

Behavior of weakly adsorbing impurities in flow-through ion-exchange chromatography

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Abstract

Flow-through ion-exchange chromatography is frequently used in polishing biotherapeutics, but the factors that contribute to impurity persistence are incompletely understood. A large number of dilute impurities may be encountered that exhibit physicochemical diversity, making the flow-through separation performance highly sensitive to process conditions. The analysis presented in this work develops two novel correlations that offer transferable insights into the chromatographic behavior of weakly adsorbing impurities. The first, based on column simulations and validated experimentally, delineates the relative contributions of thermodynamic, transport, and geometric properties in dictating the initial breakthrough volume of dilute species. The Graetz number for mass transfer was found to generalize the transport contributions, enabling estimation of a threshold in the equilibrium constant below which impurity persistence is expected. Impurity adsorption equilibria are needed to use this correlation, but such data are not typically available. The

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second relationship presented in this work may be used to reduce the experimental burden of estimating adsorption equilibria as a function of ionic strength. A correlation between stoichiometric displacement model parameters was found by consolidating isocratic retention data for over 200 protein-pH-resin combinations from the extant literature. Coupled with Yamamoto’s analysis of linear gradient elution data, this correlation may be used to estimate retentivity approximately from a single experimental measurement, which could prove useful in predicting host-cell protein chromatographic behavior.

Keywords: Flow-through, Ion-exchange, Impurity, Clearance, Breakthrough, Stoichiometric displacement model

1. Introduction

The biopharmaceutical market has grown substantially over the past few decades, with over 300 biologics having received regulatory approval and hundreds more in development pipelines [1, 2]. Monoclonal antibodies (mAbs) comprise the majority of these biologics, partly because platform purification processes have enabled their rapid development [3, 4]. One stage in a typical platform process is polishing, where trace impurities such as host-cell proteins (HCPs) are removed prior to product formulation using one or more chromatographic operations [5]. Despite their low concentrations, some of these impurities may pose a risk to therapeutic safety and stability, and polishing operations are designed to remove them completely [6, 7].

Polishing may be performed using ion-exchange (IEX), hydrophobic interaction or multimodal resins. Since the majority of secreted HCPs are

14 more acidic than the typical mAb [8], anion-exchange (AEX) resins are more
15 naturally suited to flow-through operations [9], in which impurities are in-
16 tended to adsorb to the resin, but they may be used in bind-and-elute mode
17 as well [10]. The inverse is true of cation-exchange (CEX) stationary phases.
18 The flow-through operational mode offers the advantage of relatively high
19 throughput; as a heuristic, 1 g of mAb usually requires 1 ml of resin in flow-
20 through IEX [11]. For mAb concentrations on the order of 20 mg/ml, this
21 corresponds to an apparent processing capacity on the order of 50 column
22 volumes (CV). Such large capacities can enable high productivity operations
23 with relatively small columns. If convective media are used instead of resin
24 particles, there is the potential to increase productivity beyond the limita-
25 tions inherently associated with packed column flow rate constraints [12].
26 These process intensification benefits have led to an increasing consideration
27 of flow-through operations for applications outside of polishing, particularly
28 in the development of continuous downstream processes [11, 13, 14].

29 Despite the utility of flow-through IEX steps, relatively few studies have
30 systematically investigated their development and limitations. This is partly
31 because impurity behavior is essential to understanding flow-through separa-
32 tions, but it is difficult to interrogate experimentally. Total HCP concentra-
33 tions encountered in mAb polishing are usually on the order of 1000 ppm [15],
34 rendering in-line detection and quantification infeasible [16, 17]. Hundreds
35 of HCPs may be present, and their biophysical diversity leads to heteroge-
36 neous chromatographic behavior. Although process conditions are tuned to
37 maximize HCP adsorption, they are generally less conducive to strong reten-
38 tion than in bind-and-elute mode. This may make impurity clearance highly

39 sensitive to the mobile phase composition and the resin.

40 Coupled with the plethora of available resins, the high sensitivity of sep-
41 aration performance typically necessitates screening studies during process
42 development. Commercial IEX resins are available that differ in particle
43 size, pore size and morphology, base matrix, ligand chemistry, ionic capac-
44 ity, and surface functionalization [18, 19]. Screening studies to determine
45 the best resin among several alternatives can provide valuable application-
46 specific data, and perhaps furnish general resin retentivity heuristics [20], but
47 they offer limited transferable insights into individual HCP chromatographic
48 retention and capacity. Column modeling has therefore been suggested as a
49 complementary technique to elucidate the factors that contribute to impurity
50 persistence [16, 17]. A better understanding of this phenomenon could po-
51 tentially improve flow-through process design, expedite development, reduce
52 costs, and increase consistency with quality by design principles. It could also
53 help direct future *in silico* optimization efforts, which to date have focused
54 primarily on product molecules rather than impurities.

55 Two HCP persistence mechanisms have been hypothesized for flow-through
56 processes: product association and weak adsorption [5]. The relative im-
57 portance of these mechanisms remains unclear. Product association is ex-
58 pected to vary mechanistically with the therapeutic molecule and the impu-
59 rity species, which may hinder a general understanding of the phenomenon.
60 However, it may be tractable to analyze generally the breakthrough of weakly
61 adsorbing impurities. Two attributes of the flow-through process simplify the
62 analysis, namely that the process is isocratic, and that the adsorption equi-
63 lbria of weakly adsorbing species are expected to be approximately linear

64 and independent. Assuming HCP concentrations on the order of 1000 ppm,
65 column capacities on the order of 100 mg/ml, and the load heuristic of 1 g
66 mAb/ml of column, only $\sim 1\%$ of the column is expected to saturate with
67 HCPs. The majority of the column is therefore available for weakly retained
68 HCPs to adsorb with negligible competition for the IEX surface.

69 This work focuses on developing transferable insights into the break-
70 through of weakly adsorbing impurities in flow-through IEX. We placed em-
71 phasis on understanding contributions to the initial breakthrough volume, as
72 the goal of flow-through polishing is the complete removal of trace impuri-
73 ties. To maintain generalizability across diverse sets of HCPs, we simulated
74 the chromatographic behavior of dilute species with a variety of transport
75 and thermodynamic properties. Simulated initial breakthrough volumes were
76 analytically related to the Graetz number for mass transfer, and this rela-
77 tionship was validated experimentally. Transport and thermodynamic pa-
78 rameters need to be estimated to use this relationship, but HCP adsorption
79 equilibrium constants are usually unknown. To gain a better understanding
80 of IEX adsorption equilibria, we consolidated dilute isocratic retention data
81 from the extant literature on model species. From these data, a correlation
82 was observed between stoichiometric displacement model (SDM) parameters
83 that are commonly used to relate the adsorption equilibrium constant to
84 ionic strength [21]. This thermodynamic correlation was corroborated by
85 linear gradient elution data, suggesting a way to estimate SDM parameters
86 approximately from one experimental measurement. These relationships pro-
87 vide novel insights into properties that contribute to flow-through impurity
88 clearance.

2. Theory and simulation

2.1. Column chromatography model

The 1D general rate model of column chromatography was used in this work, which describes the transport of solutes within the column interstitial volume as [19, 22, 23]:

$$\frac{\partial c}{\partial t} + v \frac{\partial c}{\partial z} = D_{ax} \frac{\partial^2 c}{\partial z^2} - \frac{3}{r_p} \left(\frac{1 - \varepsilon_c}{\varepsilon_c} \right) k_f \left(c - c_p|_{r=r_p} \right) \quad (1a)$$

with Danckwerts' boundary conditions:

$$v \left(c_{in} - c|_{z=0} \right) = -D_{ax} \frac{\partial c}{\partial z} \Big|_{z=0} \quad (1b)$$

$$\frac{\partial c}{\partial z} \Big|_{z=L_{col}} = 0 \quad (1c)$$

where c is the solute concentration in the interstitial volume, c_p is the solute concentration in the resin bead pore space, t is time, z is the column axial coordinate, r is the resin bead radial coordinate, c_{in} is the column inlet concentration, L_{col} is the column length, r_p is the resin bead radius, v is the interstitial velocity, D_{ax} is the axial dispersion coefficient, k_f is the film mass transfer coefficient, and ε_c is the column porosity. Solute transport within the resin beads is described by:

$$\varepsilon_p \frac{\partial c_p}{\partial t} + (1 - \varepsilon_p) \frac{\partial q}{\partial t} = \varepsilon_p D_p \left(\frac{\partial^2 c_p}{\partial r^2} + \frac{1}{r} \frac{\partial c_p}{\partial r} \right) + (1 - \varepsilon_p) D_s \left(\frac{\partial^2 q}{\partial r^2} + \frac{1}{r} \frac{\partial q}{\partial r} \right) \quad (2a)$$

with boundary conditions of spherical symmetry at the bead center and a mass balance at the bead edge, respectively:

$$\frac{\partial c_p}{\partial r} \Big|_{r=0} = 0, \quad \frac{\partial q}{\partial r} \Big|_{r=0} = 0 \quad (2b)$$

105

$$\varepsilon_p D_p \frac{\partial c_p}{\partial r} \Big|_{r=r_p} + (1 - \varepsilon_p) D_s \frac{\partial q}{\partial r} \Big|_{r=r_p} = k_f \left(c - c_p \Big|_{r=r_p} \right) \quad (2c)$$

106 where q is the adsorbed solute concentration, ε_p is the resin bead porosity
 107 accessible to the solute, D_p is pore diffusivity, and D_s is surface diffusivity.
 108 Typically, the relevant initial conditions are:

$$c|_{t=0} = 0, \quad c_p|_{t=0} = 0, \quad q|_{t=0} = 0 \quad (3)$$

109 An isotherm relating q to c_p is needed to complete the column model,
 110 along with a description of the adsorption kinetics. Since adsorption and des-
 111 orption steps are usually much faster than the other transport processes, in-
 112 stantaneous equilibration was assumed in this work. The Langmuir isotherm
 113 was used:

$$q = q_{max} \left(\frac{K_L c_p}{K_L c_p + 1} \right) \quad (4)$$

114 where q_{max} is the resin saturation capacity and K_L is a thermodynamic pa-
 115 rameter (equal to the ratio of the adsorption and desorption rate constants,
 116 k_a/k_d). The adsorption equilibrium constant, K_{eq} , is defined by the initial
 117 isotherm slope, which for the Langmuir model is:

$$K_{eq} \equiv \lim_{c_p \rightarrow 0} \frac{q}{c_p} = q_{max} K_L \quad (5)$$

118 Dimensions of volume concentration were used for q in this work (as opposed
 119 to excess surface concentration), making K_{eq} a dimensionless parameter.

120 Column model equations were solved with the Chromatography Analysis
 121 and Design Toolkit (CADET, versions 4.1.0 and 4.2.0) [24].

122 2.2. Simulations for analyzing breakthrough volumes

123 To ascertain qualitative differences between the breakthrough of concen-
 124 trated and dilute species, simulations were performed for single-component
 125 systems with load concentrations between 10 mg/ml and 1 μ g/ml with q_{max}
 126 fixed at 100 mg/ml of packed column, K_{eq} varied from 1 to 10000, and trans-
 127 port parameters selected from representative calibrations to model species.
 128 Exploratory simulations were then performed for a load concentration of 1
 129 μ g/ml at variable v , D_p , L_{col} , and r_p . D_{ax} was estimated as a function of
 130 v from correlations for beds packed with solid particles [25], using a dilute
 131 solution diffusivity of 7.5×10^{-11} m²/s to represent general protein behav-
 132 ior [26]. Film mass transfer was assumed to be relatively fast, and k_f was
 133 set to 1×10^{-3} m/s for all simulations. D_s was estimated as a function of
 134 K_{eq} using results reported for a mAb of the form $D_s = aK_{eq}^b$, where the
 135 power law coefficient $a = 1.66 \times 10^{-12}$ m²/s and $b = -0.24$ [27]. Results
 136 from these simulations were correlated to relate breakthrough volume with
 137 system parameters, making use of an effective intraparticle diffusivity (D_{eff})
 138 to describe the combined effects of pore and surface diffusion [28]:

$$D_{eff} \equiv D_p + \left(\frac{1 - \varepsilon_p}{\varepsilon_p} \right) K_{eq} D_s \quad (6)$$

139 This expression may be derived from Equation 2a by assuming instantaneous
 140 equilibration and linear chromatographic conditions, as given by:

$$q = K_{eq} c_p \quad (7)$$

141 A linear isotherm was used for comparing simulations with experimental
 142 data, and the extra-column volume, which consisted of valves and 0.75 mm

143 ID tubing, was described as a continuously stirred tank reactor (CSTR) in
 144 series with a dispersed plug flow reactor (PFR) [29]. The fraction of the
 145 extra-column volume allocated to the CSTR was fit as a function of flow
 146 rate, and the PFR axial dispersion coefficient was set to 1×10^{-12} m²/s.

147 2.3. Models for ion-exchange adsorption equilibria

148 A number of models have been proposed to relate protein IEX adsorp-
 149 tion equilibria to solution conditions, with perhaps the simplest and most
 150 commonly cited being the stoichiometric displacement model (SDM), which
 151 describes adsorption as a strict ion-exchange process [21]. From the law of
 152 mass action, the adsorption equilibrium constant is related to ionic strength,
 153 I , as:

$$K_{eq} = \alpha I^{-\nu} \quad (8)$$

154 where α is a measure of adsorption strength and ν is the protein charac-
 155 teristic charge, which represents the stoichiometry of ion exchange. These
 156 parameters are commonly estimated by fitting isocratic retention data at
 157 different ionic strengths or regressing linear gradient elution data according
 158 to Yamamoto’s method [30]. The fundamental equation of ideal linear chro-
 159 matography predicts that retention factors should also exhibit a power law
 160 dependence on ionic strength [22]:

$$k' = \phi K_{eq} = \phi \alpha I^{-\nu} \quad (9)$$

161 where $k' = (V_R - V_0)/V_0$ is the retention factor for the solute and solution
 162 conditions of interest, V_R is the retention volume, and V_0 is the flow-through
 163 volume under non-adsorbing conditions. For dimensionless K_{eq} , $\phi = (1 -$

164 $\varepsilon_t)/\varepsilon_t$ is a dimensionless phase ratio where $\varepsilon_t = \varepsilon_c + (1 - \varepsilon_c)\varepsilon_p$ represents the
 165 total column porosity.

166 More sophisticated colloidal models that are based on statistical thermo-
 167 dynamics have also been proposed for estimating K_{eq} from the free energy
 168 change of molecular adsorption, ΔF , using some form of the general expres-
 169 sion [31]:

$$K_{eq}(I, \text{pH}) = \int_{\Omega} \int_{z_0}^{\infty} (e^{-\Delta F(z, \Omega, I, \text{pH})/k_B T} - 1) dz d\Omega \quad (10)$$

170 where Ω represents the protein orientation with respect to the resin and z is
 171 the separation distance. Previous models have used continuum electrostatics
 172 and van der Waals equations to estimate ΔF , often making use of mean-field
 173 approximations [32, 33]. Notably, the K_{eq} estimates from these models are
 174 quite sensitive to ΔF due to the Boltzmann weighting.

175 **3. Materials and methods**

176 *3.1. Chemicals and buffers*

177 Sodium hydroxide, hydrochloric acid, sodium chloride, monobasic sodium
 178 phosphate, dibasic sodium phosphate, acetic acid, sodium acetate, boric
 179 acid, and sodium bicarbonate were purchased from Fisher (Fair Lawn, NJ).
 180 Sodium carbonate, ethanolamine, and 2000 kDa blue dextran were pur-
 181 chased from Sigma (St. Louis, MO). Fluorescein isothiocyanate (FITC) and
 182 dimethylformamide were purchased from Thermo Scientific (Rockford, IL).
 183 All chemicals were used without any further purification.

184 Buffer solutions were prepared to the desired constituent concentrations
 185 at room temperature with deionized water from an EMD Millipore Milli-Q

186 system ($> 18.2 \text{ M}\Omega \text{ cm}$). Low and high ionic strength buffers were prepared
187 with 0 and 1 M added NaCl, respectively. Buffer pH and conductivity were
188 measured with a Cole-Parmer PC200 meter, and pH adjustments were made
189 with concentrated sodium hydroxide and hydrochloric acid solutions. Prior
190 to use, buffer solutions were filtered with Fisher $0.2 \mu\text{m}$ aPES membranes
191 (Pittsburgh, PA).

192 *3.2. Proteins*

193 Lyophilized hen egg white lysozyme was purchased from Sigma (St. Louis,
194 MO). A mAb sample was obtained from the protein A eluate pool of a
195 manufacturing process at Bristol Myers Squibb (Devens, MA). The mAb
196 was supplied at 35 mg/ml and stored at -80°C . It was thawed prior to use
197 and exchanged into the desired buffer using a GE Sephadex G25 desalting
198 column, and protein solution concentrations were measured with a Thermo
199 Scientific NanoDrop Lite spectrophotometer.

200 *3.3. Resins and chromatography equipment*

201 All chromatographic measurements were performed using an Amersham
202 Biosciences Äkta Explorer equipped with a P-960 sample pump, fraction
203 collector, 10 mm UV flow cell, and in-line pH and conductivity meters. SP
204 Sepharose FF, a strong cation-exchanger, was purchased from GE Healthcare
205 (Uppsala, Sweden). It was exchanged three times into a pH 7.0 (25 mM
206 sodium phosphate) buffer by centrifugation and decantation prior to slurry
207 packing (50%) into a $0.5 \times 10 \text{ cm}$ Waters AP chromatography column to
208 a final bed volume of 2.0 ml. Column packing was validated at pH 7.0

209 by injecting a 100 μ l pulse of a 1 M NaCl buffer and verifying that the
210 conductivity trace asymmetry fell within commonly accepted limits [18].

211 3.4. *Linear gradient elution*

212 The retention of lysozyme on SP Sepharose FF was measured with lin-
213 ear gradient elution at pH 5.0, 7.0, and 9.0 (in 75 mM sodium acetate, 25
214 mM sodium phosphate, and 25 mM ethanolamine buffers, respectively) at a
215 superficial velocity of 300 cm/h. Feed solutions were prepared by dissolving
216 lysozyme in the appropriate low ionic strength buffer at \sim 20 mg/ml, and
217 lyophilized excipients were removed with three buffer exchange cycles using
218 EMD Millipore Amicon centrifugal filter units (Cork, Ireland). Lysozyme
219 solutions were filtered using Thermo Scientific 0.2 μ m PVDF membranes
220 (Rockwood, TN) and diluted to \leq 10 mg/ml prior to use. The SP Sepharose
221 FF column was equilibrated in the relevant low ionic strength buffer for 5
222 CV, and gradient elution from 0 to 1 M NaCl began shortly after a 100 μ l
223 sample injection. The gradient elution volume was varied from 10 to 50 CV
224 in increments of 10 CV, and the conductivity at peak elution was determined.
225 This was used with a correlation for the instrument’s conductivity response
226 to estimate the peak elution ionic strength. Columns were regenerated at
227 least once every five runs via 15 minutes of contact with 0.5 M NaOH.

228 3.5. *Breakthrough measurements during isocratic elution*

229 To validate corresponding simulation results, frontal loading chromatog-
230 raphy was performed with dilute lysozyme solutions on SP Sepharose FF
231 at pH 7.0 (20 mM sodium phosphate) under conditions of weak to moder-
232 ate retention. The requisite ionic strength for such retention was estimated

233 from linear gradient elution measurements and tuned empirically to target
234 a breakthrough volume of ~ 10 CV. A feedstock of $10\ \mu\text{g}/\text{ml}$ lysozyme was
235 used to mimic the low impurity concentrations encountered in flow-through
236 polishing, and outlet concentrations were estimated from the absorbance at
237 215 nm with a computed extinction coefficient [34]. At such low protein con-
238 centrations, appreciable variability in component separation was observed
239 between replicate feedstock preparations. For this reason, feedstock batches
240 were prepared at the desired ionic strength in sufficient volume to service
241 the entire set of measurements, and a batch exhibiting minimal component
242 separation was selected for use. For each measurement, a 10 CV equilibra-
243 tion period preceded a 20 CV load through the Äkta's sample pump, after
244 which the column was washed as described previously. This was performed
245 at superficial velocities ranging from 30 to 305 cm/h in a randomized order,
246 and comparable breakthrough measurements were made under non-adsorbing
247 conditions (at high ionic strength).

248 To qualitatively validate simulated trends under conditions of greater
249 relevance to flow-through polishing, breakthrough behavior was also demon-
250 strated with fluorescently labelled lysozyme in the presence of a mAb. Lysozyme
251 was conjugated with FITC according to the manufacturer's protocol, produc-
252 ing a complex product mixture with different label ratios and conjugation
253 sites. A fraction of the conjugation products exhibiting relatively homo-
254 geneous chromatographic behavior was required to effectively represent the
255 breakthrough of an individual impurity. The conjugation product mixture
256 was therefore subjected to repeated fractionation on SP Sepharose FF at
257 pH 9.5 (20 mM sodium carbonate) using shallow ionic strength steps during

258 elution. Average label ratios and FITC-lysozyme concentrations in the col-
 259 lected fractions were estimated from the absorbance profiles at 280 and 495
 260 nm. Once a sufficiently homogeneous fraction was obtained, it was spiked
 261 to $\sim 10 \mu\text{g}/\text{ml}$ in a mAb solution at pH 9.5, where the mAb was observed
 262 to have negligible retention on SP Sepharose FF. As with lysozyme break-
 263 through measurements, an ionic strength was identified to achieve weak to
 264 moderate FITC-lysozyme retention, and breakthrough profiles were acquired
 265 over a range of superficial velocities in randomized order. The mAb concen-
 266 tration was dilute due to material constraints, and the eluate absorbance at
 267 495 nm was used to distinguish FITC-lysozyme breakthrough from the mAb
 268 flow-through.

269 *3.6. Parameter estimation for test simulations*

270 The breakthrough of lysozyme fed in dilute solution on SP Sepharose FF
 271 was simulated in CADET as described in Section 2.2. Sequential parameter
 272 estimation was used to reduce the dimensionality of the optimization space
 273 when fitting the experimental data. Duplicate column bypass profiles were
 274 acquired with lysozyme at each flow rate used in breakthrough measurements.
 275 These were fit with a trust region optimization algorithm interfaced by the
 276 `Scipy least_squares` function to determine the extra-column volume (which
 277 is invariant with flow rate) and the fraction of that volume allocated to the
 278 CSTR in the system model (which varies with flow rate). Triplicate blue
 279 dextran pulses, monitored with the absorbance at 280 nm, were then passed
 280 through the column to measure ε_c . Peak tailing was observed, which is
 281 attributable to size heterogeneity in the blue dextran tracer. For this reason,
 282 the average peak mode was used instead of the average first moment to

283 estimate ε_c .

284 Duplicate lysozyme pulses under non-adsorbing conditions (high ionic
285 strength) were then passed through the column at each flow rate. Retention
286 volumes under non-adsorbing conditions were computed from the first mo-
287 ment of the absorbance profiles and used to estimate ε_p . These profiles were
288 then fit to estimate D_p (which is invariant with flow rate) and D_{ax} (which
289 varies with flow rate). An evolutionary algorithm interfaced by the `Scipy`
290 `differential_evolution` function was used to estimate D_p and a coarse
291 dependence of D_{ax} on flow rate. The estimated value of D_p was retained,
292 and the coarse D_{ax} estimates were refined using the `least_squares` func-
293 tion. Without further refinement, the estimated parameters were validated
294 by modeling dilute lysozyme breakthrough profiles under non-adsorbing con-
295 ditions (at high ionic strength). Dilute breakthrough profiles under adsorbing
296 conditions (at lower ionic strength) were then simulated by fitting K_{eq} and
297 D_s (which are invariant with flow rate) using the `differential_evolution`
298 function.

299 4. Results and discussion

300 4.1. Breakthrough volume correlation

301 In the context of polishing operations, the value of flow-through IEX is its
302 ability to completely remove as many trace HCPs as possible from a mAb so-
303 lution. Challenges inherent in this task may not be readily apparent because
304 it is difficult to study the chromatographic behavior of dilute solutes em-
305 pirically. A column simulation was therefore used to investigate differences
306 between the breakthrough of overloaded products and dilute impurities. An

307 initial set of single-component simulations were performed at different feed
 308 concentrations and K_{eq} values. Transport and geometric parameters were
 309 held fixed, and a Langmuir isotherm with constant $q_{max} = 100$ mg/ml of
 310 column was used. Results for extreme feed concentrations are juxtaposed
 311 in Figure 1, and analogous plots for intermediate concentrations are shown
 312 in Supplementary Figure S1. As may be expected for the system with a 10
 313 mg/ml feed, retention increased with K_{eq} until the column saturated, and
 314 breakthrough profiles became sharper as column saturation was approached.
 315 This self-sharpening behavior did not occur for the 1 μ g/ml feed over the vol-
 316 ume scale simulated, revealing dilute solute breakthrough profiles to become
 317 more diffuse as retention increases due to the essentially linear isotherm. An
 318 order-of-magnitude difference can be observed between the load volumes cor-
 319 responding to the initial breakthrough and the inflection point in the more
 320 strongly retained profiles. This illustrates an appreciable challenge; even if
 321 trace impurities exhibit strong to moderate retention, their diffuse distribu-
 322 tion on the column may lead to relatively early breakthrough and preclude
 323 adequate clearance.

324 To better understand this challenge, the load volume corresponding to 1%
 325 breakthrough was identified and plotted against K_{eq} (Figure 2). A couple
 326 of trends may be observed. When column saturation is not approached, the
 327 breakthrough volume appears to scale linearly with K_{eq} . An ideal limit on the
 328 K_{eq} dependence may be roughly estimated as $CV_{breakthrough} = \varepsilon_t + (1 - \varepsilon_t)K_{eq}$
 329 based on the fundamental equation of ideal linear chromatography. As
 330 shown, the slope of the dilute solute series differs markedly from the ideal
 331 limit, due largely to finite transport rates that limit the system's approach to

equilibrium. The discrepancy between the observed and ideal behavior therefore suggests that transport rate optimization may provide a useful means of improving impurity clearance in flow-through processes.

Further simulations showed that the slope of the $CV_{1\%}$ vs. K_{eq} curve for dilute solutes varies with transport and geometric parameters. This observation indicates that the initial breakthrough volume may be approximately described as:

$$CV_{breakthrough} = \varepsilon_t + (1 - \varepsilon_t)K_{eq}f \quad (11)$$

where f is a function of transport parameters that modifies the breakthrough volume dependence on K_{eq} , with $0 \leq f \leq 1$. The form of this relationship has two implications: it suggests that thermodynamic and transport contributions to impurity breakthrough may be independent, and that transport contributions may be described by a single factor, which can presumably be expressed generally in terms of a dimensionless group.

Based on this rationale, a second set of simulations were performed for a 1 $\mu\text{g}/\text{ml}$ feed. A variety of thermodynamic, transport, and geometric parameters were used, and f was computed from the results by rearranging Equation 11. However, ε_c was used in place of the ε_t intercept when computing f from Equation 11 because this was observed to better describe the simulated breakthrough volumes in the limit of $K_{eq} \rightarrow 0$. Based on the dynamic binding capacity correlation presented by Chen et al. [35], f is plotted in Figure 3 against the dimensionless group:

$$Gz_{eff} = \frac{vd_{part}^2}{D_{eff}L_{col}} = Pe_{p-eff} \frac{d_{part}}{L_{col}} \quad (12)$$

which represents a Graetz number for mass transfer, written as a product of two dimensionless subgroups. The first is the particle Péclet number,

355 which represents the ratio of convective to diffusive transport rates on the
 356 length scale of the resin particle, when D_{eff} is used to describe the diffusional
 357 transport. The second subgroup is a ratio of characteristic length scales,
 358 namely the resin particle diameter and the column length.

359 Figure 3 indicates that Equation 11 with a modified intercept may be
 360 written more specifically as:

$$CV_{\%} = \varepsilon_c + (1 - \varepsilon_t)K_{eq}f_{\%} \left(\frac{vd_{part}^2}{D_{eff}L_{col}} \right) \quad (13)$$

361 where $CV_{\%}$ is the load volume at a given percent breakthrough threshold,
 362 and $f_{\%}$ is the corresponding function of transport and geometric parameters.
 363 Shown are two series for illustrative breakthrough thresholds, but any arbitrary
 364 threshold could be selected. Some noise is apparent, but it is largely
 365 attributable to the approximation that $CV_{\%}$ is invariant with transport parameters
 366 when $K_{eq} = 0$. Within the noise, it is clear that $CV_{\%}$ decays
 367 monotonically with the value of the Graetz number.

368 To maximize the load volume before breakthrough, which is approxi-
 369 mated by $CV_{1\%}$, the Graetz number should be minimized. Unfortunately,
 370 doing so comes at a cost to throughput if v is reduced or an increase in col-
 371 umn pressure drop if d_{part} is decreased or L_{col} is increased. This correlation
 372 does therefore not suggest a free way of improving flow-through processing.
 373 What it does quantify, however, is the inherent balance between separa-
 374 tion performance and throughput. Notably, the initial breakthrough volume
 375 decays much more quickly with the Graetz number than the intermediate
 376 breakthrough volume. The benefit of optimizing the system geometry and
 377 transport rates is expected to be only marginal for typical process conditions,
 378 which correspond to Graetz numbers on the flat part of the 1% breakthrough

379 curve in Figure 3. However, if the Graetz number could be decreased below
 380 ~ 5 , the benefit would become much more pronounced.

381 An interesting subtlety that is implicit in this correlation is the effect
 382 of thermodynamics on intraparticle transport rates, which is described by
 383 the dependence of D_{eff} on K_{eq} . D_{eff} captures the combined effects of pore
 384 and surface diffusion in the dilute solute limit by describing the effective
 385 intraparticle diffusivity as a weighted sum, where K_{eq} weights the relative
 386 importance of surface diffusion. IEX surface diffusivities have been shown
 387 to follow a power law of the form $D_s = aK_{eq}^b$, where $b < 0$ [27]. This
 388 leads to competing effects: increasing K_{eq} decreases the surface diffusivity
 389 but simultaneously increases the driving force for surface diffusion, with the
 390 effect that dominates being determined by whether the power law exponent
 391 $b > -1$. If this is the case, increasing K_{eq} leads to an increase in D_{eff}
 392 and a reduction in the Graetz number, meaning that both thermodynamic
 393 and transport contributions to delaying impurity breakthrough are improved
 394 simultaneously.

395 Equation 13 also enables estimation of the problematic K_{eq} threshold
 396 below which impurities will persist via weak adsorption. To gain a sense for
 397 the threshold's order of magnitude, an illustrative calculation was performed
 398 with a spline fit to the $f_{1\%}$ curve shown in Figure 3. Results for a 20 cm
 399 column with a 6 minute residence time are shown in Figure 4 as a function
 400 of load volume using $\varepsilon_c = 0.35$, $\varepsilon_p = 0.5$, $d_{part} = 50 \mu\text{m}$, $D_p = 10^{-11} \text{ m}^2/\text{s}$,
 401 and D_s estimated from the power law discussed previously. The results show
 402 that, for load volumes on the order of 100 CV, HCPs with $K_{eq} < \sim 400$ are
 403 liable to break through before the end of loading. This would be equivalent to

404 a retention factor of ~ 200 for an input feed pulse under identical conditions.

405 4.2. Validation of the breakthrough volume correlation

406 To validate the breakthrough volume correlation that was developed from
407 simulation results, frontal loading chromatography was performed using di-
408 lute feeds as described in Section 3.5. Figure 5 shows breakthrough profiles
409 acquired by loading lysozyme onto SP Sepharose FF at $10 \mu\text{g/ml}$ under high
410 and low ionic strength conditions. The flow rate was varied to change the
411 value of the Graetz number, and an increase in breakthrough volume was ob-
412 served at lower flow rates. Equation 13 indicates that transport parameters
413 should have a more pronounced effect on the initial breakthrough volume
414 when retention is stronger, due to the K_{eq} weighting of $f\%$. This is consis-
415 tent with the observed behavior at low ionic strength, where K_{eq} is higher.
416 Column models with fit parameters showed excellent agreement at high ionic
417 strength. Although not perfect, the agreement was also quantitatively close
418 at low ionic strength. Discrepancies from simulation under these conditions
419 may be attributable to feedstock component separation, as well as inaccura-
420 cies in describing extra-column effects with the simplified model of a CSTR
421 in series with a PFR, which are more pronounced at low flow rates.

422 The breakthrough volume correlation was also qualitatively validated us-
423 ing FITC-lysozyme in the presence of a mAb. As with lysozyme measure-
424 ments, the flow rate was varied to change the value of the correlation variable
425 under conditions of weak FITC-lysozyme retention. Figure 6 shows break-
426 through profiles that were computed from absorbance measurements at 495
427 and 280 nm, using the average FITC-lysozyme label ratio estimated during
428 fractionation of the conjugation products. Appreciable measurement noise

429 is apparent in the FITC-lysozyme profiles due to the low load concentra-
 430 tion of $\sim 10 \mu\text{g/ml}$. Nonetheless, the observed trend is consistent with the
 431 previous results: using lower flow rates delayed the onset of FITC-lysozyme
 432 breakthrough. This was not modeled explicitly due to the multicomponent
 433 nature of the FITC-lysozyme conjugation products, but it does support the
 434 breakthrough volume correlation qualitatively.

435 4.3. Correlation of SDM parameters

436 A knowledge of phenomenological properties is required to estimate break-
 437 through volumes using Equation 13, specifically values of D_p , D_s , and K_{eq} .
 438 However, such information is typically unknown for impurities such as HCPs
 439 on IEX resins. Methods of estimating these properties could therefore be
 440 useful, and some heuristics already exist for estimating the two intraparti-
 441 cle diffusivities. For instance, D_s is typically an order of magnitude smaller
 442 than D_p under the relevant conditions of weak adsorption, and D_p should
 443 theoretically scale with the free solution diffusivity, D_0 , according to [18]:

$$D_p = \frac{\varepsilon_p \psi_p}{\tau_p} D_0 \quad (14)$$

444 where ψ_p and τ_p are the diffusional hindrance coefficient and the resin tor-
 445 tuosity factor, respectively. If a putative weakly adsorbing HCP has been
 446 identified, its molar mass may be used with the Stokes-Einstein equation or
 447 correlations to estimate D_0 [26]. Appreciable uncertainty surrounds the value
 448 of ψ_p/τ_p , but 0.2 appears to be representative of its order of magnitude [36].
 449 Assuming a value like this enables rough estimation of D_p and D_s based on
 450 protein mass.

451 This leaves the estimation of K_{eq} , which varies with the solution condi-
 452 tions, as the main obstacle to applying the breakthrough volume correlation
 453 in practice. It is expected that K_{eq} will follow a power law in ionic strength
 454 of the SDM form, but the dependence on pH is less well defined. Several
 455 electrostatics models have been proposed for describing this behavior, but
 456 doing so predictively remains an open problem. In the absence of such pre-
 457 dictive tools, insights may be drawn from experimental data on the retention
 458 of model proteins. To facilitate observation of system-independent trends,
 459 isocratic k' measurements at different ionic strengths were consolidated from
 460 the extant literature on 230 protein-pH-resin combinations, as shown in Sup-
 461plementary Figure S2 [20, 29, 37–44]. These data were regressed according to
 462 Equation 9 to extract the SDM parameter ν and the quasi-SDM parameter
 463 $\phi\alpha$, which are plotted against each other in Figure 7 and observed to follow a
 464 significant intrinsically linear correlation (as determined by regressor t-tests).

465 This previously unobserved correlation is expected to be a consequence of
 466 adsorption thermodynamics rather than resin morphology, so the true rela-
 467 tionship represented in Figure 7 is suspected to be between ν and α . Inverse
 468 size exclusion chromatography data are unavailable for the majority of the
 469 resins studied, which precludes estimation of ϕ values that are specific to
 470 protein-resin pairs. However, all phase ratios are expected to be of compara-
 471 ble magnitude, and α may span several orders of magnitude, so the inclusion
 472 of ϕ is not expected to introduce much noise in the correlation. The fact
 473 that $\phi\alpha$ spans several orders of magnitude makes the prediction interval ap-
 474 preciably broad in terms of absolute values, and explaining some of the noise
 475 with additional factors would be advantageous. The ion-exchange type was

476 tested for this purpose, and a significant difference was found between the
477 correlations for AEX and CEX isocratic data (by including an interaction
478 with the categorical variable). The mechanisms underlying this difference
479 are not understood.

480 The utility of these relationships lies in their ability to remove one degree
481 of freedom from the analysis of retention data. A series of measurements
482 are usually performed to estimate SDM parameters, either from isocratic
483 retention at different ionic strengths or elution peak ionic strength under
484 linear gradient salt elutions of different volumes. The identified correlation
485 could potentially enable the estimation of SDM parameters from only one
486 experimental measurement. This concept is illustrated in Figure 8, which
487 shows linear gradient elution data for lysozyme on SP Sepharose FF, collected
488 as part of this study, plotted in the regression space for Yamamoto’s GH
489 analysis [30]. Juxtaposed with these data are predictions from the correlation
490 of isocratic CEX SDM parameters. Close agreement is observed between
491 predictions and experiment at each of the pH values tested. One point in each
492 series would be sufficient to estimate roughly the value of ν , and therefore
493 that of $\phi\alpha$ when using the correlation. However, because the uncertainty in
494 $\phi\alpha$ is with respect to its order of magnitude, the absolute value of its estimate
495 needs to be interpreted with caution.

496 The linear gradient elution data were regressed according to Yamamoto’s
497 method, and the SDM parameters are plotted in Figure 7. Analogous CEX
498 gradient elution data for a mAb and its aggregates that had relatively large
499 SDM parameters were also obtained from the literature and included in Fig-
500 ure 7 [45]. Both sets of gradient elution data are consistent with the correla-

tion of isocratic CEX data within the 95% prediction interval. This confirms the correlation’s utility in removing a degree of freedom from the analysis of retention data. Unfortunately, it does not eliminate the need for some experimental data in estimating K_{eq} , but it may reduce the burden of doing so. As proteomic techniques advance, it may become possible to quantitatively measure HCP retention. This would foreseeably be an expensive operation, and it may be essential to minimize the number of requisite measurements. The SDM parameter correlation may be useful in such an application.

From an intuitive perspective, the essential features of this correlation appear to be broadly consistent with theory. If the characteristic charge indeed represents the number of attractive point charge interactions between the protein and the IEX resin, it seems reasonable to hypothesize that increasing this number at constant ionic strength would result in an approximately proportional increase in the adsorption free energy. This would result in an order-of-magnitude increase in K_{eq} , which at the unit concentration of ionic strength is equivalent to α ; such an argument may rationalize the positive and log-linear correlation between ν and $\phi\alpha$. The reality is necessarily more complex, however, as the adsorption free energy would theoretically be a function of the pH, resin, protein, and the protein’s adsorbed orientation. These are incorporated in a statistical thermodynamic calculation of K_{eq} in Equation 10, albeit implicitly with respect to the resin and protein species. Perhaps the dependence on all four variables can be generalized approximately by the characteristic charge, but this would require evaluation and proof using a rigorous biophysical model. Developing that proof, or at least exhibiting behavior that is consistent with the empirical SDM parameter cor-

526 relation (Figure 7), may provide a good validity test for molecular adsorption
527 models.

528 **5. Conclusions**

529 Unlike concentrated solutes, the approximately linear chromatographic
530 behavior of dilute impurities can lead to diffuse breakthrough. This can
531 make it challenging to remove flow-through impurities completely, but it
532 also enables breakthrough volumes to be analytically related to phenomeno-
533 logical properties. Specifically, the Graetz number can describe transport
534 contributions to dilute solute breakthrough volumes generally when an effec-
535 tive intraparticle diffusivity is used. Knowledge of this relationship enables
536 a problematic equilibrium constant threshold to be estimated, which is on
537 the order of 400 for typical process conditions. However, for this to be used
538 in practice, the IEX adsorption equilibria of impurities of interest must be
539 known. The correlation of SDM model parameters may be useful in estimat-
540 ing such data approximately from one linear gradient elution measurement,
541 and it may serve as a validity test for molecular adsorption models as well.

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546 **Declaration of competing interest**

547 The authors declare that they have no known competing financial inter-
548 ests or personal relationships that could have appeared to influence the work
549 reported in this paper.

550 **CRedit authorship contribution statement**

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560 **Supplementary material**

561 Supplementary material is associated with this article.

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