

IM equation in $\alpha\beta$ reference frame

Induction motor equation derivation

- stator voltage equation
- stator flux linkage equation
- rotor voltage equation
- rotor flux linkage equation
- torque equation

Stator voltage equation

$$\begin{bmatrix} v_a \\ v_b \\ v_c \end{bmatrix} = \begin{bmatrix} R_s & 0 & 0 \\ 0 & R_s & 0 \\ 0 & 0 & R_s \end{bmatrix} \begin{bmatrix} i_a \\ i_b \\ i_c \end{bmatrix} + \frac{d}{dt} \begin{bmatrix} \lambda_a \\ \lambda_b \\ \lambda_c \end{bmatrix}$$

times $K_{abc2\alpha\beta}$ on both side of the equation and we get

$$\begin{bmatrix} v_\alpha \\ v_\beta \\ v_0 \end{bmatrix} = \begin{bmatrix} R_s & 0 & 0 \\ 0 & R_s & 0 \\ 0 & 0 & R_s \end{bmatrix} \begin{bmatrix} i_\alpha \\ i_\beta \\ i_0 \end{bmatrix} + K_{abc2\alpha\beta} \frac{d}{dt} (K_{\alpha\beta2abc} \begin{bmatrix} \lambda_\alpha \\ \lambda_\beta \\ \lambda_0 \end{bmatrix})$$

$$K_{abc2\alpha\beta} \frac{d}{dt} (K_{\alpha\beta2abc} \begin{bmatrix} \lambda_\alpha \\ \lambda_\beta \\ \lambda_0 \end{bmatrix}) =$$

$$K_{abc2\alpha\beta} \frac{d}{dt} (K_{\alpha\beta2abc}) \begin{bmatrix} \lambda_\alpha \\ \lambda_\beta \\ \lambda_0 \end{bmatrix} + K_{abc2\alpha\beta} K_{\alpha\beta2abc} \frac{d}{dt} \begin{bmatrix} \lambda_\alpha \\ \lambda_\beta \\ \lambda_0 \end{bmatrix}$$

because $K_{abc2\alpha\beta}$ and $K_{\alpha\beta2abc}$ are constant matrix and the inverse of each other, we have

$$K_{abc2\alpha\beta} \frac{d}{dt} (K_{\alpha\beta2abc}) \begin{bmatrix} \lambda_\alpha \\ \lambda_\beta \\ \lambda_0 \end{bmatrix} = 0, K_{abc2\alpha\beta} K_{\alpha\beta2abc} \frac{d}{dt} \begin{bmatrix} \lambda_\alpha \\ \lambda_\beta \\ \lambda_0 \end{bmatrix} = \frac{d}{dt} \begin{bmatrix} \lambda_\alpha \\ \lambda_\beta \\ \lambda_0 \end{bmatrix} \text{ thus, stator}$$

$$\text{voltage equation obtained } \begin{bmatrix} v_\alpha \\ v_\beta \\ v_0 \end{bmatrix} = \begin{bmatrix} R_s & 0 & 0 \\ 0 & R_s & 0 \\ 0 & 0 & R_s \end{bmatrix} \begin{bmatrix} i_\alpha \\ i_\beta \\ i_0 \end{bmatrix} + \frac{d}{dt} \begin{bmatrix} \lambda_\alpha \\ \lambda_\beta \\ \lambda_0 \end{bmatrix}$$

Stator flux linkage equation

$$\begin{bmatrix} \lambda_a \\ \lambda_b \\ \lambda_c \end{bmatrix} = \begin{bmatrix} L_{ms} & -\frac{1}{2}L_{ms} & -\frac{1}{2}L_{ms} \\ -\frac{1}{2}L_{ms} & L_{ms} & -\frac{1}{2}L_{ms} \\ -\frac{1}{2}L_{ms} & -\frac{1}{2}L_{ms} & L_{ms} \end{bmatrix} \begin{bmatrix} i_a \\ i_b \\ i_c \end{bmatrix} + \begin{bmatrix} L_{sleak} & 0 & 0 \\ 0 & L_{sleak} & 0 \\ 0 & 0 & L_{sleak} \end{bmatrix} \begin{bmatrix} i_a \\ i_b \\ i_c \end{bmatrix} +$$

$$L_{ms} \begin{bmatrix} \cos(\theta_r) & \cos(\theta_r + \frac{2}{3}\pi) & \cos(\theta_r - \frac{2}{3}\pi) \\ \cos(\theta_r - \frac{2}{3}\pi) & \cos(\theta_r) & \cos(\theta_r + \frac{2}{3}\pi) \\ \cos(\theta_r + \frac{2}{3}\pi) & \cos(\theta_r - \frac{2}{3}\pi) & \cos(\theta_r) \end{bmatrix} \begin{bmatrix} i_{ar} \\ i_{br} \\ i_{cr} \end{bmatrix}$$

times $K_{abc2\alpha\beta}$ on both sides of the equation

$$\begin{bmatrix} \lambda_\alpha \\ \lambda_\beta \\ \lambda_0 \end{bmatrix} = K_{abc2\alpha\beta} \begin{bmatrix} L_{ms} & -\frac{1}{2}L_{ms} & -\frac{1}{2}L_{ms} \\ -\frac{1}{2}L_{ms} & L_{ms} & -\frac{1}{2}L_{ms} \\ -\frac{1}{2}L_{ms} & -\frac{1}{2}L_{ms} & L_{ms} \end{bmatrix} K_{\alpha\beta2abc} \begin{bmatrix} i_\alpha \\ i_\beta \\ i_0 \end{bmatrix} +$$

$$\begin{bmatrix} L_{sleak} & 0 & 0 \\ 0 & L_{sleak} & 0 \\ 0 & 0 & L_{sleak} \end{bmatrix} \begin{bmatrix} i_\alpha \\ i_\beta \\ i_0 \end{bmatrix} +$$

$$K_{abc2\alpha\beta} L_{ms} \begin{bmatrix} \cos(\theta_r) & \cos(\theta_r + \frac{2}{3}\pi) & \cos(\theta_r - \frac{2}{3}\pi) \\ \cos(\theta_r - \frac{2}{3}\pi) & \cos(\theta_r) & \cos(\theta_r + \frac{2}{3}\pi) \\ \cos(\theta_r + \frac{2}{3}\pi) & \cos(\theta_r - \frac{2}{3}\pi) & \cos(\theta_r) \end{bmatrix} K_{\alpha\beta2abc} \begin{bmatrix} i_{\alpha r} \\ i_{\beta r} \\ i_{0r} \end{bmatrix}$$

Here, $K_{\alpha\beta2abc}$ is not the same as $K_{\alpha\beta2abc}$, the first one converts $\alpha\beta$ variables to rotor abc variables while the second one transforms $\alpha\beta$ variables to stator abc variables. Calculate these transformation, we get

$$\begin{bmatrix} \lambda_\alpha \\ \lambda_\beta \\ \lambda_0 \end{bmatrix} = \begin{bmatrix} \frac{3}{2}L_{ms} & 0 & 0 \\ 0 & \frac{3}{2}L_{ms} & 0 \\ 0 & 0 & 0 \end{bmatrix} \begin{bmatrix} i_{\alpha r} \\ i_{\beta r} \\ i_{0r} \end{bmatrix} + \begin{bmatrix} L_{sleak} & 0 & 0 \\ 0 & L_{sleak} & 0 \\ 0 & 0 & L_{sleak} \end{bmatrix} \begin{bmatrix} i_\alpha \\ i_\beta \\ i_0 \end{bmatrix} +$$

$$\begin{bmatrix} \frac{3}{2}L_{ms} & 0 & 0 \\ 0 & \frac{3}{2}L_{ms} & 0 \\ 0 & 0 & 0 \end{bmatrix} \begin{bmatrix} i_{\alpha r} \\ i_{\beta r} \\ i_{0r} \end{bmatrix}$$

Stator flux linkage equation is done.

Rotor voltage equation

Now we devrive rotor vlotage equation

$$\begin{bmatrix} v_{ar} \\ v_{br} \\ v_{cr} \end{bmatrix} = \begin{bmatrix} R_r & 0 & 0 \\ 0 & R_r & 0 \\ 0 & 0 & R_r \end{bmatrix} \begin{bmatrix} i_{ar} \\ i_{br} \\ i_{cr} \end{bmatrix} + \frac{d}{dt} \begin{bmatrix} \lambda_{ar} \\ \lambda_{br} \\ \lambda_{cr} \end{bmatrix}$$

Times $K_{rabc2\alpha\beta}$ on both sides

$$\begin{bmatrix} v_{\alpha r} \\ v_{\beta r} \\ v_{0r} \end{bmatrix} = \begin{bmatrix} R_r & 0 & 0 \\ 0 & R_r & 0 \\ 0 & 0 & R_r \end{bmatrix} \begin{bmatrix} i_{\alpha r} \\ i_{\beta r} \\ i_{0r} \end{bmatrix} + K_{rabc2\alpha\beta} \frac{d}{dt} \left(K_{\alpha\beta2rabc} \begin{bmatrix} \lambda_{\alpha r} \\ \lambda_{\beta r} \\ \lambda_{0r} \end{bmatrix} \right)$$

Calculate this with matlab, we obtain

$$\begin{bmatrix} v_{\alpha r} \\ v_{\beta r} \\ v_{0r} \end{bmatrix} = \begin{bmatrix} R_r & 0 & 0 \\ 0 & R_r & 0 \\ 0 & 0 & R_r \end{bmatrix} \begin{bmatrix} i_{\alpha r} \\ i_{\beta r} \\ i_{0r} \end{bmatrix} + \omega_r \begin{bmatrix} 0 & 1 & 0 \\ -1 & 0 & 0 \\ 0 & 0 & 0 \end{bmatrix} \begin{bmatrix} \lambda_{\alpha r} \\ \lambda_{\beta r} \\ \lambda_{0r} \end{bmatrix} + \frac{d}{dt} \begin{bmatrix} \lambda_{\alpha r} \\ \lambda_{\beta r} \\ \lambda_{0r} \end{bmatrix}$$

Rotor flux linkage equation

$$\begin{bmatrix} \lambda_{ar} \\ \lambda_{br} \\ \lambda_{cr} \end{bmatrix} = \begin{bmatrix} L_{ms} & -\frac{1}{2}L_{ms} & -\frac{1}{2}L_{ms} \\ -\frac{1}{2}L_{ms} & L_{ms} & -\frac{1}{2}L_{ms} \\ -\frac{1}{2}L_{ms} & -\frac{1}{2}L_{ms} & L_{ms} \end{bmatrix} \begin{bmatrix} i_{ar} \\ i_{br} \\ i_{cr} \end{bmatrix} + \begin{bmatrix} L_{rleak} & 0 & 0 \\ 0 & L_{rleak} & 0 \\ 0 & 0 & L_{rleak} \end{bmatrix} \begin{bmatrix} i_{ar} \\ i_{br} \\ i_{cr} \end{bmatrix} +$$

$$L_{ms} \begin{bmatrix} \cos(\theta_r) & \cos(\theta_r - \frac{2}{3}\pi) & \cos(\theta_r + \frac{2}{3}\pi) \\ \cos(\theta_r + \frac{2}{3}\pi) & \cos(\theta_r) & \cos(\theta_r - \frac{2}{3}\pi) \\ \cos(\theta_r - \frac{2}{3}\pi) & \cos(\theta_r + \frac{2}{3}\pi) & \cos(\theta_r) \end{bmatrix} \begin{bmatrix} i_{as} \\ i_{bs} \\ i_{cs} \end{bmatrix} \quad \text{Times } K_{rabc2\alpha\beta} \text{ on}$$

both sides, we get

$$\begin{bmatrix} \lambda_{\alpha r} \\ \lambda_{\beta r} \\ \lambda_{0r} \end{bmatrix} = K_{rabc2\alpha\beta} \begin{bmatrix} L_{ms} & -\frac{1}{2}L_{ms} & -\frac{1}{2}L_{ms} \\ -\frac{1}{2}L_{ms} & L_{ms} & -\frac{1}{2}L_{ms} \\ -\frac{1}{2}L_{ms} & -\frac{1}{2}L_{ms} & L_{ms} \end{bmatrix} K_{\alpha\beta2rabc} \begin{bmatrix} i_{\alpha r} \\ i_{\beta r} \\ i_{0r} \end{bmatrix} +$$

$$\begin{bmatrix} L_{rleak} & 0 & 0 \\ 0 & L_{rleak} & 0 \\ 0 & 0 & L_{rleak} \end{bmatrix} \begin{bmatrix} i_{\alpha r} \\ i_{\beta r} \\ i_{0r} \end{bmatrix} +$$

$$L_{ms} K_{rabc2\alpha\beta} \begin{bmatrix} \cos(\theta_r) & \cos(\theta_r - \frac{2}{3}\pi) & \cos(\theta_r + \frac{2}{3}\pi) \\ \cos(\theta_r + \frac{2}{3}\pi) & \cos(\theta_r) & \cos(\theta_r - \frac{2}{3}\pi) \\ \cos(\theta_r - \frac{2}{3}\pi) & \cos(\theta_r + \frac{2}{3}\pi) & \cos(\theta_r) \end{bmatrix} K_{\alpha\beta2abc} \begin{bmatrix} i_{\alpha s} \\ i_{\beta s} \\ i_{0s} \end{bmatrix}$$

Note this mutual inductance matrix is the transpose of the previous one in stator flux equation, not the same!

Calculate this with matlab

$$\begin{bmatrix} \lambda_{\alpha r} \\ \lambda_{\beta r} \\ \lambda_{0r} \end{bmatrix} = \begin{bmatrix} \frac{3}{2}L_{ms} & 0 & 0 \\ 0 & \frac{3}{2}L_{ms} & 0 \\ 0 & 0 & 0 \end{bmatrix} \begin{bmatrix} i_{\alpha r} \\ i_{\beta r} \\ i_{0r} \end{bmatrix} + \begin{bmatrix} L_{rleak} & 0 & 0 \\ 0 & L_{rleak} & 0 \\ 0 & 0 & L_{rleak} \end{bmatrix} \begin{bmatrix} i_{\alpha r} \\ i_{\beta r} \\ i_{0r} \end{bmatrix} +$$

$$\begin{bmatrix} \frac{3}{2}L_{ms} & 0 & 0 \\ 0 & \frac{3}{2}L_{ms} & 0 \\ 0 & 0 & 0 \end{bmatrix} \begin{bmatrix} i_{\alpha s} \\ i_{\beta s} \\ i_{0s} \end{bmatrix}$$

Thus rotor flux equation obtained.

Torque equation

According to the book Analysis of electric machinery and drive system. We know torque is

$$T_e = \frac{\partial W_c(\mathbf{i}, \theta_{rm})}{\partial \theta_{rm}} = \frac{p}{2} \frac{\partial W_c(\mathbf{i}, \theta_r)}{\partial \theta_r}$$

$$W_c = W_f = \frac{1}{2}(\mathbf{i}_{abcs})^T \mathbf{L}_s \mathbf{i}_{abcs} + (\mathbf{i}_{abcs})^T \mathbf{L}'_{sr} \mathbf{i}'_{abcr} + \frac{1}{2}(\mathbf{i}'_{abcr})^T \mathbf{L}'_r \mathbf{i}'_{abcr}$$

since \mathbf{L}_s and \mathbf{L}'_r are not functions of θ_r , take of derivative we have

$$\mathbf{T}_e = \left(\frac{p}{2}\right)(\mathbf{i}_{abcs})^T \frac{\partial}{\partial \theta_r} [\mathbf{L}'_{sr}] \mathbf{i}'_{abcr} \quad \text{This is the abc frame, now we change into } \alpha\beta \text{ reference frame}$$

$$\mathbf{T}_e = \left(\frac{p}{2}\right)(K_{\alpha\beta 2abc} K_{abc 2\alpha\beta} \mathbf{i}_{abcs})^T \frac{\partial}{\partial \theta_r} [\mathbf{L}'_{sr}] (K_{\alpha\beta 2rabc} K_{rabc 2\alpha\beta} \mathbf{i}'_{abcr})$$

$$\mathbf{T}_e = \left(\frac{p}{2}\right) \mathbf{i}_{\alpha\beta 0}^T K_{\alpha\beta 2abc}^T \frac{\partial}{\partial \theta_r} [\mathbf{L}'_{sr}] K_{\alpha\beta 2rabc} \mathbf{i}'_{abcr}$$

calculate with matlab and we get

$$\mathbf{T}_e = -\frac{3}{2} L_m (i_{\alpha s} i_{\beta r} - i_{\alpha r} i_{\beta s})$$