

Astro 204

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1 Streamlines

- a) The streamline in spherical coordinates are determined by the equation

$$\frac{dr}{v_r} = r \frac{d\theta}{v_\theta} = \frac{dz}{v_z}. \quad (1)$$

For the case $v_r = a$, $v_\theta = b$, $v_z = 0$, the equation of the stream lines becomes

$$\frac{dr}{d\theta} = r \frac{a}{b}, \quad (2)$$

a first order differential equation. The equation has the solution

$$r(\theta) = Ce^{(a/b)\theta}, \quad (3)$$

where C is a constant of integration. This is the form of a logarithmic spiral, which is plotted in fig. 1.

- b) For the case $v_r = ar^2$, $v_\theta = br^2$, $v_z = 0$, the equation of the stream lines remains the same

$$\frac{dr}{d\theta} = r \frac{a}{b}, \quad (4)$$

which is identical to case (a).

c) The change in mass, \dot{M} along a circular shell is

$$\dot{M} = 2\pi r \Sigma v_r \quad (5)$$

Rearranging gives

$$\Sigma = \dot{M} / (2\pi r v_r), \quad (6)$$

which becomes $\Sigma(r) = \dot{M} / (2\pi b r)$ for part (a) and $\Sigma = (\dot{M}) / (2\pi b r^3)$ for part (b).

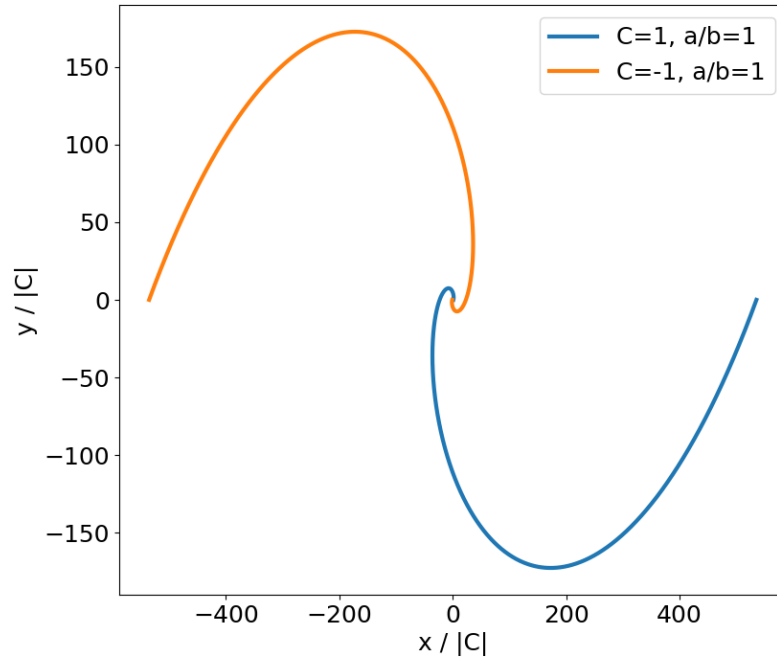


Figure 1: The streamlines for part (a) and part (b)

2 The Energy Equation

Since the no work is being done on the system by external forces $F \cdot \vec{v} = 0$, which can be stated as

$$\frac{\partial E}{\partial t} + \vec{\nabla} \cdot (F_E \vec{v}) = 0 \quad (7)$$

where $F_E = E + P$ and $E = \frac{1}{2}\rho v^2 + \rho\epsilon$. Plugging in yields

$$0 = \frac{1}{2}v^2 \frac{\partial \rho}{\partial t} + \rho \vec{v} \cdot \frac{\partial \vec{v}}{\partial t} + \rho \frac{\partial \epsilon}{\partial t} + \epsilon \frac{\partial \rho}{\partial t} + \frac{1}{2}\rho v^2 \vec{\nabla} \cdot \vec{v} + \vec{v} \cdot \vec{\nabla} \left(\frac{1}{2}\rho v^2 \right) + \rho \epsilon \vec{\nabla} \cdot \vec{v} + \vec{v} \cdot \vec{\nabla} (\rho \epsilon) + P \vec{\nabla} \cdot \vec{v} + \vec{v} \cdot \vec{\nabla} P. \quad (8)$$

Grouping like terms and doing algebra gives

$$\begin{aligned} & \left(\rho \frac{\partial \epsilon}{\partial t} + \rho \vec{v} \cdot \vec{\nabla} \epsilon + P \vec{\nabla} \cdot \vec{v} \right) + \epsilon \left(\vec{v} \cdot \vec{\nabla} \rho + \frac{\partial \rho}{\partial t} + \rho \vec{\nabla} \cdot \vec{v} \right) \\ & + \frac{1}{2}v^2 \left(\frac{\partial \rho}{\partial t} + \rho \vec{\nabla} \cdot \vec{v} + \vec{v} \cdot \vec{\nabla} \rho \right) + \vec{v} \cdot \left(\vec{\nabla} P + \frac{\partial \vec{v}}{\partial t} + \rho \left(\vec{v} \cdot \vec{\nabla} \right) \vec{v} \right), \end{aligned} \quad (9)$$

which can be further simplified by realizing the ϵ and $\frac{1}{2}v^2$ term is 0 by continuity ($\frac{\partial \rho}{\partial t} + \vec{\nabla} \cdot (\rho \vec{v}) = 0$) and the \vec{v} term is 0 by momentum conservation. Therefore,

$$\rho \frac{\partial \epsilon}{\partial t} + \rho \vec{v} \cdot \vec{\nabla} \epsilon + P \vec{\nabla} \cdot \vec{v} = 0 \quad (10)$$

The fundamental equation of thermodynamics is $d\epsilon = Tds + \frac{P}{\rho^2}d\rho$, which can be rewritten as

$$\rho T \frac{ds}{dt} = \rho \frac{d\epsilon}{dt} - \frac{P}{\rho} \frac{d\rho}{dt} \quad (11)$$

Using the chain rule on $\frac{d\epsilon}{dt}$ gives

$$\frac{d\epsilon}{dt} = \frac{\partial \epsilon}{\partial t} + \vec{v} \cdot \vec{\nabla} \epsilon, \quad (12)$$

likewise using the chain rule for $\frac{d\rho}{dt}$ and plugging in the continuity equation gives

$$\frac{d\rho}{dt} = \frac{\partial \rho}{\partial t} + \vec{v} \cdot \vec{\nabla} \rho = -\rho \vec{\nabla} \cdot \vec{v}. \quad (13)$$

Plugging into eq. 11 gives

$$\rho T \frac{ds}{dt} = \rho \frac{\partial \epsilon}{\partial t} + \rho \vec{v} \cdot \vec{\nabla} \epsilon + P \vec{\nabla} \cdot \vec{v} \quad (14)$$

Which when plugged into eq. 10 gives

$$\frac{ds}{dt} = 0 \quad (15)$$

3 Entropy

- a) Starting from the statistical mechanics definition of entropy $\sigma = \log g$, where g is the number of available states and given the distribution of particles per unit volume in 6D phase space $f(\vec{x}, \vec{v}, t)$ we can understand the provided equation (4). Assuming each constant volume element in phase space can hold an equal number of states, the amount of volume occupied by a particle is equal to the number of equivalent states for that particle. Therefore, the number of states per particle can be thought of as f^{-1} and the entropy per particle becomes $\sigma = -\log f$. The total entropy of the system per unit volume at a point in space and time can be calculated by averaging over all velocity states, and weighting by the number of particles per state. Calculating the thermodynamic entropy $S = k\sigma$, and writing the weighted statistical average explicitly gives

$$s = -k \int_{\text{all } \vec{v}} f \ln f d^3v, \quad (16)$$

where s is the entropy per unit volume of the system.

- b) For a maxwellian, $f(\vec{x}, \vec{v}, t) = n f_{\text{Max}}(\vec{v})$ plugging into equation eq. 16 gives

$$S = -4ka^3\pi^{-3/2}n \int_{\mathbb{R}} v^2 e^{-(av)^2} \ln \left[n \left(\frac{a^2}{\pi} \right)^{3/2} e^{-(av)^2} \right] dv \quad (17)$$

where $a = \sqrt{m/(2kT)}$, and I have made the substitution $d^3v = r^2 dr d\theta d\phi$ and integrated over θ and ϕ . Further simplification can be made by making the substitution $u = av$ giving and rewriting in terms of entropy per unit mass

$$s = -4k\pi^{-1/2}m^{-1} \int_{\mathbb{R}} u^2 e^{-u^2} \left[\ln \left(na^3\pi^{-3/2} \right) - u^2 \right] dv. \quad (18)$$

Notice that all pressure / density dependance is in the variable a , since s needs to be calculated to an additive constant, we can drop all terms with no a dependence resulting in

$$s = -4k\pi^{-1/2}m^{-1} \ln(na^3) \int_{\mathbb{R}} u^2 e^{-u^2} dv. \quad (19)$$

where evaluating the integral $\int_{\mathbb{R}} u^2 e^{-u^2} dv = \sqrt{\pi}/2$ gives

$$s = -km^{-1} \ln(na^3) \quad (20)$$

where we can plug the definition of a and $n = \rho/m$ in to get

$$s = -\frac{k}{m} \ln \left(\frac{\rho}{m} \frac{m}{2kT} \right) \quad (21)$$

using the Ideal gas law and dropping all constants gives

$$s = -\frac{k}{m} \ln \left(\rho P^{-3/2} \rho^{3/2} \right) \quad (22)$$

which can be simplified to

$$s = \frac{3k}{2m} \ln \left(P \rho^{-5/3} \right) \quad (23)$$

4 The Lane-Emden Equation for Stellar Structure

a) The condition for hydrostatic equilibrium is

$$\frac{1}{\rho} \frac{dP}{dr} = -G \frac{M}{r^2} \quad (24)$$

where M is the enclosed mass, which satisfies the differential equation

$$\frac{dM}{dr} = 4\pi r^2 \rho. \quad (25)$$

To use plug eq. 25 into eq. 24 we must take the derivative of both sides of eq. 24

$$\frac{d}{dr} \left(\frac{r^2}{\rho} \frac{dP}{dr} \right) = -G \frac{dM}{dr} = -4\pi G r^2 \rho. \quad (26)$$

Since $P = K \rho^\gamma$

$$\frac{d}{dr} \left(\frac{r^2}{\rho} \frac{dP}{dr} \right) = \frac{d}{dr} \left(r^2 K \gamma \rho^{\gamma-2} \frac{d\rho}{dr} \right) = K \frac{\gamma}{\gamma-1} \frac{d}{dr} \left(r^2 \frac{d\rho^{\gamma-1}}{dr} \right), \quad (27)$$

Upon substituting $\gamma = 1 + \frac{1}{n}$, $\xi = r/a$ and $\theta = (\rho/\rho_c)$ eq. 24 becomes

$$\frac{1}{a^2} K(n+1) \rho^{1/n} \frac{d}{d\xi} \left(\xi^2 \frac{d\theta}{d\xi} \right) = 4\pi G \xi^2 \theta^n \rho_c \quad (28)$$

which is equivalent to

$$\frac{d}{d\xi} \left(\xi^2 \frac{d\theta}{d\xi} \right) = \theta^n \left(a^2 \frac{4\pi G}{K} \xi^2 \rho_c^{1-1/n} \right) \quad (29)$$

which can be simplified to

$$\frac{d}{d\xi} \left(\xi^2 \frac{d\theta}{d\xi} \right) = \theta^n \quad (30)$$

upon substitution of $a^2 = (n+1)K\rho_c^{1/(n-1)}(4\pi G)^{-1}$

- b) See fig. 2 and code provided in problem4.py. As the polytropic index increases the density profile becomes less concentrated.
- c) The ideal gas law is $PV = nkT/\mu$ so $kT/\mu = K\rho^{1/n}$. The OOM estimate then is good if a $GM/r \approx KT/\mu = K\rho^{1/n}$. A good estimate from our numerical models is that the density reaches zero at $\xi = 3a$. We can plug this in $GM/R = GM/3a$ and numerically integrate M. We can also estimate M if assume $M \approx 4/3\pi a^3 \rho$ and get $GM/3a \approx Ga^2\rho$. How well our estimate does, will depend on the value of K.

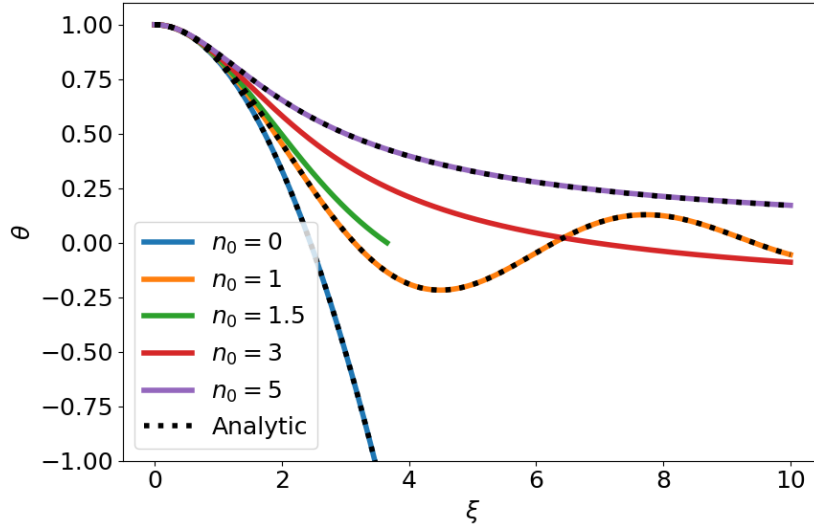


Figure 2: The numerical solutions for part (b). Negative solutions are unphysical.