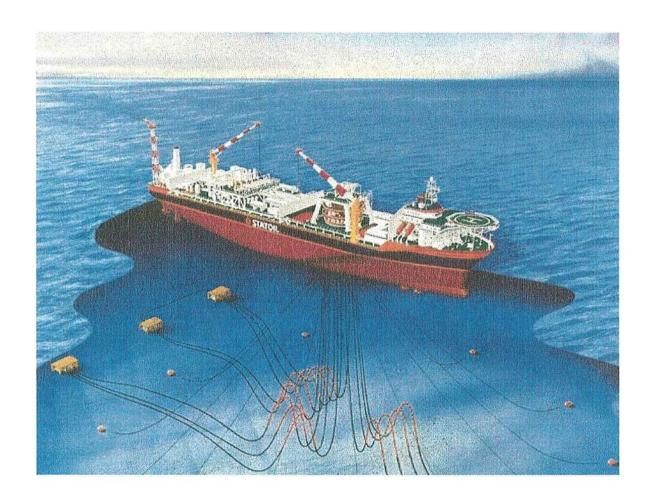


# **NORNE**



Geological and Petrophysical Report Norne Field PL 128 Wells 6608/10-B-4 AH and BH NOR-2002-06R







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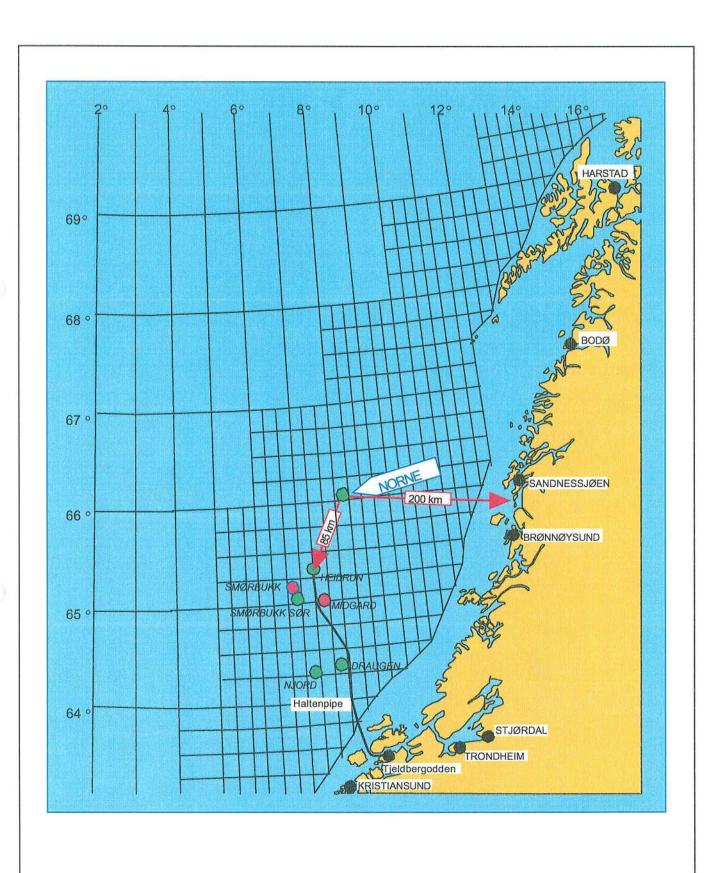
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### 1 Summary

The objective of well 6608/10-B-4 AH was as a pilot hole for well 6608/10-B-4 BH. This pilot hole gave information about the present OWC and depths to different formation tops in the D-segment, information vital for an exact placement of well 6608/10-B-4BH. It also added to a better understanding of the pressure balance and regimes in the D-segment by means of MDT pressure testing. Another objective of the 12 ½" section was to land the wellpath in the target, easing the drilling of the 8 ½ " sections, and to ensure that at least 10m MD of good quality Garn Formation sandstone was available for perforating through the 9 5/8" liner. The pilot well 6608/10-B-4 AH met its objectives.

The primary objective of well 6608/10-B-4 BH was to drill a horizontal section of 600m within the Ile2 Formation. Data from the pilot well was used, attempting to place the horizontal section approximately 40m TVD over the present day OWC. The OWC was thought to be penetrated at 2653m TVD MSL. The wellpath was landed at 2614m TVD MSL and a horizontal section of 483m MD in the upper parts of the Ile -2 Formation was achieved. Later petrophysical evaluation of wireline logs show an OWC at 2678m TVD MSL. The well was perforated in Garn -3 and Ile -2 Formations and a gas lift valve was installed over the Garn perforations. The heal section of the well shall be available for perforating after gas has been produced from the top of the structure. The well is currently (Sep. 2001) producing oil from Ile-2 at a rate of 5100-5200 m $^3$ /day, with a GOR of 106-108.

Both wells were logged with LWD. One wireline run in the pilot well, 6608/10-B-4 AH, to ensure high quality data and pressure points. Both 12 ¼" and 8 ½" sections were drilled with oil based mud, which ensured proper hole and thus data quality.

# 2 Drilling Results

### 2.1 12 1/4" section

The well was kicked off underneath the 13 3/8" casing in 6608/10-B-4 H

The motor assy performed good in the upper part of the section, following the wellpath nicely in the first bitrun. In the second bitrun, the well was accidentally sidetracked on the low side at a ledge at 2020m MD. This gave a bad start for the steering of the rest of the section. The wellpath stayed on the low side of the plan for a long time. The formations were difficult to steer in, the motor kept stalling out, causing lost toolface. Slow steering as well, ROP of 5-10m/hr. Eventually, the wellpath came back on the plan track. Then after evaluating the steering so far and the wellpath ahead, the desicion was made to POOH and mobilize a 12 1/4" RSS. The used bit came out 3/16" undergauge, this migth explain some of the difficulties seen steering the last part. RIH with 12 1/4" PowerDrive BHA. Had some initial problems in setting the tool. Eventually, the tool performed well. The problems related to mud losses are commented upon in ch. 6.

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#### 2.2 8 1/2" section 6608/10-B-4 AH

The section was drilled in one bitrun without any significant problems. Details are given in the section report.

### 2.3 8 1/2" section 6608/10-B-4 BH

There were no major problems with steerability or ROP. At 90deg incl. the assembly had a tendence to build, and some adjustments had to be made in order to keep the wellpath in the Ile-2 Formation. Details are given in the section report.

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# 3 Petrophysical Evaluation

### 3.1 General well and mud data

NORNE	6608/10-B-4 AH / BH	12.06.2001 - 18.07.2001
OPERATION TYPE	Measurement while drilling (N	MWD) / Electric Wireline (EWL)
STATOIL ENGINEERS	D. Tuppen	/ O. W. Lind
LOGGING COMPANY	Sperry Sun (MWD) / Baker Hughes	Inteq (MWD) / Schlumberger (EWL)

LOGGING ENGINEER		Lyngre, O. Fossli, M. Økso Haarberg (Sperry Sun) ui, B. Boddy, G. Wattley (S	1
WELI	LDATA M. AISSO		DATA
Well Type	Water Injector	Туре	CARBO SEA OBM
Block	6608/10	Density	1,30 g/cc
Template Slot	B-4 H	Funnel Viscosity	73 mPa s
Rig	Borgland Dolphin	Fluid Loss [HTHP]	2.2 ml
UTM East	7 322 136.39 m N	Salinity	95 700 mg/l
UTM North	457 114.16 m E	Barite	-
Geo East	66° 00' 55,4733"	Other, Kcl	-
Geo North	08° 03' 16.3715"	Ca++	-
RKB	31 m	Mg++	-
Water Depth	376 m	Oil /Water ratio	73 / 27
Max Deviation	72.9° / 93.0°	Solids	15.2 vol %
@ Depth	2221 / 4436 m MD RKB	Rm	n/a
Avg Dev in Reservoir	~70° / ~88°	Rmf	n/a
Avg Azim in Reservoir	~70° / ~70°	Rmc	n/a
TD driller	3900 / 4346 m MD RKB		
TD logger	Not tagged	Bottomhole Temp	perature (From MDT)
Csg shoe Driller	3271.2 m MD RKB	T [deg C]	101.3 DegC
Csg shoe Logger	3271.2 m MD RKB	Depth	3837 m MD RKB
Csg	9 5/8"	Time	11.07.2001

Table I: General well and mud data

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# 3.2 Logging Programme

D	ate	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	Interval m MD RT				
Start	Stop	Tool Combination	Run	Bit size	Top	Bot	
12-jun-2001	17-jun-2001	DIR-FE-NUKE	Sperry Sun	1	12.25	1257	2094
19-jun-2001	24-jun-2001	DIR-GR	Sperry Sun	2	12.25	2020	2884
25-jun-2001	29-jun-2001	DIR-FE-NUKE	Sperry Sun	3	12.25	2884	3280
3-jul-2001	06-jul-2001	DIR-FE-NUKE	Sperry Sun	4	8.5	3280	3900
12-jul-2001	15-jul-2001	DIR-FE-NUKE	Sperry Sun	5	8.5	3215	4091
15-jul-2001	18-jul-2001	DIR-FE-NUKE	Sperry Sun	6	8.5	4091	4347

Table II: Logging While Drilling runs

Da	ate					al m MD RT	
Start	Stop	Tool Combination	Company	Bit size	Top Bot		
8-jul-2001	11-jul-2001	MDT-PEX-DSI-AIT-GR	Schlumberger	8.5 "	3164	3552	
11-jul-2001	12-jul-2001	MDT-PEX-DSI-AIT-GR	Schlumberger	8.5 "	3515	3890	

Table III: Wireline Logging runs

Spliced curve	Original curve	Depth interval [m MD RKB]	Comments
		6608/10-B-4AH	•
GR	SGRC	1307 - 3287	Sperry Sun MWD data
	GR	3287 - 3870	Schlumberger WL data
	SGRC	3870 - 3892.4	Sperry Sun MWD data
RT	SEDP	1307 - 3267	Sperry Sun MWD data
	RT	3274 - 3892.2	Sperry Sun MWD data
RHOB	SBD2	1320 - 3264,2	Sperry Sun MWD data
	RHOZ	3273 – 3867	Schlumberger WL data
	SBD2	3867 - 3919.6	Sperry Sun MWD data
NPHI	SPLF	1300 - 3272	Sperry Sun MWD data
	NPHI	3272 - 3870.5	Schlumberger WL data
	SPLF	3870.5 - 3919,6	Sperry Sun MWD data
		6608/10-D-4 BH	
GR	SGRC	1307 - 4336,3	Sperry Sun MWD data
RT	SEDP	1307 - 4334	Sperry Sun MWD data
RS	SEXP	1307 - 4334	Sperry Sun MWD data
RHOB	SBD2	1320 - 4329.3	Sperry Sun MWD data
NPHI	SPLF	1300 - 4325.5	Sperry Sun MWD data

Table IV Log splice, OpenWorks database

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Porosity calculations on Norne are based on the density log by using following equation:

$$\phi_{density} = \frac{\rho_{matrix} - \rho_{bulk}}{\rho_{matrix} - \rho_{fluid}}$$

This formula gives total porosity, based on correlation from helium core porosity from cored wells.

Table VII shows the parameters used for the equation.  $\rho_{fluid}$  is iterated from SXO, mudweight and salinity using the formula:

$$\rho_{fluid} = S_{XO} \cdot \rho_{formationwater} + (1 - S_{XO}) \cdot \rho_{mudfiltate}$$

Permeability was calculated from a log-linear correlation of porosity and permeability from the following equation:

$$K_{\log} = 10^{\left(a \cdot \phi_{density} + b\right)}$$

Water saturation is calculated using Archies equation. Rt is taken from the Sperry Sun Deep Phase Shift Resistivity from MWD log.

$$SW = \left(\frac{a}{\left(\phi_{density}\right)^m} \cdot \frac{R_w}{R_t}\right)^{\left(\frac{1}{n}\right)}$$

The model used for the reservoir rock properties table is as follows:

а	0.1
m	1.84
n	2.2 for Garn 3, Ile 2, Tilje
	1.84 for Garn 1, Garn 2, Not, Ile 3, Ile 1, Åre.
	2.02 for Tofte
Rw	0.054 Ohmm at 98°C
Rt	Sperry Sun Deep Phase Shift Resistivity from MWD
	Schlumberger RT from AIT WL logging

Table V: Reservoir rock properties used in calculations

The oil-water contact has rised from orginal 2692.3 m TVD MSL to 2678 m TVD MSL. The gas-oil contact was observed at 2566 m TVD MSL.

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Shale volume (VSH) is estimated from the minimum method, using the minimum og VSH from the GR-log and DensityNeutron based on clean sand and shale picks.

$$VSH = MIN \left\{ \frac{NPHI_{env} - \phi \cdot H_f}{\phi_{shale}}, \frac{GR - GR_{\min}}{GR_{\max} - GR_{\min}} \right\}$$

Net sand is calculated from permeability and VSH cut-off. Following parameters are used:

Fluid	Permeability cut-off	Shale content cut-off
	(mD)	(Frac.)
Gas	<0.1	>0.3
Oil/ Water	<1.0	>0.3

Table VI: Cut-off values

The petrophysical properties is slightly different from well C-4 H, but almost equal to the nearest well, F-3 H. Ile 1 and lower Tofte 3 and Tofte 2 seems to have lower porosity / permeability compared to C-4 H, but theses zones are equal to well F-3 H.

The initial oil-water contact was found at 2593 m TVD MSL. The discrepancy between log depth and official depth (2688.5 m TVD MSL) is due to depth error incurred during drilling.

The rise in the oil-water level to 2678 m TVD MSL gives a rise of 15 meters, which is less than the expected 30-40 meters rise. This indicate that the water-rise at Norne is more complex than expected.

The following water saturations and expected changes were found.

Formation	Initial water saturation (taken from well C-4 H) (frac.)	Watersaturati on in well B-4 BH  (frac.)	Different in water saturaion (frac.)	Comment
Tofte 2	0.40	0.44	0.04	OWC between
Tofte 1.2	0.24	0.52	-0.28	Tofte 2 and
Tofte 1.1	0.30	0.69	-0.39	Tofte 1.2

Table VII: Water saturations in flooded zones.

Residual oil saturation found from SCAL gives a saturation of 0.12, which indicate that Tofte 1 Formation is not fully flooded.

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Т	<sup>T</sup> 6608/10-B-4 AH												
Zone	Fluid phase	A	М	N	GR MIN	GR MAX	PHIN SH	RHO MA	RHO FL	KA KLO GH	KB KLO GH	KA KLO GV	KB KLOG V
GARN3	Gas	1	1.84	2,20	60	150	0.5	2.67	0.23	-0.611	11.14	-0.823	11.04
GARN2	Gas	1	1.84	2,20	60	160	0.5	2.67	0,22	-3.518	21.69	-5.420	27.71
	Oil	1	1.84	2,20	60	160	0.5	2.67	0.83	-3.518	21.69	-5.420	27.71
GARN1	Oîl	1	1.84	1,84	60	170	0.5	2.67	0.86	-3.518	21.69	-5.420	27.71
NOT	Oil	1	1.84	1,84	80	180	0.5	2.67	0.92	-3.518	21.69	-5.420	27,71
ILE3	Oil	1	1.84	1,84	50	150	0,5	2.67	0,81	-3.518	21.69	-6.281	32.13
iLE2	Oil	1	1.84	2,20	50	150	0.5	2.67	0.79	-0.898	13.43	-6.281	32.13
ILEI	Oil	1	1.84	1,84	50	150	0.5	2.67	0.81	-0.898	13.43	-6.281	32.13
TOFTE4	Oil	1	1.84	2,02	50	150	0,5	2.67	0.81	-2.026	15.99	-6.281	32,13
TOFTE3	Oil	1	1.84	2,02	50	130	0.5	2.65	0.80	-4.370	25.07	-6.281	32.13
TOFTE2	Oil	1	1.84	2,02	50	130	0.5	2.65	0.87	-4.370	25.07	-6.281	32.13
TOFTE1	Water	ı	1.84	2,02	50	130	0.5	2.71	0.93	-2.536	19.49	-4.670	26.30
TILJE4	Water	1	1.84	2,20	50	140	0.5	2.67	0.98	-2.536	19.49	-4.670	26.30
TILJE3	Water	- 1	1.84	2,20	50	140	0.5	2.67	0.98	-1.946	16.44	-4.670	26.30
TILJE2	Water	1	1.84	2,20	50	140	0.5	2.67	1.0	-2.536	19.49	-4.670	26.30
TILJE1	Water	1	1.84	2,20	50	140	0.5	2,67	0,99	-2,536	19.49	-4.670	26.30
ÅRE	Water	1	1.84	2,20	NaN	NaN	0.5	2.67	NaN	-2.536	19.49	-4.670	26.30
					6	608/	10-B	-4 BI	1				
Zone	Fluid phase	A	М	N	GR MIN	GR MAX	PHIN SH	RHO MA	RHO FL	KA KLO GH	KB KLO GH	KA KLO GV	KB KLOG V
GARN3	Gas	1	1,84	2,20	60	150	0.5	2.67	0.23	-0,611	11.14	-0.823	11.04
GARN2	Gas	. 1	1.84	2,20	60	160	0.5	2.67	0.22	-3.518	21.69	-5.420	27,71
1	Oil	- 1	1.84	2,20	60	160	0.5	2.67	0.83	-3.518	21.69	~5,420	27.71
GARN1	Qil	1	1.84	1,84	60	180	0.5	2.67	0.86	-3.518	21.69	-5.420	27.71
T <sub>NOT</sub>	Oil	1	1.84	1,84	60	160	0.4	2.67	0.92	-3.518	21.69	-5.420	27,71
ILE3	Oil	l	1.84	1,84	60	150	0.4	2.67	0.81	-3.518	21.69	-6.281	32.13
ILE2	Oil	1	1.84	2,20	60	150	0.4	2,67	0.79	-0.898	13.43	-6.281	32.13

Table VIII: Parameters used in petrophysical calculations

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				6608/	10-B-4	AH		_	_		
Formation	Top (m MD RKB)	Bot (m MD RKB)	Thic. (m)	Top (m TVD MSL)	Bot (m TVD MSŁ)	Isoc. (m)	NTG (frac.)	SW (frac.)	VSH (frac.)	Net Poro (frac.)	Net Arit. H. Perm (mD)
Garn3	3196.0	3231.0	35.0	2575.2	2586.9	11.8	0.989	0.133	0.165	0.240	214.6
Garn2	3231.0	3282.0	51.0	2586.9	2601.1	14.2	0.740	0.193	0.170	0.230	146.9
Garn1	3282.0	3328.5	46.5	2601.1	2611.7	10.5	0.668	0.308	0.287	0.196	9.8
Not	3328.5	3368.0	39.5	2611.7	2618.0	6.4	0.031	0.482	0.316	0.179	2.7
lle3.2	3368.0	3464.0	96.0	2618.0	2630.4	12.3	0.881	0,212	0.142	0.238	98.3
Ile3.1	3464.0	3515.5	51.5	2630.4	2640.9	10.5	0.929	0.189	0.086	0.244	79.7
Ile2.2.2	<b>35</b> 15.5	3551.0	35.5	2640.9	2649.7	8.8	0.986	0.119	0.052	0.276	802.5
lle2.2.1	3551.0	3569.0	18.0	2649.7	2654.7	5.0	1.000	0.142	0.027	0.272	867.6
lle2.1	3569.0	3590.5	21.5	2654.7	2661.0	6.3	1.000	0.167	0.042	0.283	937.7
Ile1	3590.5	3602.5	12.0	2661.0	2664.8	3.8	0.967	0.174	0.092	0.208	319.9
Tofte4	3602.5	3621.0	18.5	2664.8	2671.1	6.3	1.000	0.236	0.186	0.232	64.5
Tofte3.4.2	3621.0	3636.0	15.0	2671.1	2676.6	5.5	1.000	0.092	0.033	0.300	1621.3
Tofte3.4.1	3636.0	3649.5	13.5	2676.6	2681.9	5.3	1.000	0.093	0.050	0.291	941.9
Tofte3.3.2	3649.5	3657.0	7.5	2681.9	2684.9	3.0	1.000	0.123	0.050	0.278	414.4
Tofte3.3.1	3657.0	3671.0	14.0	2684.9	2690.6	5.7	0.956	0.162	0.078	0.263	215.7
Tofte3.2	3671.0	3692.5	21.5	2690.6	2700.3	9.7	1.000	0.229	0.093	0.260	149.4
Tofte3.1	3692.5	3700.0	7.5	2700.3	2703.7	3.4	1.000	0.320	0.120	0.243	57.8
Tofte2	3700.0	3710.5	10.5	2703.7	2709.0	5.2	0.976	0.441	0.125	0.224	42.1
Tofte1.2	3710.5	3731.5	21.0	2709.0	2719.6	10.6	0.929	0.516	0.034	0.262	1261.7
Tofte1.1	3731.5	3741.0	9.5	2719.6	2724.7	5.1	0.804	0.694	0.063	0.264	1160.3
Tilje4	3741.0	3758.0	17.0	2724.7	2733.8	9.2	0.823	0.823	0.200	0.201	271.0
Tilje3	3758.0	3796.0	38.0	2733.8	2756.9	23.0	0.842	0.873	0.079	0.246	486.9
Tilje2	3796.0	3850.5	54.5	2756.9	2792.5	35.6	0.579	0.911	0.210	0.188	182.0
Tilje1	3850.5	3888.0	37.5	2792.5	2818.8	26.3	0.811	0.915	0.050	0.259	961.0
Aare	3888.0	3900.0	12.0								
	I			6608/	/10-B-4	вн		· · · · · · · · · · · · · · · · · · ·			'
Formation	Top (m MD RKB)	Bot (m MD RKB)	Thic.	Top (m TVD MSL)	Bot (m TVD MSL)	Isoc.	NTG (frac.)	SW (frac.)	VSH (frac.)	Net Poro (frac.)	Net Arit. H. Perm (mD)
Garn3	3196.0	3231.0	35.0	2575.2	2586.9	(m) 11.8	0.995	(frac.) 0.137	0.166	0.228	204.1
Garn2	3231.0	3282.0	51.0	2586.9	2601.2	14.3	0.333	0.137	0.100	0.248	223.7
Garn1	3282.0	3328.5	46.5	2601.2	2612,4	11.2	0.777	0.260	0.319	0.232	78.3
Not	3328.5	3352.5	24.0	2612.4	2617.8	5.4	0.046	0.237	0.046	0.189	9.8
Ite3.2	3352.5	3564.5	212.0	2617.8	2635.1	17.3	0.040	0.185	0.052	0.169	262.2
lie3.1	3564.5	3751.0	186.5	<del>                                     </del>	2644.2	9.1	0.799	0.201	0.032	0.258	178.0
			596.0	1			0.799	0.105	0.021	0.294	1195.6
lle2	3751.0	4347.0	0.080	2044.2	2647.1	2.9	0.841	0.105	U.000	0.284	1 (90.0

**Table IX: Statistics for Petrophysical Evaluation** 

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#### **Stratigraphic Tops** 4

Stratigraphic Top	Depth,	Prognosis	Actual, m	Difference,	UTM N	UTM E
• • •	m MD	m TVD	TVD	m TVD		
		MSL	MSL			
		660	8/10-B-4 AH	•	•	
Kai Formation	1369,0	1319,0	1321,0	+2 m	7322166,5	456974,75
Brygge Formation	1618,0	1563,0	1559,8	-3,2 m	7322224,0	456940,6
Brygge Tuff Mbr	1700,5	1643,0	1637,2	-5,8 m	7322252,0	456938,25
Tare Formation	1912,5	1823,0	1824,5	+1,5 m	7322351,0	456942,5
Tang Formation	1977,5	1880,0	1878,9	-1,1 m	7322385,0	456951,88
Springar Formation	2025,0	1911,0	1917,6	+6,6 m	7322411,5	456959,88
Lyr Formation	2816,0	2371,0	2375,8	+4,8 m	7322956,5	457271,31
Spekk Formation	2857,0	2407,0	2395,4	-11,6 m	7322984,5	457294,16
Melke Formation	2860,0	2420,0	2396,9	-23,1 m	7322986,5	457295,88
Garn - 3	3196,0	2553,0	2544,2	-8,8 m	7323160,5	457539,78
Garn - 2	3231,0	2561,0	2555,9	-5,1 m	7323175,5	457569,13
Garn - 1	3282,0	2572,0	2570,1	-1,9 m	7323196,0	457613,66
Not Formation	3328,0	2582,0	2580,6	-1,4 m	7323213,0	457655,63
Ile - 3	3368,0	2588,0	2587,0	-1 m	7323226,5	457692,13
Ile - 2	3569,0	2605,0	2609,9	+4,9 m	7323291,0	457878,38
Ile - 1	3590,5	2615,0	2630,0	+15 m	7323299,5	457897,19
Tofte - 4	3602,5	2618,0	2633,8	+15,8 m	7323304,0	457907,47
Tofte - 3	3671,0	2625,0	2640,1	+15,1 m	7323331,0	457964,81
Tofte - 2	3700,0	2649,0	2672,7	+23,7 m	7323341,5	457988,5
Tofte - 1	3710,5	2654,0	2677,9	+23,9 m	7323345,0	457996,91
Tilje - 4	3741,0	2667,0	2693,6	+26,6 m	7323355,0	458021,10
Tilje - 3	3758,0	2677,0	2702,8	+25,8 m	7323360,5	458034,38
Tilje - 2	3796,0	2695,0	2725,8	+30,8 m	7323371,0	458062,59
Tilje - 1	3850,0	2728,0	2761,5	+33,5 m	7323384,5	458101,47
Åre Formation	3888,0	2755,0	2787,8	+32,8 m	7323392,5	458126,94
TD	3900,0	N/A	2796,4	N/A	7232395,0	458134,91
		660	8/10-B-4 BH			
Ile - 2	3750,0	2605,0	2614,0	+9 m		
TD	4346,0	2600,0	2615,9	N/A	7323548,21	458613,51

#### 5 **Geological Summary**

#### 5.1 **Nordland Group to Rogaland Group**

The Nordland, Hordaland and Rogaland Groups were drilled before the geologists arrived at the rig. Please refer to BHI's mudlogging report for lithological descriptions.

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# 5.2 Shetland Group

#### **Springar Formation**

The Springar Formation consists of claystone with limestone stringers.

The claystone varies between medium dark grey to dark grey and greenish grey. It is mostly firm, blocky to subblocky in shape, non to sligthly calcareous, and with traces of pyrite and glauconite.

The limestone is brownish grey to white to yellowish brown. It is mostly firm, blocky and argillaceous

### 5.3 Cromer Knoll Group

#### Lyr Formation

The Lyr Formation is recognized by a marked decrease in GR readings and corresponding increase in resistivity readings compared to the Springar Formation

The Lyr Formation consists predominantly of claystone with some limestone and siltstone stringers.

The claystone varies from medium grey, dark grey to greenish grey. It is soft to firm and varies from blocky to subblocky in shape. Mostly non calcareous.

The limestone varies from mostly medium brownish gray to white and yellowish brown. It is firm to hard in hardness and mostly blocky to subblocky in shape.

The siltstone varies from dark yellowish brown to dark grey.

#### 5.4 Viking Group

#### **Spekk Formation**

The Spekk Formation is recognized by a sharp increase in GR readings, up to 220-230API. The GR readings stay high throughout the thin Spekk Formation.

#### Melke Formation

The Melke Formation is recognized by a decrease in GR readings from what seen in the Spekk Formation. Still, the GR readings are at least 1 decimal of the scale (15 API) higher than what seen in the Springar and Lyr Formations.

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The claystone is dark grey to greenish grey, firm, subblocky to blocky, sligthly calcareous, silty with traces of limestone and dolomite.

The limestone is moderately brownish white with occational black specks. It is occationally white or yellowish brown, blocky, firm and argillaceous.

The sandstone is dark yellow to ligth brown with loose quartz grains in silty clay matrix. The grains are well to moderately sorted, very fine to coarse, subangular to subrounded and generally moderately sorted.

#### 5.5 **Fangst Group**

The Fangst Group in this section is represented by the Garn Formation. It is recognized by a sharp decrease to low GR readings coinciding with high resistivity readings and a dens/neut crossover representing gas filled clean sandstones.

#### **Garn Formation**

The Garn Fm is a coarsening upward sequence which is initiated from the top of the Not Fm. The boundary between the Garn and the Not Fm is diffuse and is picked by the first appearence of silty sand layers.

The sandstone consists of clear to light brownish quartz grains, in places in a light grey calcite matrix. The grains are very fine to medium sized, well sorted, subangular to subrounded. The sandstone often grades to siltstone which is medium grey to grey, soft to firm, subblocky, micropyritic and slightly calcareous.

The claystone is moderately to dark grey, firm, blocky, calcareous.

The limestone is ligth grey to grey, firm to hard, blocky, microcrystalline and argillaceous.

#### **Not Formation**

The claystone is moderate to dark brownish grey, firm to moderately hard, blocky to platy. It contains calcite rich zones, traces of mica and carbonaceous materias. It is silty in places.

#### **Ile Formation**

The Ile Formation consists of sandstone with occasional limestone and claystone interbeds The sandstone consists of clear to light brown transparent quartz grains with a very fine to fine grainsize. The grains are moderately to well sorted, subrounded in most samples. The sandstone varies from loose to firm blocks and lumps. Calcite cementation is seen in some

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samples, as is a moderate grey clay matrix. Silica cement is also occasionally observed generating hard aggregates. Traces of mica, pyrite and glauconite is seen on occasions.

The claystone is varicolored, grey, brownish grey and brownish black. Claystone fragments are blocky to platy, firm, in places hard and in places crumbly. The claystone is calcareous. It contains traces of mica, pyrite and glauconite. Silty developments are seen throughout the samples.

The limestone is grey to bluish grey. On occations brownish fragments are seen. The limestone is firm to hard, microcrystalline and argillaceous.

## 5.6 Båt Group

The Båt Group is represented by the Tofte, Tilje and Åre Formations in B-4AH. TD in B-4AH is set in the top of the Åre Fm. The Båt Group is not represented in B-4BH.

#### **Tofte Formation**

The Tofte Formation consists of sandstone and claystone interbeds with occasional limestone. The sandstone consists of light grey to clear quartz grains in a grey clay matrix. Large amounts of calcite cementation is seen in some of the samples. The grains are fine to medium sized and moderately to well sorted. There is often an abundance of loose clear fine to medium quartz grains seen in the samples.

The claystone is moderately to dark brownish grey, firm, platy occationally blocky. It contains calcite and traces if mica, silt and sand

The limestone is light grey to blue grey, brown grey on occasions. It is crumbly to firm, hard in places, microcrystalline and locally sacroidal. The limestone is locally very arenaceous and argillaceous grading to cemented sandstones og marly clays.

#### Tilje Formation.

The Tilje Fm consists of sandstone and claystone interbeds with occasional limestone stringers. Occasionally highly carbonaceous layers are observed. These are thin and rarely developed into coal.

The sandstone consists of moderately grey, brownish grey to transparent quartz grains. The grains are very fine to medium and occasionally coarse to very coarse. The sand is moderately sorted, subangular to angular and situated in a light grey clay matrix. Loose clear to translucent quartz grains are frequently observed in the samples.

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The claystone is moderately to dark greenish grey, with local traces of bluish grey layers. It is blocky to platy, dominantly non calcareous but with local occurrences of calcite. Micropyrite and pyritic nodules were also observed in the samples.

The limestone is ligth grey to bluish grey, brown grey on occations. It is firm, hard in places, microcrystalline and laminated. The limestone is locally very arenaceous and argillaceous grading to cemented sandstones og marly clays.

Only a small interval of the Åre Formation were penetrated by the B-4AH wellbore, not enough for a lithological description.

# 6 Pore Pressure and Hole Stability

# 6.1 Pore Pressure

#### 6.1.1 12 1/4" section

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The direct observations in the well shows the pore pressure of the drilled sequence to be significantly lower than 1,47 sg EMW, the lowest mudweigth used when drilling the section. Calculations and observations indicate hydrostatic pressure down to 1420m TVD RT, in the middle of the Naust formation, a slow pressure increase down to 1470 m TVD RT, then a rapid pressure increase to 1,17 sg EMW at top of the Brygge Formation (1597m TVD RT). A rapid pressure increase from 1,17 - 1,35sg EMW is inferred from 1597 - 1800m TVD RT in the Brygge Formation, followed by a slower increase to the interpreted pressure maximum, 1,39sg EMW at 1950m TVD RT, the base of the Tang Formation. Pressure prediction in the lower parts of the Springar Formation is difficult. The gas data and parameter trends suggest a rapid pressure decrease beneath the maximum pressure at 2000m TVD RT, down to a pore pressure of 1,30sg EMW at 2060m TVD RT and 1,16sg EMW at 2350m TVD RT. The pore pressure gradient in the lower parts of the Springar Formation, the Lyr- and Melke Formation is interpreted to decrease, meeting the initial hydrostatic pressure on the top of the middle Jurassic Fangst Group. Pore pressure calculations support this interpretation.

#### 6.1.2 8 ½" section 6608/10-B-4AH

The following pore pressures in the reservoir section were measured by the MDT-logging:

Formation	Depth interval m TVD MSL	Measured pressure	Equivalent mudweigth
Garn-1	2575-2577	278 bar	1,09 sg (from RT)
Ile	2588-2630	237-242 bar	0,93 sg (from RT)

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Tofte 4-2	2630-2676	242-249 bar	0,93 sg (from RT)
Tofte-1	2676-2692	249 bar	0,93 sg (from RT)
Tilje-4	2692-2700	251 bar	0,94 sg (from RT)
Tilje-3	2700-2722	257-259 bar	0,96 sg (from RT)
Tilje-2	2722-2735 (lowest MDT)	268 bar	0.99 sg (from RT)

The initial pore pressure in the reservoir is 273,2 bar at 2639 m TVD MSL. RT is 31m aMSL. The pore pressure in the 8 ½" section in 6608/10-B-4BH are interpreted to be equal to the measured pressure in the pilot hole.

## 6.2 Formation Strength/Mud Losses

#### 6.2.1 12 1/4" section

A FIT to 1,70 sg EMW were performed after kicking off from the B-4H wellpath at 1352m MD. Mud losses were reported after taking a connection at 2089m MD. Drilled further, 4m, and lost returns immediately. Approximately 393m³ were lost the next 24hrs when trying to stabilize well. Minor (<15m3) losses were experienced twice later when passing the shoe area. The observed fracture pressure in B-4 AH is consistent with the observations in the XLOT in Well 6608/10-7 (Svale 2). This test had a formation breakdown pressure at 1.94 sg (1st cycle), a fracture reopening pressure at 1.56 sg (2nd cycle), fracture propagation pressures of 1.60 sg / 1.56 sg (1st / 2nd cycle) and a fracture closure pressure in the range 1.46 sg - 1.50 sg, with 1.49 sg as the most probable value. The data from the MWD pressure sensors indicate that the fracture in Well 6608/10-B-4 AH appears to have been initiated at 1.71 sg (fracture breakdown), and has shown reopening and propagation at 1.56 sg (initially, just after initiation) and eventually at pressures as low as 1.49 sg (during the cement squeeze) and 1.50 + sg (in the failed attempt to increase the mud density to 1.50 sg)

# 6.2.2 8 ½" sections, 6608/10-B-4AH and -BH

No FIT or LOT were performed. The PWD recording of 1,52sg from the TD of the 12 1/4" section was used as the basis for formation integrity. No loss zones observed in the 8 1/2" sections.

### 6.3 Hole Stability

There were small amounts of cavings in the 12 ¼" section during bitruns #2 and #3, after lowering the mudweigth. They seem to originate from the Tang- and Springar Formations. The amount of cavings seen in this well do not indicate hole stability problems. It is worth noting that parts of this section was drilled with significantly lower mudweigth than previous 12 ¼" sections on the Norne Field. No indications of hole instability in the 8 ½" sections.

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App A Final Directional Survey



Wellbore								
Name		Created				Last Rev	vised	
B-4 AH		1-Feb-2	2002			1-Feb-2	002	
Well					-			
Name		Governr	nont ID			Lest De	uland .	
6608/10-B-4 AH		Govern	nentio			Last Re	2002	
						11100	2002	
Slot								
Name	Grid Northing	Grid Easting	Latitude		L	ongitude	North	East
Slot #4	7322136.3874	457114.1614	N66	0 55.473		E8 3 16.3715		3.64W
Installation					100	VIII WE SEE		
Name	Easti	ng	Northing	10	Coord Sv	stem Name		North Alignment
Nome B		457117.800		22129.400	ED50-U	TM-32N on EUROF	PEAN DATUM 1950	Gri
							datur	n
Name NORNE	Easti	458667.000	Northing 732	3438.000	ED50-UT	tem Name FM-32N on EUROF	EAN DATUM 1950 datun	North Alignment Gri
Created By							New York Control of the Control of t	
				Marian Maria				
Comments								



MD[m]	Inc[dea]	Dirfdeal	TVD[m]	North[m]	East[m]	Dogleg [deg/30m]	Vertical Section[m]
402.70	0.00	0.00	402.70	6.99N	3.64W	0.00	0.0
1320.00	14.31	288.97	1304.70	34.60N	130,66V	0.47	-115.
1330.00	13.72	293.58	1314.41	35.47N	132.91W	3.79	
1340.00		297.80	1324.12	36.50N	135.04W	3.00	
1350.00	13.86	299.87	1333.84	37.65N	137.13W	1.59	
1360.00	14.41	301.34	1343.53	38.89N	139.23W	1.97	
1370.00		301.72	1353.21	40.22N	141.39W	1.70	
1380.00	15.57	303.22	1362.85	41.63N	143.61W	2.15	
1390.00		304.24	1372.48	43.14N	145.87W	1.48	
1400.00		305.66	1382.08	44.75N	148.17W	2.29	
1410.00 1420.00		307.90	1391.64	46.49N	150.51W	2.68	
1430.00	17.51	309.45 312.28	1401.18		152.84W	1.61 2.61	
1440.00			1410.72 1420.24	50.34N	155.12W		
1450.00		314.80 316.97	1420.22	52.44N 54.63N	157,33W 159,45W	2.34	
1460.00		319.48	1439.30	56.88N	161.46W	2.47	
1470.00	17.18	322.27	1448.85		163.34W	2.58	
1480.00		325.35	1458.41	61.55N	165.07W	2.79	
1490.00	16.48	327.80	1467.98		166.66W	2.56	
1500.00	15.87	331.53	1477.59		168.07W	3.61	
1510.00		334.93	1487.22	68.76N	169.28W	2.99	
1520.00		337.95	1496.86	71.20N	170.34W	2.44	
1530.00	15.29	340.09	1506.50	73.66N	171,29W	1.70	
1540.00		342.88	1516.15		172.13W	2.22	
1550.00	15.15	346.71	1525.80	78.68N	172.81W	3.01	
1560.00		348.95	1535.45	81.26N	173.37W	1.96	
1570.00		351.08		83.90N	173.83W	1,90	
1580.00	16.35	353.38			174.20W	2.73	-144.1
1590.00	16.61	353.79	1564.28	89.45N	174.52W	0.85	
1600.00	16.91	353.94	1573.86	92.32N	174.83W	0.91	
1610.00	17.46	354.37	1583.41	95.26N	175.13W	1.69	-142.
1620.00		354.59	1592.93	98.30N	175.42V	1.99	
1630.00		354.92	1602.43	101.43N	175.71W	1.24	
1640.00		355.40	1611.89		175.98V	1.77	
1650.00		355.56	1621.33	107.931	176.24V	1.06	
1660.00		355.45	1630.74	111.30N	176.51W	1.92	
1670.00		355.32	1640.12	114.771	176.79W	1.75	
1680.00		355.12	1649.46		177.08V	1.37	
1690.00		355.42	1658.77	121.98N	177.39V		
1700.00		356.52	1668.00	125.80N	177.65W	3.93	
1710.00		356.55	1677.18		177.89V	1.38	
1720.00		356.16	1686.31	133.831	178.15W		
1730.00							
1740.00				142.50N			-133. -133.
1750.00 1760.00							
1770.00							
1780.00			1730.98	160.921			-130.
1790.00							-128.
1800.00							
1810.00							
1820.00							
1830.00							
1840.00				188.821			
1850.00							-120.
1860.00							
1870.00	30.02						



MD[m]	Inc[dea]	Dir[deq]	TVD[m]	North[m]	East[m]	Dogleg [deg/30m]	Vertical Section[m]
1880.			1827.77	208.36N	176.46W	1.55	-114.8
1890.		9,59	1836.42	213.32N	175.70W	2.50	-112.7
1900.		11.40	1845.04	218.30N	174.78V		-110.6
1910.			1853.62	223.32N	173.70W		-108.2
1920.			1862.16	228.38N	172.51W	1.63	-105.8
1930.			1870.65	233.50N	171.21W		-103.2
1940.		15.53	1879.09	238.67N	169.81W	2.08	-100.5
1950.			1887.47	243.94N	168.33W		-97.7
1960.			1895.76	249.31N	166.80V	2.44	-94.8
1970.			1904.01	254.74N	165.23W		-91.9
1980.		16.77	1912.25	260.17N	163.62V	0.91	-89.0
1990.			1920.47	265.62N	161.97W	1.16	-86.0
2000.			1928.65	271.13N	160.29V	1.73	-82.9
2010.		16.87	1936.77	276.71N	158.58V	1.57	-79.8
2020.			1944.85	282.35N	156.88W		-76.7
2030.			1952.93	287.99N	155.19W		-73.6
2040.			1961.04	293.59N	153.51W		-70.5
2050.		16.58	1969.17	299.17N	151.84W	0.12	-67.5
2060.			1977.31	304.74N	150.17W	0.79	-64.4
2070.		16.95	1985.45	310.29N	148.47W	0.14	-61.4
2080. 2090.		16.98 16.99	1993.57 2001.62	315.87N	146.77W	0.96	-58.3
2100.			2009.56	321.55N	145.04W	3.18	-55.1 -51.9
2110.	38.69	17.26 17.95	2017.40	327.36N 333.27N	143.25V	3.31 2.44	-51.5 -48.5
2120.	39.22	18.37	2025.18	339.24N	141.37W 139.41W	1.78	-45.1 -45.1
2130.			2032.90				
2130.		19,31 19,93	2040.55	345.26N 351.33N	137.36W 135.19W	2.28 2.84	-41.6 -37.9
2150.		20.10	2048.07	357.52N	132.94W	4.09	-34.1
2160.			2055.45	363.85N	130.60W	3.14	-30.2
2170.			2062.72	370.28N	128.18W		-26.2
2180.			2069.83	376.85N	125.71W	4.44	-22.1
2190.		19.80	2076.86	383.53N	123.25W		-18.0
2200.			2083.86	390.25N	120.83W		-14.0
2210.		20.01	2090.79	397.02N	118.37W	1.95	-9.8
2220.		20.19	2097.60	403.90N	115.86W	3.95	-5.6
2230.		20.12	2104.22	410.94N	113,27W	4.83	-1.3
2240.			2110.65	418.13N	110.64W		3.0
2250.			2116.94	425.43N	107.97W	2.21	7.5
2260.		20.28	2123.14	432.80N	105.26W	1.94	12.0
2270.			2129.26	440.20N	102.48V		16.6
2280.			2135.33	447.62N	99.62W	1.61	21.3
2290.	the state of the s		2141.33	455,04N	96.65W	2.75	26.1
2300.			2147.22	462.50N	93.55W	3.85	
2310.				470.07N		4.46	
2320.			2158.45	477.71N		2.24	41.2
2330.				485.40N	83.69W		
2340.					80.28W	1.42	
2350.	00 57.05			500.70N	76.78W		
2360.				508.27N	73.13W		
2370.							
2380.					65.31W		
2390.							
2400.					56.76W		86.
2410.							
2420.							
2430.				560.00N			
2440.							111.



[m]	Inc[dea]	Dirfdeal	TVD[m]	North[m]	East[m]	Dogleg [deg/30m]	Vertical Section[m]
2450.0					33.93W	1.10	117.5
2460.0					29.17W	0.35	124.0
2470.0					24.41W	0.47	130.5
2480.0					19.65W	1.54	136.9
2490.0					14.87W	1.19	143.4
2500.0					10.04W	2.03	149.8
2510.0			2257.68	617.13N	5.17W	1.86	156.4
2520.0			2262.68		0.28W	0.32	163.0
2530.0		34.79		631.39N	4.63E	1.79	169.5
2540.0				638.45N	9.57E	1.33	176.2
2550.0 2560.0			2277.78 2282.78		14.57E	0.99	182.8
2570.0				652.58N 659.62N	19.58E	0.73 0.83	189.5
2580.0		35.55	2287.81		24.60E		196.1
2590.0		35.58			29.63E 34.66E	0.50 0.34	202.8 209.5
2600.0					39.67E	0.54	216.2
2610.0					44.70E	0.67	222.8
2620.0		35.88			49.75E	0.67	229.5
2630.0			2318.05		54.83E	1.03	236.2
2640.0						1.36	243.0
2650.0	- Definited to	36.63			65.13E	1.14	249.8
2660.0					70.34E	0.56	256.7
2670.0					75.55E	0.48	263.5
2680.0					80.77E	0.85	270.3
2690.0				743.63N	86.04E	1.85	277.2
2700.0				750,58N	91.39E	2.71	284.2
2710.0			2357.03	757.52N	96.84E	1,17	291.3
2720.0					102.33E	0.90	298.4
2730.0					107.84E	0.54	305.5
2740.0		38.57	2371.10		113.36E	0.24	312.6
2750.0		38.81	2375.80		118.88E	0.80	319.7
2760.0				792.00N	124.41E	0.51	326.8
2770.0	61.53	38.95			129.95E	1.56	333.9
2780.0	61.75	39.11	2389.97	805.69N	135.49E	0.78	341.
2790.0	61.74			812.53N	141.04E	0.40	348.2
2800.0	61.54	38.91	2399.46		146.57E	0.61	355,3
2810.0	61.47	39.01	2404.23		152.10E	0.34	362.4
2820.0					157.63E	0,57	369.5
2830.0			2413.74	839.89N	163.16E	0.48	376.6
2840.0			2418.53		168.69E	1.89	383.7
2850.0	61.24	40.03			174.29E	1.90	390.9
2860.0		40.88			179.96E	2.74	398.
2870.0					185.73E	2.63	405.4
2880.0					191.59E	3.29	412.7
2890.0							420.
2900.0				885.52N			427.
2910.0							435.
2920.0							442.
2930.0							450.
2940.0						2.73	458.4
2950.0							466.
2960.0							474.
2970.0							482.
2980.0							490.
2990.0		The state of the s					498.1
3000.0							506.3
3010.0	62.71	55.49	2502.53	945.86N	277.57E	4.62	514.



MD[m]	Inc[deq]	Dirfdeal	TVD[m]	North[m]	East[m]	Dogleg [deg/30m]	Vertical Section[m]
3020	0.00 63.4	9 56.38	2507.06	950.86N	284.95E	3.34	523.0
3030	0.00 64.5	56.90	2511.44	955.80N	292.46E	3.37	531.5
3040	0.00 65.1	4 57.54	2515.69	960.701	300.07E	2.57	540.2
3050	0.00 65.1	9 57.98	2519.89	965.54N	307.75E	1.21	548.8
3060	0.00 65.7	7 58.31	2524.04	970.34N	315.47E	1.96	557.5
3070	0.00 66.0	8 58.66	2528.12	975.121	323.26E		566.3
3080	0.00 66.1	7 58.98	2532.17	979.85N	331.08E	0.92	575.1
3090	0.00 66.8	59.47	2536.16	984.54N	338.96E	2.35	583.9
3100	0.00 67.0	6 59.98	2540.08			1.60	592.8
3128	3.60 68.0	4 57.18	2551.00	1002.96N	369.46E	2.90	618.1
3157	7.50 68.5	60.90	2561.70	1016.77N	392.47E	3.62	643.9
3186	69.2	59.83	2572.02	1029.96N	415.66E	1.27	669.7
3215	5.40 70.0	4 64.38	2582.23	1042.80N	439.93E	4.45	696.5
3244	1.10 72.6	64.00	2591.4	1054.64N	464.40E	2.73	723.2
3268	3.00 75.2	65.99	2598.02	1064.34N	485.21E	4.09	745.8
3306	3.00 76.6	68.70	2607.24	1078.54N	519.23E	2.34	782.3
3306	5.60 76.6	68.74	2607.38	1078.75N	519.77E	2.19	782.9
3325	5.00 78.5	68.40	2611.33	1085.32N	536.50E	3.13	8.008
3351	1.50 80.8	69.62	2616.08	1094.65N	560.84E	2.90	826.7
3378	3.40 83.6	70.42	2619.72	1103.76N	585.89E	3.23	853.3
3410	0.00	8 73.69	2623.1	1113.44N	615.77E	3.11	884.6
3439	9.00 82.0	72.52	2626.67		643.31E	2.33	913.4
3467	7.60 79.6	72.12	2631.22	1130.37N	670.21E	2.57	941.6
3497	7.00 77.8	71.41	2636.98	1139.40N	697.59E	2.00	970.4
3526	3.00 75.8	68.81	2643.59	1149.00N	724.14E	3.31	998.5
3553	3.30 74.3	67.55	2650.62	1158,80N	748.63E	2.15	1024.7
3583	3.70 73.1				775.43E	1.97	1053.6
361	1.70 69.8	63.83	2668.02	1181.62N	799.46E	4.09	1079.7
364	1.10 67.1	9 64.69	2678.79	1193.50N	824.10E	2.83	1106.6
3670		9 65.63	2690.64	1204.76N	848.42E	2.32	1133.0
3698	3.50 61.4	66.87	2703.28	1214.871	871.38E	4.07	1157.8
3727	7.60 58.8	67.99	2717.70	1224.56N	894.69E		1182.8
3757			2733.60				
378							1230.
3843	3.30 47.5						
387	Michigan Company			1263.17N			
3900				1269.13N			1314.7



Diameter [in]	Start MD[m]	Start TVD[m]	Start North[m]	Start Eastfml	End MD[m]	End TVD[m]	End North[m]	Start East[m]	Wellbore
36.000									B-4 H
17 1/2	478.00				1315.00				B-4 H
12 1/4	1315.00				2564.00		655.40N	21.59E	B-4 H
12 1/4	1320.00	1304.70	34.60N	130.66V	3280.00	2601.03	1068,991	495.86E	B-4 AH
8 1/2	3280.00	2601.03	1068,99N	495.86E	3900.00	2827.35	1269.13N	1019.34E	B-4 AH

Casings						NAME OF			
Name	Top MD[m]	Top TVD[m]	Top North[m]	Top East[m]	Shoe MD[m]	Shoe TVD[m]	Shoe North[m]	Shoe East[m]	Wellbore
30,000in Conductor	402.70	402.70	6.99N	3.64W	476.00				B-4 H
13 3/8in Casing	402.70	402.70	6.99N	3.64W	1307.60				B-4 H
9 5/8in Casing	402.70	402.70	6.99N	3.64W	2556.20				B-4 H
9 5/8in Casing	402.70	402.70	6.99N	3.64W	3271.20	2598.83	1065.60N	488.05E	B-4 AH
7,000in Liner	3241.10	2590.51	1053.391	461.83E	4341.00	2647.49	1420.57N	1492.18E	B-4 BH



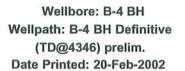
Wellbore Name							
TACILIC		Create	ed		Last Revised		
B-4 BH		1-Feb	-2002		1-Feb-2002		
Well							
Name		I a	115	4 11 11			
6608/10-B-4 BH		Govern	nment ID		Last Revised 1-Feb-2002	d	
0000/10-B-4 BI1					1 1-Feb-2002		
Slot							5 700 75.
Name	Grid Northing	Grid Easting	Latitude	I	Longitude	North	East
Slot #4	7322136.3874	457114.1614			E8 3 16.3715	6.99N	3.64W
Installatio				4.6 X			
Name	East	ina	Northing	Coord S	vstem Name		North Alignment
Nome B		457117.800	7322129.40	0 ED50-L	JTM-32N on EUROPEAN	Grid	
						datun	1
Name NORNE	Easti	458667.000	Northing 7323438.00	0 ED50-U	vstem Name JTM-32N on EUROPEAN	DATUM 1950 datum	North Alianment Grid
Created B	V						



ml	Inc[deq]	Dirfdeq1	TVD[m]	North[m]	East[m]	Doglea [dea/30m]	Vertical Section[m]
402.70			402.70	6.99N	3.64W	0.00	
1320.0		288.97	1304.70	34.60N	130,66V	0.47	
1330.0		293.58	1314.41	35.47N	132.91\	3.79	-74.5
1340.0			1324.12		135.04W	3.00	
1350.0			1333.84	37.65N	137.13W	1.59	
1360.0		301.34	1343.53	38.89N	139.23W	1.97	-76.7
1370.0		301.72	1353.21	40.22N	141.39V	1.70	
1380.0		303.22	1362.85		143.61W	2.15	
1390.0 1400.0			1372.48		145.87W		
1410.0			1382.08 1391.64		148.17W 150.51W	2.29 2.68	
1420.0			1391.64				
1430.0		312.28	1410.72		152.84W 155.12W	2.61	-80.4 -80.4
1440.0			1420.24	50.34N 52.44N	157.33W		
1450.0			1420.22	52,44N 54,63N	157.33W	2.00	-80.6
1460.0		319.48	1439.30	56.88N	161.46W	2.47	-80.6
1470.0			1448.85	59.18N	163.34W	2.58	
1480.0			1458.41	61.55N	165.07W	2.79	
1490.0			1467.98		166.66W	2.56	
1500.0		331.53	1477.59		168.07W	3.61	-78.9
1510.0			1487.22	68.76N	169,28V	2.99	
1520.0			1496.86		170.34W	2.44	
1530.0		340.09	1506.50		171.29W		
1540.0		342.88	1516.15		172.13W	2.22	-75.
1550.0			1525.80	78.68N	172.81W	3.01	-73.9
1560.0			1535.45		173.37W	1.96	
1570.0		351.08	1545.08		173.83W	1.90	
1580.0			1554.69		174.20W	2.73	
1590.0		353.79	1564.28	89.45N	174.52W	0.85	
1600.0			1573.86		174.83W	0.91	-66.0
1610.0			1583.41	95.26N	175.13W	1.69	
1620.0	18.12	354.59	1592.93	98.30N	175.42W	1.99	-62.3
1630.0	18.52	354.92	1602.43	101.43N	175,71W	1.24	
1640.0	19.09	355.40	1611.89	104.64N	175.98W	1.77	-58.4
1650.0	19.44	355.56	1621.33	107.93N	176.24V	1.06	-56.3
1660.0			1630.74	111.30N	176.51\	1.92	
1670.0		355.32	1640.12	114.77N	176.79W	1.75	-52.0
1680.0			1649.46	118.33N	177.08V	1,37	
1690.0			1658.77	121.98N	177.39V		
1700.0			1668.00		177.65W		
1710.0		356.55	1677.18		177.89V	1.38	
1720.0			1686.31	133.83N	178.15W	3.04	
1730.0	25.91	356.76	1695.36	138.09N	178.42V	4.03	-37.
1740.0						2.13	-34.5
1750.0							
1760.0							
1770.0					179.22W	0.78	
1780.0			1739.83				
1790.0							
1800.0		0.10	1757.5		179.43V	1.15	-15.
1810.0							-12.
1820.0							
1830.0				184.12N			
1840.0					178,54V		
1850.0							
1860.0 1870.0			1810.43 1819.1				4.3



(m)	Inc[dea]	Dir[dea]	TVD[m]	North[m]	East[m]	Dogleg [deg/30m]	Vertical Section[m
1880.00	30.14		1827.77	208.36N	176.46W	1.55	12.3
1890.00	30.11		1836.42	213.32N	175.70W	2.50	16.3
1900.00	30.71		1845.04		174.78W	3.29	20.4
1910.00	31.16		1853.62		173.70W	2.63	24.0
1920.00	31.54		1862.16		172.51W	1.63	29.0
1930.00	32.13		1870.65		171.21W	2.61	33.
1940.00	32.71		1879.09		169.81W	2.08	38.
1950.00	33.55		1887.47	243,94N	168.33W	2.54	42.
1960.00	34.34		1895.76	249.31N	166.80V	2.44	47.
1970.00	34.54		1904.01	254.74N	165.23W	0.66	52.
1980.00	34.51	16.77	1912.25		163,62W	0.91	57.
1990.00 2000.00	34.89		1920.47	265.62N	161.97W	1.16	62.
2010.00	35.46 35.97				160.29W	1.73	67.
2020.00	36.20	16.87 16.77	1936,77 1944.85	276.71N 282.35N	158.58W 156.88W	1.57 0.71	72.
2030.00	35.96		1952.93	287.99N	155.19W	0.71	77. 82.
2040.00	35.60	16.65	1961.04		153.51W	1.08	87
2050.00	35.60	16.58	1969.17	293.39N 299.17N	151.84W	0.12	92
2060.00	35.49		1977.31	304.74N	150.17W	0.79	97.
2070.00	35.53		1985.45		148.47W	0.14	102
2080.00	35.85		1993.57	315.87N	146.77W	0.96	107
2090.00	36.91		2001.62		145.04W	3.18	112
2100.00	38.00	17.26			143.25W	3.31	118
2110.00	38.69		2017.40		141.37W	2.44	123
2120.00	39.22		2025.18		139.41W	1.78	129
2130.00	39.69	19.31	2032.90	345.26N	137.36W	2.28	134
2140.00	40.55		2040.55		135.19W	2.84	140
2150.00	41.91	20.10	2048.07	357.52N	132.94W	4.09	146
2160.00	42.92	20.50	2055.45	363.85N	130.60W	3.14	152
2170.00	43.89		2062.72	370.28N	128.18W	2.92	158
2180.00	45.37	20.62	2069.83	376.85N	125.71W	4.44	164
2190.00	45.37	19.80	2076.86	383.53N	123.25W	1.75	171
2200.00	45.78	19.85	2083.86	390.25N	120.83W	1.23	177
2210.00	46.42		2090.79	397.02N	118.37W	1.95	184
2220.00	47.73		2097.60		115.86W	3.95	190
2230.00	49.34		2104.22	410.94N	113.27W	4.83	197
2240.00	50.66		2110.65		110.64W	3.97	204
2250.00	51.39		2116.94		107.97W	2.21	211
2260.00	52.03	20.28	2123.14		105.26W	1.94	218
2270.00	52.46		2129.26		102.48W	1.87	225
2280.00	52.82				99.62W	1.61	232
2290.00	53.38		2141.33	455,04N	96.65W	2.75	239
2300.00	54.54	22.94	2147.22	462.50N	93.55W	3.85	247
2310.00				470.07N		4.46	
2320.00				477.71N	87.03W	2.24	262
2330.00					83.69W		269
2340.00					80.28W	1.42	277
2350.00				500.70N	76.78W		
2360.00					73.13W		
2370.00					69.32W	3.10	301
2380.00					65.31W	4.38	
2390.00					61.10W	3.98	
2400.00					56.76W	1.61	325
2410.00					52.33W	1.63	
2420.00		PATHELY PARK	The state of the s		47.85W		
2430.00 2440.00						1.62 2.45	





1]	Inc[dea]	Dir[dea]	TVD[m]	North[m]	East[m]	Dogleg [dea/30m]	Vertical Section[m]
2450.00	59.36				33.93W	1.10	367.1
2460.00	59.28					0.35	375.5
2470.00	59.34	33.52				0.47	383.9
2480.00	58.90	33.83				1.54	392.3
2490.00	58.64	34.18				1.19	400.6
2500.00	59.30	34.36				2.03	409.0
2510.00 2520.00	59.92	34.37	2257.68			1.86	417.4
2530.00	60.02 59.52	34.41 34.79	2262.68 2267.71	624.27N 631.39N		0.32 1.79	425. 434.
2540.00	59.75			638.45N		1.79	434.
2550.00						0.99	451.
2560.00		35.47	2282.78		19.58E	0.73	459.
2570.00			2287.8	659.62N	24.60E	0.83	468.
2580.00		35.55				0.50	476.
2590.00	59.73	35.58				0.34	485.
2600.00						0.54	493.
2610.00			2307.99			0.67	502.
2620.00		35.88	2313.04	694.71N	49.75E	0.43	510.
2630.00	60.02		2318.05	701.71N		1.03	519.
2640.00	60.46			708.71		1.36	527.
2650.00		36.63				1.14	536.
2660.00						0.56	544.
2670.00						0.48	553.
2680.00						0.85	561
2690.00					86.04E	1.85	570.
2700.00	The second secon			750.58N		2.71	579.
2710.00	61.93	38.31	2357.03			1.17	587.
2720.00	61.95					0.90	596.
2730.00	62.13 62.07	38.63				0.54 0.24	605
2740.00 2750.00	61.91	38.57 38.81	2371.10			0.24	614 622
2760.00	62.05					0.80	631
2770.00				792.00N		1.56	640
2780.00	61.75					0.78	649
2790.00	61.74	38.96		812.53N		0.40	657
2800.00	61.54					0.61	666
2810.00	61.47		2404.23			0.34	675
2820.00	61.66					0.57	684
2830.00	61.63		2413.74			0.48	692
2840.00			2418.53			1.89	701
2850.00	61.24	40.03	2423.34	853.46N	174.29E	1.90	710
2860.00	60.71	40.88	2428.19	860.111	179.96E	2.74	718
2870.00	60.79	41.88	2433.08	866.66N	185.73E	2.63	727
2880.00						3.29	736
2890.00							744
2900.00							753
2910.00							762
2920.00						2.37	770
2930.00						2.34	779
2940.00						2.73	788
2950.00							796
2960.00 2970.00							805
2980.00							814 822
2990.0							822
3000.0							
3010.0				945.86			



[m](	Inc[deq]	Dir[deq]	TVD[m]	North[m]	East[m]	Dogleg [deg/30m]	Vertical Section[m]
3020.00	63.49	56.38	2507.06	950.86N	284.95E	3.34	857.4
3030.00	64.51	56.90	2511.44	955.80N	292.46E	3.37	866.3
3040.00	65.14	57.54	2515.69	960.70N	300.07E	2.57	875.2
3050.00	65.19	57.98	2519.89	965.54N	307.75E	1.21	884.1
3060.00	65.77	58.31	2524.04	970.341	315,47E	1.96	893.0
3070.00		58.66	2528.12	975.12N	323.26E	1.34	901.9
3080.00	66.17	58.98	2532.17	979.85N	331.08E	0.92	910.9
3090.00	66.81	59.47	2536.16	984.541	338.96E	2.35	919.8
3100.00	67.06	59.98	2540.08	989.18N	346.90E	1.60	928.8
3128.60	68.04	57.18	2551.00	1002.96N	369.46E	2.90	954.7
3157.50	68.51	60.90	2561.70	1016.771	392.47E	3.62	980.9
3186.10	69.20	59.83	2572.02	1029,96N	415.66E	1.27	1006.8
3215.40	70.04	64.38	2582.23	1042.80N	439.93E	4.45	1033.3
3244.10	72.63	64.00	2591.41	1054.64N	464.40E	2.73	1059.2
3268.00	75.27	65.99	2598.02	1064.34N	485.21E	4.09	1081.0
3290.00	THE RESERVE OF THE PERSON NAMED IN COLUMN 1	67.56	2603.47	1072.75N	504.80E	2.34	1101.0
3315.70	76.03	69.88	2609.67	1081.80N	528.04E	2.63	1124.1
3346.80	76.68	69.22	2617.00	1092.36N	556.36E	0.88	
3373.90		68.67	2622.27	1101.91N	581.16E	4.72	1176.6
3401.90	83.80	69.58	2625.99	1111.79N	607.09E	3.24	1202.2
3429.80	85.96	70.17	2628.48	1121.35N	633.18E	2.41	1227.8
3459.70	87.38	73.27	2630.22	1130.71N	661.52E	3.42	1254.8
3488.90	87.12	69.60	2631.62	1140.00N	689.16E	3.78	1281.3
3517.90 3548.00	87.37 86.57	69.08 65.22	2633.01 2634.61	1150.22N	716.26E 743.96E	0.60 3.92	1308.0 1336.2
3574.70	88.05	67.05		1161.89N			
3602.60		68.69	2635.86 2636.99	1172,68N	768.35E	2.64 1.93	1361.3
3631.80		69.70	2638.29	1183.18N 1193.54N	794.17E 821.44E	1.93	1387.3 1414.3
3660.90	86.32	71.60					
3688.60	88.11	73.13	2639.85 2641.19	1203.17N 1211.55N	848.85E 875.22E	2.34 2.55	1440.8 1465.7
3719.70	86.27	71.36	2642.72	1211.03N	904.80E	2.55	1493.8
3748.60	87.19	71.30	2644.37	1229.80N	932.28E	2.40	1519.8
3777.00		73.06	2645.74	1238.02N	952.28E 959.43E	0.18	1545.2
3806.50	88.54	73.44	2646.83	1246.52N	987.66E	1.37	1571.5
3834.70	89.65	73.14	2647.27	1254.63N	1014.678	1.22	1596.8
3863.70	89.53	74.05	2647.48	1262.82N	1042.48E	0.95	1622.6
3892.60		74.63	2647.51	1270.62N	1070.31E	1.03	1648.2
3921.10	90.02	73.03	2647.42	1278.55N	1097.68E	1.72	1673.6
3949.90		71.25	2647.55	1287.39N	1125.09E	1.94	1699.6
3979.00	90.58	70.73	2647.54	1296.87N	1152.618	1.26	1726.
4007.90	90.14	69.95	2647.36	1306.59N	1179.828	0.93	1752.6
4034.80	90.08	69.08	2647.31	1316.00N	1205.02E	0.97	1777.4
4065.00		68.73	2646.79	1326.87N	1233.19E	1.81	1805.3
4094.90						1.50	
4124.40			2644.90	1349.79N		4.26	1860.9
4151.70				1361.27N		2.84	1886.8
4180.80		68.41	2646.95			3.53	
4208.90		70.25	2647.49			2.60	
4236.20						2.03	
4266.60			2647.16			2.06	
4294.90			2647.06			0.56	
4319.60		75.21	2647.20			2.48	
4346.00			2647.56				



Diameter [in]	Start MD[m]	Start TVD[m]	A THE RESERVE AND ADDRESS OF THE PARTY OF TH	Start East[m]	End MD[m]	CONTRACTOR OF THE PARTY OF THE	End North[m]	Start East[m]	Wellbore
36.000	402.70	402.70			478.00				B-4 H
17 1/2	478.00				1315.00				B-4 H
12 1/4	1315.00				2564.00		655.40N	21.59E	B-4 H
12 1/4	1320.00	1304.70	34.60N	130.66W	3280.00	2601.03	1068,99N	495.86E	B-4 AH
8 1/2	3280.00	2601.03	1068.99N	495.86E	3900.00	2827.35	1272.61N	1077.44E	B-4 AH
8 1/2	3290.00	2603.47	1072.75N	504.80E	4346.00	2647.56	1421.85N	1497.02E	B-4 BH

Casings									
Name	Top MD[m]	Top TVD[m]	Top North[m]	Top East[m]	Shoe MD[m]	Shoe TVD[m]	Shoe North[m]	Shoe East[m]	Wellbore
30,000in Conductor	402.70	402.70	6.99N	3.64W	476.00				B-4 H
13 3/8in Casing	402.70	402.70	6.99N	3.64W	1307.60				B-4 H
9 5/8in Casing	402.70	402.70	6.99N	3.64W	2556.20				B-4 H
9 5/8in Casing	402.70	402.70	6.99N	3.64W	3271.20	2598.83	1065.60N	488.05E	B-4 AH
7.000in Liner	3241.10	2590.5	1053.39N	461.83E	4341.00	2647.49	1420.571	1492.18E	B-4 BH