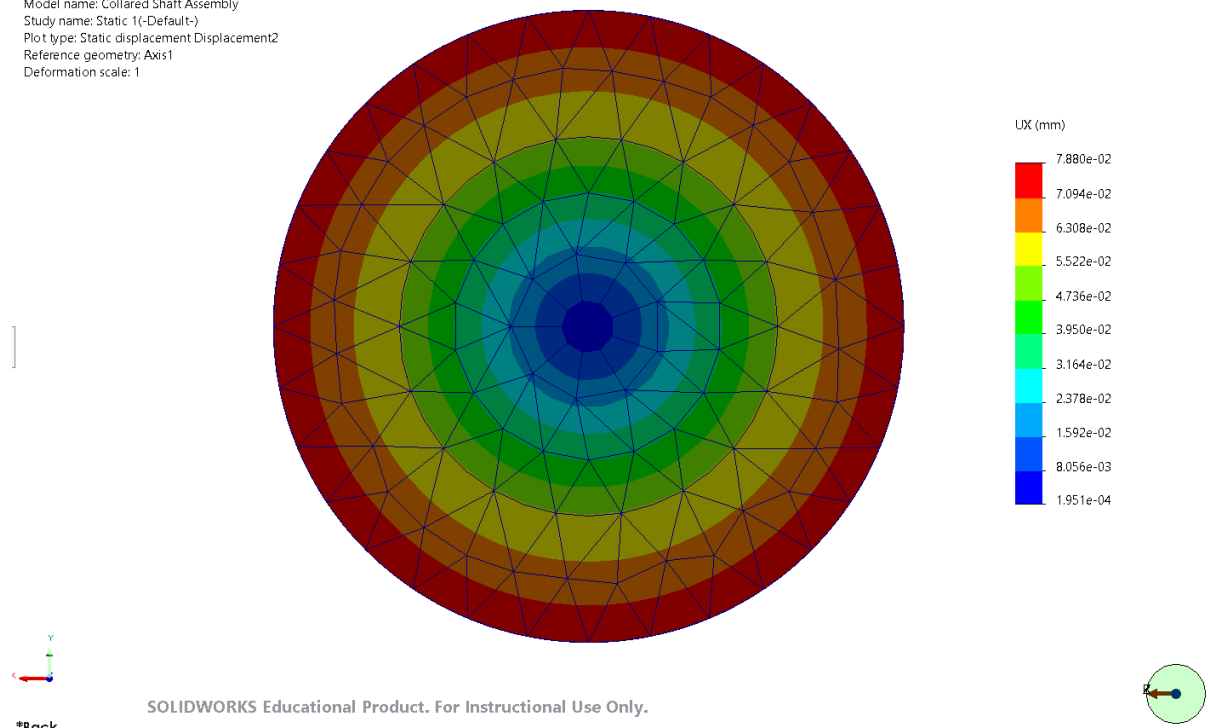
Radial stress distribution contours for the assembly shown below:

Model name: Collared Shaft Assembly
Study name: Static 1(-Default-)
Plot type: Static nodal stress Stress2
Reference geometry: Axis1
Deformation scale: 1



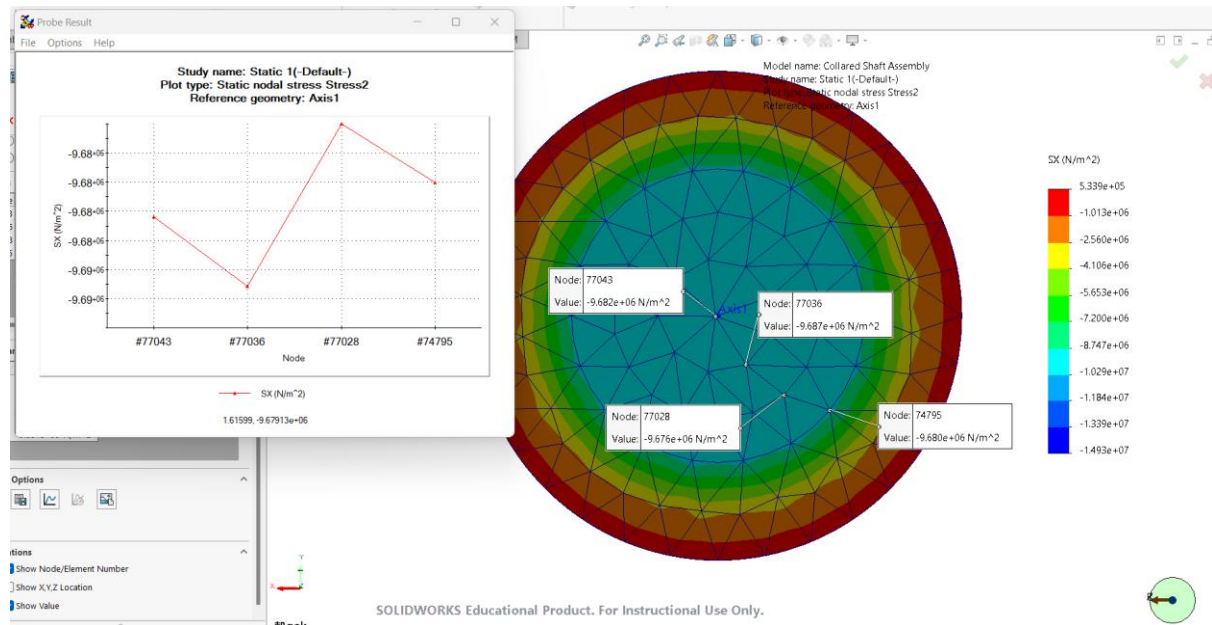
Radial displacement contours for the assembly shown below:

Model name: Collared Shaft Assembly
Study name: Static 1(-Default-)
Plot type: Static displacement Displacement2
Reference geometry: Axis1
Deformation scale: 1

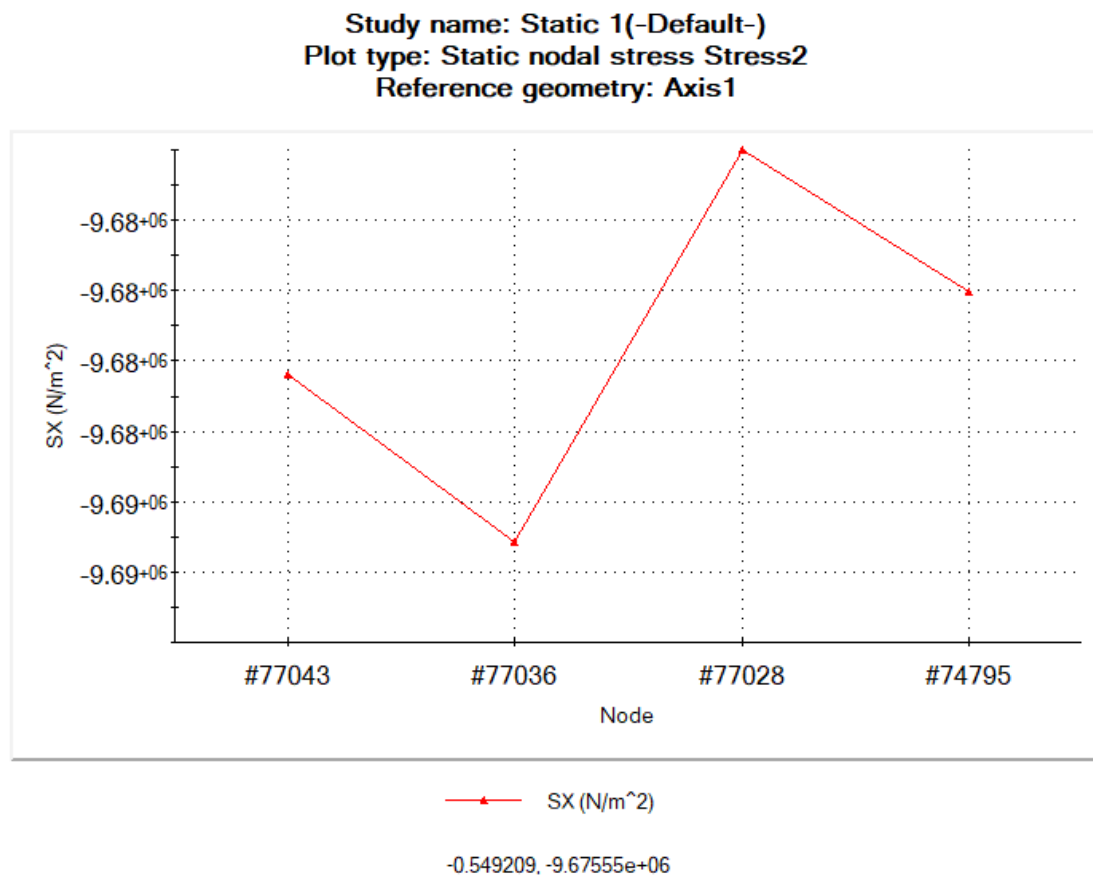


XY plots for shaft given below:

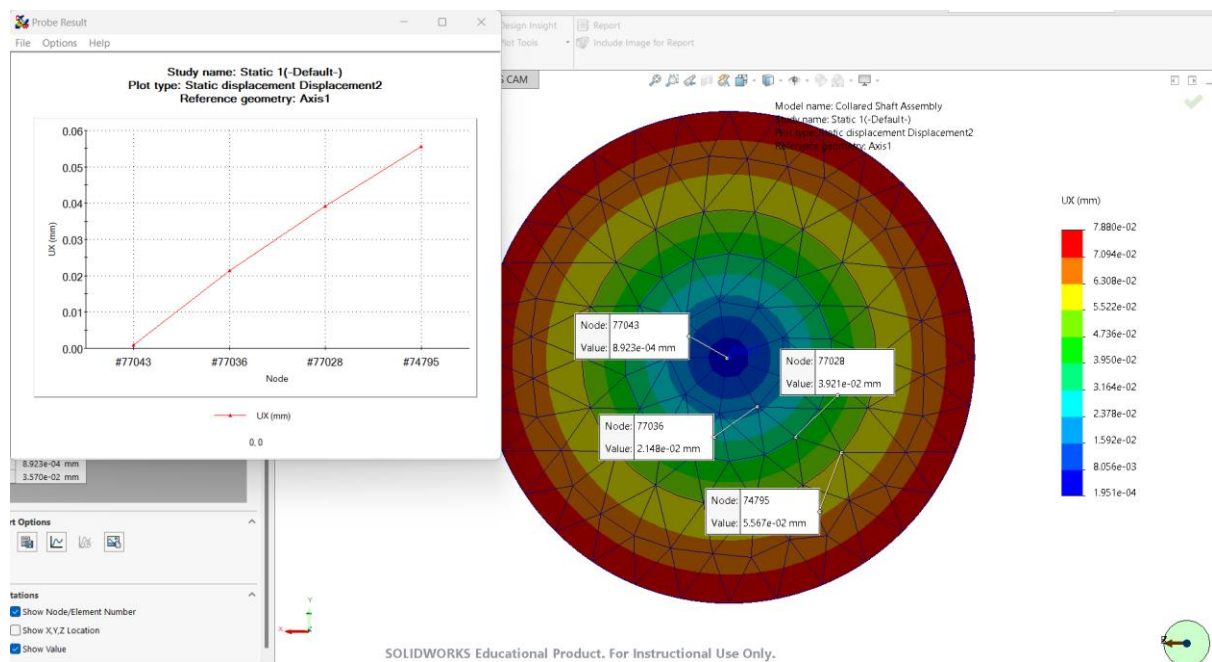
a. Radial Stress in shaft for probe locations from centre to its boundary below:



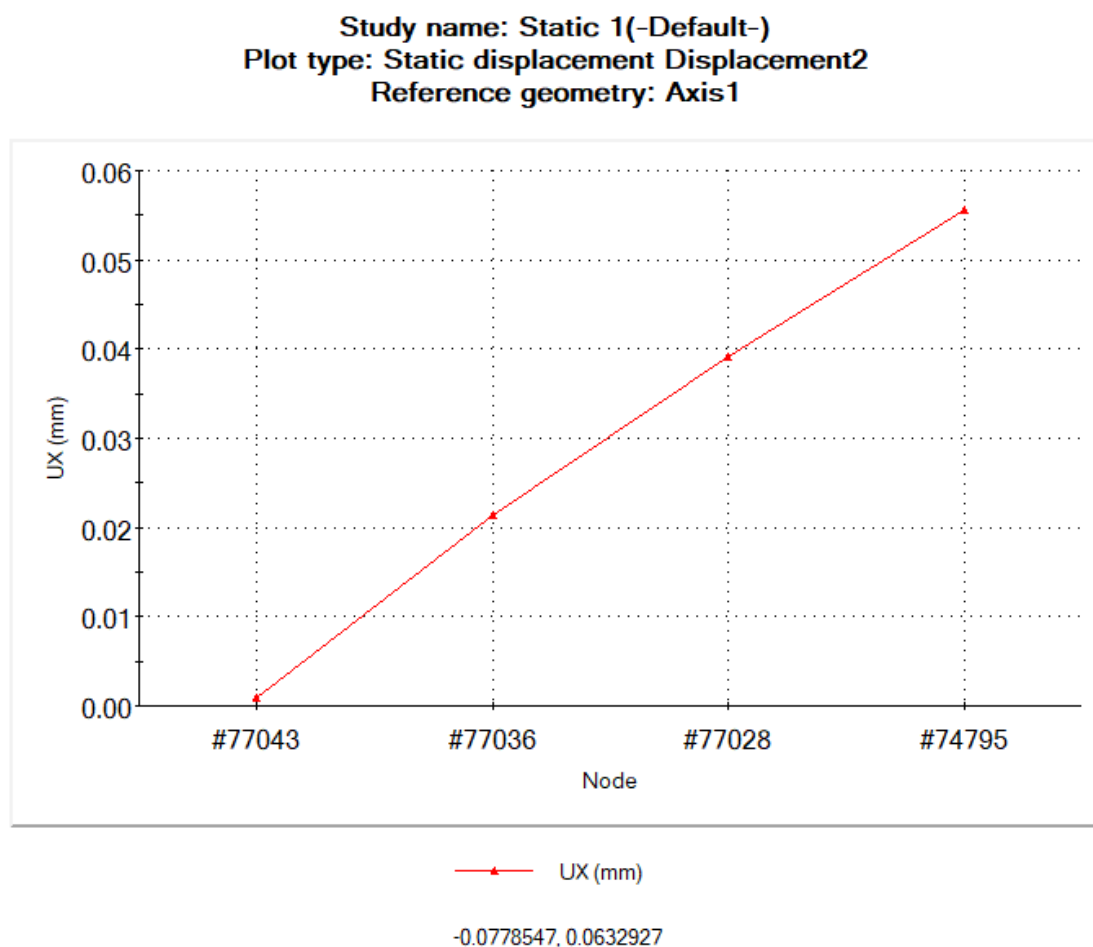
Larger view of the XY plot for radial stress in shaft from above is given below:



b. Radial displacement in shaft for probe locations from centre to its boundary below:

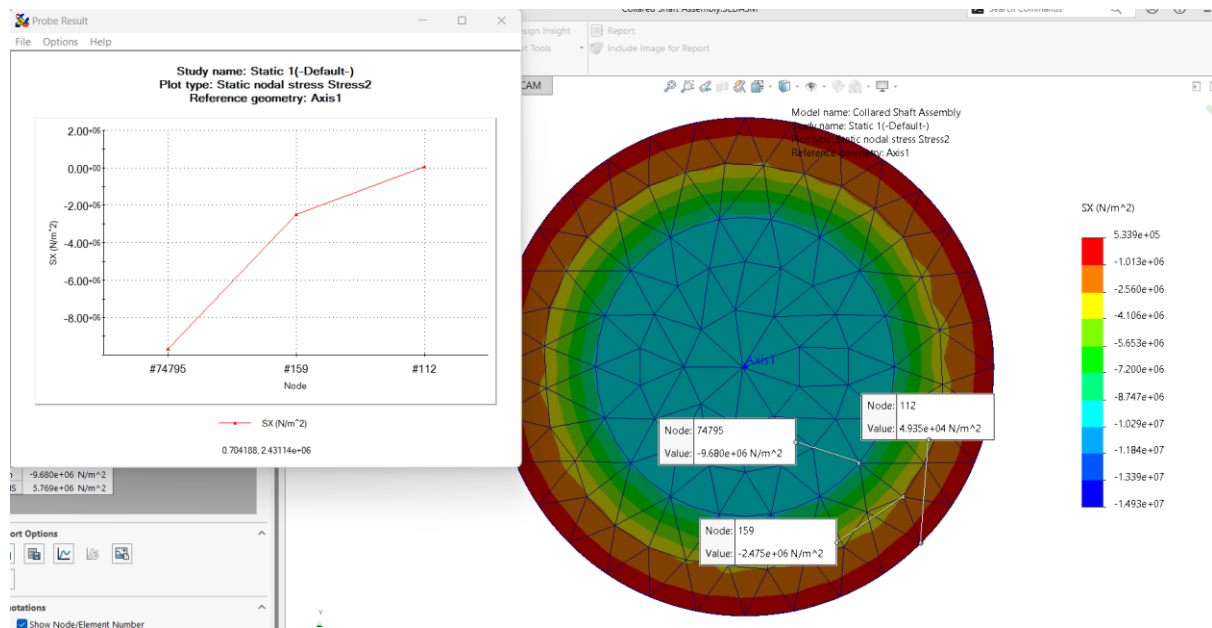


Larger view of the XY plot for radial displacement in shaft from above is given below:

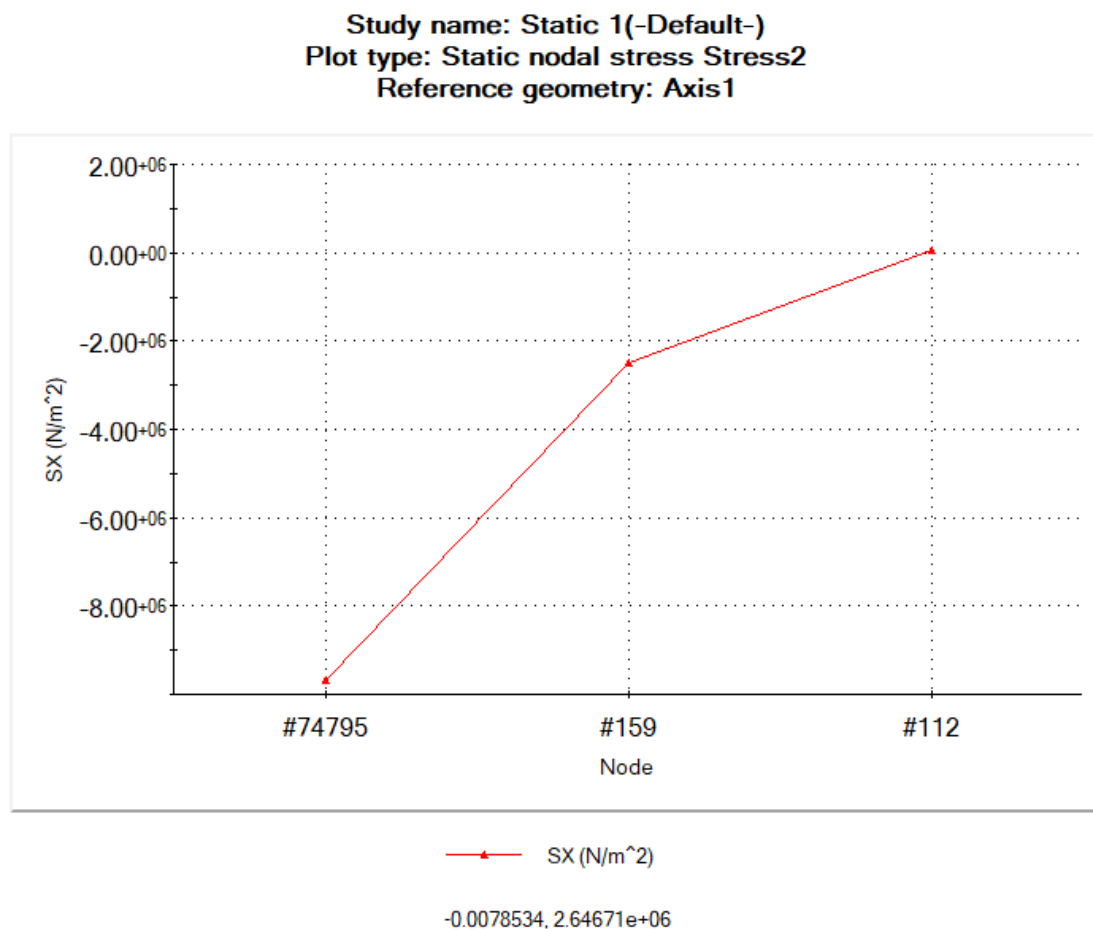


XY plots for shaft-cover given below:

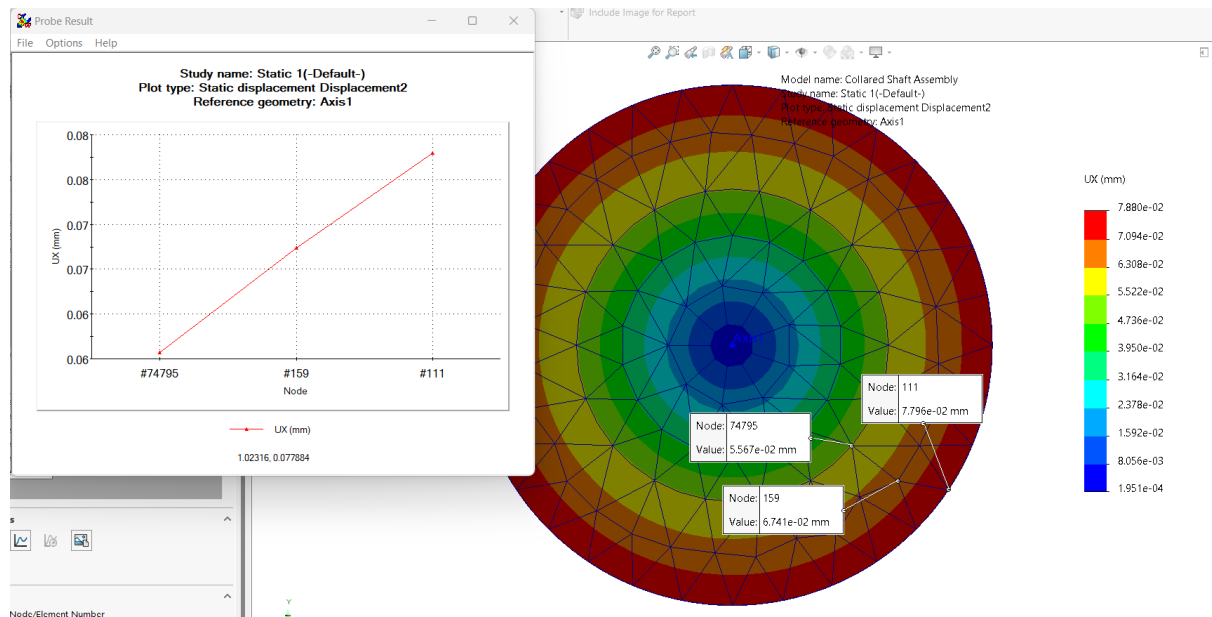
a. Radial Stress in shaft-cover for probe locations from inner to outer radius below:



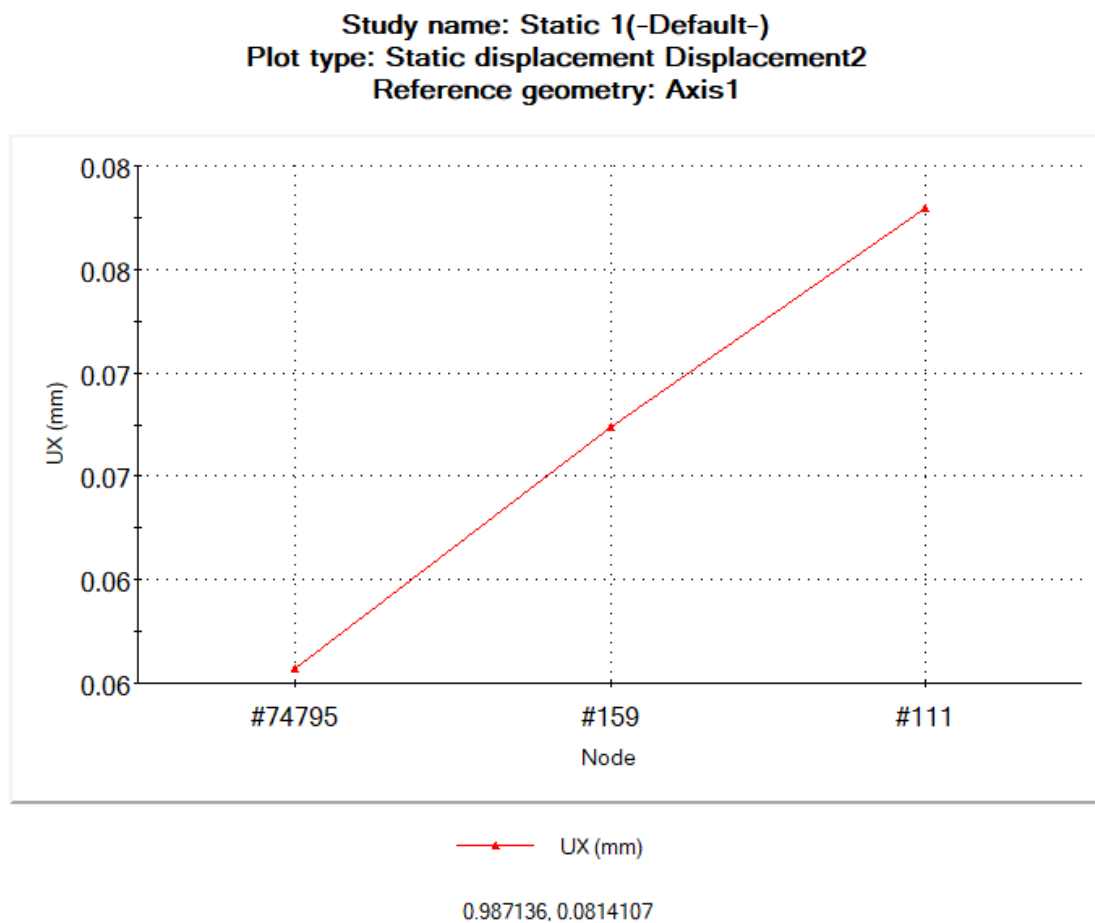
Larger view of the XY plot for radial stress in shaft-cover from above is given below:



- b. Radial displacement in shaft-cover for probe locations from inner to outer radius below:

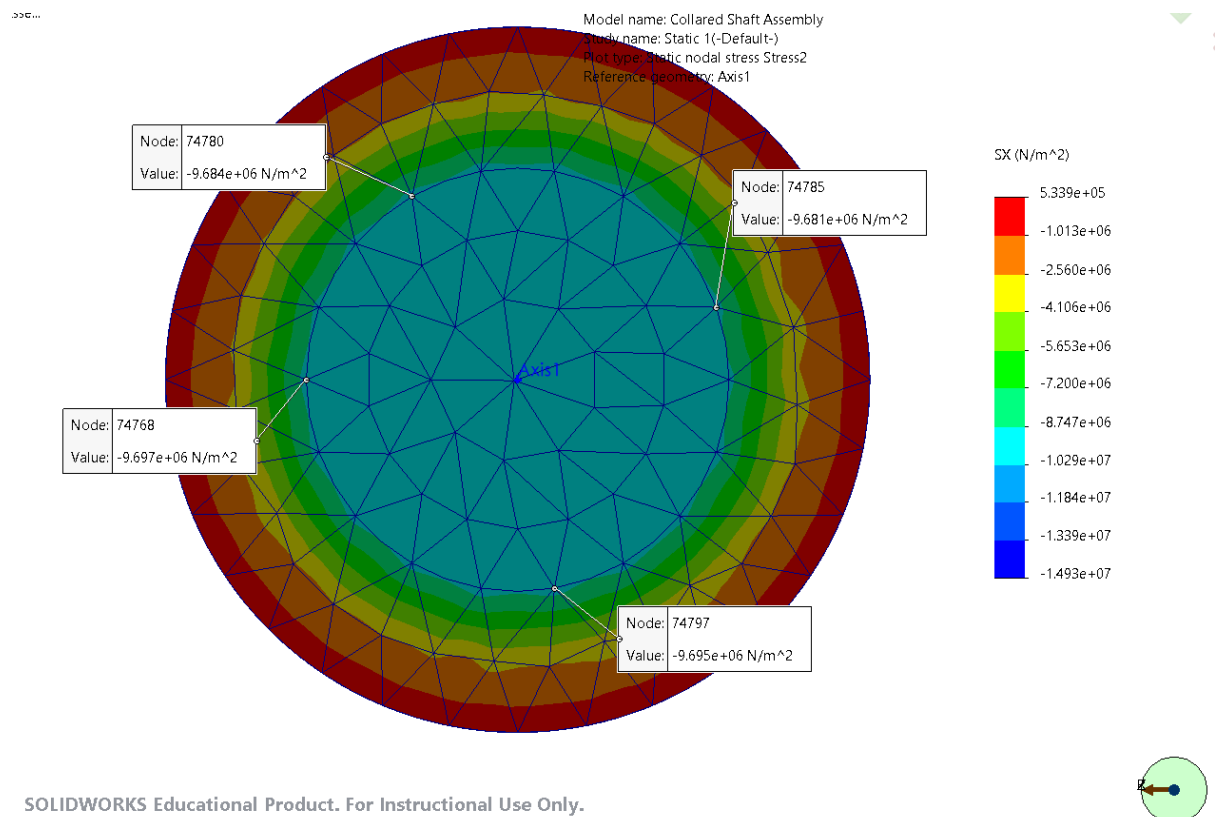


Larger view of the XY plot for radial displacement in shaft-cover from above is given below:



Validating the simulation results:

Radial thermal stress at boundary between shaft and shaft-cover from FEA shown below:



We can see, FEA simulation gives us a radial stress value of 9.68×10^6 to 9.7×10^6 N/m² (or Pa).

Calculations using classical equations given below:

$$P = \frac{(\alpha_s - \alpha_{sc}) \Delta T}{\frac{1}{E_o} \left(\frac{r_o^2 + R^2}{r_o^2 - R^2} + \nu_o \right) + \frac{1}{E_i} \left(\frac{R^2 + r_i^2}{R^2 - r_i^2} - \nu_i \right)}$$

Shaft \Rightarrow 2014 Al alloy

$$E_i = 7.3 \times 10^{10} \text{ N/m}^2 [\text{Pa}] \approx 73 \text{ GPa}$$

$$\nu_i = 0.33$$

$$\alpha_i = 2.3 \times 10^{-5} \text{ } ^\circ\text{C}^{-1}$$

$$r_i = 0 \text{ mm}$$

$$R = 300 \text{ mm} = 0.3 \text{ m}$$

$$\Delta T = 20 \text{ K}$$

Shaft collar \Rightarrow Alloy steel

$$E_o = 2.1 \times 10^{11} \text{ N/m}^2 [\text{Pa}] \approx 210 \text{ GPa}$$

$$\nu_o = 0.28$$

$$\alpha_o = 1.3 \times 10^{-5} \text{ } ^\circ\text{C}^{-1}$$

$$r_o = 500 \text{ mm} = 0.5 \text{ m}$$

$$\therefore P = \frac{(2.3 \times 10^{-5} - 1.3 \times 10^{-5})(20)}{\frac{1}{2.1 \times 10^{11}} \left(\frac{0.5^2 + 0.3^2}{0.5^2 - 0.3^2} + 0.28 \right) + \frac{1}{7.3 \times 10^{10}} \left(\frac{0.3^2 + 0}{0.3^2 - 0} - 0.33 \right)}$$

$$= \frac{20 \times 10^{-5}}{\frac{1}{10^{10}} \left[\frac{1}{21} \left(\frac{0.34}{0.16} + 0.28 \right) + \frac{1}{7.3} (1 - 0.33) \right]}$$

$$\therefore P = \frac{20 \times 10^{-5} \times 10^{10}}{\frac{1}{21} (2.405) + \frac{1}{7.3} (0.67)}$$

$$= \frac{20 \times 10^5}{0.1145 + 0.0918}$$

$$\therefore P = 96.9462 \times 10^5 \text{ Pa}$$

$$\sigma_{\text{thermal}} = P \left(\frac{R^2 + r_i^2}{R^2 - r_i^2} \right)$$

$$= P \left(\frac{0.3^2 + 0}{0.3^2 - 0} \right)$$

$$\therefore \sigma_{\text{thermal}} = P = 9.69462 \times 10^6 \text{ Pa}$$

From classical equations, we get thermal stress in radial direction as $9.695 \times 10^6 \text{ N/m}^2$ (or Pa).

Conclusion:

Thus, we can infer that the FEA and classical calculations yield similar results for radial stress due to 20°C increase in surrounding temperature. And that the error is within 0.15% of the analytical solution.