CFD Code Development Frameworks Python, C, OpenFOAM, Fenics

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Incompressible Navier-Stokes Equations (INSE) in Eulerian form:

$$\partial_t \rho + \rho \nabla \cdot \mathbf{u} = 0 \tag{1}$$

$$\partial_t \mathbf{u} + \mathbf{u} \cdot \nabla \mathbf{u} = -\frac{1}{\rho} \nabla p + \nu \nabla^2 \mathbf{u} + \mathbf{g}$$
 (2)

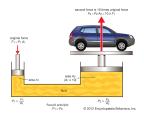
Egn. 1: Density can be omitted, but let's keep it for now. Eqn. 2:

- LHS is acceleration which is intrinsically Lagrangian and when it is translated to Eulerian coordinates it becomes non-linear
- RHS describes influence of pressure gradient, viscosity and body forces.

Complexities

Difficulties for numerical solution:

- Nonlocality of pressure gradient (Solution: None)
- Nonlinearity of acceleration term (Solution: e.g. Picard's Method)
- Pressure and velocity are coupled and there is no separate equation for pressure (Solution: e.g. SIMPLE, PISO and ACM)



Artificial Compressibility Method

ACM first was developed by A.J. Chorin in 1967 and assumes a small compressibility for the fluid and isothermal condition for the flow:

$$\rho = \rho(p) :: \partial_t \rho = \frac{\partial \rho}{\partial p} \frac{\partial p}{\partial t} = \frac{1}{c^2} \frac{\partial p}{\partial t}$$

where c is artificial sound speed. So INSE becomes:

$$\partial_t P + c^2 \nabla . \mathbf{u} = 0$$
$$\partial_t \mathbf{u} + \mathbf{u} . \nabla \mathbf{u} = -\nabla P + \nu \nabla^2 \mathbf{u} + \mathbf{g}$$

where
$$P = \frac{p}{\rho}$$
.

Remarks on ACM

- Limited scope of applicability: incompressible steady state problems.
- Small time step: t is pseudo-time step and depends on c. Therefore, if an explicit discretization method is used time step should have a small value.
- Efficient parallelization: no elliptic PDE

Although applicability of the method is very limited, ACM provides a simple yet informative framework for pedagogical purposes



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Pseudo Code

- Initialization of the domain and the variables (u, v, p)
- 2 While convergence is reached do:
 - 1 Solve momentum equation in x-direction to get u
 - Solve momentum equation in y-direction to get v
 - Update the boundary conditions for u and v
 - Solve continuity equation to get *P*
 - 5 Check convergence criteria
- 3 Output the fields data

Boundary Conditions

The two common boundary conditions can be formulated as follows:

- Dirichlet: $\phi_g = 2\phi_b \phi_i$
- Neumann: $\phi_g = \phi_i \left(\Delta n \frac{\partial \phi}{\partial n}\right)_h$

Indicies: g, b and i denote a ghost, boundary and inner node, respectively

Variables: ϕ is a quantity of interest (u, v or P) and n represents a direction normal to the boundary cell face

Convergence Criteria

$$\blacksquare E_u = \sqrt{(\Delta t \Delta x \Delta y) \sum_{i,j} (u_{i,j}^{n+1} - u_{i,j}^n)^2}$$

$$E_{v} = \sqrt{(\Delta t \Delta x \Delta y) \sum_{i,j} (v_{i,j}^{n+1} - v_{i,j}^{n})^{2}}$$

3
$$E_p = \sqrt{\frac{\Delta t \Delta x \Delta y}{c^2} \sum_{i,j} (P_{i,j}^{n+1} - P_{i,j}^n)^2}$$

$$E_{\nabla} = (\Delta t \Delta x \Delta y) \nabla . \mathbf{u}$$

5
$$E_{total} = \max\{E_u, E_v, E_p, E_{\nabla}\} < \varepsilon$$

where ε is the desired tolerance.

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1 Governing Equations

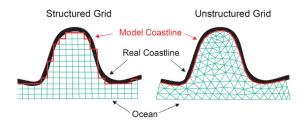
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Grid

Structured vs. Unstructured

- Structured: regular connectivities, high quality and memory efficient
- Unstructured: irregular connectivities, highly automated and handles complex geometries



Chen, C., R.C. Beardsley, and G. Cowles. 2006. An unstructured grid, finite-volume coastal ocean model (FVCOM) system. Oceanography 19(1):78-89, https://doi.org/10.5670/oceanog.2006.92.

Grid

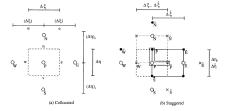
Staggered vs. Collocated

Collocated: all the variables at the node centers; easier to implement and extend while issues such as checkerboard problem arise

Grid

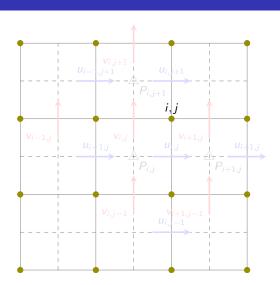
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Staggered: scalar variables at the node centers and vector variables at the face centers; more accurate though more difficult to implement

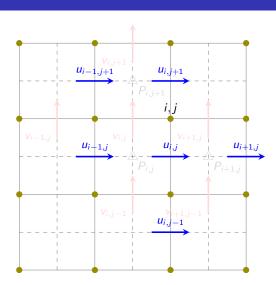


Meier, H. F., Alves, J. J. N., & Mori, M. (1999). Comparison between staggered and collocated grids in the finite-volume method performance for single and multi-phase flows. Computers & Chemical Engineering

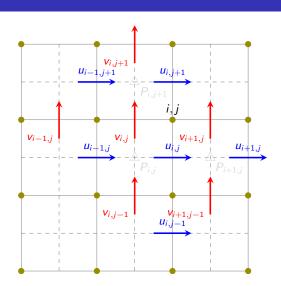
Grid Staggered Grid



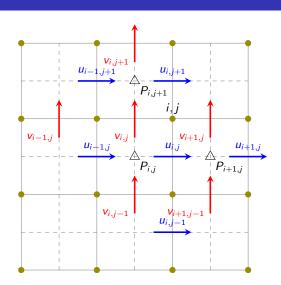
Staggered Grid



Staggered Grid



Staggered Grid



Discretization

Spatial: central difference, second order

$$\partial_{\mathsf{x}}\phi = \frac{\phi_{i+1} - \phi_{i-1}}{2\Delta\mathsf{x}}$$

Grid

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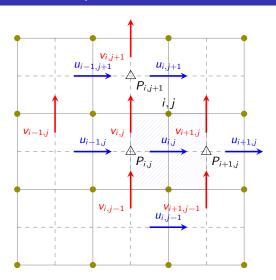
Temporal: backward difference, first order

$$\partial_t \phi = \frac{\phi^{n+1} - \phi^n}{\Delta t}$$

Note: for brevity we use the superscript n + 1 to denote the variable in the current time step and no superscript for the previous time step.

Let's discretize the equations based on a staggered grid node numbering.

Control Volume for Momentum Equation in x-direction



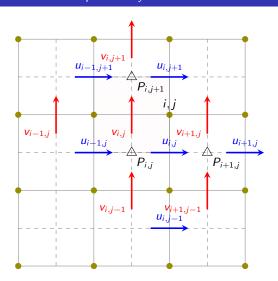
Momentum Equation in x-direction

$$\begin{split} \partial_{t}u + \partial_{x}(uu) + \partial_{y}(uv) &= -\partial_{x}P + \nu\left(\partial_{xx}u + \partial_{yy}u\right) \\ \frac{u_{i,j}^{n+1} - u_{i,j}}{\Delta t} + \frac{\left(\frac{u_{i+1,j} + u_{i,j}}{2}\right)^{2} - \left(\frac{u_{i,j} + u_{i-1,j}}{2}\right)^{2}}{\Delta x} \\ &+ \frac{\left(\frac{u_{i,j+1} + u_{i,j}}{2}\right)\left(\frac{v_{i+1,j} + v_{i,j}}{2}\right) - \left(\frac{u_{i,j} + u_{i,j-1}}{2}\right)\left(\frac{v_{i+1,j-1} + v_{i,j-1}}{2}\right)}{\Delta y} \\ &= \\ &- \frac{P_{i+1,j} - P_{i,j}}{\Delta x} \\ &+ \nu\left(\frac{u_{i+1,j} - 2u_{i,j} + u_{i-1,j}}{\Delta x^{2}} + \frac{u_{i,j+1} - 2u_{i,j} + u_{i,j-1}}{\Delta y^{2}}\right) \end{split}$$

Grid

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Control Volume for Momentum Equation in y-direction



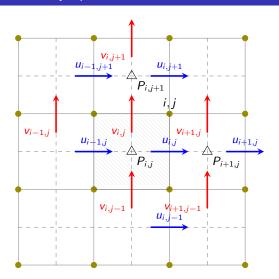
Momentum Equation in *y*-direction

$$\begin{split} \partial_{t}v + \partial_{x}(uv) + \partial_{y}(vv) &= -\partial_{y}P + \nu\left(\partial_{xx}v + \partial_{yy}v\right) \\ \frac{v_{i,j}^{n+1} - v_{i,j}}{\Delta t} + \frac{\left(\frac{u_{i,j+1} + u_{i,j}}{2}\right)\left(\frac{v_{i+1,j} + v_{i,j}}{2}\right) - \left(\frac{u_{i-1,j+1} + u_{i-1,j}}{2}\right)\left(\frac{v_{i,j} + v_{i-1,j}}{2}\right)}{\Delta x} \\ + \frac{\left(\frac{v_{i,j+1} + v_{i,j}}{2}\right)^{2} - \left(\frac{v_{i,j} + v_{i,j-1}}{2}\right)^{2}}{\Delta y} \\ &= \\ - \frac{P_{i,j+1} - P_{i,j}}{\Delta y} \\ + \nu\left(\frac{v_{i+1,j} - 2v_{i,j} + v_{i-1,j}}{\Delta x^{2}} + \frac{v_{i,j+1} - 2v_{i,j} + v_{i,j-1}}{\Delta y^{2}}\right) \end{split}$$

Grid

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Control Volume for Continuity Equation



Continuity Equation

$$\frac{P_{i,j}^{n+1} - P_{i,j}}{\Delta t} + c^2 \left(\frac{u_{i,j}^n - u_{i-1,j}^n}{\Delta x} + \frac{v_{i,j}^n - v_{i,j-1}^n}{\Delta y} \right) = 0$$

 $\partial_t P + c^2 (\partial_x u + \partial_y v) = 0$

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1 Governing Equations

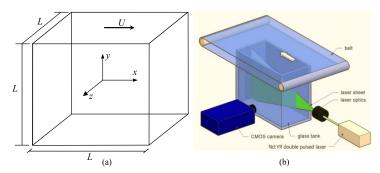
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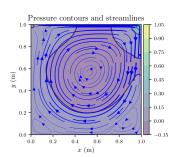
Problem Statement

Lid-Driven Cavity

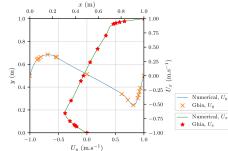
- Characteristics: steady-state, incompressible
- Boundary Conditions: walls everywhere (top wall is moving)
 - Velocity: Dirichlet ($\mathbf{U}_x = \mathbf{U}_v = 0$ except for the top wall where $\mathbf{U}_{x}=1$ and $\mathbf{U}_{v}=0$)
 - Pressure: Neumann ($\nabla p = 0$)



Problem Statement Outputs



Velocity profile along the middle of axes for Re=1000



Problem Statement

Workshop

A numerical solution to this benchmark problem will be presented based on:

- (Finite Difference) Coding from scratch: Python, C
- (Finite Volume) Modifying one of the solvers in OpenFOAM
- (Finite Element) Using libraries provided by FEniCS



Final Remarks

Some other interesting open source CFD projects to look into:

■ Basilisk: solution of partial differential equations on adaptive Cartesian meshes. (C)

http://basilisk.fr

 FluidDyn: some Python packages specialized for different tasks, in particular for 2D and 3D Fast Fourier Transforms, numerical simulations, laboratory experiments and processing of images of fluid.

https://fluiddyn.readthedocs.io/en/latest

■ **Firedrake**: an automated system for the solution of partial differential equations using the finite element method. (Python)

https://firedrakeproject.org

Let's Get Started!

```
$ mkdir UHWS
$ cd UHWS
$ git clone https://github.com/taataam/UHOFWorkshop.git
$ cd UHOFWorkshop/workshop3
```