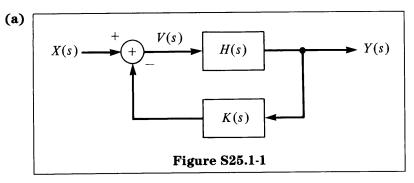
# 25 Feedback

### Solutions to Recommended Problems

S25.1



We have

$$V(s) = X(s) - Y(s)K(s)$$
 (S25.1-1)

and

$$Y(s) = V(s)H(s)$$
 (S25.1-2)

From eq. (S25.1-2),

$$V(s) = \frac{Y(s)}{H(s)} \tag{S25.1-3}$$

Substituting eq. (S25.1-3) into eq. (S25.1-1), we have

$$\frac{Y(s)}{H(s)} = X(s) - Y(s)K(s),$$

$$Y(s)[1 + H(s)K(s)] = H(s)X(s),$$

$$\frac{Y(s)}{X(s)} = \frac{H(s)}{1 + H(s)K(s)}$$

Similarly,

$$\frac{Y(z)}{X(z)} = \frac{H(z)}{1 + H(z)K(z)}$$

**(b)** 
$$Q(s) = \frac{H(s)}{1 + KH(s)}, \qquad Q(z) = \frac{H(z)}{1 + KH(z)}$$

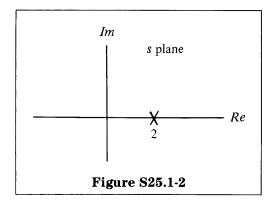
For 
$$H(s) = 2/(s-2)$$
 and  $H(z) = 2/(z-2)$ ,

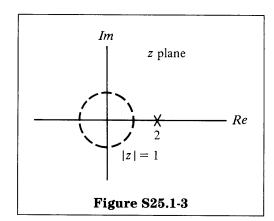
$$Q(s) = \frac{2}{(s-2) + 2K} = \frac{2}{s - 2(1 - K)}$$
$$Q(z) = \frac{2}{(z-2) + 2K} = \frac{2}{z - 2(1 - K)}$$

For K = 0,

$$Q(s) = \frac{2}{s-2}$$
 and  $Q(z) = \frac{2}{z-2}$ ,

as shown in Figures S25.1-2 and S25.1-3, respectively.

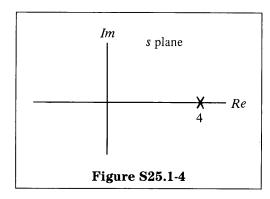


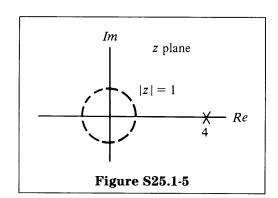


For K = -1,

$$Q(s) = \frac{2}{s-4} \quad \text{and} \quad Q(z) = \frac{2}{z-4},$$

as shown in Figures S25.1-4 and S25.1-5, respectively.

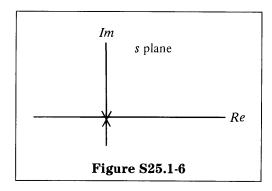


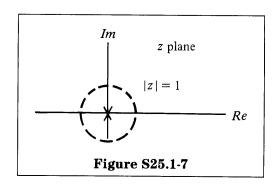


For K = 1,

$$Q(s) = \frac{2}{s}$$
 and  $Q(z) = \frac{2}{z}$ ,

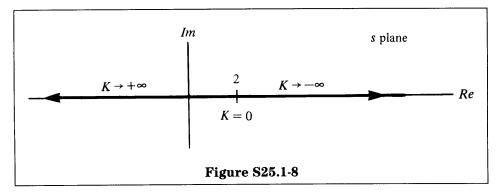
as shown in Figures S25.1-6 and S25.1-7, respectively.





(c) 
$$Q(s) = \frac{2}{s - 2(1 - K)}$$

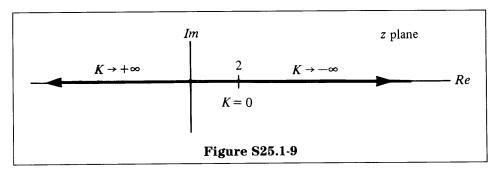
The pole is located at s = 2(1 - K), as shown in Figure S25.1-8.



Hence, the locus of the pole is the line  $Re\{s\} = 0$ . Similarly, for

$$Q(z)=\frac{2}{z-2(1-K)},$$

the locus of the pole is also the line  $Re\{z\} = 0$ , shown in Figure S25.1-9.



The root location decreases as K moves to infinity and increases as K moves to negative infinity.

(d) 
$$Q(s) = \frac{2}{s - 2(1 - K)}$$

The system is stable for 2(1 - K) < 0, or K > 1.

$$Q(z) = \frac{2}{z - 2(1 - K)}$$

The system is stable for -1 < 2(1 - K) < 1, or  $\frac{1}{2} < K < \frac{3}{2}$ .

### S25.2

We use Problem P25.1.

(a) (i) 
$$\frac{Y(s)}{X(s)} = \frac{H(s)}{1 + G(s)H(s)}$$
(ii) 
$$E(s) = X(s) - R(s)$$

$$= X(s) - Y(s)G(s)$$

$$= X(s) - E(s)H(s)G(s),$$

$$E(s)[1 + H(s)G(s)] = X(s),$$

$$\frac{E(s)}{X(s)} = \frac{1}{1 + H(s)G(s)}$$

(iii) 
$$\frac{Y(s)}{E(s)} = H(s)$$

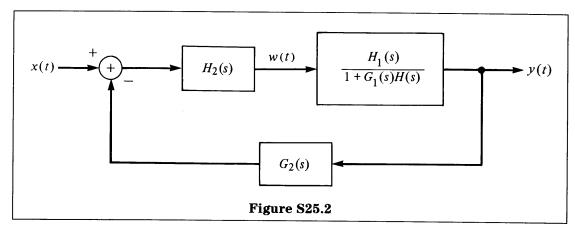
(iv) 
$$\frac{Y(s)}{R(s)} = \frac{1}{G(s)}$$

(b) 
$$W(z) = X(z) \frac{H_1(z)}{1 + G(z)H_1(z)},$$
  
 $Y(z) = W(z) + X(z)H_0(z),$   
 $Y(z) = \frac{X(z)H_1(z)}{1 + G(z)H_1(z)} + X(z)H_0(z)$ 

Thus,

$$\frac{Y(z)}{X(z)} = \frac{H_1(z)}{1 + G(z)H_1(z)} + H_0(z)$$

(c) 
$$\frac{Y(s)}{W(s)} = \frac{H_1(s)}{1 + G_1(s)H(s)}$$
, as shown in Figure S25.2.

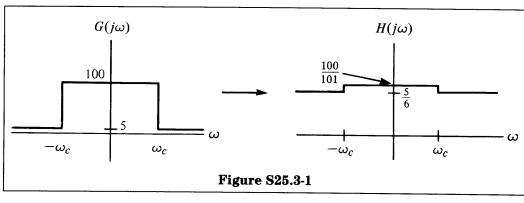


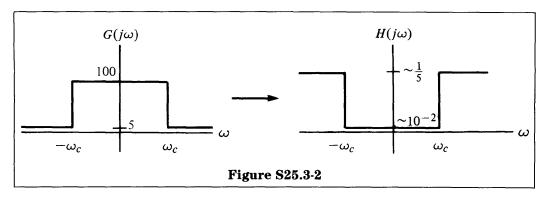
$$\frac{Y(s)}{X(s)} = \frac{\frac{H_1(s)H_2(s)}{1 + G_1(s)H_1(s)}}{1 + \frac{G_2(s)H_1(s)H_2(s)}{1 + G_1(s)H_1(s)}}$$

$$= \frac{H_1(s)H_2(s)}{1 + G_1(s)H_1(s) + G_2(s)H_1(s)H_2(s)}$$

S25.3

(a)



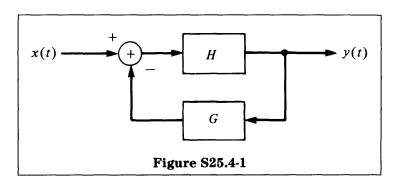


**(b)** From the frequency response in part (a), clearly system 1 tends to make the response more constant and system 2 tends to resemble the inverse of  $G(j\omega)$ .

#### S25.4

For the system in Figure S25.4-1, we denote the closed-loop system function by

$$V = \frac{H}{1 + GH}$$



(a) 
$$V(s) = \frac{\frac{1}{(s+1)(s+3)}}{1 + \frac{1}{(s+1)(s+3)}} = \frac{1}{(s+1)(s+3) + 1}$$
$$= \frac{1}{s^2 + 4s + 4} = \frac{1}{(s+2)^2}$$

Therefore,

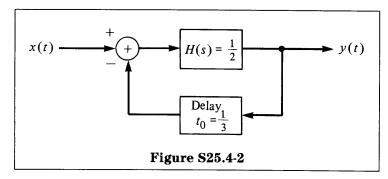
$$v(t) = te^{-2t}u(t)$$

**(b)** 
$$V(s) = \frac{\frac{1}{s+3}}{1 + \left(\frac{1}{s+3}\right)(s+1)} = \frac{1}{(s+3) + (s+1)}$$
$$= \frac{1}{2s+4} = \frac{1}{2} \frac{1}{s+2}$$

In this case,

$$v(t) = \frac{1}{2}e^{-2t}u(t)$$

(c) The system function  $G(s) = e^{-s/3}$  corresponds to a delay of  $\frac{1}{3}$ , i.e., the feedback system of Figure P25.4(a) becomes that shown in Figure S25.4-2.



We can now recursively obtain the impulse response by inspection. With  $x(t) = \delta(t)$ ,

$$y(t) = \frac{1}{2}\delta(t) - \frac{1}{2}\left[\frac{1}{2}\delta(t - \frac{1}{3})\right] + \frac{1}{2}\left[\frac{1}{4}\delta(t - \frac{2}{3})\right] - \cdots$$
$$= \frac{1}{2}\sum_{n=0}^{\infty} \left(-\frac{1}{2}\right)^{n} \delta\left(t - \frac{n}{3}\right)$$

$$(d) V(z) = \frac{\frac{z^{-1}}{1 - \frac{1}{2}z^{-1}}}{1 + \left(\frac{z^{-1}}{1 - \frac{1}{2}z^{-1}}\right)\left(\frac{2}{3} - \frac{1}{6}z^{-1}\right)}$$

$$= \frac{z^{-1}}{(1 - \frac{1}{2}z^{-1}) + (\frac{2}{3}z^{-1} - \frac{1}{6}z^{-2})}$$

$$= \frac{z^{-1}}{1 + \frac{1}{6}z^{-1} - \frac{1}{6}z^{-2}}$$

$$= \frac{z^{-1}}{(1 - \frac{1}{3}z^{-1})(1 + \frac{1}{2}z^{-1})}$$

$$= \frac{\frac{6}{5}}{1 - \frac{1}{3}z^{-1}} - \frac{\frac{6}{5}}{1 + \frac{1}{2}z^{-1}}$$

Therefore,

$$v[n] = \frac{6[(\frac{1}{3})^n u[n] - (-\frac{1}{2})^n u[n]]}{1 + H(z)G(z)} = \frac{\frac{2}{3} - \frac{1}{6}z^{-1}}{1 + (\frac{2}{3} - \frac{1}{6}z^{-1})(\frac{z^{-1}}{1 - \frac{1}{2}z^{-1}})}$$

$$= \frac{(\frac{2}{3} - \frac{1}{6}z^{-1})(1 - \frac{1}{2}z^{-1})}{(1 - \frac{1}{2}z^{-1}) + (\frac{2}{3} - \frac{1}{6}z^{-1})z^{-1}}$$

$$= \frac{\frac{2}{3} - \frac{2}{3}z^{-1} + \frac{1}{12}z^{-2}}{1 + \frac{1}{6}z^{-1} - \frac{1}{6}z^{-2}}$$

Thus,

$$v[n] = \frac{2}{3}\tilde{v}[n+1] - \frac{2}{3}\tilde{v}[n] + \frac{1}{12}\tilde{v}[n-1].$$

where  $\tilde{v}[n]$  is v[n] in part (d).

## Solutions to Optional Problems

S25.5

$$y(t) = K_2 w(t) + K_1 K_2 v(t)$$
 (S25.5-1)

By taking the transform of eq. (S25.5-1), we have

$$Y(s) = K_2 W(s) + K_1 K_2 V(s)$$

Also

$$V(s) = X(s) + \frac{s}{s + \alpha} Y(s)$$

Therefore,

$$Y(s) = K_2W(s) + K_1K_2\left[X(s) + \frac{s}{s+\alpha}Y(s)\right],$$

$$Y(s)\left(1 - \frac{K_1K_2s}{s+\alpha}\right) = K_2W(s) + K_1K_2X(s),$$

and

$$Y(s) = \frac{K_2W(s) + K_1K_2X(s)}{1 - \frac{K_1K_2s}{s + \alpha}}$$
$$= \frac{(s + \alpha)[K_2W(s) + K_1K_2X(s)]}{(1 - K_1K_2)s + \alpha}$$

S25.6

(a) The system function of the system given in Figure P25.6 must be determined first. So we write down the difference equation

$$y[n] = x[n] + y[n-1] + 4y[n-2]$$

Taking the z-transform of the equation, we have

$$Y(z)(1-z^{-1}-4z^{-2})=X(z), \quad \text{or} \quad H(z)=\frac{Y(z)}{X(z)}=\frac{1}{1-z^{-1}-4z^{-2}}$$

The poles of this system are located at

$$z^2 - z - 4 = 0$$
, or  $z = \frac{1}{2} \pm \frac{\sqrt{17}}{2}$ 

Since |z| > 1 for at least one pole the system is unstable.

(b) With closed-loop feedback, the difference equation is

$$y[n] = x_e[n] - Ky[n-1] + y[n-1] + 4y[n-2]$$

Thus,

$$H(z) = \frac{z^2}{z^2 + (K-1)z - 4}$$

The poles are now located at

$$z = \frac{-(K-1) \pm \sqrt{(K-1)^2 + 16}}{2}$$

Note that the roots are purely real because the term inside the square root is always positive. For z = 1,

$$1 + \frac{K}{2} - \frac{1}{2} = \pm \frac{\sqrt{(K-1)^2 + 16}}{2},$$
  

$$K + 1 = \pm \sqrt{(K-1)^2 + 16}$$

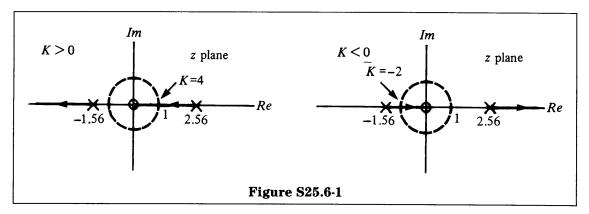
Thus,

$$K^{2} + 2K + 1 = K^{2} - 2K + 17,$$
  
 $4K = 16,$  or  $K = 4$ 

We can also calculate  $z_2$ :

$$z_2 = -4$$

Similarly,  $z_1 = -1$ ,  $z_2 = 4$  for K = -2. Observe the root locus in Figure S25.6-1.



Observe that if one of the poles is inside  $|z| \le 1$ , the other is outside. Hence, the system is unstable for all values of K.

(c) The difference equation can be written as

$$y[n] = x_e[n] + y[n-1] + (4-K)y[n-2]$$

Therefore,

$$H(z) = \frac{z^2}{z^2 - z + (K - 4)}$$

In this case, the poles are located at

$$z = \frac{1}{2} \pm \frac{\sqrt{17 - 4K}}{2}$$

For a stable system, we want

$$|z| < 1,$$

$$|z| = \left| \frac{1}{2} \pm \frac{\sqrt{17 - 4K}}{2} \right|$$

If we set 17 - 4K > 0, then

$$\left|\frac{1}{2}\pm\frac{\sqrt{17-4K}}{2}\right|<1,$$

or

$$\pm \frac{\sqrt{17-4K}}{2} < \frac{1}{2},$$

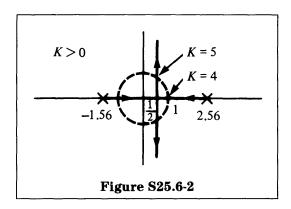
$$17-4K < 1,$$

$$K > 4$$

Now suppose 17 - 4K < 0. Then

$$\left| \frac{1}{2} \pm j \sqrt{|\frac{17}{4} - K|} \right| < 1$$
 or  $\frac{17}{4} - K > -\frac{3}{4},$   $-K > -\frac{20}{4},$   $K < 5$ 

Thus, for K in the range 4 < K < 5, we have a stable system. The root locus is shown in Figure S25.6-2.



#### S25.7

- (a) The dc gain of the amplifier is |H(0)| = |G|.
- **(b)**  $h(t) = Gae^{-at}u(t)$ . Therefore, the time constant is 1/a.

(c) 
$$|H(j\omega_c)|^2 = \frac{G^2a^2}{a^2 + \omega_c^2} = \frac{1}{2}G^2$$

Thus  $\omega_c = \pm a$ . Hence the bandwidth is a.

(d) The closed-loop transfer function is

$$V(s) = \frac{\frac{Ga}{s+a}}{1 + \frac{KGa}{s+a}} = \frac{Ga}{(1 + KG)a + s}$$

From part (a), the time constant is

$$\frac{1}{(1+KG)a}$$

From part (c), the bandwidth is (1 + KG)a. From part (a), the dc gain is

$$\left| \frac{G}{1 + KG} \right|$$

(e) We require (GK + 1)a = 2a. Hence, K = 1/G. So the bandwidth becomes 2a. The time constant is 1/(2a), and |H(0)| = |G/2|, the dc gain.

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