

Title

PALAGRAM¹

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Abstract

Particle-laden gravity currents (PLGCs) are driven by a mass difference between a heavy fluid-particle mixture and a lighter ambient liquid. We focus our attention on finite volume current, generated here by lock-release device over a controlled constant slope bottom at the laboratory scale. The main objective of the present chapter is to provide a comprehensive flow regime associated with the relevant dimensionless parameters which characterize the current at the macroscopic scale, i.e. average over the current depth.

1 Introduction

1.1 Control parameters

Particle-laden gravity currents (PLGCs) are driven by a mass difference between a heavy fluid-particle mixture and a lighter ambient liquid. A major difference between compositional currents and PLGCs is therefore the existence of typical length and time scales associated with the particle dynamics. Particularly, the own settling velocity of a heavy particle only allows the existence of these gravity currents on finite time and length scales. Nevertheless, prediction of these finite scales is difficult as it shall strongly depends on the interaction between particle dynamics and the local turbulence of the carrying fluid and/or ambient fluid at the upper interface, which modifies entrainment and associated dissipation, and in turn can delay or enhance settling. Accordingly, their dynamics are controlled by several dimensionless parameters leading to a wide variety of flow regimes. In particular, beyond the slope α , the dimensionless density difference between the current and the ambient At and the ratio between available inertia and dissipation, say a Reynolds number Re , as usually introduced as a control parameter for compositional currents, the initial solid fraction of particles ϕ and a dimensionless settling velocity St have now to be considered as potentially affecting flow regimes. It shall be noted that in some specific situations, some of these dimensionless parameters could be linked as, for instance, ϕ and At for heavy particles in a single-phase liquid for the carrying and ambient fluids

1.2 Literature

- literature slope
- literature settling

- literature volume fraction
- other effects: lock geometry, non-boussinesq, entrainment, erosion/deposition \rightarrow ignored here

2 Dimensional analysis at the macroscopic scale of the current

Here, the dimensionless parameters are based on a characteristic length L_0 and a characteristic velocity $U_0 = \sqrt{g'H_0}$ where L_0 and H_0 are the horizontal length and depth of the initial container, respectively, g' is the modified gravity $rg \cos \alpha$ and $r = (\rho_m - \rho_a)/\rho_a$ with ρ_m and ρ_a the current density and ambient fluid density respectively. Note that $\rho_m = \phi\rho_p + (1 - \phi)\rho_f$ with ρ_p the particles density and ρ_f the fluid phase density initially in the current. In the set of experiments presented here $\rho_f \leq \rho_a$. The velocity scale U_0 corresponds to an idealized transfer of initial potential energy to kinetic energy along the slope, i.e. a collapse of the initial column.

Accordingly,

$$a = \frac{H_0}{L_0}, \quad (1)$$

$$Re = \frac{U_0 H_0 \rho_m}{\eta_f}, \quad (2)$$

$$At = \frac{\rho_m - \rho_a}{\rho_a}, \quad (3)$$

$$St = \frac{V_s}{U_0}, \quad (4)$$

with η_f the interstitial fluid viscosity and V_s the Stokes settling velocity in the interstitial fluid phase labelled f .

Then, the dynamics of the current are characterized by several dimensionless variables. The most common

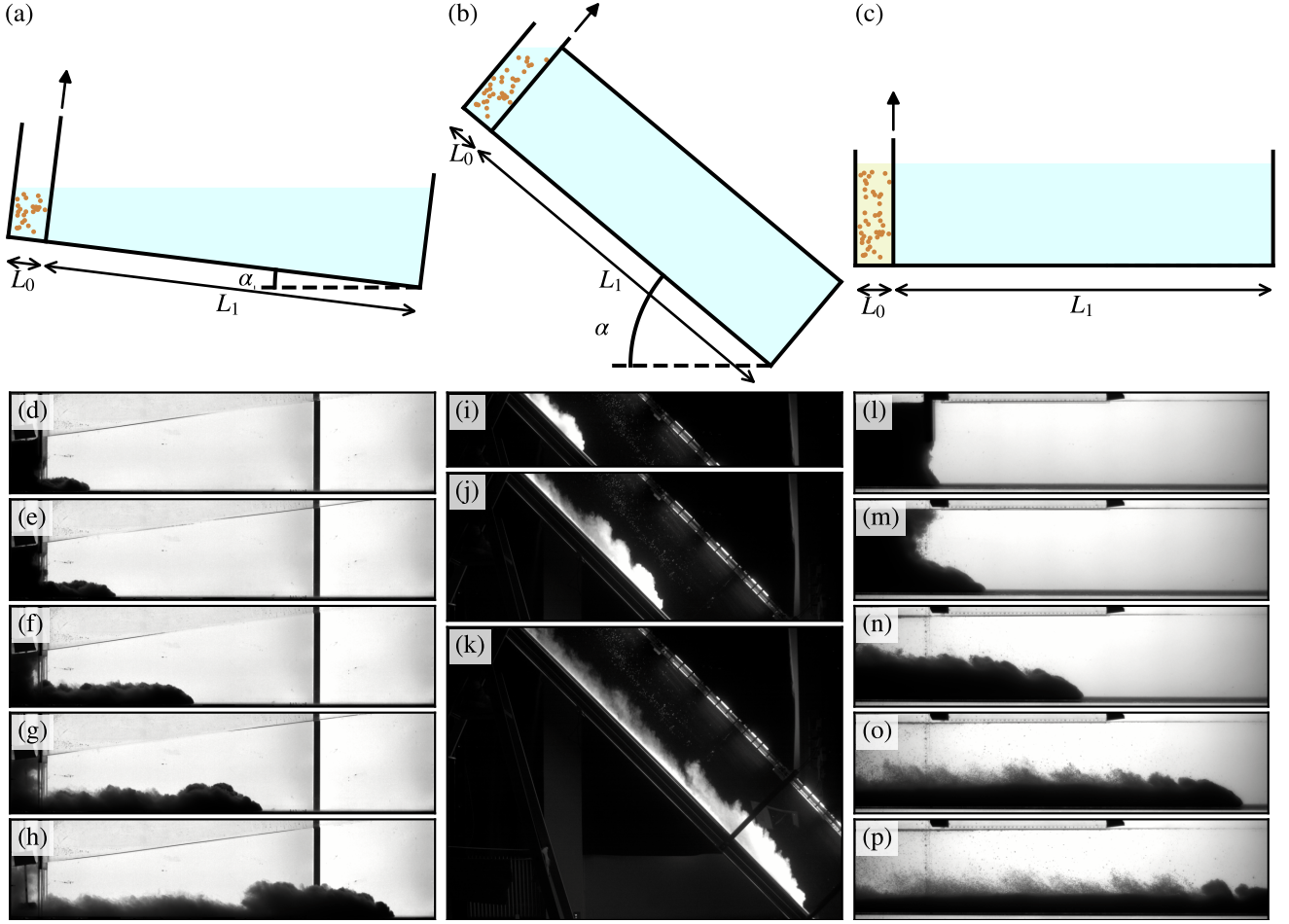


Figure 1: **Experimental set-ups used in this study.** (a–c) Sketches of the three experimental set-ups. Below are shown snapshots of corresponding experimental images. (d–h) Set-up 1, $\alpha = 7^\circ$, $\phi \sim 3\%$, $St =$ (i–k) Set-up 2, $\alpha =$, $\phi \sim$, $St =$ (l–p) Set-up 3, $\alpha =$, $\phi \sim$, $St =$.

one to be analyzed in gravity-driven avalanches is the dimensionless front velocity, also referred to as the Froude number,

$$\mathcal{Fr} = \frac{U_c}{U_0}, \quad (5)$$

where U_c is the front velocity of the current. Note that U_c is time-dependent, and so is \mathcal{Fr} , i.e. that \mathcal{Fr} as defined here is not a control parameter. (The Froude number which would be defined as a control parameter for a lock-release configuration would be $Fr \equiv 1$, and is thus not relevant to predict the flow dynamics.)

3 Methods

3.1 Experimental setups

Even if the dynamics of PLGCs is associated with several complex processes, a general consequence is observed on the front dynamics, often referred to as the \mathcal{Fr} number, and the front shape. Then prediction of the different flow regimes associated with PLGCs shall be en-

tirely included into these observables. In order to characterize the different flow regimes for PLGCs induced by a finite volume of material initially at “rest”, 3 dam-break-type devices have been used to cover a wide range of control parameters, as $\alpha \in [0^\circ, 30^\circ]$, $\phi \in [0.1\%, 20\%]$, $At \in [??]$, $Re \in [??]$, $St \in [??]$, $a \in ??$, as specifically defined in section 2. These experimental devices are supplemented with Euler-Euler numerical simulations to confirm the relevance of such flow regime description to characterize the dynamics of PLGCs.

Set-up 1 Specifications of IMFT set-up

Set-up 2 Specifications of LEGI set-up

Set-up 3 Specifications of LEMTA set-up

3.2 Datasets

On these 3 devices, a total of N experiments are presented here, complemented by N numerical simulations

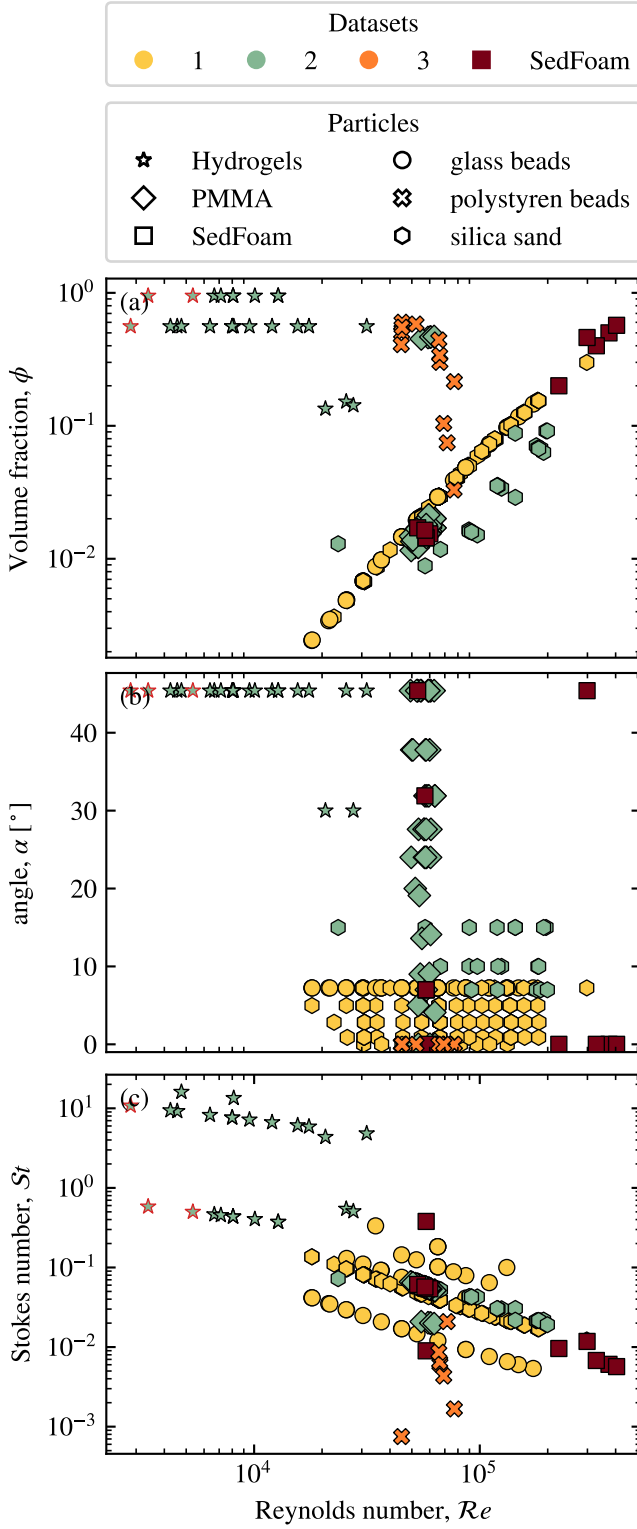


Figure 2: **Explored parameter space.** Each symbol correspond to a single experimental run.

using SedFoam (see description below). They are classified into 4 different datasets, described below.

Dataset 1 Description Dataset LEGI

Dataset 2 Description Dataset IMFT

Dataset 3 Description Dataset LEGI/IMFT

Dataset 4 Description Dataset LEMTA

SedFoam Description Dataset SedFoam

3.3 Fitting procedure and front position analysis

For each experimental/numerical run, we extract the current front position as a function of time (see Fig. 3a). A few selected runs are shown on figure 3b in non-dimensional time coordinates. After a short transient acceleration phase, most currents exhibit at first a constant velocity corresponding to the so-called *slumping* regime. After this, the velocity can decrease, either because of settling induced buoyancy loss, or because the current enters the *inertial* regime.

It can be qualitatively seen that increasing the bottom slope increases the slumping velocity, while increasing the Stokes number shortens the duration of the constant-velocity regime. To properly quantify that, we fit all front propagation curves (except Dataset 4) with the following equation:

$$\frac{x_f}{L_0} = x_i + \mathcal{F}r \frac{t}{t_0} - \frac{\tilde{\lambda}}{2} \left(\frac{t}{t_0} \right)^2, \quad (6)$$

where $\mathcal{F}r$ corresponds now to the non-dimensional current velocity during the slumping regime, and $\tilde{\lambda}$ to the dissipation. The fit is performed between $t/t_0 = 5$, to avoid the initial transient phase, and $t/t_0 = 30$, the transition time from the slumping to the inertial regime (?). Note that x_i is kept constant equal to 0 for Dataset 1, 2 and 3, but had to be left free to adjust for the SedFoam simulations **comment this**. For runs with strong dissipation ($\tilde{\lambda} > 2 \times 10^{-2}$), we add a quartic term to (6) to improve the fit quality and obtain a better estimation of $\mathcal{F}r$ and $\tilde{\lambda}$. We checked that our results does not depend on the presence of this quartic term, and that the linear and quadratic ones remain much larger.

For Dataset 4, the time resolution as well as the experiment duration does not allow to extract the dissipation. Therefore, we simply fit the whole available points with a linear function.

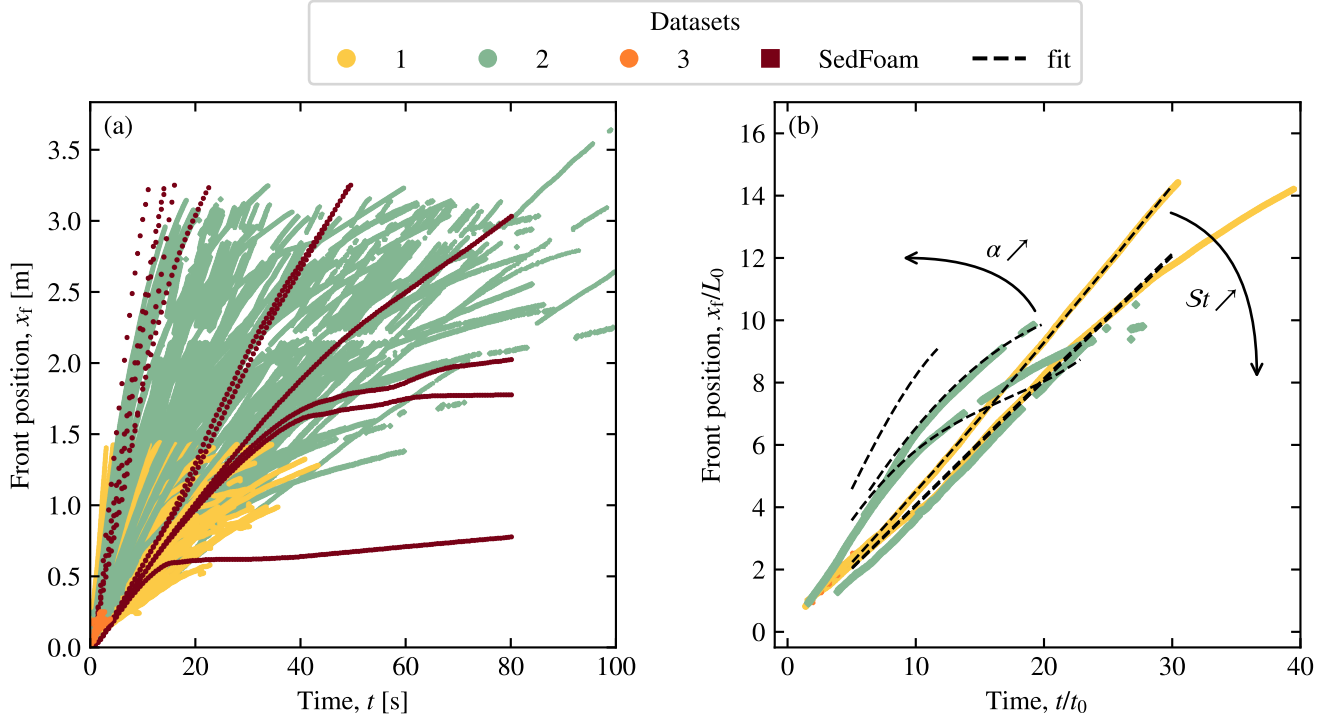


Figure 3: (a) Current front position as a function of time for all experimental runs (b) Selected runs plotted in non-dimensional coordinates.

4 Results

4.1 Influence of the slope on the front velocity

The influence of the slope angle α on the dimensionless front velocity $\mathcal{F}r$ is presented in figure 4. Even if the entire set of experiments and numerical simulations are reported here, results are highlighted for a nearly constant $St \approx 5 \times 10^{-2}$ and $\phi < 0.4$ for clarity.

4.2 Influence of St

Discuss figure 5

4.3 Influence of volume fraction, ϕ

Discuss figure 6

Acknowledgment

Fundings

References

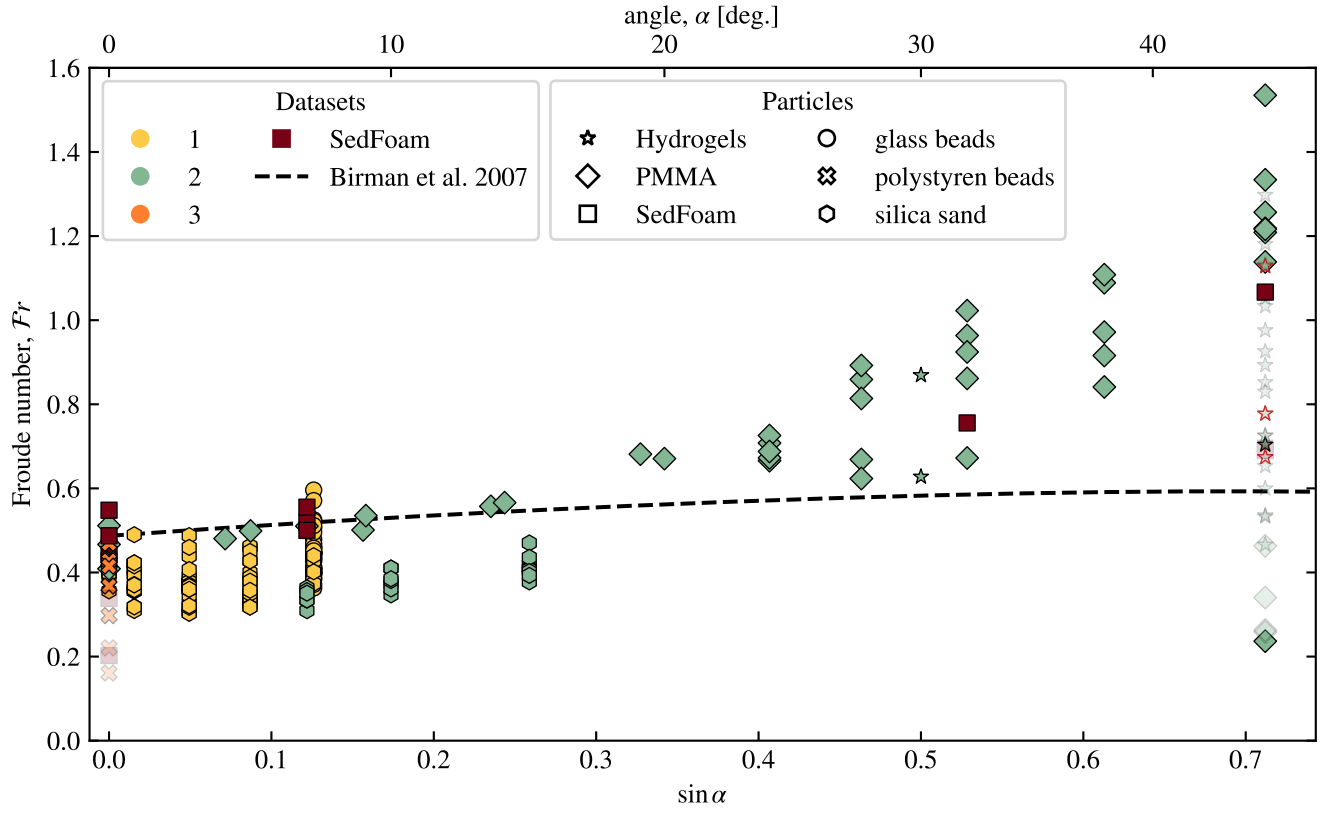


Figure 4: **Influence of the bottom slope.** (a) Current Froude number as a function of the bottom slope. (b) Current Froude number corrected by a prefector \sqrt{a} as a function of the bottom slope. Here, plain symbols corresponds to $\phi < 0.45$, while transparent symbols are for $\phi \geq 0.45$ (see section 4.3 for details on the influence of ϕ).

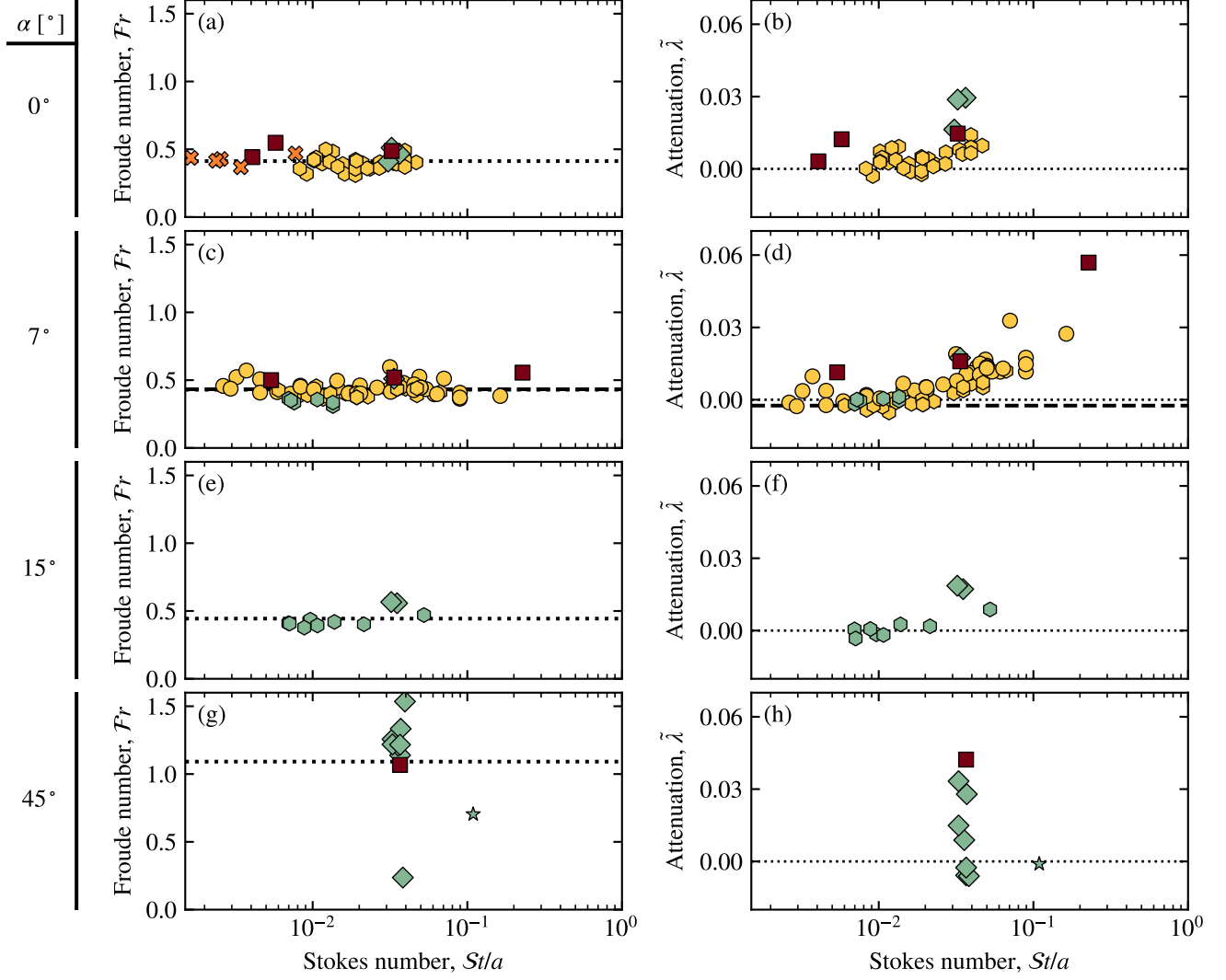


Figure 5: **Influence of particle settling.** Current Froude number Fr and attenuation $\tilde{\lambda}$ as a function of the ratio between the Stokes number and the lock aspect-ratio, for different ranges of bottom slopes. Here, we selected runs for $\phi < 0.45$ (see section 4.3 for details on the influence of ϕ).

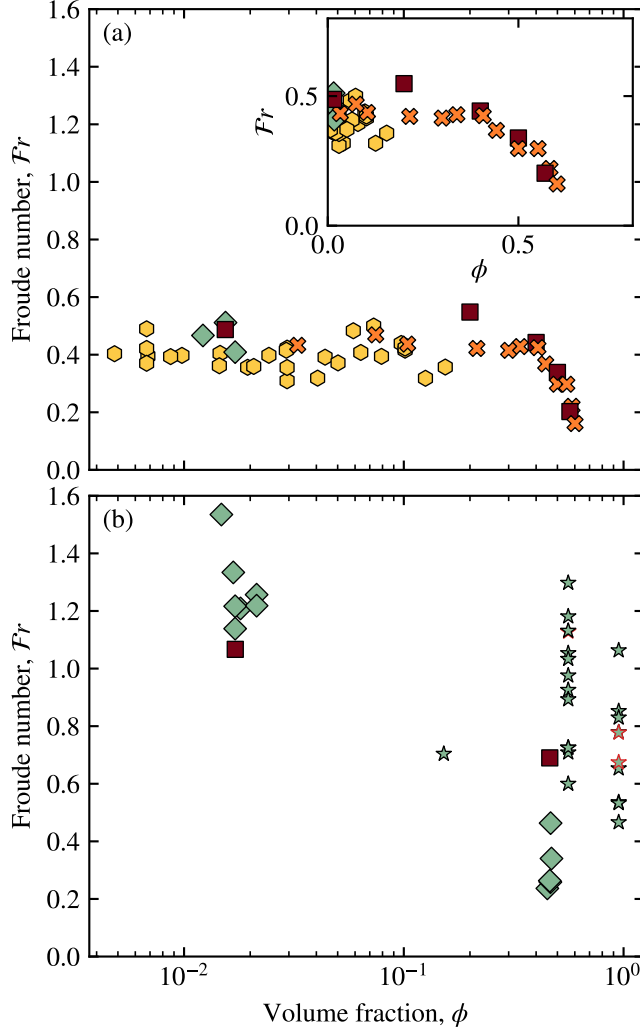


Figure 6: **Influence of particle volume fraction.** Current Froude number as a function of the initial particle volume fraction for (a) $\alpha \approx 0^\circ$, and (b) $\alpha \approx 45^\circ$. The inset in (a) shows the plot in linear scale.