

**1 Local wind regime induced by giant linear dunes:
2 comparison of ERA5-Land reanalysis with surface
3 measurements**

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10 Abstract

11 Emergence and growth of sand dunes results from the dynamic interaction
12 between topography, wind flow and sediment transport. While feedbacks be-
13 tween these variables are well studied at the scale of a single and relatively
14 small dune, the average effect of a periodic large-scale dune pattern on atmo-
15 spheric flows remains poorly constrained, due to a lack of data in major sand
16 seas. Here, we compare local measurements of surface winds to the predictions
17 of the ERA5-Land climate reanalysis at four locations in Namibia, within and
18 outside the giant linear dune field of the Namib sand sea. In the desert plains
19 to the north of the sand sea, observations and predictions agree well. This
20 is also the case in the interdune areas of the sand sea during the day. Dur-
21 ing the night, however, an additional wind component aligned with the giant
22 dune orientation is measured, in contrast to the easterly wind predicted by

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the ERA5-Land reanalysis. We link these discrepancies, with wind deviation and velocity attenuation larger than 50° and 60 %, to the daily cycle of the turbulent atmospheric boundary layer over a complex topography, and to the associated flow regimes. During the night, a shallow boundary layer induces a flow confinement associated with a strong streamline compression above the giant dunes, resulting in large flow deviations, especially for the lower winds. During the day, the flow confinement is reduced by a thicker boundary layer and higher wind velocities, and the feedback of the giant dunes on the atmospheric flow is negligible. We finally propose that this mechanism and the resulting wind deflections by the giant dunes could explain the occurrence of smaller-scale secondary dune patterns, elongating along a different orientation compared to the primary dunes between which they develop.

Keywords Atmospheric boundary layer · Sand dunes · Flow over hills

³⁶ CITE Chandler et al. (2022)

³⁷ **1 Introduction**

³⁸ The description of turbulent flows over complex topography is relevant for
³⁹ a large variety of different environmental systems (Sherman 1978; Walmsley
⁴⁰ et al. 1982; Baines 1995; Wood 2000; Venditti et al. 2013; Finnigan et al.
⁴¹ 2020). For example, the flow over hills is of primary interest for wind power,
⁴² meteorological and air pollution phenomena (Taylor et al. 1987). The proper-
⁴³ ties of these flows are also key to the understanding of geophysical phenom-
⁴⁴ ena, including the formation of wind-driven waves on the ocean surface (Sulli-
⁴⁵ van and McWilliams 2010), dissolution bedforms (Claudin et al. 2017; Guérin
⁴⁶ et al. 2020), or sedimentary ripples and dunes (Bagnold 1941; Charru et al.
⁴⁷ 2013; Courrech du Pont 2015). Importantly, the troposphere presents a vertical
⁴⁸ structure, with a lower convective boundary layer, of typical kilometer-scale
⁴⁹ thickness, capped by a stably stratified region (Stull 1988). The largest topo-
⁵⁰ graphic obstacles, such as mountains, can therefore interact with this upper
⁵¹ region and lead to internal wave generation or significant wind disturbances,
⁵² such as lee-side downslope winds (Durran 1990).

⁵³ Compared to hills and mountains, aeolian sand dunes offer idealized ele-
⁵⁴ vation profiles for the study of atmospheric turbulent flow over topographies,
⁵⁵ due to their smooth shape, free of canopies. Besides, dunes provide a rather
⁵⁶ wide range of scales, from decameters to kilometers, and very often come in
⁵⁷ a fairly regular pattern, which further simplifies the flow structure analysis.
⁵⁸ Past studies have highlighted two important topographic feedbacks on the
⁵⁹ wind flow close to the dune/hill surface. First is the effect on wind speed, with
⁶⁰ documented flow acceleration on upwind slopes (Weaver and Wiggs 2011) and
⁶¹ deceleration on downwind slopes (Baddock et al. 2007), where the speed-up
⁶² factor is essentially proportional to the obstacle aspect ratio (Jackson and
⁶³ Hunt 1975). Importantly, the velocity maximum is typically shifted upwind
⁶⁴ of the obstacle crest (Jackson and Hunt 1975; Claudin et al. 2013). This be-
⁶⁵ haviour has been theoretically predicted by means of asymptotic analysis of
⁶⁶ a neutrally stratified boundary-layer flow over an obstacle of vanishing as-
⁶⁷ pect ratio (Jackson and Hunt 1975; Mason and Sykes 1979; Sykes 1980; Hunt
⁶⁸ et al. 1988; Belcher and J.C.R. 1998; Kroy et al. 2002). Experiments in flumes
⁶⁹ (Zilker et al. 1977; Zilker and Hanratty 1979; Frederick and Hanratty 1988;
⁷⁰ Poggi et al. 2007; Bristow et al. 2022), in wind tunnels (Gong and Ibbetson
⁷¹ 1989; Finnigan et al. 1990; Gong et al. 1996) and in field conditions at all
⁷² scales (Taylor and Teunissen 1987; Claudin et al. 2013; Fernando et al. 2019;
⁷³ Lü et al. 2021), have also documented this effect. Interestingly, a similar be-
⁷⁴ haviour exists for the pressure perturbation, but with a slight downwind shift
⁷⁵ for the pressure minimum (Claudin et al. 2021). The second effect, much less
⁷⁶ studied, is the flow deflection that occurs when the incident wind direction is
⁷⁷ not perpendicular to the ridge crest. While predicted to be small (less than
⁷⁸ 10°) in the linear regime valid for shallow topography (Gadal et al. 2019),

79 significant flow steering has been reported in the field on the downwind side of
80 steep enough obstacles, such as well-developed sand dunes (Tsoar and Yaalon
81 1983; Sweet and Kocurek 1990; Walker and Nickling 2002; Smith et al. 2017)
82 and in particular coastal foredunes (e.g. Hunter et al. (1983), Rasmussen
83 (1989), Walker et al. (2006), Walker et al. (2009), Hesp et al. (2015), Walker
84 et al. (2017), de Winter et al. (2020)), mountain ranges (Kim et al. 2000; Lewis
85 et al. 2008; Fernando et al. 2019), and valley topographies (Wiggs et al. 2002;
86 Garvey et al. 2005).

87 Wind measurements over sand dunes has been mainly performed over small
88 bedforms, typically a few meters high (corresponding to several tens of me-
89 ters long) (e.g. Mulligan (1988), Hesp et al. (1989), Lancaster et al. (1996),
90 Mckenna Neuman et al. (1997), Sauermann et al. (2003), Andreotti et al.
91 (2002), Walker and Nickling (2002), Weaver and Wiggs (2011)). For prac-
92 tical reasons, fewer studies performed similar measurements on giant dunes
93 (Havholm and Kocurek 1988), with kilometer-scale wavelengths and heights
94 of tens of meters. However, such large dunes provide a choice configuration
95 for the study of turbulent flows over a complex topography. First, one ex-
96 pects larger wind disturbances for larger obstacles. Secondly, their large size
97 can make them interact with the vertical structure of the atmosphere (An-
98 dreotti et al. 2009). Third, they usually form large patterns in sand seas and
99 thus behave as rather clean periodic perturbations, in contrast with isolated
100 dunes. Finally, because the morphodynamics of aeolian bedforms is strongly
101 dependent on the local wind regime (Livingstone and Warren 2019), one can
102 expect to see the consequences of windflow disturbance by large dunes on
103 neighbouring small dunes (Brookfield 1977; Ewing et al. 2006). A similar ef-
104 fect is observed on the properties of impact ripple patterns due to the presence
105 of dunes (Howard 1977; Hood et al. 2021).

106 Atmospheric flows have been much studied at the desert-scale with climate
107 reanalyses based on global atmospheric models (Blumberg and Greeley 1996;
108 Livingstone et al. 2010; Ashkenazy et al. 2012; Jolivet et al. 2021; Hu et al.
109 2021; Gunn et al. 2021b), such as ERA-40, ERA-Interim or ERA5 (Uppala
110 et al. 2005; Dee et al. 2011; Hersbach et al. 2020). However, the spatial reso-
111 lution of these reanalyses (tens of kilometers) implies average quantities that do
112 not resolve the smaller scales of interest, which range from individual dunes
113 to small mountains (Livingstone et al. 2010). Recently, the release of ERA5-
114 Land has partly resolved this limitation by providing up to 70 years of hourly
115 wind predictions at a 9 km spatial resolution (Muñoz-Sabater et al. 2021).
116 However, its validity remains to be studied, especially in remote desert areas
117 where assimilation of measured data is very low.

118 In this work, we compare local wind speeds and directions measured by
119 meteorological stations at four different locations inside and north of the giant
120 linear dune field of the Namib sand sea to the regional predictions of the ERA5-
121 Land climate reanalysis. Where the meteorological stations are surrounded by
122 a relatively flat environment, we show that local measurements and regional
123 predictions agree well. The agreement is also good in the interdune areas of
124 the sand sea, except for some weak winds blowing at night, which exhibit an

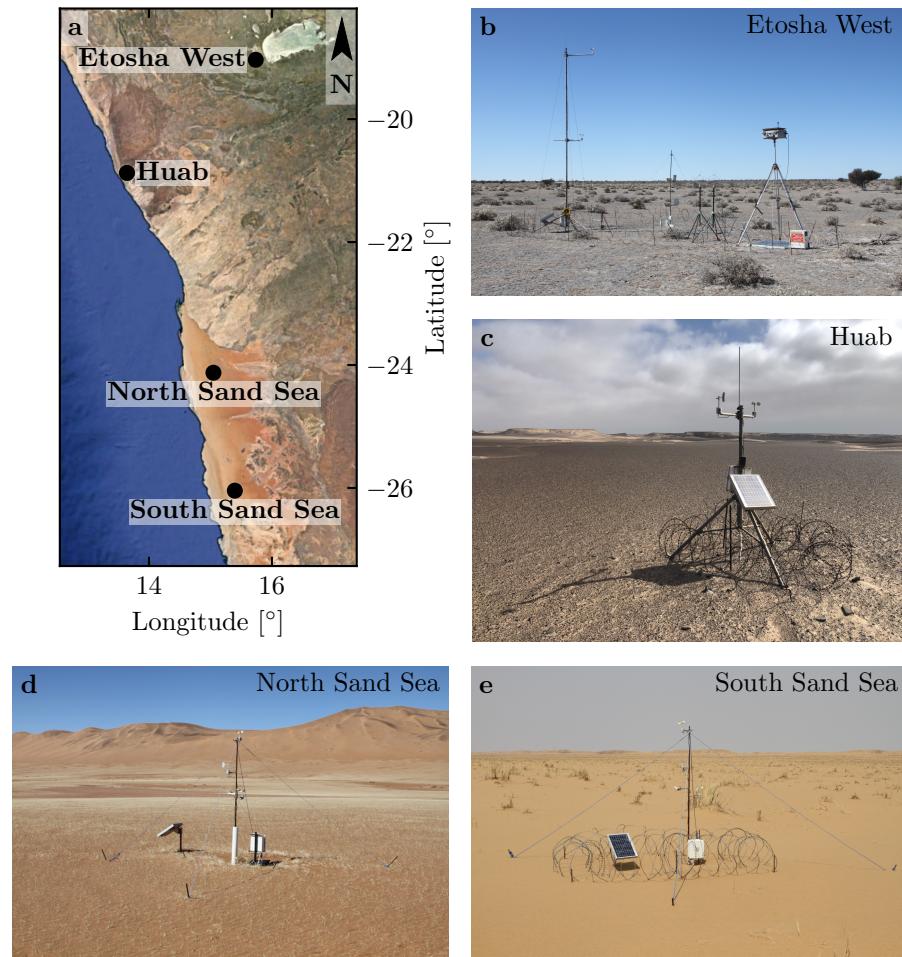


Fig. 1 Studied field sites. **a:** Location of the different sites in Namibia. **b–e:** Photographs of the meteorological stations.

125 additional component aligned with the giant dune orientation. These winds
 126 are not predicted by the ERA5-Land reanalysis (section 2). Further, we are
 127 able to link the magnitude of these differences to the circadian cycle of the
 128 atmospheric boundary layer (section 3). Finally, we draw implications for the
 129 wind disturbances on smaller-scale dunes (section 4), suggesting a possible
 130 origin for crossing dunes.

131 **2 Wind regimes across the Namib Sand Sea**

132 We measured the wind regime at four different locations in Namibia, represen-
 133 tative of various arid environments across the Namib desert (Fig. 1, Fig. 2).

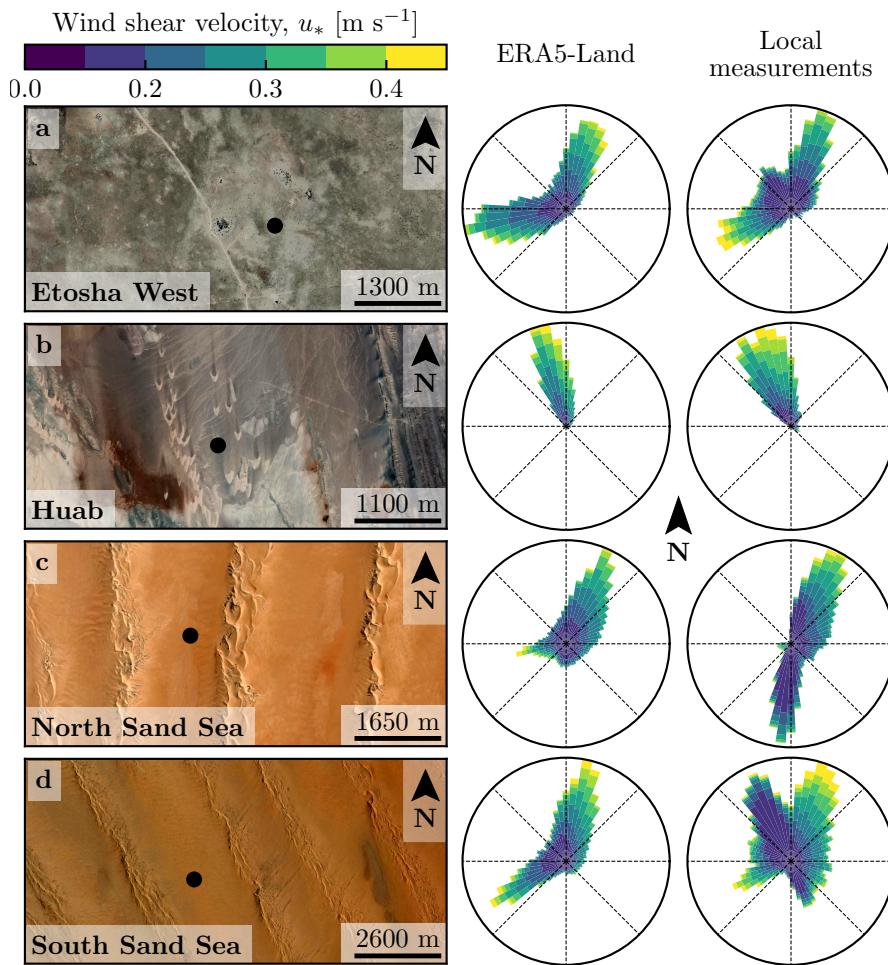


Fig. 2 Wind data used in this study. Satellite images of the different environments (Google-Earth, Maxar Technologies, CNES/Airbus) are shown on the left. The black dots show the location of the wind measurements stations. On the right of the photos, the corresponding wind roses representing the data from the ERA5-Land climate reanalysis and the local wind stations are displayed. Note: the graphical convention for the wind roses is that the bars show the direction towards which the wind blows (see color bar for velocity scale).

134 The Etosha West station was located at the Adamax waterhole to the west
 135 of Etosha Pan in northern Namibia, in a sparsely vegetated area. The Huab
 136 station was near the coast on a hyper-arid flat gravel plain lying north the
 137 ephemeral Huab river. Here, barchan dunes up to a few meters in height de-
 138 velop from the sediment blowing out of the river valley (Nield et al. 2017;
 139 Hesp and Hastings 1998). These two stations were both located in relatively
 140 flat environments. In contrast, the North Sand Sea and South Sand Sea sta-
 141 tions were located in the interdunes between linear dunes with kilometer-scale

wavelengths, hectometer-scale heights and superimposed patterns. In this section, we describe and compare winds from local measurements and climate reanalysis predictions.

2.1 Wind and elevation data

At each meteorological station (Fig. 1), wind speed and direction were sampled every 10 minutes using cup anemometers (Vector Instruments A100-LK) and wind vanes (Vector Instruments W200-P) at a single height, which was between 2 m and 3 m depending on the station. The available period of measurements at each station ranged from 1 to 5 discontinuous years distributed between 2012 and 2020 (Online Resource Fig. S1). We checked that at least one complete seasonal cycle was available for each station. Regional winds were extracted at the same locations and periods from the ERA5-Land dataset, which is a replay at a smaller spatial resolution of ERA5, the latest climate reanalysis from the ECMWF (Hersbach et al. 2020; Muñoz-Sabater et al. 2021). This dataset provided hourly predictions of the 10-m wind velocity and direction at a spatial resolution of $0.1^\circ \times 0.1^\circ$ ($\simeq 9$ km in Namibia).

To enable direct comparison, the local wind measurements were averaged into 1-hr bins centered on the temporal scale of the ERA5-Land estimates (Online Resource Fig. S2). As the wind velocities of both datasets were provided at different heights, we converted them into shear velocities u_* (Online Resource section 1), characteristic of the turbulent wind profile. Wind roses in Fig. 2 show the resulting wind data.

Dune properties were computed using autocorrelation on the 30-m Digital Elevation Models (DEMs) of the shuttle radar topography mission (Farr et al. 2007). For the North and South Sand Sea stations, we obtain, respectively, orientations of 85° and 125° with respect to the North, wavelengths of 2.6 km and 2.3 km and amplitudes (or half-heights) of 45 m and 20 m (Online Resource Fig. S4 for more details). This agrees with direct measurements made on site.

2.2 Comparison of local and regional winds

The measured and predicted wind regimes are shown in Fig. 2. In the Namib, the regional wind patterns are essentially controlled by the sea breeze, resulting in strong northward components (sometimes slightly deviated by the large scale topography) present in all regional wind roses (Lancaster 1985). These daytime winds are dominant during the period October-March (Fig. 3f and Online Resource Fig. 4f). During April-September, an additional (and often nocturnal) easterly component can also be recorded, induced by the combination of katabatic winds forming in the mountains, and infrequent ‘berg’ winds, which are responsible for the high wind velocities observed (Lancaster et al. 1984). The frequency of these easterly components decreases from inland to the coast. As a result, bidirectional wind regimes within the Namib Sand Sea

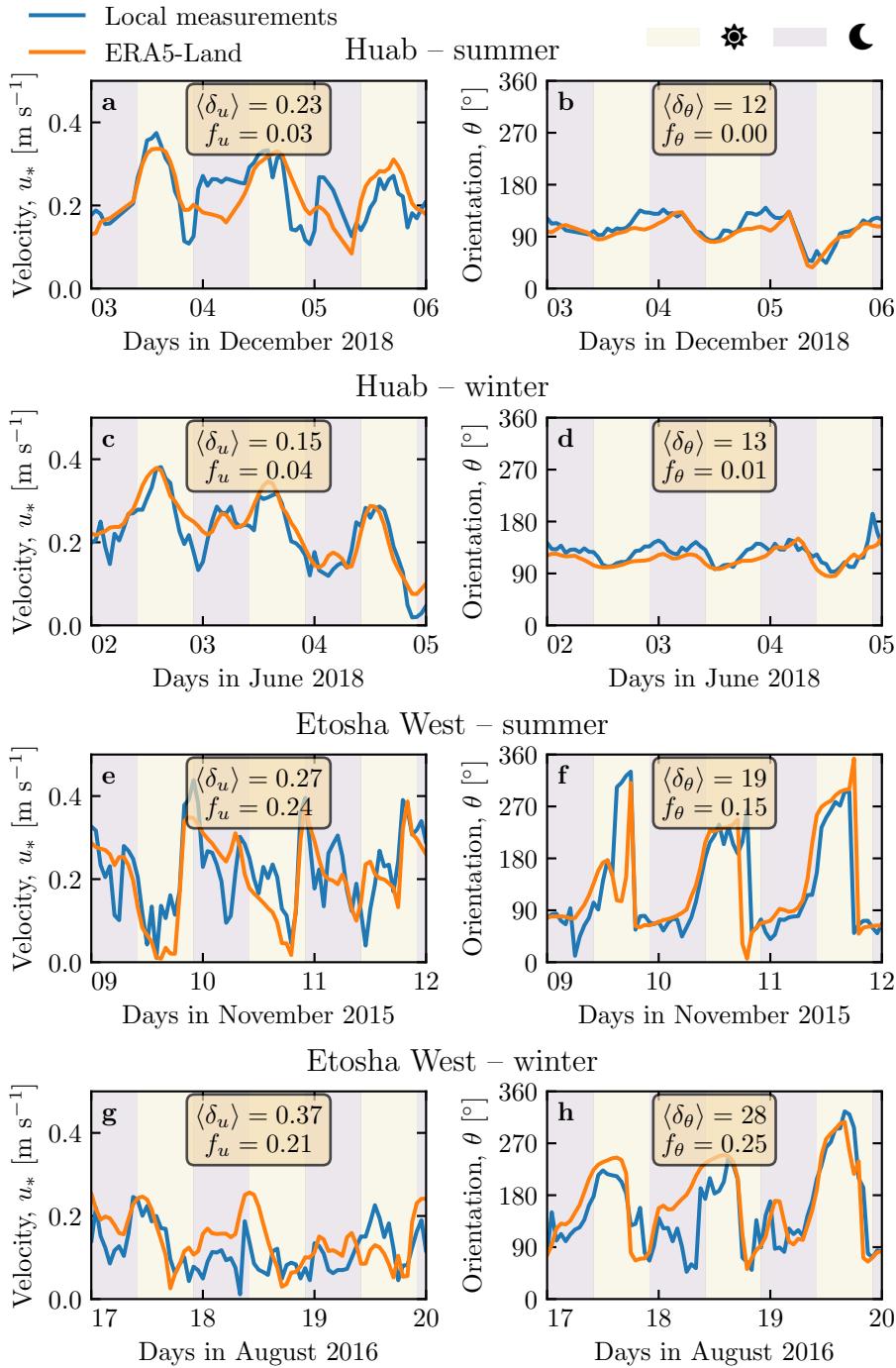


Fig. 3 Temporal comparison between the wind data coming from the ERA5-Land climate reanalysis (orange lines) and from the local measurements (blue lines). Coloured swathes indicate day (between 10.00 UTC and 22.00 UTC) and night (before 10.00 UTC or after 22.00 UTC). Numbers in legends indicate the average flow deflection δ_θ and relative wind modulation δ_u over the displayed period (see section 3.2 for their definitions), as well as the percentage f_θ and f_u of occurrence of extreme events ($\delta_\theta > 50^\circ$, $|\delta_u| > 0.6$). **a–b**: Huab station in summer. **b–c**: Huab station in winter. **d–e**: Etosha West station in summer. **f–g**: Etosha West station in winter. Time series of the two other stations are shown in Fig. 5.

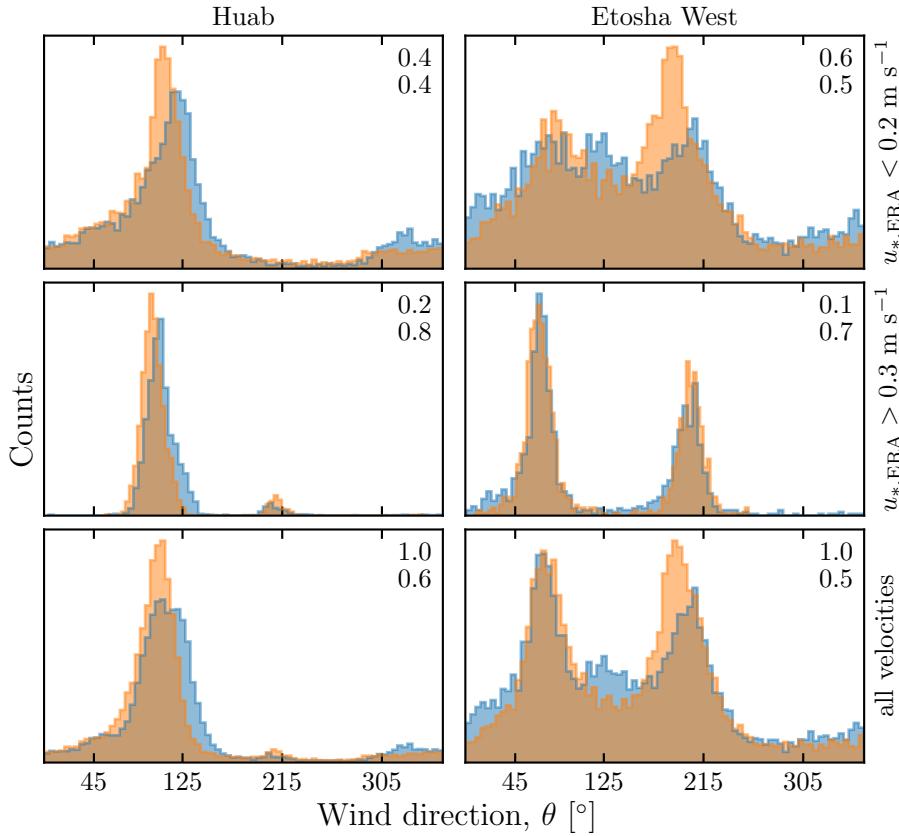


Fig. 4 Distributions of wind direction at Huab and Etosha West stations for the ERA5-Land climate reanalysis (orange) and the local measurements (blue). In each subplot, both distributions are plotted from the same time steps, selected for different ranges of the wind wind velocity (rows) in the ERA5-Land dataset. The numbers at the upper right corners give the percentage of time steps selected in each sub-range (top), as well as the percentage of them corresponding to the day – defined between 10.00 UTC and 22.00 UTC (bottom).

182 and at the west Etosha site (Fig. 2a,c,d) and a unidirectional wind regime on
183 the coast at the outlet of the Huab River (Fig. 2b) are observed.

184 In the case of the Etosha West and Huab stations, the time series of wind
185 speed and direction from the regional predictions quantitatively match those
186 corresponding to the local measurements (Figs. 3, 4 and Online Resource
187 Fig. S5). For the North Sand Sea and South Sand Sea stations within the giant
188 linear dune field, we observe that this agreement is also good, but limited to the
189 October-March time period (Fig. 4a, b, e, f). However, the field-measured wind
190 roses exhibit additional wind components aligned with the dune orientation,
191 as evidenced on the satellite images (Fig. 2c,d).

192 More precisely, during the April-September period, the local and regional
193 winds in the interdune match during daytime only, i.e when the southerly/southwesterly
194 sea breeze dominates (Figs. 5c,d,g,h and 6). In the late afternoon and during

the night, when the easterly ‘berg’ and katabatic winds blow, measurements and predictions differ. In this case, the angular wind distribution of the local measurements exhibits two additional modes corresponding to reversing winds aligned with the dune orientation (purple frame in Fig. 6, Online Resource Fig. S6). This deviation is also associated with a general attenuation of the wind strength (Online Resource Fig. S7). Remarkably, all these figures show that these wind reorientation and attenuation processes occur only at low velocities of the regional wind, typically for $u_*^{\text{ERA5-Land}} \lesssim 0.2 \text{ m s}^{-1}$. For shear velocities larger than $u_*^{\text{ERA5-Land}} \simeq 0.3 \text{ m s}^{-1}$, the wind reorientation is not apparent. Finally, for intermediate shear velocities, both situations of wind flow reoriented along the dune crest and not reoriented can be successively observed (Online Resource Fig. S6). Importantly, these values are not precise thresholds (and certainly not related to the threshold for sediment transport), but indicative of a crossover between regimes, whose physical interpretation is discussed in the next section.

3 Influence of wind speed and circadian cycle on the atmospheric boundary layer

The wind deflection induced by dunes has previously been related to the incident angle between wind direction and crest orientation, with a maximum deflection evident for incident angles between 30° and 70° (Walker et al. 2009; Hesp et al. 2015). In the data analysed here, the most deflected wind at both the North and South Sand Sea stations is seen to be where the incident angle is perpendicular to the giant dunes (Figs. 2 and 6). It therefore appears that in our case, the incident wind angle is not the dominant control on maximum wind deflection. Further, and as shown in Fig. 6, winds of high and low velocities show contrasting behaviour in characteristics of deflection. This suggests a change in hydrodynamical regime between the winds. In this section, we discuss the relevant parameters associated with the dynamical mechanisms that govern the interactions between the atmospheric boundary layer flow and giant dune topographies. This analysis allows us to provide a physics-based interpretation of our measured wind data.

3.1 Flow over a modulated bed

Taking as a reference the turbulent flow over a flat bed, the general framework of our study is understanding and describing the flow response to a bed modulation (e.g. a giant dune). Without loss of generality, we can consider in this context an idealised bed elevation in the form of parallel sinusoidal ridges, with wavelength λ (or wavenumber $k = 2\pi/\lambda$) and amplitude ξ_0 , and where the reference flow direction makes a given incident angle with respect to the ridge crest (Andreotti et al. 2012). Part of this response, on which we focus here, is the flow deflection by the ridges. In a simplified way, it can be understood

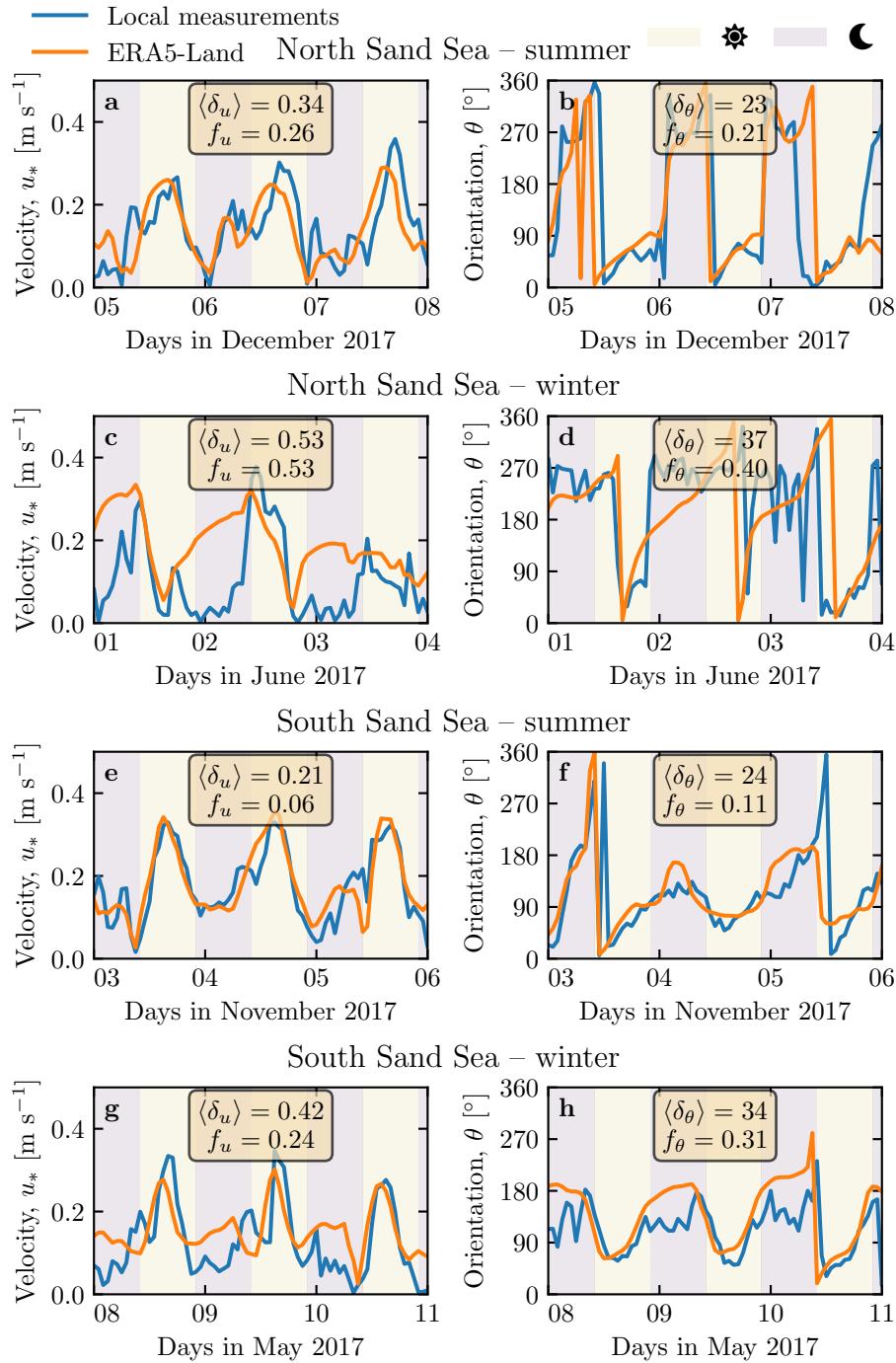


Fig. 5 Same as Fig. 3 for North Sand Sea station in summer (a–b), North Sand Sea station in winter (b–c), South Sand Sea station in summer (d–e) and South Sand Sea station in winter (f–g).

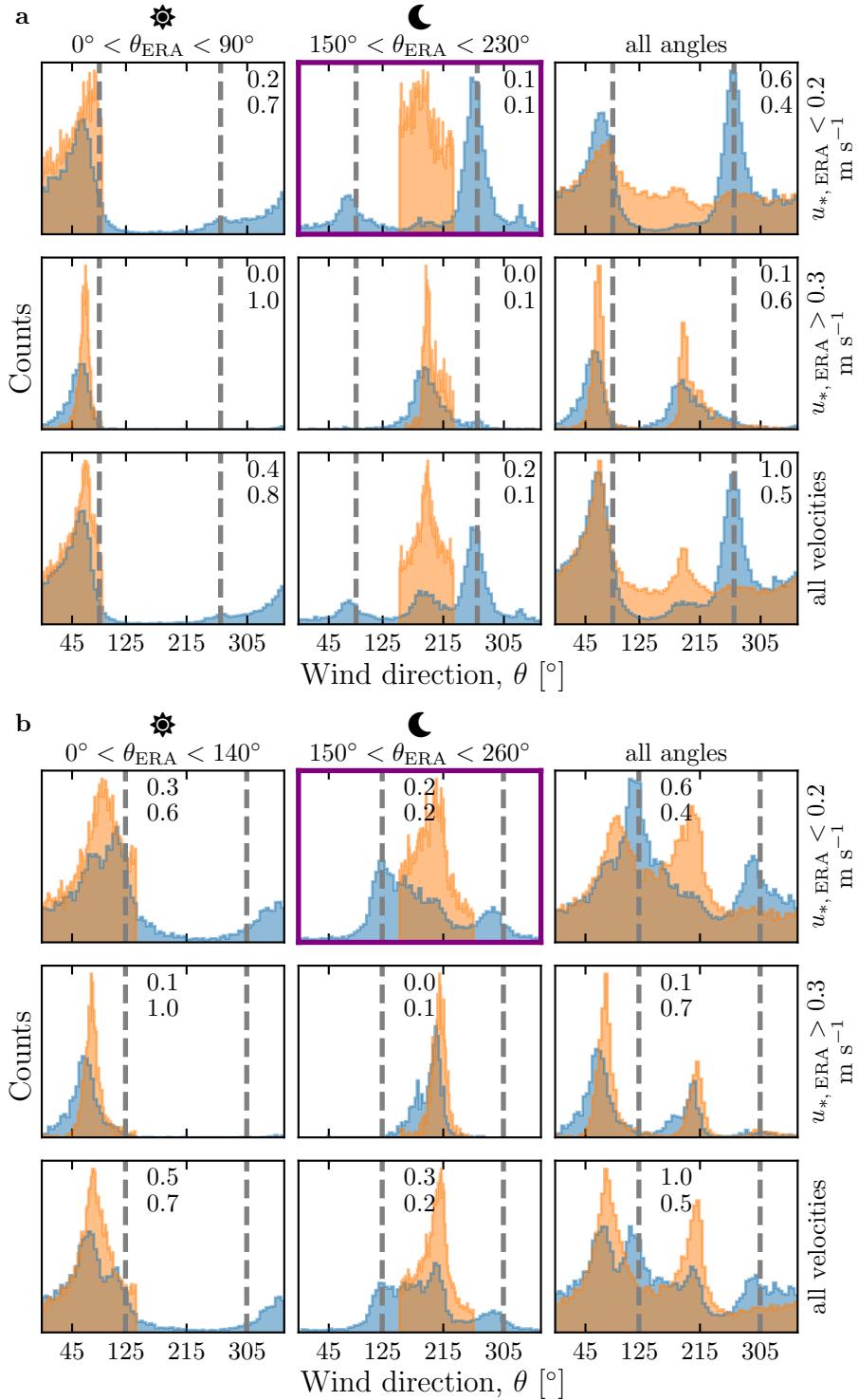


Fig. 6 Same as Fig. 4 but for North Sand Sea (a) and South Sand Sea (b) stations. Here, subplots correspond to different ranges for the wind direction (columns) and wind velocity (rows) of the ERA5-Land dataset. The grey vertical dashed lines indicate the main dune orientation. In contrast with observations at the Huab and Etosha West stations (Fig. 4), histograms do not match well at low wind velocities, and the purple frame highlights the regime (low wind velocities, nocturnal easterly wind) in which the data from both datasets differ most.

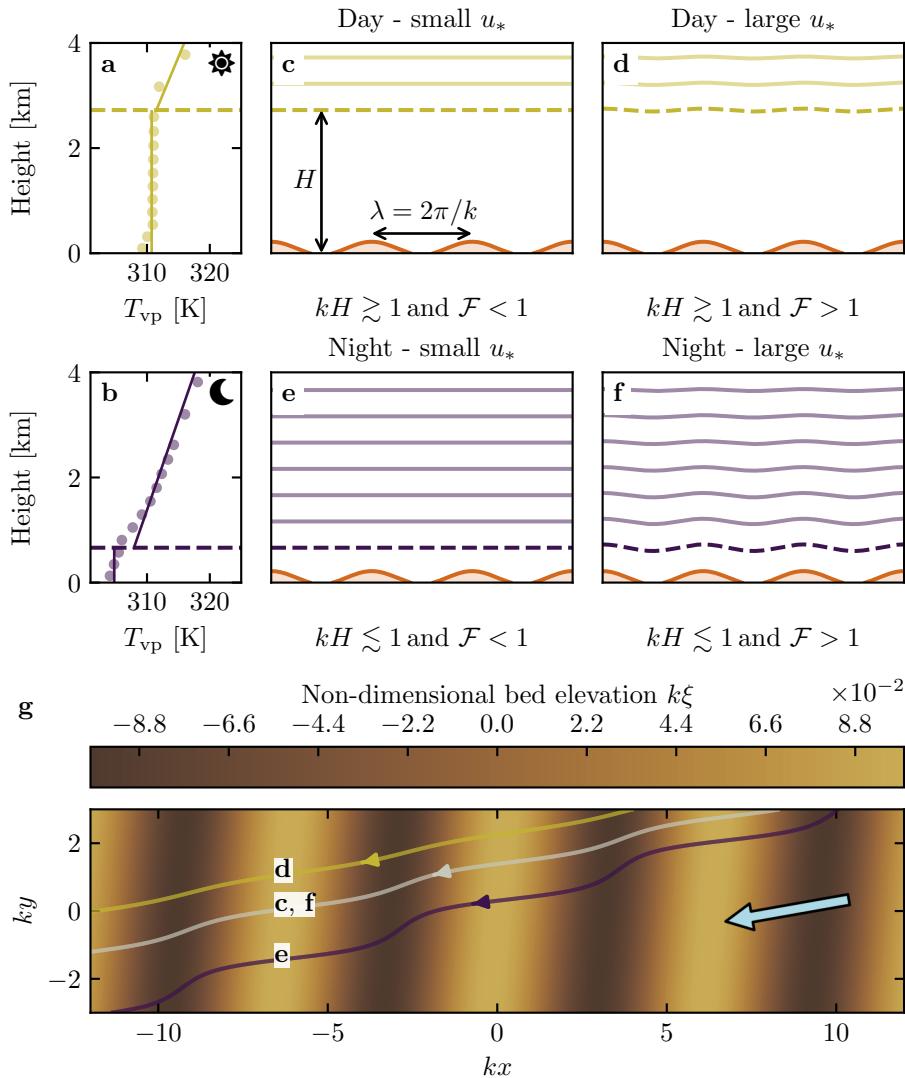


Fig. 7 **a–b:** Vertical profiles of the virtual potential temperature T_{vp} at two different time steps (day - 03/11/2015 - 12.00 UTC, night - 01/13/2013 - 09.00 UTC) at the North Sand Sea station. Dots: data from the ERA5 reanalysis. Dashed lines: boundary layer height given by the ERA5 reanalysis (Online Resource section 2). Plain lines: vertical (boundary layer) and linear (free atmosphere) fits to estimate the stratification properties. **c–f:** Sketches representing the interaction between the giant dunes and the atmospheric flow for different meteorological conditions. **g:** Streamlines over a sinusoidal topography $\xi(x, y)$ qualitatively representing the effect of low, medium and strong flow confinement, in relation to the above panels (see Appendix 1 for more details). The blue arrow indicates the undisturbed wind direction.

from the Bernoulli principle (Hesp et al. 2015): as the flow approaches the ridge crest, the compression of the streamlines results in larger flow velocities, and thus lower pressures (Jackson and Hunt 1975). An incident flow oblique to the ridge is then deflected towards lower pressure zones, i.e towards the crest. Turbulent dissipation tends to increase this effect downstream, resulting in wind deflection along the crest in the lee side (Gadal et al. 2019).

Flow confinement below a capping surface, which enhances streamline compression, has a strong effect on the hydrodynamic response and typically increases flow deflection. This is the case for bedforms forming in open channel flows such as rivers (Kennedy 1963; Chang and Simons 1970; Mizumura 1995; Colombini 2004; Fourrière et al. 2010; Andreotti et al. 2012; Unsworth et al. 2018). This is also relevant for aeolian dunes as they evolve in the turbulent atmospheric boundary layer (ABL) capped by the stratified free atmosphere (FA) (Andreotti et al. 2009). Two main mechanisms, associated with dimensionless numbers must then be considered (Fig. 7). First, topographic obstacles typically disturb the flow over a characteristic height similar to their length. As flow confinement is characterised by a thickness H , the interaction between the dunes and the wind in the ABL is well captured by the parameter kH . The height H is directly related to the sensitive heat flux from the Earth surface. It is typically on the order of a kilometre, but significantly varies with the circadian and seasonal cycles. Emerging and small dunes, with wavelengths in the range 20 to 100 m, are not affected by the flow confinement, corresponding to $kH \gg 1$. For giant dunes with kilometer-scale wavelengths, however, their interaction with the FA can be significant (Andreotti et al. 2009). This translates into a parameter kH in the range 0.02–5, depending on the moment of the day and the season. A second important mechanism is associated with the existence of a thin intermediate so-called capping layer between the ABL and the FA. It is characterised by a density jump $\Delta\rho$, which controls the ‘rigidity’ of this interface, i.e. how much its deformation affects streamline compression. This is usually quantified using the Froude number (Vosper 2004; Stull 2006; Sheridan and Vosper 2006; Hunt et al. 2006; Jiang 2014):

$$\mathcal{F} = \frac{U}{\sqrt{\frac{\Delta\rho}{\rho_0} g H}}, \quad (1)$$

where U is the wind velocity at the top of the ABL and ρ_0 its average density. The intensity of the stratification, i.e. the amplitude of the gradient $|\partial_z \rho|$ in the FA, also impacts the ability to deform the capping layer under the presence of an underlying obstacle, and thus affects the influence of flow confinement. This can be quantified using the internal Froude number (Vosper 2004; Stull 2006; Sheridan and Vosper 2006; Hunt et al. 2006; Jiang 2014) $\mathcal{F}_I = kU/N$, where $N = \sqrt{-g\partial_z \rho / \rho_0}$ is the Brunt-Väisälä frequency (Stull 1988). Both Froude numbers have in practice the same qualitative effect on flow confinement (a smaller Froude corresponding to a stiffer interface), and we shall restrict the main discussion to \mathcal{F} only.

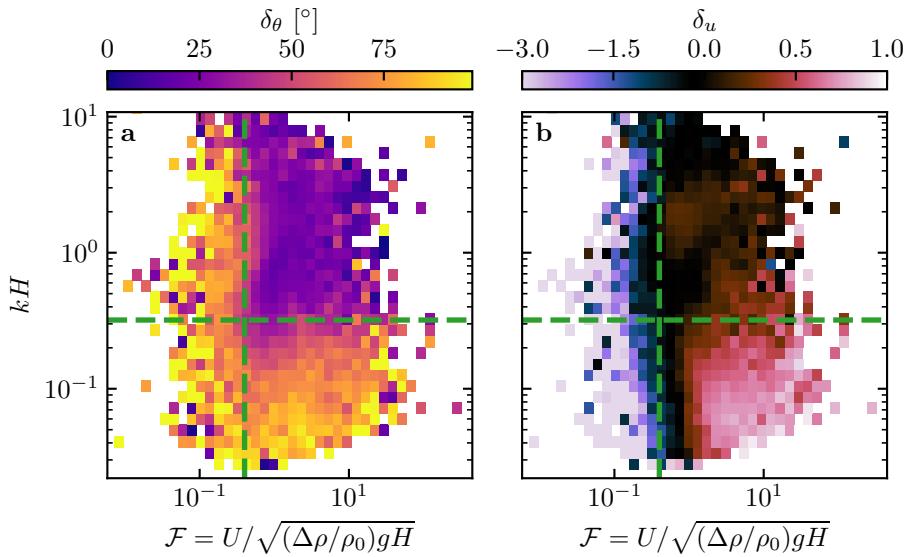


Fig. 8 Regime diagrams of the wind deviation δ_θ (a) and relative attenuation/amplification δ_u (b) in the space (\mathcal{F}, kH) , containing the data from both the North Sand Sea and South Sand Sea stations. The green dashed lines empirically delimit the different regimes. The point density in each bin of the diagrams is shown in Online Resource Fig. S10 – 95% of the data occur in the range $-1 < \delta u < 1$. Similar regime diagrams in the spaces (\mathcal{F}_I, kH) and $(\mathcal{F}_I, \mathcal{F})$ are shown in Online Resource Fig. S11.

With this theoretical framework in mind, and in the context of the measured wind data in the North and South Sand Sea stations, the smallest wind disturbances are expected to occur during the day, when the ABL depth is the largest and comparable to the dune wavelength ($kH \gtrsim 1$), which corresponds to a weak confinement situation (Fig. 7c,d). In contrast, large wind disturbances are expected to occur during the night, when the confinement is mainly induced by a shallow ABL (Fig. 7e). However, this strong confinement can be somewhat reduced in the case of strong winds, corresponding to large values of the Froude number and a less ‘rigid’ interface (Fig. 7f). This is in qualitative agreement with the transition from deflected to non-deflected winds related to low and high velocities observed in our data (Sec. 2.2).

3.2 Data distribution in the flow regimes

We can go one step further and analyse how our data quantitatively spread over the different regimes discussed above. For that purpose, one needs to compute kH and \mathcal{F} from the time series. H , U and the other atmospheric parameters can be deduced from the various vertical profiles (temperature, humidity) available in the ERA5 climate reanalysis (Online Resource section 2). We quantify the flow deflection δ_θ as the minimal angle between the wind orientations comparing the local measurements and the regional predictions.

295 We also compute the relative velocity modulation as

$$\delta_u = \frac{u_*^{\text{ERA5-Land}} - u_*^{\text{Local mes.}}}{u_*^{\text{ERA5-Land}}}. \quad (2)$$

296 These two quantities are represented as maps in the plane (\mathcal{F}, kH) (Fig. 8a,b),
 297 and one can clearly identify different regions in these graphs. Small wind dis-
 298 turbances (small δ_θ and δ_u) are located in the top-right part of the diagrams,
 299 corresponding to a regime with low-interaction as well as low-confinement (kH
 300 and \mathcal{F} large enough, Fig. 7d). Lower values of kH (stronger interaction) or of
 301 Froude number (stronger confinement) both lead to an increase in wind dis-
 302 turbances, both in terms of orientation and velocity. Below a crossover value
 303 $kH \simeq 0.3$, wind disturbance is less sensitive to the \mathcal{F} -value. This is probably
 304 due to enhanced non-linear effects linked to flow modulation by the obstacle
 305 when confinement is strong (e.g. wakes and flow recirculations). The Froude
 306 number also controls a transition from damped to amplified wind velocities
 307 in the interdune, with a crossover around $\mathcal{F} \simeq 0.4$ (Fig. 8b). Such an ampli-
 308 fication is rather unexpected. Checking the occurrence of the corresponding
 309 data, it appears that these amplifications are associated with the southerly
 310 sea breeze, and occur dominantly during the October-March period, when the
 311 other easterly wind is not present (Online Resource Fig. S12a–b). Further-
 312 more, they occur less frequently during the afternoon, and more frequently
 313 at the end of the day (Online Resource Fig. S12c). This effect may be linked
 314 to a change in the flow behaviour in the lee side of the obstacles but further
 315 measurements are needed in order to assess the different possibilities (Baines
 316 1995; Vosper 2004).

317 It is important to discuss the sensitivity of the results with respect to
 318 the choice of the hydrodynamic roughnesses (see Online Resource section 4).
 319 In fact, the only quantities dependent on this choice are those which involve
 320 the amplitude of the velocities: wind shear velocities, Froude number \mathcal{F} and
 321 relative velocity modulation δ_u . Those associated with wind direction are inde-
 322 pendent of this choice. Considering the possible range of realistic roughnesses
 323 values, the uncertainty on velocities estimated using the law of the wall is
 324 at most 30%. A similar maximum uncertainty applies to the Froude number.
 325 This uncertainty also propagates to δ_u , for which Figure S14 shows that the
 326 choice of roughness has little influence of its temporal variations, even if it can
 327 induce a global increase or decrease of its values. As such, the choice of z_0 will
 328 not qualitatively affect the overall aspect of the regime diagram presented in
 329 Figure 8b. It may only change the crossover value of δ_u at which the transition
 330 between regimes is observed (dashed green lines in that figure). Our conclu-
 331 sions are thus robust with respect to the somewhat arbitrary choice of the
 332 hydrodynamic roughnesses in the use of the data from ERA5-Land reanalysis.

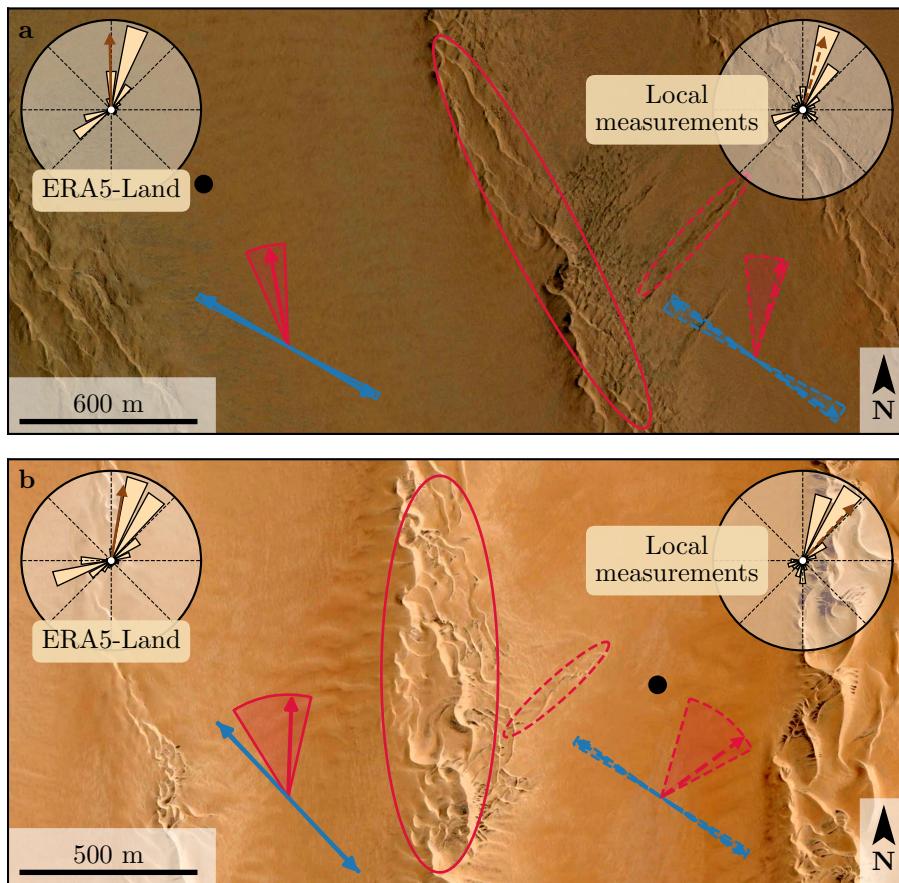


Fig. 9 Implications for smaller scale patterns in (a) the South Sand Sea and (b) North Sand Sea. The ellipses indicate the different types of elongating dunes, at large (plain line) and small (dashed line) scales. Dune orientation are predicted using the model of Courrech du Pont et al. (2014) from the sand flux angular distributions, shown here (roses) along with the resultant transport direction (brown arrow) for typical values (grain size $180 \mu\text{m}$, flux-up ratio of 1.6). Code for corresponding arrows: use of ERA5-Land data (plain line), use of local measurements (dashed line), prediction for the bed instability growth mechanism (blue), prediction for the elongation growth mechanism (red). Wedges show the uncertainty on the orientation calculation when parameters are varied. The black dots indicate the location of the meteorological stations in the interdune. See Appendix 2 for additional details.

333 4 Discussion and conclusion

334 The feedback of the giant dunes on the wind flow has important implications
 335 for smaller scales bedforms. As illustrated in Fig. 9, small linear dunes ($\sim 50 \text{ m}$
 336 wide) are often present in the 1–2 km interdune between giant linear dunes
 337 in the Namib Sand Sea (Livingstone et al. 2010). These smaller dunes do not
 338 exhibit the same orientation as the large ones, and are sometimes named ‘cross-
 339 ing dunes’ (Chandler et al. 2022). Whilst differences between large and small

scale dune patterns are observed ubiquitously, they are usually attributed to the presence of two different dune growth mechanisms, leading to two different dune patterns (orientations and/or morphologies) for the same wind regime (Courrech du Pont et al. 2014; Runyon et al. 2017; Lü et al. 2017; Song et al. 2019; Gadal et al. 2020; Hu et al. 2021). Here, however, our arguments enable the development of differing orientations for the small and giant linear dunes governed by the same dune growth mechanism (elongating mode). Figure 9 shows how the orientations for the small and giant dunes can be derived from the locally measured and regionally predicted winds respectively (red arrows in Fig. 9). These predictions require to specify the threshold of aeolian sand transport. Importantly, its value (a shear velocity estimated $u_{\text{th}} \simeq 0.15 \text{ m s}^{-1}$) is reached in the winds which are deflected – recall that the larger winds are not deflected, see Fig. 6. The feedback of the giant dunes on the wind described in this study thus provides a potential explanation for the existence of these small linear dunes elongating across the interdune, a dynamic which has remained unresolved to date. These crossing dunes could provide additional constraints for the inference of local winds from bedforms, similarly to that currently performed on Mars using ripple orientations (Liu and Zimbelman 2015; Hood et al. 2021). Further work is needed to investigate these processes in more detail, including measurements of sediment transport and flow on the top of dunes.

This study presents the evidence that wind flow patterns around giant dunes are influenced by the atmospheric boundary layer, particularly during nocturnal conditions. However, we do not address here the question of the limitation of their pattern coarsening, and leave open the debate as to whether the size of giant dunes is controlled by the depth of this layer (Andreotti et al. 2009), in contrast to sediment supply limited and ever-slower growth with size (Werner and Kocurek 1999; Gunn et al. 2021a). More field evidence is definitively needed from additional dune fields, but this mechanism would allow for the inference of the ABL depth from giant bedform wavelengths where measurements are not feasible or available, such as Titan (Lorenz et al. 2010).

To conclude on conditions under which the ERA5-Land reanalysis data can reliably be used to study dune morphodynamics, we summarise the comparison of local (direct measurements) and regional (climate reanalysis) wind data as follows. In flat areas, the agreement between the two confirms the ability of the ERA5-Land climate reanalysis to predict the wind regime down to scales $\sim 10 \text{ km}$, i.e. the model grid. When smaller scale topographies are present (giant dunes in our case), locally measured winds can significantly differ from the regionally predicted ones. This is the case when the disturbances induced by the dunes interact with the lower part of the ABL vertical structure, which presents circadian variations. During the day, when the capping layer is typically high, this interaction is small, and the ERA5-Land predictions are also quantitatively consistent with the local data. During the night, however, the presence of a shallow atmospheric boundary layer induces a strong confinement of the flow, and is associated with large wind deflection by the dunes.

386 Importantly, we find that this effect can be counterbalanced for large wind
387 velocities, which are capable of deforming the capping layer, thus decreasing
388 the influence of the confinement.

389 The theoretical computation of the wind disturbances induced by sinu-
390 soidal ridges under flow confinement has been performed in the linear limit
391 (Andreotti et al. 2009, 2012), i.e. when the aspect ratio of these ridges is small
392 ($k\xi_0 \ll 1$). These models are able to qualitatively reproduce the observed
393 wind deflection (Appendix 1, Online Resource Figs. S11 and S13), and thus
394 provide the physical support for the interpretation we propose here based on
395 hydrodynamic regimes. However, these models cannot quantitatively predict
396 the magnitude of our observations, probably due to the presence of expected
397 non-linearities in high confinement situations linked to strong flow modula-
398 tions. Besides, these linear calculations only predict wind attenuation in the
399 interdune, in contrast with the observed enhanced velocities associated with
400 particular evening winds from the South during the period October–March
401 (Online Resource Fig. S12). Some other models predict different spatial flow
402 structures in response to a modulated topography, such as lee waves and
403 rotors (Baines 1995; Vosper 2004). However, our measurements are located at a
404 single point in the interdune, and we are thus unable to explore these types of
405 responses. Data at different places along and across the ridges are needed to
406 investigate and possibly map such flow structures, and for further comparisons
407 with the models.

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435 **Appendix 1: Linear theory of wind response to topographic pertur-**
436 **bation**

437 Following the work of Fourrière et al. (2010), Andreotti et al. (2012) and
438 Andreotti et al. (2009), we briefly describe in this appendix the framework
439 for the linear response of a turbulent flow to a topographic perturbation of
440 small aspect ratio. As a general bed elevation can be decomposed into Fourier
441 modes, we focus here on a sinusoidal topography:

$$\xi = \xi_0 \cos [k (\cos(\alpha)y - \sin(\alpha)x)], \quad (3)$$

442 which is also a good approximation for the giant dunes observed in the North
443 Sand Sea and South Sand Sea Station (Fig. 2 and Online Resource Fig. S4).
444 Here, x and y are the streamwise and spanwise coordinates, $k = 2\pi/\lambda$ the
445 wavenumber of the sinusoidal perturbation, α its crest orientation with respect
446 to the x -direction (anticlockwise) and ξ_0 its amplitude. The two components
447 of the basal shear stress $\tau = \rho_0 u_* \mathbf{u}_*$, constant in the flat bottom reference
448 case, can then be generically written as:

$$\tau_x = \tau_0 \left(1 + k\xi_0 \sqrt{\mathcal{A}_x^2 + \mathcal{B}_x^2} \cos [k (\cos(\alpha)y - \sin(\alpha)x) + \phi_x] \right), \quad (4)$$

$$\tau_y = \tau_0 k\xi_0 \sqrt{\mathcal{A}_y^2 + \mathcal{B}_y^2} \cos [k (\cos(\alpha)y - \sin(\alpha)x) + \phi_y], \quad (5)$$

449 where τ_0 is the reference basal shear stress on a flat bed. We have defined
450 the phase $\phi_{x,y} = \tan^{-1}(\mathcal{B}_{x,y}/\mathcal{A}_{x,y})$ from the in-phase and in-quadrature hy-
451 drodynamical coefficients $\mathcal{A}_{x,y}$ and $\mathcal{B}_{x,y}$. They are functions of k and of the
452 flow conditions, i.e the bottom roughness, the vertical flow structure and the
453 incident flow direction, and the theoretical framework developed in the above
454 cited papers proposes methods to compute them in the linear regime.

455 Following Andreotti et al. (2012), the effect of the incident wind direction
456 can be approximated by the following expressions:

$$\mathcal{A}_x = \mathcal{A}_0 \sin^2 \alpha, \quad (6)$$

$$\mathcal{B}_x = \mathcal{B}_0 \sin^2 \alpha, \quad (7)$$

$$\mathcal{A}_y = -\frac{1}{2} \mathcal{A}_0 \cos \alpha \sin \alpha, \quad (8)$$

$$\mathcal{B}_y = -\frac{1}{2} \mathcal{B}_0 \cos \alpha \sin \alpha, \quad (9)$$

457 where \mathcal{A}_0 and \mathcal{B}_0 are now two coefficients independent of the dune orienta-
458 tion α , corresponding to the transverse case ($\alpha = 90^\circ$). In the case of a fully
459 turbulent boundary layer capped by a stratified atmosphere, these coefficients
460 depend on kH , kz_0 , \mathcal{F} and \mathcal{F}_I (Andreotti et al. 2009). For their computation,
461 we assume here a constant hydrodynamic roughness $z_0 \simeq 1$ mm (Online Re-
462 source section 1). For the considered giant dunes, this leads to $kz_0 \simeq 2 \cdot 10^{-6}$,
463 as their wavelength is $\lambda \simeq 2.4$ km (or $k \simeq 2 \cdot 10^{-3}$ m $^{-1}$). Values of z_0 extracted
464 from field data indeed typically fall between 0.1 mm and 10 mm (Sherman and

⁴⁶⁵ Farrell 2008; Field and Pelletier 2018). Importantly, \mathcal{A}_0 and \mathcal{B}_0 do not vary
⁴⁶⁶ much in the corresponding range of kz_0 (Fourrière et al. 2010), and the results
⁴⁶⁷ presented here are robust with respect to this choice.

⁴⁶⁸ With capping layer height and Froude numbers computed from the ERA5-
⁴⁶⁹ Land time series, the corresponding \mathcal{A}_0 and \mathcal{B}_0 can be deduced, as displayed
⁴⁷⁰ in Online Resource Fig. S13. Interestingly, it shows similar regimes as in the
⁴⁷¹ diagrams of Fig. 8 and Online Resource Fig. S11a,b, supporting the underlying
⁴⁷² physics. However, the agreement is qualitative only. Further, the linearity
⁴⁷³ assumption of the theoretical framework requires $(|\tau| - \tau_0)/\tau_0 \ll 1$, which
⁴⁷⁴ translates into $k\xi\sqrt{\mathcal{A}_0^2 + \mathcal{B}_0^2} \ll 1$. In our case, the giant dune morphology
⁴⁷⁵ gives $k\xi_0 \simeq 0.1$, which means that one quits the regime of validity of the
⁴⁷⁶ linear theory when the coefficient modulus $\sqrt{\mathcal{A}_0^2 + \mathcal{B}_0^2}$ becomes larger than a
⁴⁷⁷ few units. In accordance with the theoretical expectations, these coefficients
⁴⁷⁸ present values on the order of unity ($\mathcal{A}_0 \simeq 3$ and $\mathcal{B}_0 \simeq 1$) in unconfined sit-
⁴⁷⁹ uations (Claudin et al. 2013; Lü et al. 2021). In contrast and as illustrated
⁴⁸⁰ in Online Resource Fig. S13a,b, larger values are predicted in case of strong
⁴⁸¹ confinement, which does not allow us to proceed to further quantitative com-
⁴⁸² parison with the data.

⁴⁸³ Finally, the linear model is also able to reproduce the enhancement of the
⁴⁸⁴ flow deflection over the sinusoidal ridges when $\sqrt{\mathcal{A}_0^2 + \mathcal{B}_0^2}$ is increased (Online
⁴⁸⁵ Resource Fig. S13). Here, using $k\xi_0 \simeq 0.1$ to be representative of the amplitude
⁴⁸⁶ of the giant dunes at the North Sand Sea station, the coefficient modulus is
⁴⁸⁷ bounded to 10.

⁴⁸⁸ Appendix 2: Sediment transport and dune morphodynamics

⁴⁸⁹ We summarise in this appendix the sediment transport and dune morphody-
⁴⁹⁰ namics theoretical framework leading to the prediction of sand fluxes and dune
⁴⁹¹ orientations from wind data.

⁴⁹² *Sediment transport* — The prediction of sand fluxes from wind data has been
⁴⁹³ a long standing issue in aeolian geomorphological studies (Fryberger and Dean
⁴⁹⁴ 1979; Pearce and Walker 2005; Sherman and Li 2012; Shen et al. 2019). Based
⁴⁹⁵ on laboratory studies in wind tunnels (Rasmussen et al. 1996; Iversen and
⁴⁹⁶ Rasmussen 1999; Creysse et al. 2009; Ho et al. 2011), as well as physical
⁴⁹⁷ considerations (Ungar and Haff 1987; Andreotti 2004; Durán et al. 2011; Páhtz
⁴⁹⁸ and Durán 2020), it has been shown that the steady saturated saltation flux
⁴⁹⁹ over a flat sand bed depends linearly on the shear stress:

$$\frac{q_{\text{sat}}}{Q} = \Omega \sqrt{\Theta_{\text{th}}} (\Theta - \Theta_{\text{th}}), \quad (10)$$

⁵⁰⁰ where Ω is a proportionality constant, $Q = d\sqrt{(\rho_s - \rho_0)gd/\rho_0}$ is a character-
⁵⁰¹ istic flux, $\Theta = \rho_0 u_*^2 / (\rho_s - \rho_0)gd$ the Shields number, and Θ_{th} its threshold
⁵⁰² value below which saltation vanishes. $\rho_s = 2.6 \text{ g cm}^{-3}$ and $d = 180 \mu\text{m}$ are
⁵⁰³ the grain density and diameter, and g is the gravitational acceleration. The

shear velocity, and consequently the Shields number as well as the sediment flux, are time dependent.

Recently, Pähzt and Durán (2020) suggested an additional quadratic term in Shields to account for grain-grain interactions within the transport layer at strong wind velocities:

$$\frac{q_{\text{sat}, t}}{Q} = \frac{2\sqrt{\Theta_{\text{th}}}}{\kappa\mu} (\Theta - \Theta_{\text{th}}) \left(1 + \frac{C_M}{\mu} [\Theta - \Theta_{\text{th}}] \right), \quad (11)$$

where $\kappa = 0.4$ is the von Kármán constant, $C_M \simeq 1.7$ a constant and $\mu \simeq 0.6$ is a friction coefficient, taken to be the avalanche slope of the granular material. The fit of this law to the experimental data of Creyssels et al. (2009) and Ho et al. (2011) gives $\Theta_{\text{th}} = 0.0035$. The fit of Eq. 10 on these same data similarly gives $\Omega \simeq 8$ and $\Theta_{\text{th}} = 0.005$. The sand flux angular distributions and the dune orientations in Fig. 9 are calculated using this law (11). We have checked that using the ordinary linear relationship (10) instead does not change the predicted dune orientations by more than a few degrees.

Dune orientations — Dune orientations are predicted with the dimensional model of Courrech du Pont et al. (2014), from the sand flux time series computed with the above transport law. Two orientations are possible depending on the mechanism dominating the dune growth: elongation or bed instability. The orientation α corresponding the bed instability is then the one that maximises the following growth rate (Rubin and Hunter 1987):

$$\sigma \propto \frac{1}{H_d W_d T} \int_0^T q_{\text{crest}} |\sin(\theta - \alpha)| dt, \quad (12)$$

where θ is the wind orientation measured with respect to the same reference as α , and H_d and W_d are dimensional constants respectively representing the dune height and width. The integral runs over a time T , which must be representative of the characteristic period of the wind regime. The flux at the crest is expressed as:

$$q_{\text{crest}} = q_{\text{sat}} [1 + \gamma |\sin(\theta - \alpha)|], \quad (13)$$

where the flux-up ratio γ has been calibrated to 1.6 using field studies, underwater laboratory experiments and numerical simulations. Predictions of the linear analysis of Gadal et al. (2019) and Delorme et al. (2020) give similar results.

Similarly, the dune orientation corresponding to the elongation mechanism is the one that verifies:

$$\tan(\alpha) = \frac{\langle q_{\text{crest}}(\alpha) \mathbf{e}_\theta \rangle \cdot \mathbf{e}_{WE}}{\langle q_{\text{crest}}(\alpha) \mathbf{e}_\theta \rangle \cdot \mathbf{e}_{SN}}, \quad (14)$$

where $\langle \cdot \rangle$ denotes a vectorial time average. The unitary vectors \mathbf{e}_{WE} , \mathbf{e}_{SN} and \mathbf{e}_θ are in the West-East, South-North and wind directions, respectively.

The resulting computed dune orientations, blue and red arrows in Fig. 9, then depend on a certain number of parameters (grain properties, flux-up ratio,

538 etc.), for which we take typical values for aeolian sandy deserts. Due to the lack
539 of measurements in the studied places, some uncertainties can be expected. We
540 therefore run a sensitivity test by calculating the dune orientations for grain
541 diameters ranging from 100 μm to 400 μm and for a speed-up ratio between
542 0.1 and 10 (wedges in Fig. 9).

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889 **Local wind regime induced by giant linear dunes**
 890 — Supplementary Material —

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897 **1. Shear velocity and calibration of the hydrodynamical roughness**

898 As the regionally predicted and locally measured velocities are available at
 899 different heights, we can not compare them directly. We therefore convert
 900 all velocities into shear velocities u_* , characteristic the turbulent logarithmic
 901 velocity profile (Spalding 1961; Stull 1988):

$$\frac{u(z)}{u_*} = \frac{1}{\kappa} \ln \left(\frac{z}{z_0} \right), \quad (15)$$

902 where z is the vertical coordinate, $\kappa = 0.4$ the von Kármán constant and z_0 the
 903 hydrodynamic roughness. Note that, strickly speaking, this logarithmic profile
 904 is valid for a neutrally stratified ABL only. Vertical density gradients occurring
 905 in other conditions may thus induce large discrepancies (Monin and Obukhov
 906 1954; Garratt 1994; Dyer 1974). However, as our wind measurements are in
 907 the flow region close enough to the surface, where these effects are negligible,
 908 this logarithmic wind profile remains a fairly good approximation in all conditions
 909 (Gunn et al. 2021b). Several measurements of hydrodynamic roughnesses
 910 are available (Raupach 1992; Bauer et al. 1992; Brown et al. 2008; Nield et al.
 911 2014). In the absence of sediment transport, it is governed by the geometric
 912 features of the bed (Flack and Schultz 2010; Pelletier and Field 2016). When
 913 aeolian saltation occurs, it is rather controlled by the altitude of Bagnold's
 914 focal point (Durán et al. 2011; Valance et al. 2015), which depends on the
 915 wind velocity and grain properties (Sherman and Farrell 2008; Zhang et al.
 916 2016; Field and Pelletier 2018). Whether associated with geometric features
 917 or with sediment transport, its typical order of magnitude is the millimetre
 918 scale on sandy surfaces.

919 We do not have precise velocity vertical profiles to be able to deduce an
 920 accurate value of z_0 in the various environments of the meteorological stations
 921 (vegetated, arid, sandy). Our approach is to rather select the hydrodynamic
 922 roughness which allows for the best possible matching between the regionally
 923 predicted and locally measured winds, i.e. minimising the relative difference δ
 924 between the wind vectors of both datasets:

$$\delta = \frac{\sqrt{\langle \| \mathbf{u}_{*,\text{era}} - \mathbf{u}_{*,\text{station}} \|^2 \rangle}}{\sqrt{\langle \| \mathbf{u}_{*,\text{era}} \|^2 \rangle \langle \| \mathbf{u}_{*,\text{station}} \|^2 \rangle}}, \quad (16)$$

where $\langle \cdot \rangle$ denotes time average. This parameter is computed for values of z_0 in ERA5-Land analysis ranging from 10^{-5} m to 10^{-2} m for the four different stations. Note that for the North Sand Sea and South Sand Sea stations, where the giant dunes feedback presumably affect the wind, we take into account the non-deflected winds only in the calculation of δ (with a 15° tolerance).

As shown in Online Resource Fig. S3, the minimum values of δ in the space $(z_0^{\text{ERA5Land}}, z_0^{\text{local}})$ form a line. We thus set the roughness in the ERA5-Land analysis to the typical value $z_0 = 10^{-3}$ m, and deduce the corresponding ones for the local stations. It leads to 2.7, 0.8, 0.1 and 0.5 mm for the Etosha West, North Sand Sea, Huab and South Sand Sea stations, respectively. Importantly, this approach somewhat impacts the calculation of the shear velocities, but not that of the wind directions. As such, most of our conclusions are independent of such a choice. However, it may affect the magnitude of the wind velocity attenuation/amplification in flow confinement situations.

2. Computation of the ABL characteristics

The estimation of the non-dimensional numbers associated with the ABL requires the computation of representative meteorological quantities. In arid areas, the vertical structure of the atmosphere can be approximated by a well mixed convective boundary layer of height H , topped by the stratified free atmosphere (Stull 1988; Shao 2008). In this context, one usually introduces the virtual potential temperature T_{vp} , which is a constant T_0 inside the boundary layer, and increases linearly in the FA (Online Resource Fig. S8a):

$$T_{\text{vp}}(z) = \begin{cases} T_0 & \text{for } z \leq H, \\ T_0 \left(1 + \frac{\Delta T_{\text{vp}}}{T_0} + \frac{N^2}{g}(z - H)\right) & \text{for } z \geq H, \end{cases} \quad (17)$$

where ΔT_{vp} is the temperature discontinuity at the capping layer and $N = \sqrt{g\partial_z T_{\text{vp}}/T_0}$ is the Brunt-Väisälä frequency, characteristic of the stratification. Note that, under the usual Boussinesq approximation, temperature and air density variations are simply related by $\delta T_{\text{vp}}/T_0 \simeq -\delta\rho/\rho_0$ (see Online Resource of Andreotti et al. (2009)), so that N can equivalently be defined from the density gradient as next to (1).

The ERA5 dataset provides vertical profiles of the geopotential ϕ , the actual temperature T and the specific humidity η at given pressure levels P . The vertical coordinate is then calculated as:

$$z = \frac{\phi R_t}{g R_t - \phi}, \quad (18)$$

where $R_t = 6371229$ m is the reference Earth radius and $g = 9.81$ m s $^{-2}$ is the gravitational acceleration. One also computes the virtual potential temperature as:

$$T_{\text{vp}} = T \left[1 + \left(\frac{M_d}{M_w} - 1\right) \eta\right] \left(\frac{P_0}{P}\right)^{R/C_p}, \quad (19)$$

where $P_0 = 10^5$ Pa is the standard pressure, $R = 8.31$ J/K is the ideal gas constant, $C_p \simeq 29.1$ J/K is the air molar heat capacity, and $M_w = 0.018$ kg/Mol and $M_d = 0.029$ kg/Mol are the molecular masses of water and dry air respectively. The specific humidity is related to the vapour pressure p_w as

$$\eta = \frac{\frac{M_w}{M_d} p_w}{p - \left(1 - \frac{M_w}{M_d}\right) p_w}. \quad (20)$$

The ERA5 dataset also provides an estimate of the ABL depth H , based on the behaviour of the Richardson vertical profile. This dimensionless number is defined as the ratio of buoyancy and flow shear terms, and can be expressed as $\text{Ri} = N^2 / (\partial_z u)^2$. It vanishes in the lower well-mixed layer where T_{vp} is constant, and increases in the stratified FA. Following the method and calibration of Vogelegang and Holtlag (1996); Seidel et al. (2012), the value $\text{Ri}(z) \simeq 0.25$ has been shown to be a good empirical criterion to give $z \simeq H$ within a precision varying from 50% for the shallower ABL (e.g. at night) to 20% for situations of stronger convection.

Examples of vertical profiles of the virtual potential temperature deduced from ERA5 are shown in Online Resource Fig. S8a. For each of them, an average temperature is computed below the ABL depth ($z < H$), and a linear function is fitted above, allowing us to extract the temperature jump ΔT_{vp} . Importantly, some profiles display a vertical structure that cannot be approximated by the simple form (17) used here (Online Resource Fig. S8b). In practice, we removed from the analysis all of those leading to the unphysical case $\Delta T_{\text{vp}} < 0$. We have noticed that these ‘ill-processed’ profiles dominantly occur in winter and are evenly spread across the hours of the day. Importantly, they represent $\simeq 12\%$ of the data only (Online Resource Fig. S8c,d), and we are thus confident that this data treatment does not affect our conclusions.

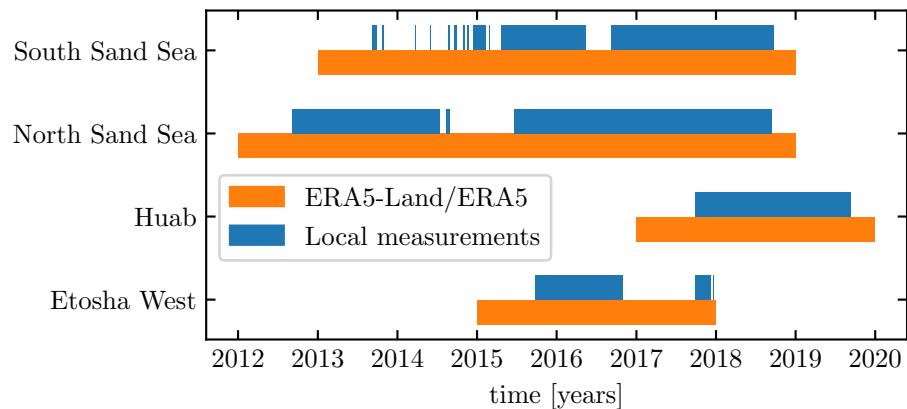


Fig. S1 Gant chart representing the valid time steps for the two data sets, for all stations.

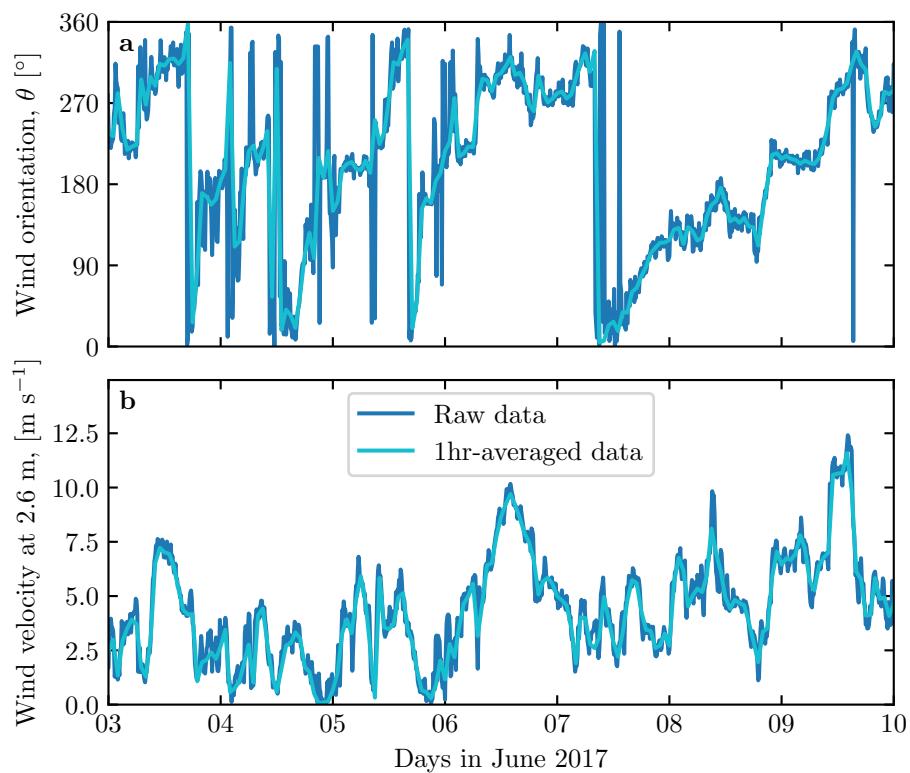


Fig. S2 Local wind measurements: comparison between raw (blue) and hourly-averaged (light blue) data from South Sand Sea station. **a:** wind direction. **b:** wind velocity at height 2.6 m.

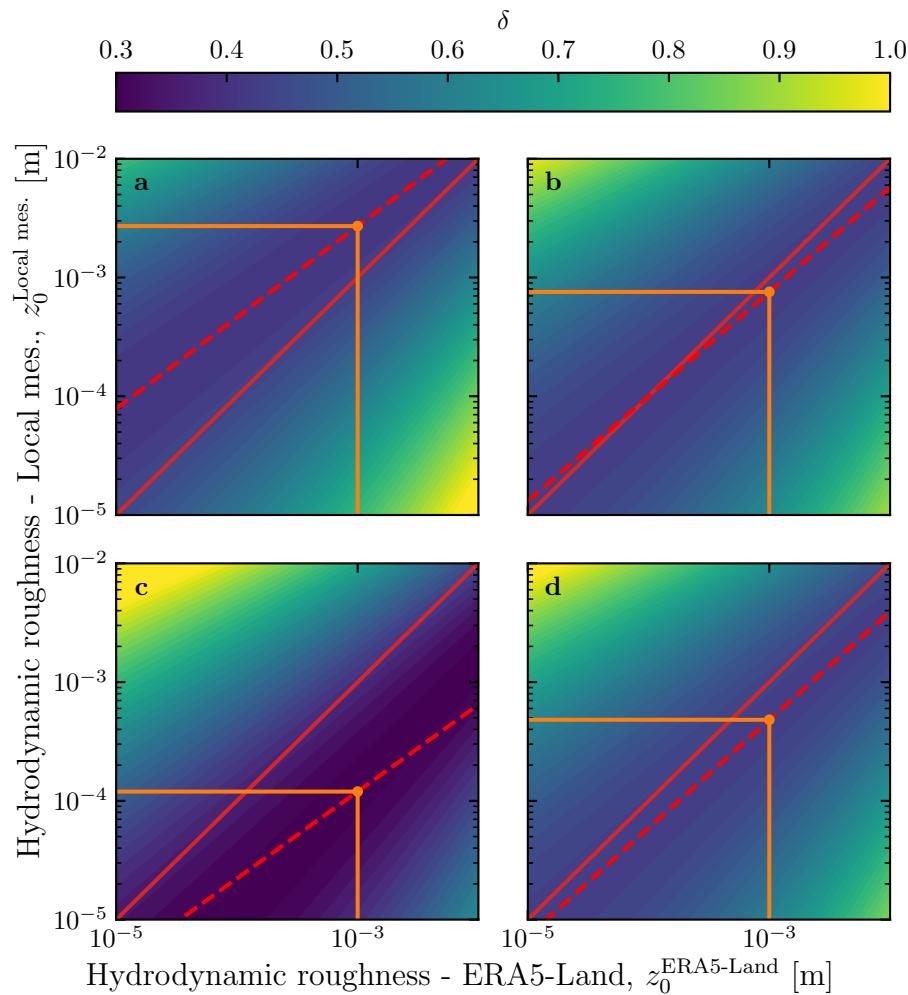


Fig. S3 Calibration of hydrodynamic roughness. The parameter δ (16) quantifying the difference between local and predicted winds is shown in color scale as a function of the hydrodynamic roughnesses chosen for the ERA5-Land and for local winds, for the (a) Etosha West, (b) North Sand Sea, (c) Huab and (d) South Sand Sea stations. The red dashed and plain lines shows the minima of δ and the identity line, respectively. The orange lines and dots highlight the chosen hydrodynamic roughnesses for the local winds deduced from setting $z_0^{\text{ERA5Land}} = 1$ mm.

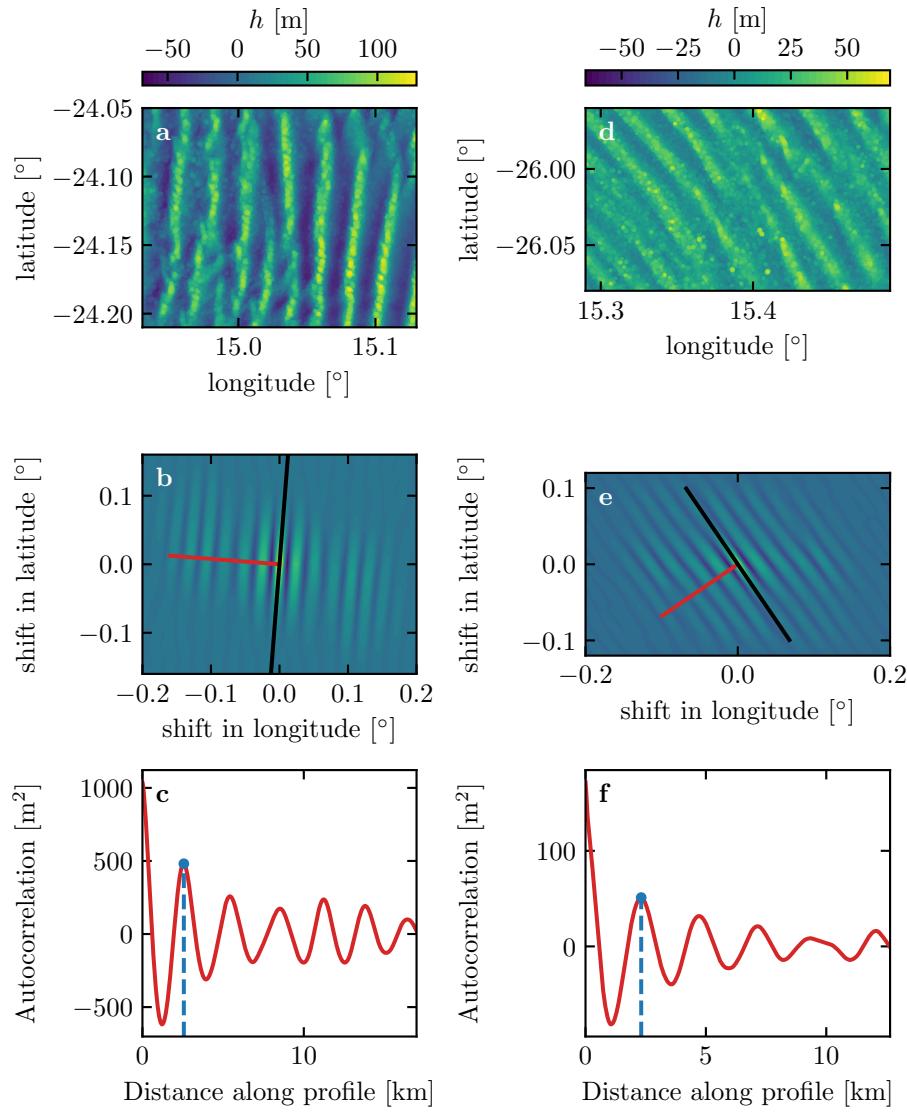


Fig. S4 Analysis of the DEMs of the North Sand Sea (left column – panels **a**, **b**, **c**) and South Sand Sea (right column – panels **d**, **e**, **f**) stations. **a–d**: Bed elevation detrended by a fitted second order polynomial base-line. **b–e**: Autocorrelation matrix shown in color scale. The black line shows the detected dune orientation, and the red line represents the autocorrelation profile along which the dune wavelength is calculated, displayed in **c–f**. The blue lines and dots show the first peak of the autocorrelation profile, whose abscissa gives the characteristic wavelength of the dune pattern.

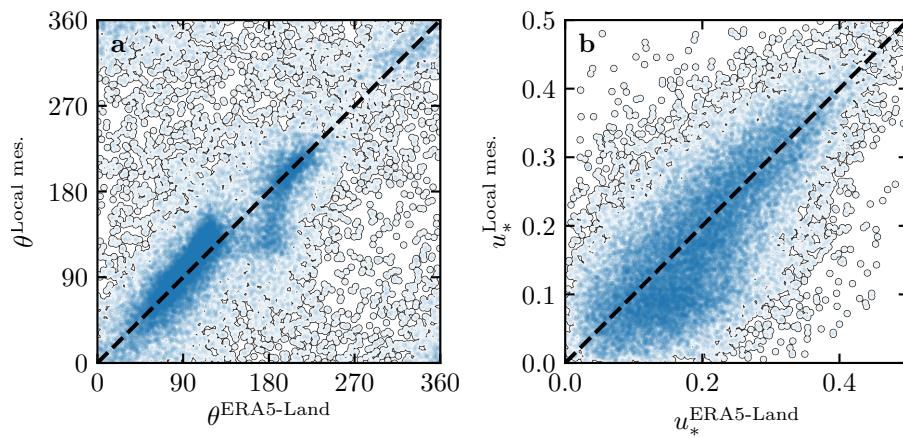


Fig. S5 Statistical comparison of the wind orientation (a) and velocity (b) between the ERA5-Land dataset and the local measurements for the Huab and Etosha West stations. Data point clustering around identity lines (dashed and black) provide evidence for agreement of the two sets.

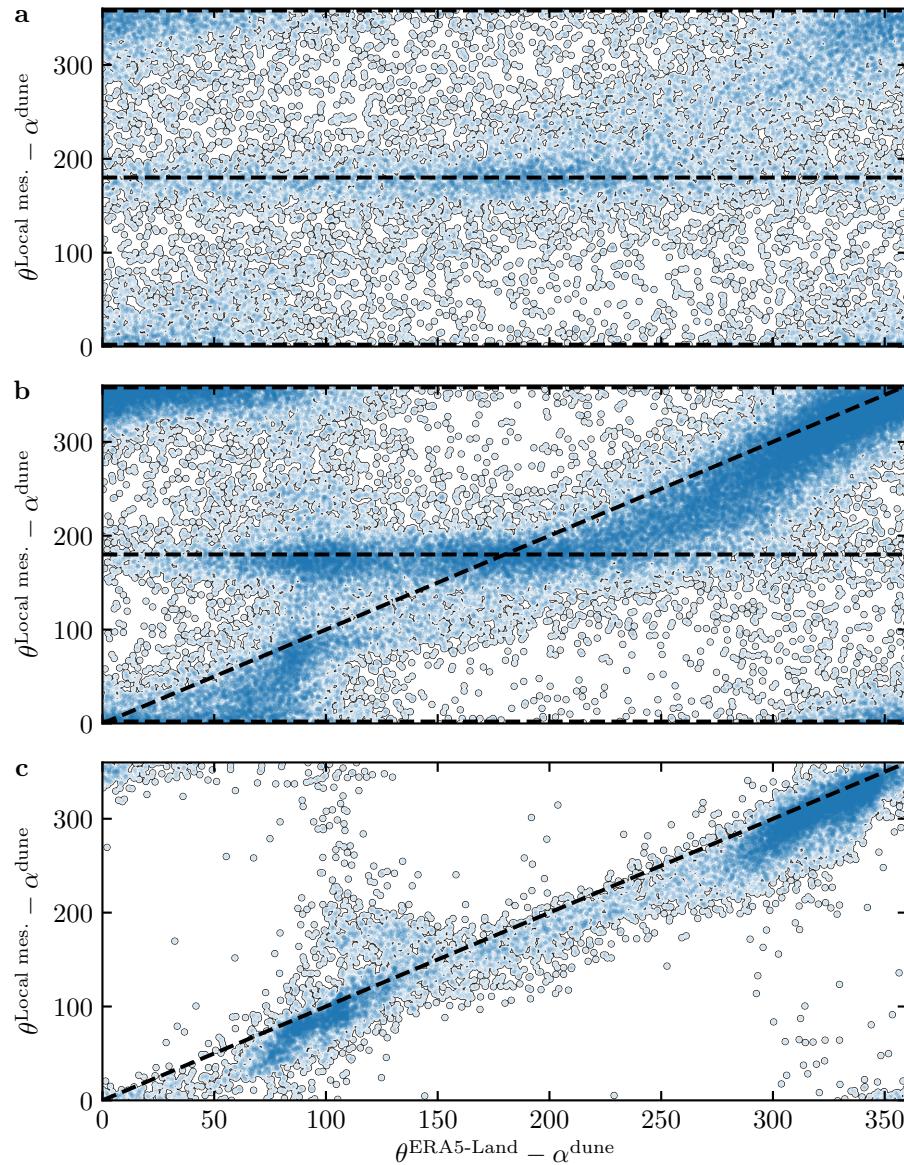


Fig. S6 Statistical comparison of the wind orientation between the ERA5-Land dataset and the local measurements for the South Sand Sea and North Sand Sea stations, for different velocity ranges. **a:** $u_*^{\text{ERA5-Land}} < 0.1 \text{ m s}^{-1}$. **b:** $0.1 < u_*^{\text{ERA5-Land}} \leq 0.25 \text{ m s}^{-1}$. **c:** $u_*^{\text{ERA5-Land}} \geq 0.25 \text{ m s}^{-1}$. The measured dune orientations are subtracted to the wind orientation, which allows us to plot both stations on the same graph. Black dashed lines indicate locally measured orientations aligned with the dune crests (here 0°, 180° and 360° – panels **a**, **b**), as well as the identity lines (panels **b**, **c**).

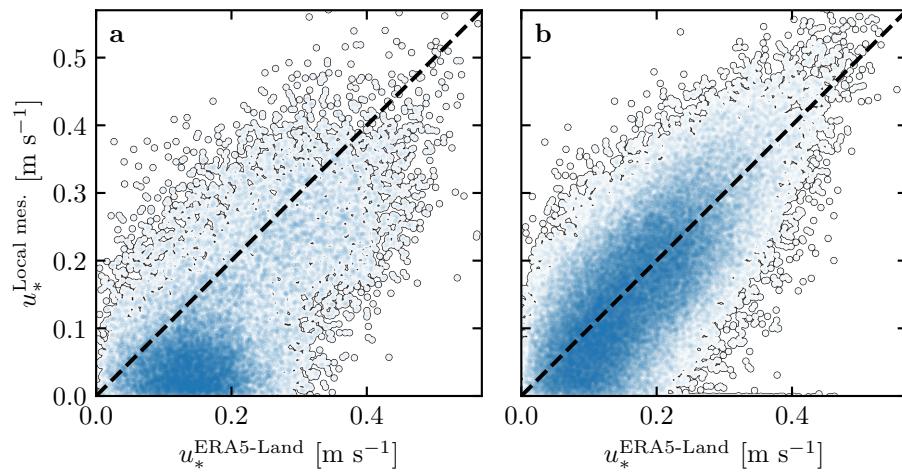


Fig. S7 Statistical comparison of the wind velocity between the ERA5-Land dataset and the local measurements for the South Sand Sea and North Sand Sea stations. **a:** Nocturnal summer easterly wind. **b:** Diurnal southerly wind. Black dashed lines are identity lines. The angle ranges used to select diurnal and nocturnal summer winds are the same as those in Figs. 4 and Figs. 6 of the main article.

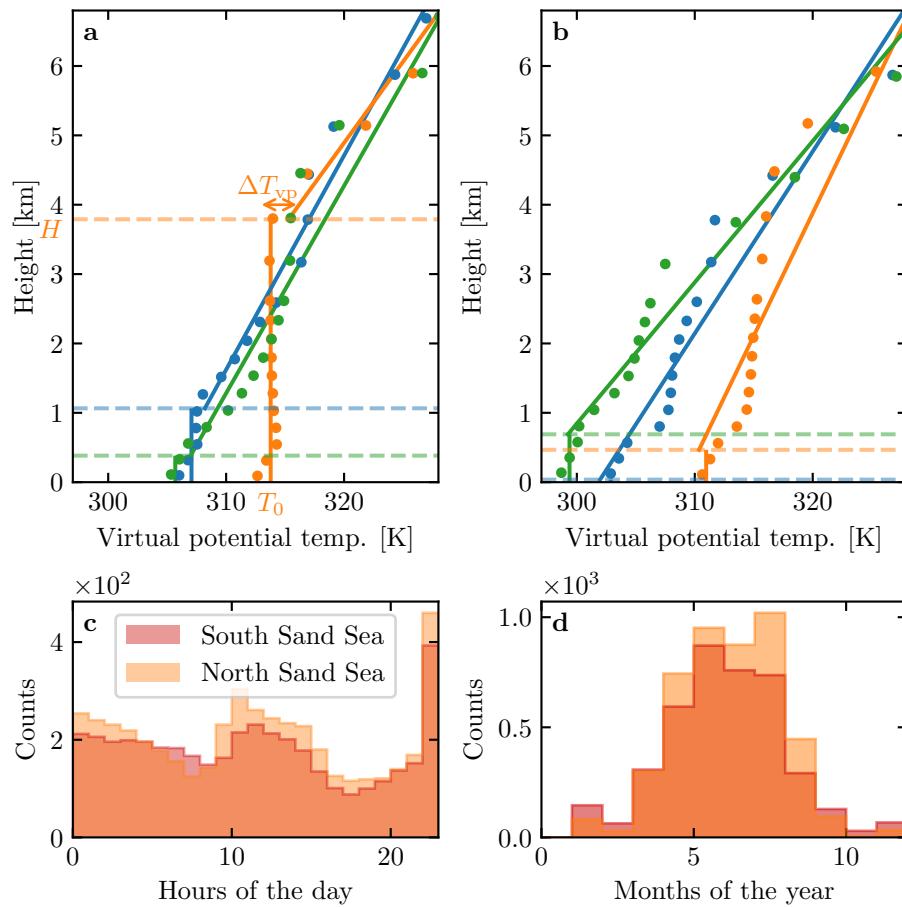


Fig. S8 **a:** Vertical profiles of the virtual potential temperature at three different times (blue: 29/11/2012 - 11.00 UTC, orange: 21/03/2017 - 12.00 UTC, green: 21/03/2017 - 20.00 UTC) at the South Sand Sea station. Dots: data from the ERA5 reanalysis. Dashed lines: boundary layer height given by the ERA5 reanalysis. Plain lines: vertical (ABL) and linear (FA) fits to estimate the quantities displayed in Online Resource Fig. S9. **b:** Examples of ill-processed vertical profiles at three different times (blue: 2/12/2013 - 23.00 UTC, orange: 20/03/2017 - 00.00 UTC, green: 14/07/2017 - 14.00 UTC) at the South Sand Sea station. Distribution of ill-processed vertical profiles at South (orange) and North (light orange) Sand Sea station: hourly **(c)** and monthly **(d)** counts.

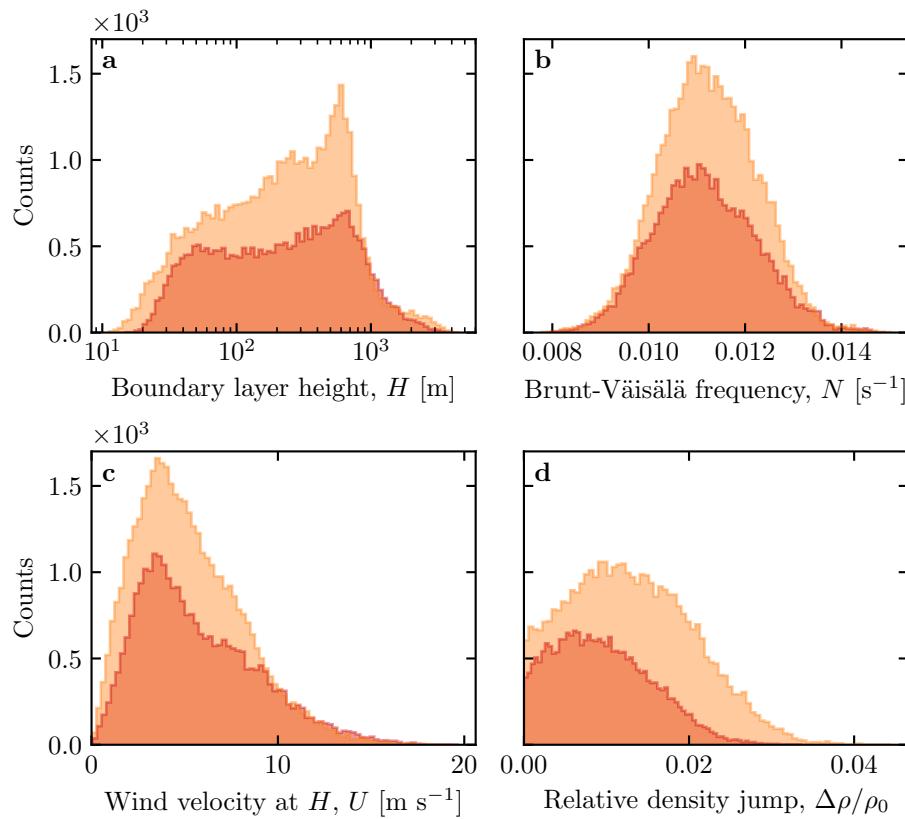


Fig. S9 Distributions of the meteorological parameters resulting from the processing of the ERA5-Land data for the South Sand Sea (orange) and the North Sand Sea (light orange) stations.

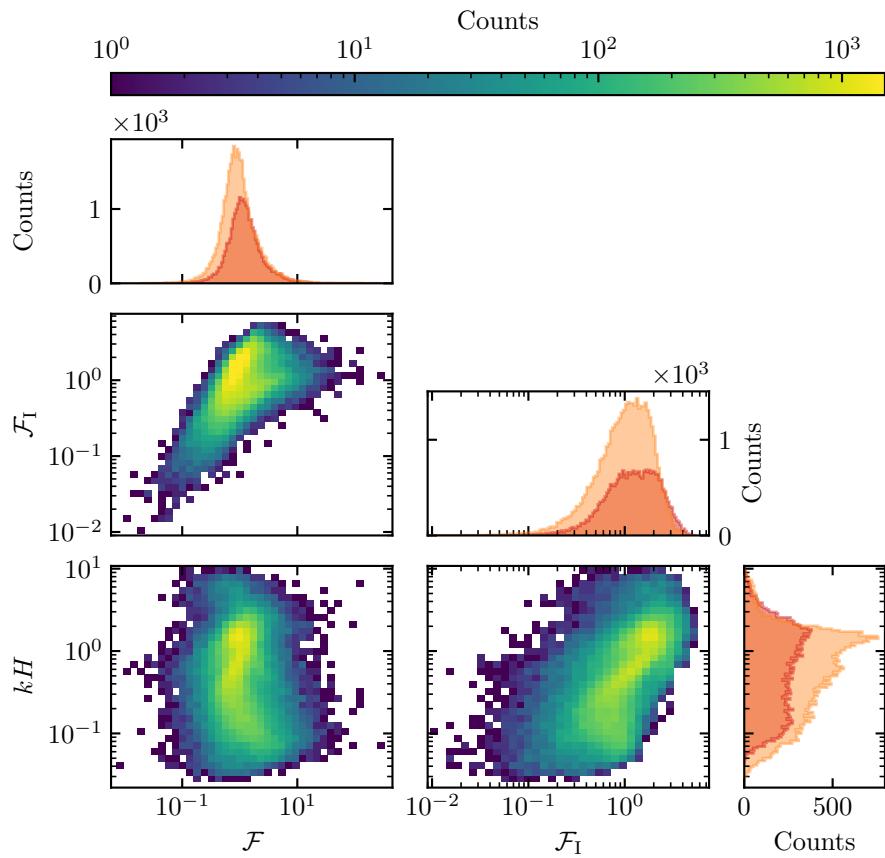


Fig. S10 Non-dimensional parameters distributions. For the marginal distributions, the light orange corresponds to the South Sand Sea station, and the orange to the North Sand Sea station.

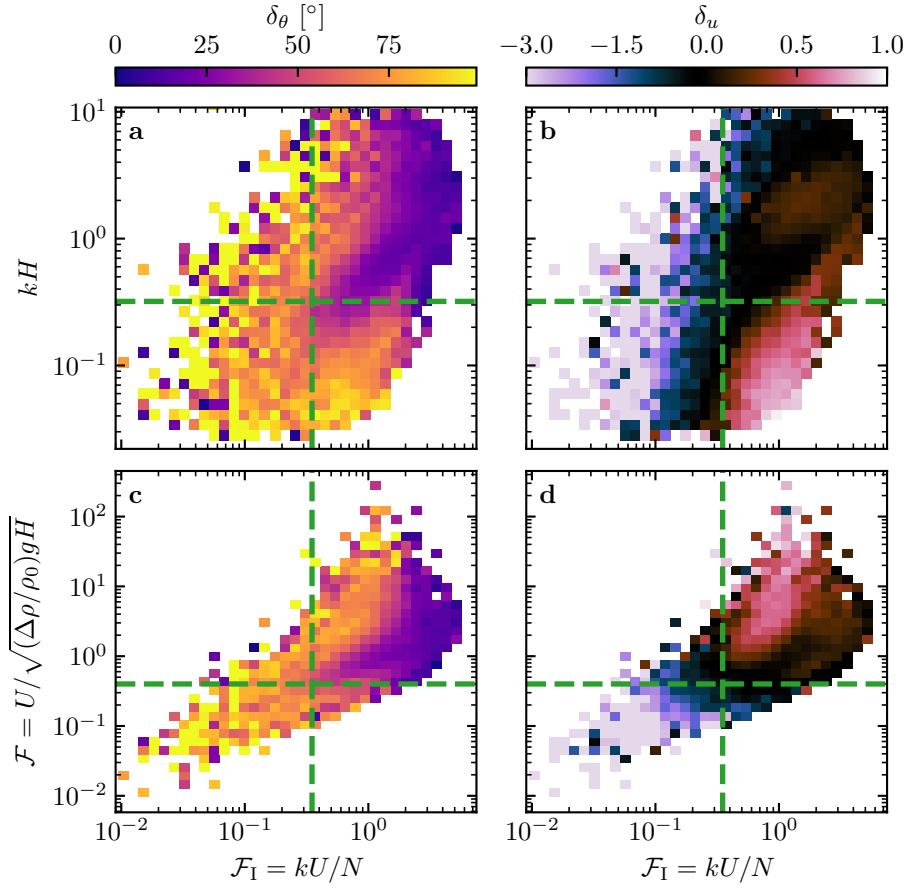


Fig. S11 Regime diagrams of the wind deviation δ_θ and relative attenuation/amplification δ_u in the spaces (\mathcal{F}_I, kH) and $(\mathcal{F}_I, \mathcal{F})$, containing the data from both the North Sand Sea and South Sand Sea stations. Green dashed lines empirically delimit the different regimes. The point density in each bin of the diagrams is shown in Online Resource Fig. S10 – 95% of the data occur in the range $-1 < \delta u < 1$. The similar regime diagrams in the space (\mathcal{F}, kH) are shown in Fig. 8.

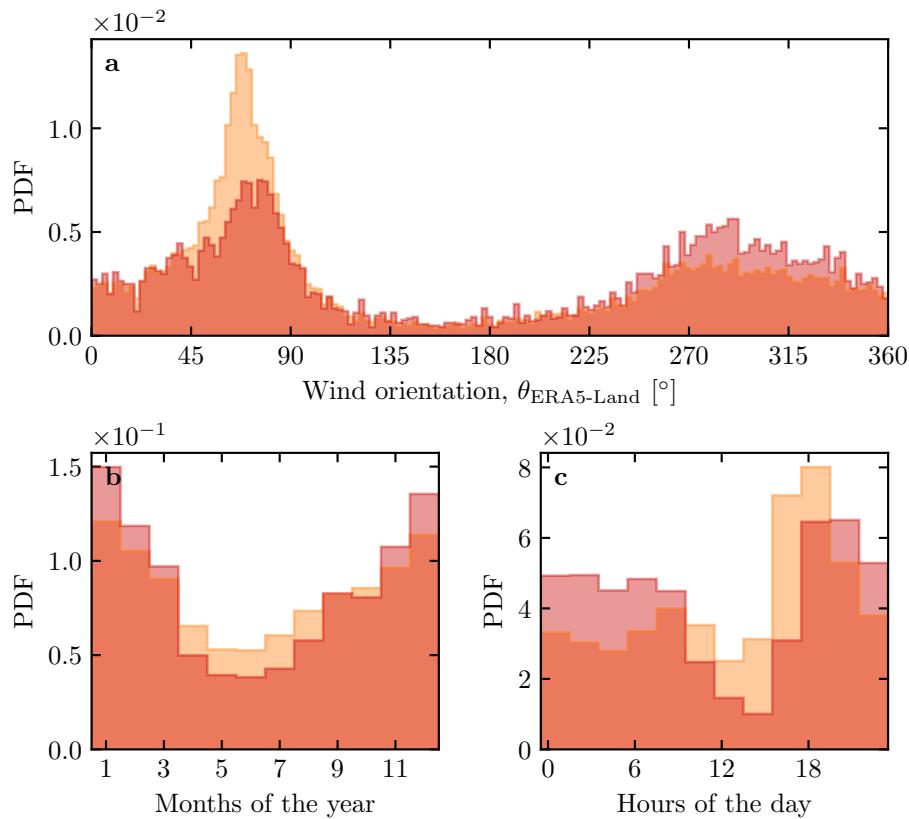


Fig. S12 Normalized distributions of amplified velocities for the North Sea (light orange: $\delta_u < 0$, orange: $\delta_u < -0.5$). **a:** Angular distributions. **b:** Monthly distributions. **c:** Hourly distributions.

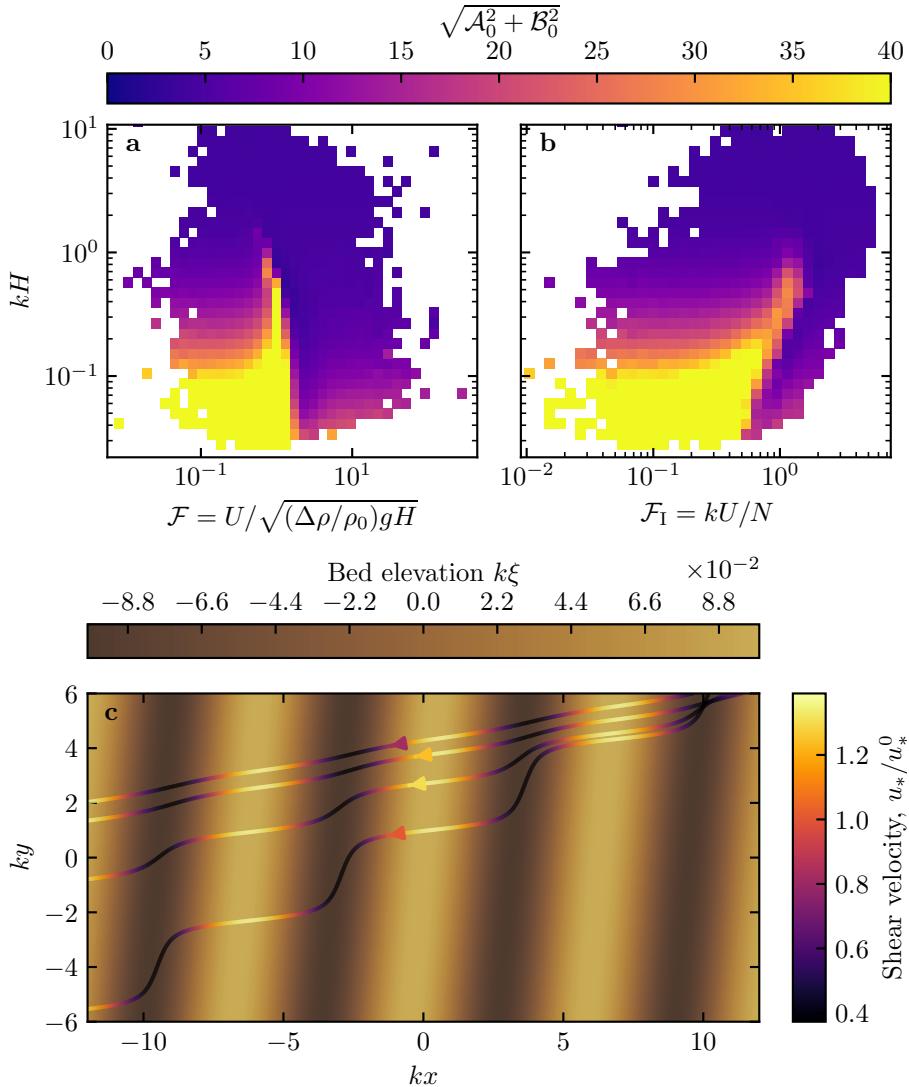


Fig. S13 Computation of the flow disturbance with the linear model of Andreotti et al. (2009). **a–b:** Magnitude of the hydrodynamic coefficients A_0 and B_0 , calculated from the time series of the non-dimensional numbers corresponding to the ERA5-Land wind data and ERA5 data on vertical pressure levels. **c** Shear velocity streamlines over sinusoidal ridges of amplitude $k\xi_0 = 0.1$ and for increasing values of $\sqrt{A_0^2 + B_0^2}$. From the upper to the lower streamline, values of $(kH, \mathcal{F}, \mathcal{F}_I, A_0, B_0, \sqrt{A_0^2 + B_0^2})$ are $(1.9, 0.6, 1.5, 3.4, 1.0, 3.5)$, $(1.5, 0.3, 0.4, 4.8, 1.4, 5.0)$, $(0.1, 3.5, 1.0, 8.6, 0.1, 8.6)$, $(0.5, 0.05, 0.04, 9.6, 2.5, 9.9)$.

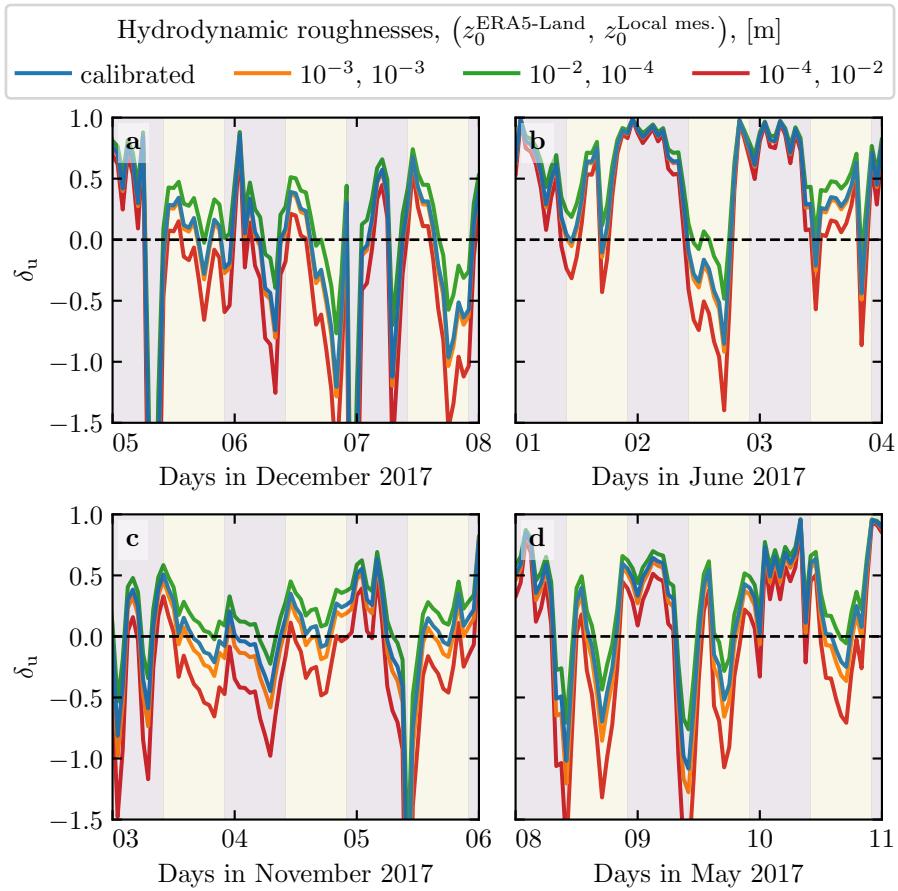


Fig. S14 Time series of the relative velocity disturbance δ_u corresponding to Fig. 5, for different values of the hydrodynamic roughnesses. **a:** North Sand Sea – summer, **b:** North Sand Sea – winter, **c:** South Sand Sea – summer, **d:** South Sand Sea – winter. Note that δ_θ is independent of the choice of $z_0^{\text{ERA5-Land}}$ and $z_0^{\text{Local mes.}}$.