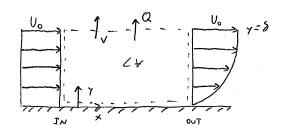
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Problem: An ion compressible fluid flows past an impermeable flat plate

MAE 104 10-16-07

biven:



 $7 = \frac{7}{8}$ $V_2 = V_0 \left(\frac{37 - 7^3}{2} \right)$

Find: Volume Flow Q across surface

Assume: Steady flow 1/3+ = 0 Incompressible 2p = 0 2D flow w=0, 40z=0

Analysis

$$\iint_{CS_{2N}} U_1 \hat{\gamma}(-\hat{i}) dA_1 + \iint_{CS_{0N}} U_2 \hat{i}(\hat{i}) dA_2 + \iint_{CS_{0N}} V_{\hat{i}}(\hat{j}) dA_3 = 0$$

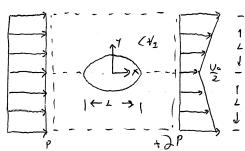
$$Q_{007} = \iint_{CS_{2}} U_{2} dA_{2} - \iint_{CS_{2}} \overline{U}_{2} dA_{2} = \iint_{0}^{n=1} b\delta U_{0} d^{n} - \iint_{0}^{n=1} b\delta U_{0} \left(\frac{3n-2}{2}\right) d^{n}$$

$$= b\delta U_{0}(1) - b\delta U_{0} \frac{1}{2} \left(\frac{3}{2}n^{2} - \frac{1}{4}n^{4}\right) \Big|_{0}^{n=1}$$

$$= b\delta U_{0} - \frac{1}{2}b\delta U_{0} \left(\frac{3}{2} - \frac{1}{4}\right) = b\delta U_{0} \left[1 - \frac{1}{2} \left(\frac{6}{4} - \frac{1}{4}\right)\right]$$

$$= 680_{\circ} \left[1 - \frac{1}{2} \left(\frac{5}{9} \right) \right] = 680_{\circ} \left[2 - \frac{5}{8} \right) \right] = \frac{3}{8} 680_{\circ} + 3$$

biven :



Find: Drug Force on cylinder

(D = 2 f/g Vo bL

need steady-flow community

Assume: Incompressible flow dp=0 Steedy flow Yst=0 Inviscid flow m=0

Analysis:

 $V_2 = \frac{V_0}{2} + \frac{V_0 \gamma}{2L}$

Conservation of Linear Momentum for helf CY

(42 3+ BV-VAY + G GOV. JS). V = - 4 PJS + 1 FT JY + FIZZERUS + FDRAG

$$\iint_{CS_2} \vec{V}_1 \cdot \vec{V}_2 d\vec{s}_1 + \iint_{CS_2} \vec{V}_2 \cdot \vec{V}_2 ds_2 = \frac{1}{2} F_{ORAG}$$

$$\frac{1}{2} F_{0} \hat{i} = \int_{0}^{L} \rho b' U_{0} \hat{i} \cdot U_{0} \hat{i} \cdot (-\hat{i}) dy + \int_{0}^{L} \rho b \left(\frac{U_{0}}{2} + \frac{U_{0}y}{2L}\right) \hat{i} \left(\frac{U_{0}}{2} + \frac{U_{0}y}{2L}\right) \hat{i}$$

$$= -\rho b U_{0}^{2} L \hat{i} + \rho b \left[\frac{U_{0}^{2}}{4l} + \frac{U_{0}^{2}y^{2}}{4lL} + \frac{U_{0}^{2}y^{3}}{l2L^{2}}\right]_{0}^{L}$$

$$= -\rho b U_{0}^{2} L \hat{i} + \rho b V_{0}^{2} L \left(\frac{7}{12}\right) \hat{i}$$

$$C_{p} = \frac{2F}{\rho V_{0}^{2} b L} \qquad C_{b}' = \frac{2F'}{\rho V_{0}^{2} L}$$

$$L_p' = \frac{2(10645, 33)^{1/2}}{(498 h \times 10^3)(4 m/s)^{2}(0.8 m)} = \frac{5}{3}$$
 4) contris

Problem: An idealized Incompressible flow has a velocity $\nabla = 4xy^2 \hat{\gamma} + f(y)\hat{\gamma} - 2y^2\hat{h}$

Given: V= 4xy21+f(4)) - zy2h

Find toy, that satisfies the continuity equation

Analysis

Incompressible, steady state

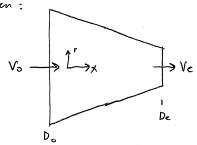
$$\frac{44y^{2} + \frac{\partial y}{\partial y} + (-y^{2}) = 0}{5y^{2} + \frac{\partial y}{\partial y}} = -3y^{2} + (-y^{2}) = 0$$

$$\frac{\partial y}{\partial y} = -3y^{2} + (-y^{2}) = -y^{3} + C$$

$$\frac{1}{\sqrt{2}} = \frac{1}{\sqrt{2}} + \frac{1}{\sqrt{2}$$

Problem: Air flows under steady ~ 1D conditions through a conical no zele

Given:



a ~ 340 m/s

Find: Minimum Delp for which we can safely neglect compressibility effects it Vo = 10 mg 6) Vo= 30 m/s

Lompressibility pertinent at M≥ 0,3 Uniform flow profile in v Assume: Steady flow

Analysis:

$$\frac{1}{4} \int_{0}^{2} V \cdot d\vec{s} = 0 \implies - \left| V_{o} AA_{i} + \right| V_{e} dA_{e} = 0$$

$$\frac{1}{4} \int_{0}^{2} V_{o} = \frac{1}{4} \int_{e^{2}}^{2} V_{e} \qquad V_{e} = \left(\frac{D_{o}}{D_{e}} \right)^{2} V_{o}$$

$$V_{c} Max = 102 m_{s}$$

$$V_{d} V_{d} V_{d} V_{d}$$

$$V_{d} V_{d} V_{d} V_{d}$$

a)
$$\frac{102 \text{ m/s}}{10 \text{ m/s}} \stackrel{\text{41}}{=} \left(\frac{D_0}{D_c}\right)^2 \text{ Vo}$$

$$\frac{102 \text{ m/s}}{10 \text{ m/s}} \stackrel{\text{2}}{=} \left(\frac{D_0}{D_c}\right)^2 \qquad \frac{D_0}{D_c} \stackrel{\text{2}}{=} 3.194 \text{ J}$$

$$\frac{102 \text{ m/s}}{100 \text{ J}} \stackrel{\text{2}}{=} \left(\frac{D_0}{D_c}\right)^2 \qquad \frac{D_0}{D_c} \stackrel{\text{2}}{=} 3.194 \text{ J}$$

b)
$$\frac{102 \text{ m/s}}{30 \text{ m/s}} \ge \left(\frac{D_o}{D_e}\right)^2$$
 $\frac{D_o}{D_e} \le 1.841 \text{ d}$

Problem: A viscous fluid falls due to gravity between two pletes

Find: Velocity profile

Assume: Steady, in compressible \$t=2p=0

slip condition with we-h)=0

No flow in xyy directions, No pressure gradients

Analysis

$$\frac{\partial^2 w}{\partial x^2} = -\frac{\rho}{2\pi}g \quad w = -\frac{\rho}{2\pi}g \quad x^2 + \zeta_1 x + \zeta_2$$

$$\frac{\partial w}{\partial x}(0) = 0 \qquad \frac{-P_3}{2} \times + C_1 = 0 \Rightarrow C_1 = 0$$

$$W(x) = (2 - \frac{1}{2} p_3 x^2)$$

$$w(h) = 0 = (2 - \frac{1}{2} f g h^2)$$
 $(2 = \frac{1}{2} f g h^2)$

$$W(x) = \frac{1}{2} \int_{0}^{2} h^{2} - \frac{1}{2} \int_{0}^{2} x^{2} = \frac{1}{2} \int_{0}^{2} (h^{2} - x^{2})$$

$$W(x) = \frac{psh^2}{2m} \left(1 - \left(\frac{x}{h} \right)^2 \right)$$

Problem: Consider a relocity field where
$$U = \frac{C \times /(x^2 + y^2)}{y^2}$$
, $V = \frac{C y}{(x^2 + y^2)}$ $C = constant$

Given:
$$\vec{V} = \frac{(x)^2}{x^2+y^2} + \frac{(y)}{x^2+y^2}$$

Assume: Incompressible

Analysis:

$$\omega \quad E_1 \quad 2.32 \qquad \nabla \cdot \vec{V} = \frac{1}{4} \quad \frac{D4}{Dt}$$

$$\nabla - \vec{v} = \frac{2}{3x} u + \frac{3}{3y} v$$

$$= \frac{(x^2 + y^2)c - cx(2x)}{(x^2 + y^2)^2} + \frac{(x^2 + y^2)c - cy(2y)}{(x^2 + y^2)^2}$$

$$= \frac{2((x^2 + y^2)^2 - 2x^2c - 2y^2c}{(x^2 + y^2)^2}$$

$$\frac{1}{1} \frac{D}{D} = 0$$

$$(x^2 + y^2)^2$$

b)
$$\vec{\xi} = \nabla \times \vec{V} = \begin{vmatrix} \hat{j} & \hat{j} & \hat{k} \\ \frac{1}{2} \times \hat{j} & \frac{3}{2} & \frac{3}{2} \\ 0 & V & V \end{vmatrix} = (3\hat{k} - 3\hat{V})\hat{i} + (3\hat{k} + 3\hat{k})\hat{i} + (3\hat{V} - 3\hat{V})\hat{k}$$

$$= \left[\frac{(x^2 + y^2)0 - cy(2x)}{(x^2 + y^2)^2} - \frac{(x^2 + y^2)^2}{(x^2 + y^2)^2} \right] \hat{k} = 0$$

Problem: Consider a relocity field where the radial and tansential components of the velocity are $V_{r} = 0$

Find: Is the flow field irrotational?

Assume: Flow is cylindrical

Analysis

$$\nabla \times \vec{V} = \left(\frac{1}{r} \frac{\partial \vec{V}_e}{\partial \theta} - \frac{\partial \vec{V}_{\theta}}{\partial z}\right) \hat{r} + \left(\frac{\partial \vec{V}_{\theta}}{\partial z} - \frac{\partial \vec{V}_{z}}{\partial r}\right) \hat{\theta} + \frac{1}{r} \left(\frac{\partial (rV_{\theta})}{\partial r} - \frac{\partial \vec{V}_{r}}{\partial \theta}\right) \hat{k}$$

$$\nabla \times \vec{V} = \frac{1}{r} \left(\frac{\partial}{\partial r} (c_{r}^{2})\right) = \frac{1}{r} \left(2c_{r}\right) = 2c$$

$$\nabla \times \vec{V} = \frac{1}{r \sin \theta} \left(\frac{\partial}{\partial \theta} \left(\vec{V}_{\theta} \sin \theta \right) - \frac{\partial \vec{V}_{\theta}}{\partial \theta} \right) \hat{\vec{v}} + \frac{1}{r} \left(\frac{1}{\sin \theta} \frac{\partial \vec{V}_{r}}{\partial \theta} - \frac{\partial}{\partial r} \left(r \vec{V}_{\theta} \right) \right) \hat{\theta}$$

$$+ \frac{1}{r} \left(\frac{\partial}{\partial r} \left(r \vec{V}_{\theta} \right) - \frac{\partial}{\partial \theta} \right) \hat{G}$$

4/4

$$\nabla \times \vec{V} = \frac{1}{r} \frac{\partial}{\partial r} \left(Cr^2 \right) = 2c$$

$$\nabla \times \vec{V} = 2c$$