

USER GUIDE  
Planetary-Code-Collection:  
Thermal and Ice Evolution Models  
for Planetary Surfaces

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# Contents

<b>1</b>	<b>Conduction of Heat: 1D Thermal Model for Planetary Surface</b>	<b>4</b>
1.1	Semi-Implicit Scheme on Irregular Grid . . . . .	4
1.1.1	Upper boundary condition . . . . .	5
1.1.2	Lower boundary condition . . . . .	6
1.2	Other Model Components . . . . .	6
1.2.1	Seasonal frost cover (Mars) . . . . .	6
1.2.2	Influence of ice on thermal properties . . . . .	6
1.2.3	Mars atmosphere . . . . .	7
	Bibliography . . . . .	8
<b>2</b>	<b>Diffusion of Water Vapor with Phase Transitions</b>	<b>9</b>
2.1	Governing Equations . . . . .	9
2.2	Discretizations . . . . .	10
2.2.1	Possible discretizations of spatial derivatives: . . . . .	10
2.2.2	Discretization of time derivative . . . . .	11
2.2.3	Complete scheme . . . . .	12
2.2.4	Upper boundary condition . . . . .	12
2.2.5	Lower boundary condition . . . . .	13
2.3	Numerical Stability . . . . .	13
	Bibliography . . . . .	13
<b>3</b>	<b>Long-Term Ice Evolution</b>	<b>14</b>
3.1	Equilibrium Models of Near-Surface Ice on Mars . . . . .	14
3.2	Asynchronous Model for Ice on Mars . . . . .	14
3.3	Asynchronous Model for Temperature, Impact Stirring, and Ice Loss on Asteroids . . . . .	15
	Bibliography . . . . .	15
<b>4</b>	<b>Terrestrial Analogs</b>	<b>16</b>
4.1	Mauna Kea atmosphere . . . . .	16
4.2	Dry Valleys of Antarctica . . . . .	17
	Bibliography . . . . .	17
<b>5</b>	<b>Radiative Heat Exchange on Topographic Surfaces</b>	<b>19</b>
5.1	Incidence on Sloped Surface . . . . .	19
5.2	Thermal Model for Planar Slopes . . . . .	19

5.3	Horizons and View Factors . . . . .	21
5.4	Governing Equations for Scattering . . . . .	22
5.5	Outline of Implementation . . . . .	24
5.6	3D Insolation with Atmosphere . . . . .	25
	Bibliography . . . . .	25
<b>6</b>	<b>Surface-bounded Exospheres</b>	<b>27</b>
6.1	Introduction . . . . .	27
6.2	Ballistic Flight on Sphere . . . . .	27
6.3	Other Model Components . . . . .	28
6.3.1	Photo-destruction . . . . .	28
6.3.2	Coriolis effect . . . . .	29
6.3.3	Event driver . . . . .	29
6.3.4	Residence times . . . . .	29
6.4	Non-uniform Gravity . . . . .	30
	Bibliography . . . . .	31

# Preface

Companion to <https://github.com/nschorgh/Planetary-Code-Collection/>

## Technical Notes:

Most of the code was developed with a **gfortran** compiler on an Intel processor. Many components were also run on various Linux clusters, sometimes using other compilers. The non-portable `real(8)` is meant to correspond to an 8-byte floating point number.

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# Part 1

## Conduction of Heat: 1D Thermal Model for Planetary Surface

1-Dimensional Numerical Model of Thermal Conduction and Surface Energy Balance

*Authors & History:* originally implemented by Samar Khatiwala in 2001 (including upper radiation boundary condition for semi-implicit scheme); extended to variable thermal properties and irregular grid by Norbert Schörghofer 2002–2003

Governing equation for the surface energy balance:

$$\rho c \frac{\partial T}{\partial t} = \frac{\partial}{\partial z} \left( k \frac{\partial T}{\partial z} \right) \quad (1.1)$$

$T$  ... temperature,  $t$  ... time,  $z$  ... depth,  $\rho c$  ... volumetric heat capacity,  $k$  ... thermal conductivity

$F = k \frac{\partial T}{\partial z}$  ... heat flux

+ various boundary conditions specified below. Note that a radiation upper boundary condition is non-linear.

### 1.1 Semi-Implicit Scheme on Irregular Grid

$$\frac{\partial}{\partial z} F_j = \frac{F_{j+\frac{1}{2}} - F_{j-\frac{1}{2}}}{(z_{j+1} - z_{j-1})/2} = 2 \frac{k_{j+\frac{1}{2}} \frac{T_{j+1} - T_j}{z_{j+1} - z_j} - k_{j-\frac{1}{2}} \frac{T_j - T_{j-1}}{z_j - z_{j-1}}}{z_{j+1} - z_{j-1}}$$

$$\begin{aligned} (\rho c)_j \frac{\partial T_j}{\partial t} &= \frac{2k_{j+\frac{1}{2}}}{(z_{j+1} - z_j)(z_{j+1} - z_{j-1})} T_{j+1} - \frac{2}{z_{j+1} - z_{j-1}} \left( \frac{k_{j+\frac{1}{2}}}{z_{j+1} - z_j} + \frac{k_{j-\frac{1}{2}}}{z_j - z_{j-1}} \right) T_j + \\ &+ \frac{2k_{j-\frac{1}{2}}}{(z_j - z_{j-1})(z_{j+1} - z_{j-1})} T_{j-1} \end{aligned}$$

$$\text{introduce } \alpha_j = \frac{\Delta t}{(\rho c)_j} \frac{k_{j+\frac{1}{2}}}{(z_{j+1} - z_j)(z_{j+1} - z_{j-1})} \quad \text{and} \quad \gamma_j = \frac{\Delta t}{(\rho c)_j} \frac{k_{j-\frac{1}{2}}}{(z_j - z_{j-1})(z_{j+1} - z_{j-1})} \quad (1.2)$$

$$\Delta t \frac{\partial T_j}{\partial t} = 2\alpha_j T_{j+1} - 2(\alpha_j + \gamma_j) T_j + 2\gamma_j T_{j-1}$$

$$T_j^{n+1} - T_j^n = \alpha_j T_{j+1}^{n+1} - (\alpha_j + \gamma_j) T_j^{n+1} + \gamma_j T_{j-1}^{n+1} + \alpha_j T_{j+1}^n - (\alpha_j + \gamma_j) T_j^n + \gamma_j T_{j-1}^n$$

$$\boxed{-\alpha_j T_{j+1}^{n+1} + (1 + \alpha_j + \gamma_j) T_j^{n+1} - \gamma_j T_{j-1}^{n+1} = \alpha_j T_{j+1}^n + (1 - \alpha_j - \gamma_j) T_j^n + \gamma_j T_{j-1}^n} \quad 1 < j < N \quad (1.3)$$

Superscript  $n$  refers to time step. Subscript  $j$  refers to position  $z_j$ . The conductivity  $k$  is defined on half-points. In the program,  $2(\rho c)_j = (\rho c)_{j+\frac{1}{2}} + (\rho c)_{j-\frac{1}{2}}$ . In this way, the parameters  $k$  and  $\rho c$  do not need to be defined at an interface of two layers with different thermal properties. Since indices in the program must be integers, we choose  $k(j) = k_{j-\frac{1}{2}}$  and the same for  $\rho c$ .

### 1.1.1 Upper boundary condition

#### a) Radiation

$$Q + k \left. \frac{\partial T}{\partial z} \right|_{z=0} = \epsilon \sigma T^4 \Big|_{z=0} \quad (1.4)$$

$Q$  is the incoming solar flux including the atmospheric contribution.

introduce auxiliary quantity  $T_0$ , such that surface temperature  $T_s = (T_0 + T_1)/2$

$$\left. \frac{\partial T}{\partial z} \right|_{z=0} = \frac{T_1 - T_0}{\Delta z} \quad \text{and} \quad T^4 \Big|_{z=0} = \left( \frac{T_0 + T_1}{2} \right)^4 \quad \text{with} \quad \Delta z = 2z_1$$

$T = T_r + T'$   $T_r$  is a reference temperature around which we linearize

$$\begin{aligned} Q + k_{1/2} \frac{T_1 - T_0}{\Delta z} &= \epsilon \sigma \left( \frac{2T_r + T'_0 + T'_1}{2} \right)^4 \\ &\approx \epsilon \sigma T_r^4 + 2\epsilon \sigma T_r^3 (T'_0 + T'_1) \\ &= -3\epsilon \sigma T_r^4 + 2\epsilon \sigma T_r^3 (T_0 + T_1) \end{aligned}$$

$$T_0 \left( \frac{k_{1/2}}{\Delta z} + B(T_r) \right) = Q + 3\epsilon \sigma T_r^4 + T_1 \left( \frac{k_{1/2}}{\Delta z} - B(T_r) \right) \quad \text{where} \quad B(T_r) = 2\epsilon \sigma T_r^3$$

introduce  $a = (Q + 3\epsilon \sigma T_r^4) / (\frac{k}{\Delta z} + B)$  and  $b = (\frac{k_{1/2}}{\Delta z} - B) / (\frac{k_{1/2}}{\Delta z} + B)$

$$-\alpha_1 T_2^{n+1} + (1 + \alpha_1 + \gamma_1 - \gamma_1 b^n) T_1^{n+1} = \alpha_1 T_2^n + (1 - \alpha_1 - \gamma_1 + \gamma_1 b^n) T_1^n + \gamma_1 \frac{Q^n + Q^{n+1} + 6\epsilon \sigma T_r^4}{\frac{k_{1/2}}{\Delta z} + B^n}$$

define  $\beta = \frac{\Delta t}{(\rho c)_1} \frac{1}{2\Delta z^2}$ , then  $\alpha_1 = \beta k_{3/2}$  and  $\gamma_1 = \beta k_{1/2}$

$$\text{surface temperature} \quad T_s = \frac{1}{2}(T_1 + T_0) = \frac{1}{2} \left( \frac{Q + 3\epsilon \sigma T_r^4}{k_{1/2}/\Delta z + B} + T_1 + bT_1 \right) = \frac{Q + 3\epsilon \sigma T_r^4 + \frac{2k}{\Delta z} T_1}{2(k_{1/2}/\Delta z + B)}$$

choose  $T_r^n = T_s^{n-1}$

implemented in `conductionQ.f`

## b) prescribed T

standard formulas (1.2,1.3) with  $T_0 = T_s$  and  $z_0 = 0$

$$\alpha_1 = \frac{\Delta t}{(\rho c)_1} \frac{k_{3/2}}{(z_2 - z_1)z_2}, \quad \gamma_1 = \frac{\Delta t}{(\rho c)_1} \frac{k_{1/2}}{z_1 z_2}$$

$$-\alpha_1 T_2^{n+1} + (1 + \alpha_1 + \gamma_1) T_1^{n+1} = \alpha_1 T_2^n + (1 - \alpha_1 - \gamma_1) T_1^n + \gamma_1 (T_s^n + T_s^{n+1})$$

implemented in `conductionT.f`

### 1.1.2 Lower boundary condition

(assume  $z_{N+1} - z_N = z_N - z_{N-1} =: \Delta z$ )

No heat flux:  $F_{N+\frac{1}{2}} = 0 \Rightarrow k_{N+\frac{1}{2}}(T_{N+1} - T_N) = 0 \Rightarrow T_{N+1} = T_N$

$$(1 + \gamma_N) T_N^{n+1} - \gamma_N T_{N-1}^{n+1} = (1 - \gamma_N) T_N^n + \gamma_N T_{N-1}^n$$

$$\gamma_N = \frac{\Delta t}{(\rho c)_N} \frac{k_{N-\frac{1}{2}}}{2(z_N - z_{N-1})^2}$$

Or geothermal heating:  $F_{N+\frac{1}{2}} = F_{\text{geothermal}} \Rightarrow k_{N+\frac{1}{2}}(T_{N+1} - T_N) = \Delta z F_{\text{geothermal}}$

$$(1 + \gamma_N) T_N^{n+1} - \gamma_N T_{N-1}^{n+1} = (1 - \gamma_N) T_N^n + \gamma_N T_{N-1}^n + \frac{\Delta t}{(\rho c)_N} \frac{F_{\text{geothermal}}}{\Delta z}$$

## 1.2 Other Model Components

### 1.2.1 Seasonal frost cover (Mars)

Add latent heat of CO<sub>2</sub> sublimation

$$Q + k \left. \frac{\partial T}{\partial z} \right|_{z=0} = \epsilon \sigma T^4|_{z=0} + L \frac{dm_{\text{CO}_2}}{dt} \quad (1.5)$$

call `conductionQ` if  $T_s$  is above CO<sub>2</sub> frost point or if  $m_{\text{CO}_2} = 0$ ; call `conductionT` if  $T_s$  is below CO<sub>2</sub> frost point or if  $m_{\text{CO}_2} > 0$ ; calculate energy difference and add CO<sub>2</sub> mass; adjust surface albedo; repeat this at every time step

### 1.2.2 Influence of ice on thermal properties

This is only one possible parametrization. In retrospective, it agrees well with the laboratory measurements by Siegler et al. (2012) for vapor-deposited ice.

$$\begin{aligned} \rho c &= (1 - \epsilon) \rho_{\text{regolith}} c_{\text{regolith}} + \epsilon f \rho_{\text{ice}} c_{\text{ice}} \\ k &= (1 - \epsilon) k_{\text{regolith}} + \epsilon f k_{\text{ice}} + (1 - f) \epsilon k_{\text{air}} \end{aligned}$$

$\rho$  ... density;  $c$  ... heat capacity;  $k$  ... thermal conductivity  
 $\epsilon$  ... porosity (void space / total volume)  
 $f$  ... ice filling fraction ( $f = \rho_f / \rho_{\text{ice}}$ ,  $\rho_f$  = density of free ice)  
Observed from orbit is ice-three thermal inertia  $I$ .

at around 200 Kelvin:  $c_{\text{ice}} \approx 1540 \text{ J/(kg K)}$ ,  $\rho_{\text{ice}} \approx 927 \text{ kg/m}^3$ ,  $k_{\text{ice}} \approx 3.2 \text{ W/(m K)}$   
See Winter and Saari (1969) for heat capacity of silicates as a function of temperature.  
See Handbook of Chemistry and Physics (Lide, 2003) for temperature dependence for ice.

In the program,  $k$  and  $\rho c$  are defined on half-points, while  $\rho_f$  and  $T$  are defined on grid points.

### 1.2.3 Mars atmosphere

The elevation  $\beta$  of the sun above an horizontal horizon is given in terms of geographic latitude  $\lambda$ , declination  $\delta$  of the sun, and the hour angle  $h$ :

$$\sin \beta = \cos \lambda \cos \delta \cos h + \sin \lambda \sin \delta. \quad (1.6)$$

The direct solar insolation is

$$Q_{\text{solar}} = \frac{S_0}{R^2} (1 - A) (1 - f)^{1/\max(\sin \beta, 0.04)} \sin \beta, \quad (1.7)$$

where  $S_0$  is the solar constant,  $R$  the distance from the sun in AU,  $A$  the albedo, and  $f$  due to the extinction in the atmosphere. The length of the path through the atmosphere is proportional to  $1/\sin \beta$  and the transmission is taken to be exponential in this path length. The nadir optical depth of the atmosphere is  $-\ln(1 - f)$ . For small extinction and away from the horizon,  $(1 - f)^{1/\sin \beta} \approx 1 - f/\sin \beta$ . The maximum atmospheric path length  $\ell_{\text{max}}$  is limited due to the curvature of the planet,  $H/\ell_{\text{max}} \approx \sqrt{H/2R} \approx 0.04$  for Mars, where  $H$  is the scale height of the atmosphere and  $R$  the radius of the planet.

Atmospheric emission is approximated by a fraction  $f_{\text{IR}}$  (typically 2–4%) of noontime insolation and is kept constant throughout a solar day (Kieffer et al., 1977):

$$Q_{\text{a,IR}} = f_{\text{IR}} \frac{S_0}{R^2} \sin \beta_{\text{noon}} \quad (\text{all day}) \quad (1.8)$$

This approximation fails in the polar regions; in this case, Kieffer et al. (1977) replaces the noontime insolation with the surface frost emission.

In addition, there is scattered light when  $\sin \beta > 0$ , which is approximated by

$$Q_{\text{a,scat}} = \frac{1}{2} f_{\text{scat}} \frac{S_0}{R^2}. \quad (1.9)$$

Half of the scattered light is assumed to be lost to space.

For the purpose of discussion, we determine the total energy budget of the atmosphere for a horizontal land mass. To first order  $(1 - f)^{1/\sin \beta} \sin \beta \approx \sin \beta - f$ , in eq. (1.7), so at any time the sun is above the horizon the energy absorbed and scattered in the atmosphere is approximately  $(S_0/R^2)f$ . Over a solar day

$$\frac{S_0}{R^2} f \int_{\text{daytime}} dh \approx \frac{S_0}{R^2} \pi f. \quad (1.10)$$



The infrared emission from the atmosphere over the same time period is

$$2\pi f_{\text{IR}} \frac{S_0}{R^2} \sin \beta_{\text{noon}} \quad (1.11)$$

and the scattered energy

$$\pi f_{\text{scat}} \frac{S_0}{R^2}. \quad (1.12)$$

The globally averaged  $\sin \beta_{\text{noon}}$  is

$$\frac{1}{\pi} \int_{-\pi/2}^{\pi/2} d\lambda \cos \lambda \sin \beta_{\text{noon}} \approx \frac{1}{\pi} \int_{-\pi/2}^{\pi/2} d\lambda \cos^2 \lambda = \frac{1}{2} \quad (1.13)$$

Global balance, (1.10)=(1.11)+(1.12), is achieved with

$$f = f_{\text{IR}} + f_{\text{scat}}.$$

This relation does not hold at an individual latitude, but it does hold globally.

This model was used in Schorghofer and Aharonson (2005) and in many subsequent modeling papers.

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## Part 2

# Diffusion of Water Vapor with Phase Transitions

1-Dimensional Diffusion of Water Vapor in Porous Medium with Phase Transitions;  
variable diffusivity; irregular grid  
3 phases: vapor, free (macroscopic) H<sub>2</sub>O ice, H<sub>2</sub>O adsorbate  
implemented in `vapordiffusioni.f`

*History:* developed 2003–2004

## 2.1 Governing Equations

indices:  $v$  ... gas (vapor),  $f$  ... free ice (solid),  $a$  ... adsorbed water  
 $\bar{\rho}$  ... mass per total volume,  $\bar{J}$  ... vapor flux per total area

**conservation of mass:**

$$\frac{\partial}{\partial t}(\bar{\rho}_v + \bar{\rho}_f + \bar{\rho}_a) + \nabla \cdot \bar{J} = 0 \quad (2.1)$$

**vapor transport:** (Landau and Lifshitz, 1987, Vol. VI, §57, §58)

$$J = -D\rho_0\nabla c \quad (2.2)$$

$c$  ... concentration  $c = \rho_v/\rho_0$

$\rho_{\text{air}}$  ... total density of air, including humidity

$\rho_v$  ... density of vapor

$$p_v = nkT = \rho_v \frac{k}{m_v} T \quad (2.3)$$

$m$  ... mass of molecule;  $k$  ... Boltzmann constant

**adsorption:**  $\bar{\rho}_a = A(p, T)$

The amount adsorbed also changes when ice is present.

$\epsilon$  ... porosity (= void space / total volume)

$\epsilon(1 - \rho_f/\rho_{\text{ice}})$  ... fraction of space available to gas

$\bar{\rho}_v = \rho_v \epsilon (1 - \rho_f / \rho_{\text{ice}})$        $\rho_v$  ... vapor density in void space  
 $\bar{\rho}_f = \rho_f \epsilon$        $\rho_f$  ... ice density in volume not occupied by regolith  
 $\bar{J} = J \epsilon (1 - \rho_f / \rho_{\text{ice}})$        $J$  ... vapor flux through void area  
 $\rho_{\text{ice}} \approx 926 \text{ kg/m}^3$  ... density of ice when it's really cold

Conservation of mass becomes

$$\frac{\partial}{\partial t} \left( \rho_v \left( 1 - \frac{\rho_f}{\rho_{\text{ice}}} \right) + \rho_f + \frac{1}{\epsilon} \bar{\rho}_a \right) + \partial_z \left( 1 - \frac{\rho_f}{\rho_{\text{ice}}} \right) J = 0$$

$$\frac{\partial}{\partial t} \left[ \rho_v \left( 1 - \frac{\rho_f}{\rho_{\text{ice}}} \right) + \rho_f + \frac{1}{\epsilon} \bar{\rho}_a \right] = \partial_z \left[ \left( 1 - \frac{\rho_f}{\rho_{\text{ice}}} \right) D \partial_z \rho_v \right]$$

introduce  $\varphi = 1 - \frac{\rho_f}{\rho_{\text{ice}}}$  and  $\gamma = \frac{k}{m} \frac{1}{\epsilon}$

$$\partial_t \left( \frac{p}{T} \varphi + \frac{k}{m_v} \rho_f \right) + \gamma \left( \frac{\partial \bar{\rho}_a}{\partial p} \partial_t p + \frac{\partial \bar{\rho}_a}{\partial T} \partial_t T \right) = \partial_z \left[ D \varphi \left( \partial_z \frac{p}{T} \right) \right] \quad (2.4)$$

This is an equation for  $p$  and  $\rho_f$ .

If there is no ice, then

$$\left( \frac{1}{T} + \gamma \frac{\partial \bar{\rho}_a}{\partial p} \right) \partial_t p + \left( -\frac{p}{T^2} + \gamma \frac{\partial \bar{\rho}_a}{\partial T} \right) \partial_t T = \partial_z \left( D \partial_z \frac{p}{T} \right)$$

## 2.2 Discretizations

### 2.2.1 Possible discretizations of spatial derivatives:

Note: These spatial discretizations are not necessarily optimal in terms of discretization error.

$$\partial_z(a \partial_z b)|_j = \frac{1}{\Delta z^2} (a_{j+1/2}(b_{j+1} - b_j) - a_{j-1/2}(b_j - b_{j-1})) + O(\Delta z^2) \quad (2.5)$$

or

$$\partial_z(a \partial_z b)|_j = \frac{1}{2\Delta z^2} ((a_{j+1} + a_j)(b_{j+1} - b_j) - (a_j + a_{j-1})(b_j - b_{j-1})) + O(\Delta z^2) \quad (2.6)$$

or

$$\begin{aligned} \partial_z(a \partial_z b)|_j &= a \partial_{zz} b + (\partial_z a) \partial_z b \\ &= \frac{1}{\Delta z^2} \left( a_j(b_{j+1} - 2b_j + b_{j-1}) + \frac{1}{4}(a_{j+1} - a_{j-1})(b_{j+1} - b_{j-1}) \right) + O(\Delta z^2) \end{aligned} \quad (2.7)$$

The most general discretization which is accurate to  $O(\Delta z^2)$ , rather than just  $O(\Delta z)$ , is of the following form (mathematica notebook discretization2.nb)

$$\begin{aligned} \partial_z(a\partial_z b)|_j &= \frac{1}{\Delta z^2} \left( ca_j b_j + \left(-1 - \frac{c}{2}\right) a_{j-1} b_j + \left(-1 - \frac{c}{2}\right) a_{j+1} b_j \right. \\ &\quad \left. - \frac{c}{2} a_j b_{j-1} + \frac{3+c}{4} a_{j-1} b_{j-1} + \frac{1+c}{4} a_{j+1} b_{j-1} \right. \\ &\quad \left. - \frac{c}{2} a_j b_{j+1} + \frac{1+c}{4} a_{j-1} b_{j+1} + \frac{3+c}{4} a_{j+1} b_{j+1} \right) + O(\Delta z^2) \end{aligned} \quad (2.8)$$

Choices (2.6) and (2.7) above correspond to  $c = -1$  and  $c = -2$ , respectively.

Another set of schemes are the ones that do not involve the corner points  $a_{j+1}b_{j-1}$  and  $a_{j-1}b_{j+1}$ . They are of the following form (mathematica notebook discretization3.nb)

$$\begin{aligned} \partial_z(a\partial_z b)|_j &= \frac{1}{\Delta z^2} \left( -a_j b_j - ca_{j-1} b_j + (-1+c)a_{j+1} b_j + \right. \\ &\quad \left. (1-c)a_j b_{j-1} + ca_{j-1} b_{j-1} + ca_j b_{j+1} + (1-c)a_{j+1} b_{j+1} \right) + \\ &\quad \left( c - \frac{1}{2} \right) O(\Delta z) + O(\Delta z^2) \\ &= \frac{1}{\Delta z^2} [(1-c)a_{j+1}(b_{j+1} - b_j) + ca_{j-1}(b_{j-1} - b_j) + a_j(cb_{j+1} - b_j + (1-c)b_{j-1})] + O(\Delta z) \end{aligned} \quad (2.9)$$

For  $c = 1/2$  this reduces to scheme (2.6) above

If starting with complete pore filling,  $c > 0$  is required for downward motion of ice table.

On irregular grid: General scheme without corner points (mathematica notebook discretization6.nb)

$$\begin{aligned} \partial_z(a\partial_z b)|_j &= -\frac{2c + (1-2c)h_+/h_-}{h_-h_+} a_j b_j + \frac{-1 + (1-2c)h_+/h_-}{h_-(h_- + h_+)} a_{j-1} b_j + \frac{2c-2}{h_+(h_- + h_+)} a_{j+1} b_j + \\ &\quad + \frac{1 + (1-2c)h_+/h_-}{h_-(h_- + h_+)} a_j b_{j-1} + \frac{1 + (2c-1)h_+/h_-}{h_-(h_- + h_+)} a_{j-1} b_{j-1} + \frac{2c}{h_+(h_- + h_+)} a_j b_{j+1} \\ &\quad + \frac{2-2c}{h_+(h_- + h_+)} a_{j+1} b_{j+1} + O(h_+ + h_-) \end{aligned} \quad (2.10)$$

where  $h_+ = z_{j+1} - z_j$  and  $h_- = z_j - z_{j-1}$ . For  $h_+ = h_- = h$  this reduces to (2.9)

## 2.2.2 Discretization of time derivative

use eq. (2.4),  $A \equiv f$

$$\begin{aligned} \frac{p_j^{n+1}}{T_j^{n+1}} \varphi_j^{n+1} - \frac{p_j^n}{T_j^n} \varphi_j^n + \frac{k}{\mu} \left( \rho_{f_j}^{n+1} - \rho_{f_j}^n \right) + \gamma \left. \frac{\partial f}{\partial p} \right|_j^n (p_j^{n+1} - p_j^n) + \\ + \gamma \left. \frac{\partial f}{\partial T} \right|_j^n (T_j^{n+1} - T_j^n) = \Delta t \left( \partial_z D \varphi \partial_z \frac{p}{T} \right)_j^n \end{aligned} \quad (2.11)$$

derivatives of the isotherm are not expanded to keep it linear

### 2.2.3 Complete scheme

using (2.11) and (2.10)

$$\begin{aligned}\xi_j^{n+1} = & \frac{p_j^n}{T_j^n} \varphi_j^n + \frac{k}{\mu} \rho_f^n + \gamma \left. \frac{\partial f}{\partial p} \right|_j^n p_j^n - \gamma \left. \frac{\partial f}{\partial T} \right|_j^n (T_j^{n+1} - T_j^n) + \\ & \frac{\Delta t}{\Delta z^2} \left[ D_j \varphi_j^n \left( \frac{p_{j+1}^n}{T_{j+1}^n} - 2 \frac{p_j^n}{T_j^n} + \frac{p_{j-1}^n}{T_{j-1}^n} \right) + \frac{1}{4} (D_{j+1} \varphi_{j+1}^n - D_{j-1} \varphi_{j-1}^n) \left( \frac{p_{j+1}^n}{T_{j+1}^n} - \frac{p_{j-1}^n}{T_{j-1}^n} \right) \right]\end{aligned}$$

$$\text{where } \xi^{n+1} = \frac{p^{n+1}}{T^{n+1}} \left( 1 - \frac{\rho_f^{n+1}}{\rho_{\text{ice}}} \right) + \frac{k}{\mu} \rho_f^{n+1} + \gamma \left. \frac{\partial f}{\partial p} \right|^{n+1} p^{n+1}$$

$$p \leq p_{sv}(T) \text{ and } 0 \leq \rho_f \leq \rho_{\text{ice}}$$



$p_{sv}$  ... saturation vapor pressure

$$\text{Try } \rho_f^{n+1} = 0 \Rightarrow p^{n+1} = \frac{T^{n+1} \cdot \xi^{n+1}}{1 + T^{n+1} \gamma \left. \frac{\partial f}{\partial p} \right|^{n+1}} \quad \text{and} \quad \rho_f^{n+1} = 0$$

$$\text{If } p^{n+1} > p_{sv}(T^{n+1}) \text{ then } p^{n+1} = p_{sv}(T^{n+1}) \quad \text{and}$$

$$\rho_f^{n+1} = \frac{\xi^{n+1} - \frac{p_{sv}(T^{n+1})}{T^{n+1}} - \gamma \left. \frac{\partial f}{\partial p} \right|^{n+1} p_{sv}(T^{n+1})}{\frac{k}{\mu} - \frac{p_{sv}(T^{n+1})}{T^{n+1} \rho_{\text{ice}}}}$$

$$\text{introduce } p_{\text{frost}}^{n+1} = p_{sv}(T^{n+1})$$

### 2.2.4 Upper boundary condition

- 1)  $p(z=0, t) = p_{\text{atm.}}(t)$
- 2)  $D(z=0) = D_0$
- 3)  $\varphi_0 = 1$

$$\partial_z \left( D \varphi \partial_z \frac{p}{T} \right) \Big|_{j=0} = \frac{1}{\Delta z^2} \left[ D_1 \varphi_1 \left( \frac{p_2}{T_2} - 2 \frac{p_1}{T_1} + \frac{p_{\text{atm}}}{T_{\text{surf}}} \right) + \frac{1}{4} (D_2 \varphi_2 - D_0 \varphi_0) \left( \frac{p_2}{T_2} - \frac{p_{\text{atm}}}{T_{\text{surf}}} \right) \right] \quad (2.12)$$

for half-shifted grid ( $z_2 = 3z_1$ ):

$$a\partial_{zz}b + (\partial_z a)\partial_z b = \frac{1}{\Delta z^2} \left[ a_1 \left( \frac{8}{3}b_s - 4b_1 + \frac{4}{3}b_2 \right) + \left( -\frac{4}{3}a_s + a_1 + \frac{1}{3}a_2 \right) \left( -\frac{4}{3}b_s + b_1 + \frac{1}{3}b_2 \right) \right] \quad (2.13)$$

### 2.2.5 Lower boundary condition

$$\text{no vapor flux (impermeable) } J = 0 \quad \Rightarrow \quad \partial_z \rho_v = 0 \quad \Rightarrow \quad \partial_z \frac{p}{T} = 0 \quad \Rightarrow \quad \frac{p_{N+1}}{T_{N+1}} = \frac{p_{N-1}}{T_{N-1}}$$

$$\partial_z \left( D\varphi \partial_z \frac{p}{T} \right) \Big|_{j=N} = \frac{1}{\Delta z^2} 2D_N \varphi_N \left( \frac{p_{N-1}}{T_{N-1}} - \frac{p_N}{T_N} \right) \quad (2.14)$$

## 2.3 Numerical Stability

von Neumann stability analysis has been carried out for various variants of the scheme; this is only relevant for discussion purposes. Typeset notes are available upon request.

Used in Schorghofer and Aharonson (2005)

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# Part 3

## Long-Term Ice Evolution

Long-term evolution of sub-surface ice due to loss to space (for asteroids) or exchange with atmosphere (for Mars) using diurnally-resolved temperatures

*History:*

2002–2004 equilibrium ice table on Mars

2006–2011 asynchronous model for ice on Mars (where re-charge can occur)

2013–2017 asynchronous model for asteroids (where impact-gardening occurs)

### 3.1 Equilibrium Models of Near-Surface Ice on Mars

The equilibrium depth to the ice table is defined by a balance between the vapor pressure at the ice table and the atmosphere. It is the end result of atmosphere-subsurface vapor exchange after an asymptotically long time. If no equilibrium is possible, then subsurface ice is “unstable”. Using the thermal model described in Part 1, this model calculates the equilibrium depth based on matching the vapor density at the ice table and the atmosphere. The thermal model is run over a number of years to equilibrate, and annual means are taken from the last year. As the ice content of the subsurface changes the thermal properties, the thermal model is repeatedly equilibrated. The code deploys an iterative root-finding procedure, using the bisection method. The iterations are performed by `mars_mapi.f`, which finds the equilibrium depth. Then `mars_mapt2.f` can be used to output additional variables for a given ice table depth.

The model is extensively used in Schorghofer and Aharonson (2005), where further description is available. With extensions described in section 5.2 for planar slopes, it also forms the core of the model used in Aharonson and Schorghofer (2006).

### 3.2 Asynchronous Model for Ice on Mars

Schorghofer (2010) provides a description of this rather complex model, which is not repeated here. In brief, the model couples a diurnally-resolved thermal model with a long-term ice evolution model. Ice (massive or interstitial) can be lost to the atmosphere and vice-versa, pore spaces can be recharged with interstitial ice. Details of the long-term ice evolution model are also described there, which involve a one-sided derivative at the moving ice table, otherwise a numerical instability occurs due to the strong contrast in thermal properties at the ice table. The model allows for up

to three layers: dry, soil with interstitial ice (plus air), and massive ice with dust. In the current implementation, one of the two interfaces is tracked explicitly. The model is extensively used in Schorghofer (2007) and Schorghofer and Forget (2012) for studies of the Martian Ice Age cycle.

### 3.3 Asynchronous Model for Temperature, Impact Stirring, and Ice Loss on Asteroids

Schorghofer (2016) describes this model and applies it to (1) Ceres and (7968) Elst-Pizarro. In brief, it combines diurnally-resolved temperatures, probabilistic impact stirring, and the long-term loss of near-surface ice to space. It was also used for the ice retreat calculations published in Prettyman et al. (2017). The main program is `asteroid_fast2`.

A significant complexity in this model arises from partially ice-filled pore spaces (necessary to incorporate the consequences of impact stirring). The re-distribution of ice within the pores due to vapor diffusion and deposition adds another governing equation. It was found that this redistribution is negligible in all cases it was considered. A simpler two-layer version is implemented in `asteroid_fast1`, which is similar to the model described in the supporting information of Sizemore et al. (2017).

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# Part 4

## Terrestrial Analogs

1-Dimensional Thermal Model, 0-Dimensional Terrestrial Atmosphere, 3-Dimensional Insolation Model (terrain shadowing)

Sun position as a function of date is based on Blanco-Muriel et al. (2001), translated into Fortran. It provides the zenith angle and azimuth of the sun, and the Earth-sun distance. Implemented in `sunpos.f90`

### 4.1 Mauna Kea atmosphere

calculate clear-sky direct and indirect short-wave irradiance on Mauna Kea in  $\text{W/m}^2$   
mostly based on Nunez (1980), corrected for typos. Implemented in `mk_atmosphere.f90`

$Z$  ... solar zenith angle (radians)

$I_0$  ... clear-sky direct irradiance;  $D_0$  ... clear-sky diffuse irradiance

$R$  ... Earth-sun distance in AU

$m, m'$  ... optical air mass (unitless)

$p_0$  ... total pressure (Pa)

$w$  ... precipitable water vapour (cm)

Transmission coefficients:

$\psi_{wa}$  ... water vapor absorption;  $\psi_{ws}$  ... water vapor scattering

$\psi_{rs}$  ... Rayleigh scattering

$\psi_{da}$  ... dust absorption;  $\psi_{ds}$  ... dust scattering

#### Relative air mass:

simplest approximation:  $m = 1/\cos Z$

better approximation (Kasten, 1966):

$$m = \frac{1}{\cos Z + 0.15 \times (93.885 - Z)^{-1.253}} \quad (4.1)$$

if ( $m < 0$ ), then  $m = \infty$

$p_0 = 610$  on Mauna Kea summit

$m' = m \times p_0/1013$

**Water vapor:**

$w = 0.16$  cm for Mauna Kea, according to [www.gemini.edu/sciops/telescopes-and-sites/observing-condition-constraints/mk-water-vapour-statistics](http://www.gemini.edu/sciops/telescopes-and-sites/observing-condition-constraints/mk-water-vapour-statistics)

$$\psi_{wa} = 1 - 0.077(wm)^{0.30} \quad \text{McDonald (1960)} \quad (4.2)$$

$$\psi_{ws} = 1 - 0.025wm \quad (4.3)$$

**Rayleigh scattering:** 8% at sea level according to Fig 3-3 in Bird and Hulstrom (1981)

$$\psi_{rs} = \exp(-0.08m') \quad (4.4)$$

**Aerosols:** aerosol optical depth on Mauna Kea  $= 0.0084 \times (\lambda/1\mu m)^{-1.26}$  (Buton et al., 2013)

$$\psi_{ds} = \exp(-m \times 0.0084 \times 0.5^{-1.26}) \quad (4.5)$$

$$\psi_{da} = \psi_{ds} \quad \text{assumes single scattering albedo of 0.5} \quad (4.6)$$

**Direct sunlight:**

$$I_0 = \psi_{wa}\psi_{da}\psi_{ws}\psi_{rs}\psi_{ds} \times (\text{solar constant})/R^2 \quad (4.7)$$

(without the last factor, this is the transmittance)

**Diffuse sunlight:**

$$D_0 = I_0 \cos(Z) \psi_{wa}\psi_{da} \frac{1 - \psi_{ws}\psi_{rs}\psi_{ds}}{2} \quad (4.8)$$

*Roundoff issue:* if  $(D_0 \leq 0)$ , then  $D_0 = 0$  because of -0

**Total short-wavelength flux:**

$$F = I_0 \cos Z + D_0 \quad (4.9)$$

*Roundoff issue:* if  $(F \leq 0)$ , then  $F = 0$  because of -0

Not included are the sensible heat flux and long-wave downward radiation.

**Atmospheric contribution with terrain shadowing:** see Part 5 and references therein.

used in Schorghofer et al. (2017)

## 4.2 Dry Valleys of Antarctica

This model calculates the loss of buried ice to the atmosphere, and involves molecular diffusion in an air-H<sub>2</sub>O mixture, including the advective contribution. The equations underlying this model are described in Schorghofer (2005). The source code has not been readied for distribution and no further documentation was written. This type of model has been superseded by implementations from other research groups. Nevertheless, source code or additional information could be available upon request.

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# Part 5

## Radiative Heat Exchange on Topographic Surfaces

Diffuse Scattering of Short-Wavelength and Thermal Infrared on Surface with Topography (3D Surface Energy Balance)

*History:*

2002–2005 Planar slopes (sec. 5.2)

2010–2018 3D topography (sec. 5.3–5.6)

### 5.1 Incidence on Sloped Surface

The elevation  $\beta$  of the sun above an horizontal horizon is given in terms of geographic latitude  $\lambda$ , declination  $\delta$  of the sun, and the hour angle  $h$ :

$$\sin \beta = \cos \lambda \cos \delta \cos h + \sin \lambda \sin \delta. \quad (5.1)$$

The angle  $\theta$  of the sun above a sloped surface is

$$\sin \theta = \cos \alpha \sin \beta - \sin \alpha \cos \beta \cos(\Delta a), \quad (5.2)$$

where  $\Delta a$  is the difference between the azimuth of the sun and the azimuth of the topographic gradient. The sun is assumed to be below the horizon if either  $\sin \beta < 0$  (horizontal horizon at infinity) or  $\sin \theta < 0$  (self shadowing of slope). For 3D topography, a distant horizon, higher than the self shadowing slope, introduces an additional cutoff  $e_{\max}$  (maximum horizon elevation).

On an airless body the direct insolation is

$$Q_{\text{solar}} = \frac{S_0}{R^2} (1 - A) \sin \theta. \quad (5.3)$$

where  $S_0$  is the solar constant,  $R$  the distance from the sun in AU, and  $A$  the albedo.

### 5.2 Thermal Model for Planar Slopes

Thermal Balance for Planar Slopes; coupled 1D Models plus 0D Atmosphere for Mars, but easily simplified to airless bodies

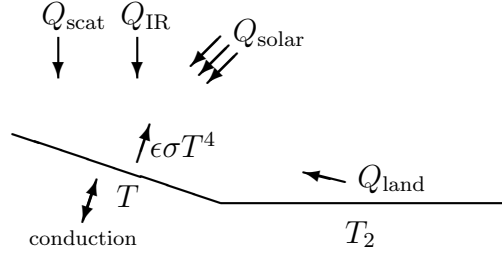


Figure 5.1: Contributions to the heat balance on a slope with surface temperature  $T$ .

Planar slopes are much simpler than the general 3D problem

$\alpha$  ... slope angle

The heat balance on the surface is

$$Q(\alpha) + k \left. \frac{\partial T}{\partial z} \right|_{z=0} = \epsilon \sigma T^4 + (\text{latent heat of CO}_2 \text{ frost}) \quad (5.4)$$

with

$$Q = Q_{\text{solar}}(\alpha) + Q_{\text{a,IR}}(\alpha) + Q_{\text{a,scat}}(\alpha) + Q_{\text{land}}(\alpha). \quad (5.5)$$

$Q$  is the incoming radiation from the sun, atmosphere, and surfaces within field of view,  $T$  temperature,  $z$  the vertical coordinate,  $k$  the thermal conductivity,  $\epsilon$  emissivity, and  $\sigma$  the Stefan-Boltzmann constant. The subscript  $a$  denotes contributions from the atmosphere.

The direct solar insolation is

$$Q_{\text{solar}} = \frac{S_0}{R^2} (1 - A) (1 - f)^{1/\max(\sin \beta, 0.04)} \sin \theta, \quad (5.6)$$

where  $f$  due to the extinction in the atmosphere. This is a generalization of (1.7). The length of the path through the atmosphere is proportional to  $1/\sin \beta$ . The maximum atmospheric path length is limited due to the curvature of the planet, which motivates the threshold of 0.04, as described in subsection 1.2.3.

The calculation of the atmospheric absorption and scattering is modified from subsection 1.2.3 to involve a slope factor of  $\cos^2(\alpha/2)$ . This slope factor for the IR emission takes into account that a tilted surface facing a horizontal horizon sees only a restricted portion of the sky. It is unclear whether this is the best approximation, see Rakovec and Zakšek (2012). An isotropic flux is another commonly-used approximation for the shortwave diffusive flux (Flo Heggem et al., 2001).

Atmospheric emission is approximated by a fraction  $f_{\text{IR}}$  (typically 2–4%) of noontime insolation and is kept constant throughout a solar day (Kieffer et al., 1977):

$$Q_{\text{a,IR}} = f_{\text{IR}} \frac{S_0}{R^2} \cos^2 \left( \frac{\alpha}{2} \right) \sin \beta_{\text{noon}} \quad (\text{all day}) \quad (5.7)$$

$$Q_{\text{a,scat}} = \frac{1}{2} f_{\text{scat}} \frac{S_0}{R^2} \cos^2 \left( \frac{\alpha}{2} \right) \quad \text{when } \sin \beta > 0 \quad (5.8)$$

The surface reemits radiation in all directions, but receives additional heat from surfaces in its field of view. This emission is weighted according to the incidence angles  $i$  and integrated over

the spherical angle  $\Omega$  subtended by the visible land surfaces. If we imagine a horizontal surface at uniform temperature  $T_2$  (Kreslavsky and Head, 2005):

$$Q_{\text{land}} = \epsilon_2 \sigma T_2^4 \int \cos i \, d\Omega = \sin^2 \left( \frac{\alpha}{2} \right) \epsilon_2 \sigma T_2^4. \quad (5.9)$$

If one assumes  $T_2 = T$  and  $\epsilon_2 = \epsilon$ , then this term can be brought to the right-hand side of eq. (5.4), leading to an effective emissivity of  $\epsilon \cos^2(\alpha/2)$ . However, this is often not a good approximation. It is more accurate to base  $T_2$  on a separate 1D model for a flat surface.

The equation of heat conduction is solved in the subsurface with a semi-implicit Crank-Nicolson scheme on a grid with spatially varying spacings, as described in Part 1 of the User Guide.

Used in Aharonson and Schorghofer (2006); Schorghofer and Edgett (2006)

### 5.3 Horizons and View Factors

Shadowing by nearby topography (terrain shading) defines local horizons and is important for the energy balance. Horizons for each surface element are determined with azimuth rays, typically every  $2^\circ$  in azimuth, and the highest horizon in each direction is stored. For the purpose of horizon calculations, the topography is represented by triangular surface elements. The horizon-finding calculation is implemented in `shadows.f90` and `shadow_subs.f90`.

The topography is defined on a rectangular coordinate grid with spatial resolution  $\Delta x$  in the longitude direction and  $\Delta y$  in the latitude direction. Curvature effects are not incorporated, i.e. the domain needs to be small compared to the radius of the body. Nor can the domain include the rotational pole. Surface normals are calculated using center-differences in  $x$ - and  $y$ -direction, and one-sided differences at the domain boundaries.

Use of spatial grids with various resolutions (multigrid method) can dramatically accelerate the horizons calculation, because cells that are far from the point of interest are larger and fewer. For a domain with  $N \times N$  pixels, the computational cost with without multigrid method is  $O(N^4)$ . With multigrid, it is  $O(N \log N)^2$ . In the current implementation of the multigrid method, up to ten grids can be used, the coarsest has  $2^{10-1}$  less resolution than the finest. If the multigrid method is not used, an optional cut-off radius `RMAX` can be introduced, so spatial distances larger than `RMAX` are ignored.

If only shadows (and direct insolation) are to be calculated, these horizon heights are all the geometrical information that is needed. The field of view for each surface element is calculated in terms of the spherical angle as viewed from the other element,  $d\Omega$ , and stored. Mutual visibility is determined by calculating the slope of the line that connects the two elements and comparing it to the maximum topographic slope along a ray in the same direction, tracing outward. (Hence there is a sort involved that is not necessary if only horizons are needed.) For the purpose of view factors, the topography is represented by rectangles. The view factor calculation is implemented in `fieldofviews.f90` and `fieldofview_subs.f90`. Neighbors in 8 directions are considered.

The result of these geometric calculations serve as input for insolation or thermal calculations.

## 5.4 Governing Equations for Scattering

The equation governing the energy balance on the surface is

$$(1 - A)(Q_{\text{direct}} + Q_{\text{refl}}) + k \frac{\partial T}{\partial z} + \epsilon Q_{\text{IR}} = \epsilon \sigma T^4 \quad (5.10)$$

where  $A$  is albedo,  $Q_{\text{direct}}$  incoming solar radiation (insolation),  $k$  thermal conductivity,  $T$  temperature,  $z$  depth below surface,  $\epsilon$  emissivity, and  $\sigma$  the Stefan-Boltzmann constant. The flux  $Q_{\text{direct}}$  is determined from the declination of the Sun, latitude, and hour angle, eqs. (5.1, 5.2). Due to topography, reflected sunlight ( $Q_{\text{refl}}$ ) and thermal emission ( $Q_{\text{IR}}$ ) from other surfaces also need to be added.

The amount of sunlight diffusely reflected depends on the spherical angle  $d\Omega$  subtended by the surface element, and similarly for infrared emission:

$$Q_{\text{refl}}(x, y) = \frac{1}{\pi} \iint A' [Q'_{\text{direct}} + Q'_{\text{refl}}] \cos i \, d\Omega(x, y, x', y') \quad (5.11)$$

$$Q_{\text{IR}}(x, y) = \frac{1}{\pi} \iint [\epsilon \sigma T'^4 + (1 - \epsilon) Q'_{\text{IR}}] \cos i \, d\Omega(x, y, x', y') \quad (5.12)$$

where primed variables are evaluated at  $(x', y')$  and unprimed variables at  $(x, y)$ . The integrals are over all surface elements within the field of view, and  $i$  is the local incidence angle. Equations (5.11) and (5.12) turn into an explicit time-stepping procedure when  $Q'_{\text{refl}}$  and  $Q'_{\text{IR}}$  on the right hand side are evaluated at the previous time step. The term with the factor  $(1 - \epsilon)$  is reflected infrared.

The model also includes 1D subsurface heat conduction, eq. (1.1). Subsurface temperatures need to be equilibrated, and hence the entire model needs to be run much longer than would be necessary without subsurface heat. Lateral subsurface heat conduction is neglected. Without subsurface conduction, equilibrium temperatures, according to eq. (5.10) with  $k = 0$ , can be used, and only a few steps of equilibration are needed in this case.

The differential solid angle can be written as

$$d\Omega = \cos e \, de \, d\varphi \quad (5.13)$$

where  $\varphi$  is azimuth and  $e$  the elevation (an angle) above the horizon. The solid angle of the entire landscape within field of view is

$$\Omega_{\text{land}} = \iint d\Omega = \int_0^{2\pi} \int_0^{e(\varphi)} de \, d\varphi \cos e = \int_0^{2\pi} d\varphi \sin(e(\varphi)) \quad (5.14)$$

The size of the visible sky is  $2\pi - \Omega_{\text{land}}$ . The sky view factor  $F$  is the spherical angle of the visible sky divided by  $2\pi$ . Hence,  $F = 1 - \Omega_{\text{land}}/(2\pi)$ . It is also helpful to introduce the abbreviation

$$G = \frac{1}{\pi} \iint \cos i \, d\Omega \quad (5.15)$$

Next several special cases, with increasing complexity, are considered:

- a) In the special case of a surface covered by a dome at uniform temperature,

$$\iint \cos i \, d\Omega = \int_0^{2\pi} d\varphi \int_0^{\pi/2} de \sin e \cos e = 2\pi \int_0^{\pi/2} de \sin e \cos e = 2\pi \frac{1}{2} \sin^2(\pi/2) = \pi$$

Hence  $G = 1$  and (5.12) becomes  $Q_{\text{IR}} = \epsilon \sigma T'^4$ .

- b) Another special case is a planar slope with a single temperature combined with a horizontal surface with another temperature, as in Figure 5.1. In this case,  $\Omega = 2\alpha$ , so that at  $\alpha = \pi/2$  a quarter of the sphere remains. For the slope, the horizon height  $e(\varphi)$  along direction  $\varphi$  is related by  $\tan \alpha \cos \varphi = \tan e$ .

For integration practice,

$$\iint d\Omega = \int_{-\pi/2}^{\pi/2} d\varphi \int_0^{e(\varphi)} de \cos e = \int_{-\pi/2}^{\pi/2} d\varphi \sin(e(\varphi)) = \int_{-\pi/2}^{\pi/2} d\varphi \frac{\tan \alpha \cos \varphi}{\sqrt{1 + \tan^2 \alpha \cos^2 \varphi}} = 2\alpha$$

where  $\sin e = \tan e / \sqrt{1 + \tan^2 e}$  was used. The integral of interest

$$\begin{aligned} \iint \cos i \, d\Omega &= \int_{-\pi/2}^{\pi/2} d\varphi \int_0^{e(\varphi)} de \sin e \cos e \\ &= \int_{-\pi/2}^{\pi/2} d\varphi \frac{1}{2} \sin^2(e(\varphi)) = \frac{1}{2} \int_{-\pi/2}^{\pi/2} d\varphi \frac{\tan^2 \alpha \cos^2 \varphi}{1 + \tan^2 \alpha \cos^2 \varphi} \\ &= \frac{\pi}{2} (1 - \cos \alpha) = \pi \sin^2 \left( \frac{\alpha}{2} \right) \end{aligned}$$

In this case,  $G = \sin^2(\alpha/2)$  and (5.12) becomes

$$Q_{\text{IR}} = \epsilon \sigma T'^4 \sin^2 \left( \frac{\alpha}{2} \right)$$

plus the reflected infrared, which reproduces (5.9).

- c) Uniform temperature, locally flat ( $\cos i = \sin \beta$ ):

$$\iint \cos i \, d\Omega = \int_0^{2\pi} \int_0^{e(\varphi)} de \, d\varphi \cos e \sin e = \frac{1}{2} \int_0^{2\pi} d\varphi \sin^2(e(\varphi))$$

$G$  is  $\sin^2 e(\varphi)$  averaged over azimuths. Note that  $G$  is not proportional to  $\Omega_{\text{land}}$  (5.14), not even for small  $e$ . And for small  $e$ , it is much smaller than  $\Omega_{\text{land}}$ .

- d) Uniform temperature, not locally flat ( $\cos i = \sin \theta$ ):

$$\sin \theta = \cos \alpha \sin \beta + \sin \alpha \cos \beta \cos(\Delta a)$$

where  $\alpha$  is the local slope angle. There is now also a lower limit on the elevation angle,  $e_{\text{min}}(\varphi)$ , from the self-shadowing of the slope, so  $\sin \theta$  will never become negative, and therefore

$$\tan e_{\text{min}} = -\tan \alpha \cos(\Delta a)$$



The integral of interest is

$$\iint \cos i \, d\Omega = \int_0^{2\pi} \int_{e_{\min}(\varphi)}^{e(\varphi)} de \, d\varphi \cos e [\cos \alpha \sin e + \sin \alpha \cos e \cos(\Delta a)] \quad (5.16)$$

and the integrals over  $e$  can be computed as

$$\begin{aligned} \frac{1}{\pi} \int de \cos e \sin e &= \frac{1}{2\pi} \sin^2 e \\ \frac{1}{\pi} \int de \cos^2 e &= \frac{1}{2\pi} (e + \sin e \cos e) \end{aligned}$$

$G$  can be pre-computed from static geometric information:

$$\begin{aligned} G &= \frac{\cos \alpha}{2\pi} \int_0^{2\pi} d\varphi (\sin^2 e - \sin^2 e_{\min}) + \\ &\quad + \frac{\sin \alpha}{2\pi} \int_0^{2\pi} d\varphi \cos(\Delta a) (e + \sin e \cos e - e_{\min} - \sin e_{\min} \cos e_{\min}) \end{aligned} \quad (5.17)$$

An approximation for small  $e$  is

$$G \approx \frac{\sin \alpha}{\pi} \int_0^{2\pi} d\varphi \cos(\Delta a) (\sin e - \sin e_{\min})$$

This is still not proportional to  $\Omega_{\text{land}}$ , because  $\Delta a$  changes with  $\varphi$ .

## 5.5 Outline of Implementation

The algorithm is separated into two parts.

The first, described in section 5.3, determines the horizons and subtended angles (view factors) of all surface elements with all other surface elements. This information is written to files **horizons.dat** and **fieldofviews.dat**, respectively. This part is easily parallelized, as calculations for each pixel are independent of one another although the entire topography has to be loaded into memory at once. For parallelization, one column or row of the spatial domain is run on each CPU core. It can be submitted to a computer cluster as an array job.

In the **horizons** file each line is preceded by the integer pixel coordinates. The file is rectangular, and the number of entries is (number of azimuth rays + 2) × (number of topographic pixels). The **fieldofviews** file is giant and it is not rectangular. Each line in the output file corresponds to a topographic pixel and at the beginning specifies the number of pixels within field of view. Each visible pixel has then three numbers stored with it: The two integer pixel coordinates and the view factor for this pixel. Non-visible pixels are not stored. When these data are read in later, they are stored as 2-byte integers and 4-byte floating point numbers respectively, half of what is common, to save memory.

Horizons-only calculations are implemented in **shadows.f90** and its subroutines. If, in addition to horizons the field of views are desired, use **fieldofviews.f90** instead, which outputs horizon heights in the same format as **shadows.f90** does, but with a slightly different algorithm.

The second part, described in section 5.4, simulates the time evolution of illumination and surface temperature, using the horizons and (optionally) the field of view as input. The surface energy balance is integrated over time at steps of a fraction (e.g., 1/50th) of a solar day. Surface temperature and illumination are updated at every time step, and thus reflection is taken into account to the order of the number of time steps within a solar day, which is large. The time step is explicit, but the subsurface model, if used, is semi-implicit. The names of the main programs start with `cratersQ_*`.

Overview of current implementations:

Main program	Task	Reflections	Parallelization
<code>shadows</code>	pre-calculate geometry, optional multigrid	no	yes, trivial
<code>fieldofviews</code>	pre-calculate horizons, no multigrid	yes	yes, trivial
<code>cratersQ_snapshot</code>	instantaneous solution for airless body	yes	none
<code>cratersQ_moon</code>	airless bodies	yes	none
<code>cratersQ_earth</code>	Earth orbit with Maunakea atmosphere	yes	none
<code>cratersQ_mars</code>	Mars orbit and atmosphere	no	no, trivial

It was found that OpenMP is incompatible with sharing of private variables within a Fortran module. Hence, any program that uses the module `newhorizons` should not be used with OpenMP.

The current implementations use the following naming convention. The input topography to `horizons.f90` is `name.xyz`, and the output will be `horizons.dat` for the sequential implementation or `horizon.arg` for the parallel implementation, where `arg` is an integer. `cratersQ_*` then expects input files `name.xyz`, `horizons.name`, and optionally `fieldofviews.name`. File names and their associated parameters are specified in module `filemanager`, that the user edits.

used in Schorghofer et al. (2017); Hayne et al. (2018)

## 5.6 3D Insolation with Atmosphere

For bodies with atmosphere, the isotropic sky radiation is approximated by sky view, both for short-wave and long-wave radiation. The size of the sky (between 0 and  $2\pi$  steradian) can be calculated from either the horizon heights or the view factors of the landscape segments. The sky view factor  $F$  is the spherical angle of the visible sky divided by  $2\pi$ . See also Rakovec and Zakšek (2012) for discussion.

For Mars, in the spirit of the Kieffer approximation (subsection 1.2.3),

$$Q_{a,IR} = Q_0 F f_{IR} \sin \beta_{noon}, \quad (5.18)$$

and if the sun is up, then

$$Q_{a,scat} = \frac{1}{2} Q_0 (1 - A) F f_{scat}, \quad (5.19)$$

otherwise  $Q_{a,scat} = 0$ . (For a planar slope  $F = 1 - \alpha/2\pi$ , so this does not match the approximation chosen in section 5.2).

For (high-elevation) regions of Earth (such as Mauna Kea), short-wavelength scattered and short-wavelength absorbed radiation are considered, as described in section 4.1.

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# Part 6

## Surface-bounded Exospheres

Monte-Carlo Model of Ballistically Hopping Molecules

*History:* developed 2012–2017

Core routines are implemented in `montecarlo.f90`

### 6.1 Introduction

The ballistic trajectories of neutral molecules or atoms in a surface-bounded exosphere are simulated with a Monte-Carlo method. Individual water molecules are launched with a probabilistically distributed cartesian velocity components that amount to a random initial azimuth and thermal speed appropriate for the local surface temperature. The model then computes the molecule's impact location and time analytically. An event-driven algorithm is used, where landing and launching events are processed in time-order. Events are scheduled and processed until the molecule is destroyed or lost or until its landing or launch time is beyond the next thermal model time step, when surface temperatures are updated.

Each molecule has a longitude  $p_r[1]$ , latitude  $p_r[2]$ , status  $p_s$  (on surface =0, in-flight =1, lost or cold-trapped < 0), and time to the next event  $p_t$  (until it arrives on surface or until it will leave the surface). Negative status values can be used to diagnostically to distinguish where it is trapped or how it was lost. Surface temperatures are calculated with a 1D thermal model, as in Part 1.

### 6.2 Ballistic Flight on Sphere

$d$  ... flight distance (measured along surface of sphere)

$t$  ... duration of flight

$\tau_{\text{res}}$  ... surface residence time

$\tau_{\text{dissoc}}$  ... photo-destruction time scale

$v_{\text{esc}}$  ... escape speed

$v_1$  ... initial velocity along longitude direction

$v_2$  ... initial velocity along meridian

$v_3$  ... initial vertical velocity component

$az$  ... azimuth

$\Delta\phi$  ... difference in longitude

$\lambda$  ... latitude  
 $M$  ... molar mass  
 $R_{\text{moon}}$  ... radius of body

The ballistic molecule moves on a plane that goes through the center of sphere/body; the ground track is thus part of a great circle.

At launch, each of the three velocity components is picked from a Gaussian distribution, which involves a scaling factor of  $\sqrt{T_{\text{surf}} 8314.5/M}$ . This will lead to a Maxwellian velocity distribution and uniformly distributed launch azimuths. Other probability distributions can be implemented, if desired. For example, an Armand distribution may be appropriate for desorbed molecules.

For constant  $g$ ,

$$t = 2v_3/g \quad (6.1)$$

$$d = \frac{2}{g} v_3 \sqrt{v_1^2 + v_2^2} \quad (6.2)$$

If  $|v| > 0.4v_{\text{esc}}$ , then use non-uniform gravity formulae (Sec. 6.4)

If  $|v| > v_{\text{esc}}$ , then gravitational escape

The landing latitude and longitude ( $\lambda_2$ ,  $\phi_1 + \Delta\phi$ ) are calculated from the starting coordinates ( $\lambda_1$ ,  $\phi_1$ ) with the following equations:

$$\cos(az) = v_2/\sqrt{v_1^2 + v_2^2} \quad (6.3)$$

$$\sin \lambda_2 = \sin(d/R_{\text{moon}}) \cos(\lambda_1) \cos(az) + \sin(\lambda_1) \cos(d/R_{\text{moon}}) \quad (6.4)$$

$$\cos \lambda_2 = \sqrt{1 - \sin^2 \lambda_2} \quad (6.5)$$

$$\cos(\Delta\phi) = \frac{\cos(d/R_{\text{moon}}) \cos(\lambda_1) - \sin(\lambda_1) \sin(d/R_{\text{moon}}) \cos(az)}{\cos \lambda_2} \quad (6.6)$$

*Roundoff issues:* if  $\cos(\Delta\phi) > +1$  then  $\cos(\Delta\phi) = +1$ ; if  $\cos(\Delta\phi) < -1$  then  $\cos(\Delta\phi) = -1$ .

$$p_r(2) = \arcsin(\sin \lambda_2)$$

$$\Delta\phi = \arccos(\cos(\Delta\phi))$$

if  $v_1 < 0$ , then  $\Delta\phi = -\Delta\phi$

$$p_r(1) = p_r(1) + \Delta\phi$$

if  $(\cos \lambda_2 == 0)$  then on pole

$p_r(1)$  is normalized to 0...360°.

$$p_t = p_t + t$$

## 6.3 Other Model Components

### 6.3.1 Photo-destruction

Molecules are lost in-flight by photo-destruction (Table 6.1), at a rate of  $t/(\tau_{\text{dissoc}} R^2)$ , where  $R$  is the distance from the sun, often approximated by the semi-major axis. Require incident flux  $Q > 0$ , since this only occurs on the dayside. A comprehensive compilation of photo-destruction rates can be found in Huebner et al. (1992). A database is maintained at <http://phidrates.space.swri.edu/>.

	$M$	$\tau_{dissoc}$	
H <sub>2</sub> O	18.015	20×3600	Potter and del Duca (1964)
H <sub>2</sub> O		1/12.6e-6	Crovisier (1989), normal sun
H <sub>2</sub> O		1/23.0e-6	Crovisier (1989), active sun
He	4.0026	1.9e7	Killen and Ip (1999)
Ar-40	39.96	3.2e6	Killen and Ip (1999)

Table 6.1: Some pertinent parameters.  $\tau_{dissoc}$  = photodissociation time scale at 1 AU

### 6.3.2 Coriolis effect

The Coriolis effect is incorporated by adding tangential velocities but subtracting the distance the surface has traveled during time of flight.

At launch:

$$v_1 = v_1 - \frac{2\pi R_{\text{moon}}}{\text{siderealDay}} \cos(p_r(2)) \quad (6.7)$$

After landing:

$$p_r(1) = p_r(1) + t/\text{siderealDay} \quad (6.8)$$

The Coriolis effect is negligible on the Moon and on Mercury, but noticeable on Ceres.

### 6.3.3 Event driver

Process events over the time step of the thermal model  $\Delta t_T$ , e.g., one hour

```

if ( $p_t > \Delta t_T$ ) exit
case( $p_s < 0$ ) exit ! not alive
case( $p_s == 0$ ) ! leaving
    hop once, update  $p_t$ 
case( $p_s == 1$ ) ! landing
    if (incoldtrap) then
         $p_t = \infty$ 
        cycle
    endif
    evaluate  $\tau_{\text{res}}(T_{\text{surf}})$ 
     $p_t = p_t + \tau_{\text{res}}$ 

```

After all events within  $\Delta t_T$  are processed, subtract  $\Delta t_T$  from all times: if ( $p_s \geq 0$ )  $p_t = p_t - \Delta t_T$ . (Moving time zero helps avoid truncation errors after a long run.)

### 6.3.4 Residence times

$E$  ... sublimation rate/flux

$\theta$  ... number of H<sub>2</sub>O molecules per area

$\theta_m = 10^{19} \text{ m}^{-2}$  ... areal number density of H<sub>2</sub>O monolayer

$T$  ... local surface temperature

Temperature also sets the residence time of water molecules on the surface, which is negligible on most of the dayside and very long on most of the nightside. Many models use a binary choice, where molecules either immediately hop on the day side or reside indefinitely on the surface on the nightside. This model uses a molecular residence time that depends continuously on temperature instead of a threshold.

For crystalline ice, the average molecular surface residence time only depends on  $T$ , but for adsorbed water it is also a function of the adsorbate density  $\theta$ . The model uses the parametrization  $\tau_{\text{res}} = c\theta_m/E(T)$ , where  $E$  is the sublimation rate of pure ice. For pure ice  $c = 1$ . For example,  $c = 1/400$  is reasonable for 0.1 monolayers (Schorghofer and Aharonson, 2014). The functional form is almost the same as using a vibration frequency multiplied by a Boltzmann factor.

For non-condensable species, e.g. He,  $\tau_{\text{res}} = 0$ .

## 6.4 Non-uniform Gravity

Ballistic travel distance  $d$  and flight duration  $t$  can also be calculated analytically for a radially dependent gravitational acceleration. These equations are not suitable for small launch velocities due to roundoff. This effect is negligible for Mercury and small on the Moon, but necessary for Ceres. Equations are derived from those in Vogel (1966) and Kegerreis et al. (2017).

$a$  ... semi-major axis of ballistic trajectory

$e$  ... eccentricity of ballistic trajectory

$\alpha$  ... zenith angle of launch velocity,  $\alpha = \arctan\left(\sqrt{v_1^2 + v_2^2}/v_3\right)$

Instead of (6.1) and (6.2) use

$$\gamma = (|v|/v_{\text{esc}})^2 \quad (6.9)$$

$$a = \frac{R_{\text{moon}}}{2(1 - \gamma)} \quad (6.10)$$

$$e = \sqrt{1 - 4\gamma(1 - \gamma)\sin^2\alpha} \quad (6.11)$$

$$d = 2R_{\text{moon}} \arccos\left(\frac{1}{e}(1 - 2\gamma\sin^2\alpha)\right) \quad (6.12)$$

$$E_p = 2 \arctan\left(\sqrt{\frac{1+e}{1-e}} \tan \frac{d}{4R_{\text{moon}}}\right) \quad (6.13)$$

$$t = \frac{R_{\text{moon}}}{v_{\text{esc}}} \frac{E_p + e \sin E_p}{(1 - \gamma)^{3/2}} \quad (6.14)$$

*Round-off issues:*

a) If  $e$  is very close to 1 (fast near horizontal launch), then based on Taylor expansion of (6.12) and (6.13)

$$d = 4\gamma R_{\text{moon}} \sin\alpha \quad (6.15)$$

$$E_p = 2 \arctan \sqrt{\frac{\gamma}{1 - \gamma}} \quad (6.16)$$

b) If  $1 - 2\gamma \sin^2 \alpha > e$  (horizontal launch), do something, otherwise  $d = \mathbf{NaN}$

Then use (6.3)–(6.6) as before.

The exosphere model was used in Schorghofer (2014) (uniform gravity) and Schorghofer et al. (2016, 2017b,a) (non-uniform gravity).

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