

Today's Lecture

- Wrapping up polyphase and multi-rate signal processing
- FIR filter design
- Linear phase filters

Announcements

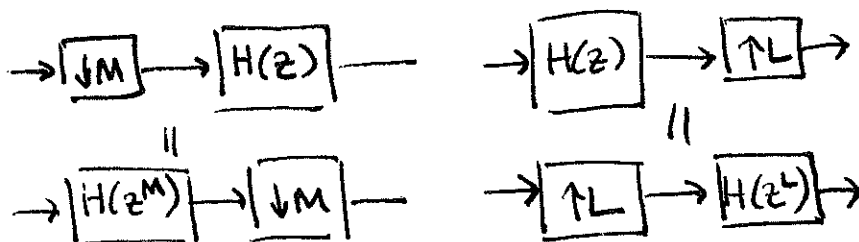
Midterm 2 11/16 on Webex

Why?

- Polyphase decomposition:
- Downsampled signal has fewer coefficients
 - Processing cost is reduced.
 - Think about Radix-2 DFT (even and odd components)
 - Original system N -tap, each of $e_i[n]$ is N/M tap

Block diagram / chaining: - Via chaining we can get rid of the delay elements z^m and z^{-m}

Equivalent systems:



Recall:
$$h[n] = h_0[n] + h_1[n-1] + \dots + h_{M-1}[n-M+1]$$

$$e_k[n] = h_k[nM] = h[nM+k] \quad \text{'polyphase components'}$$

Frequency domain

$$H(z) = \sum_{k=-\infty}^{+\infty} h[k] z^{-k}$$

$$= \sum_{l=-\infty}^{+\infty} h[lM] z^{-lM} + \sum_{l=-\infty}^{+\infty} h[lM+1] z^{-(lM+1)} + \dots$$

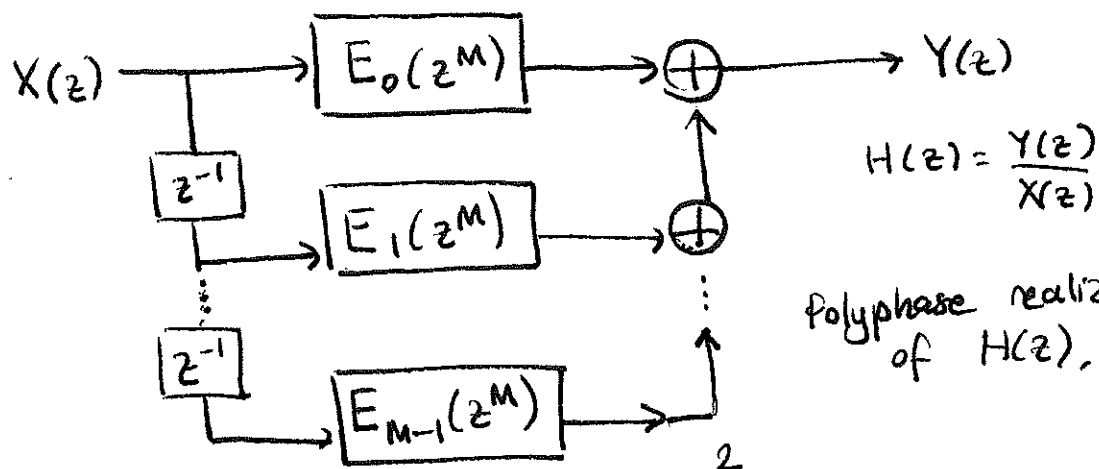
$$+ \sum_{l=-\infty}^{+\infty} h[lM+M-1] z^{-(lM+M-1)}$$

$$= \sum_{k=0}^{M-1} \sum_{l=-\infty}^{+\infty} h[lM+k] z^{-(lM+k)}$$

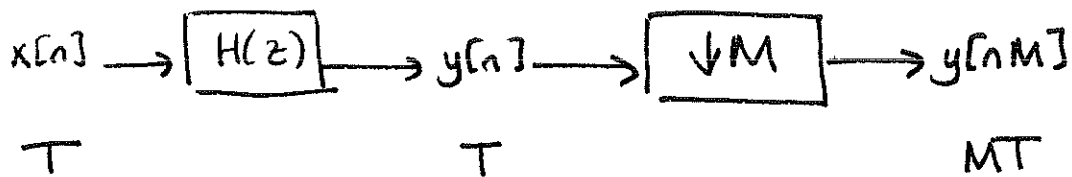
$$= \sum_{k=0}^{M-1} z^{-k} \underbrace{\sum_{l=-\infty}^{+\infty} h[lM+k] z^{-lM}}_{e_k[l]}$$

$$= \sum_{k=0}^{M-1} z^{-k} E_k(z^M) \quad \text{where } E_k(z) \text{ is the } z\text{-transform of } e_k[n].$$

Using this we can establish a connection between the z -transform of $h[n]$ and the z -transform of its polyphase components.

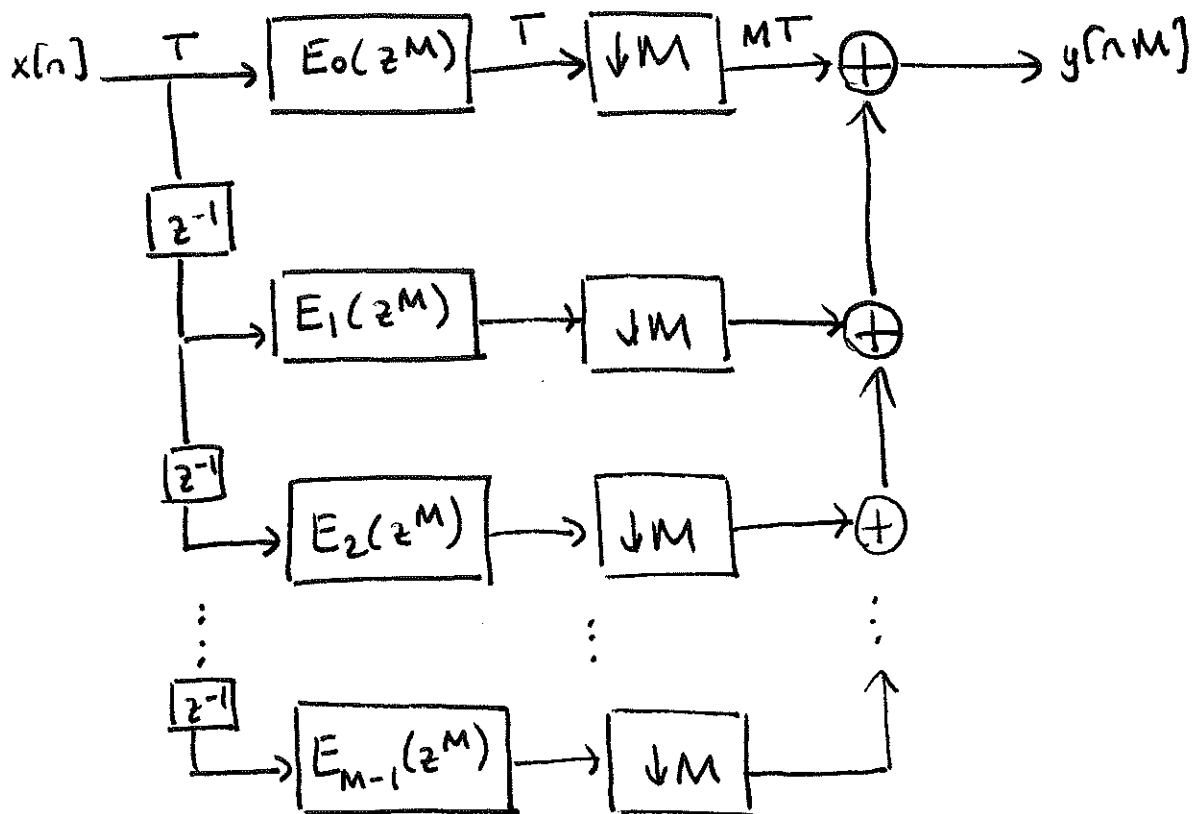


Polyphase Implementation of Decimation / Interpolation Filters

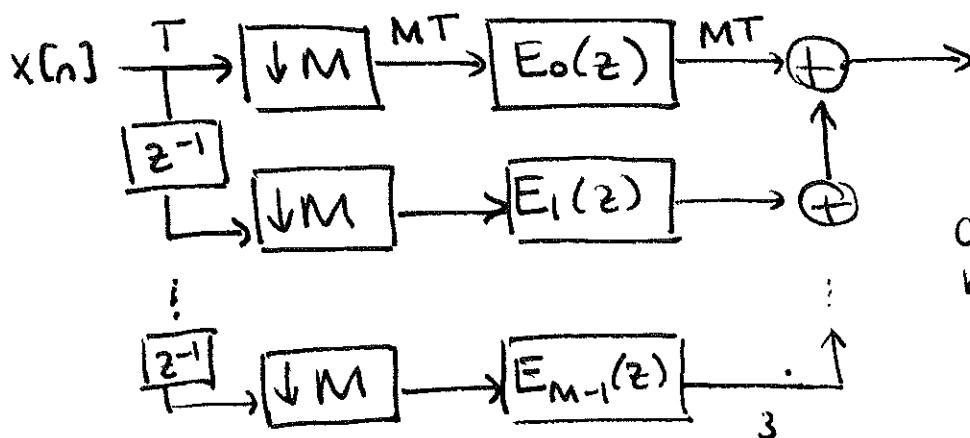


We generate and discard $\frac{M-1}{M}$ fraction of data.

Polyphase representation



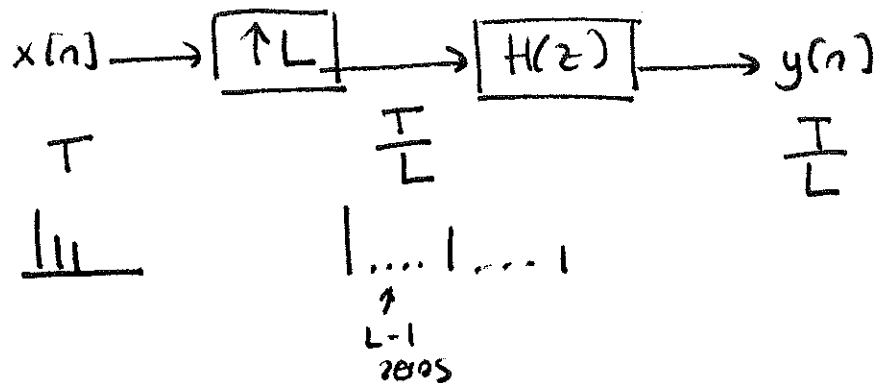
A more efficient equivalent system: (sampling frequency reduced by a factor of M)



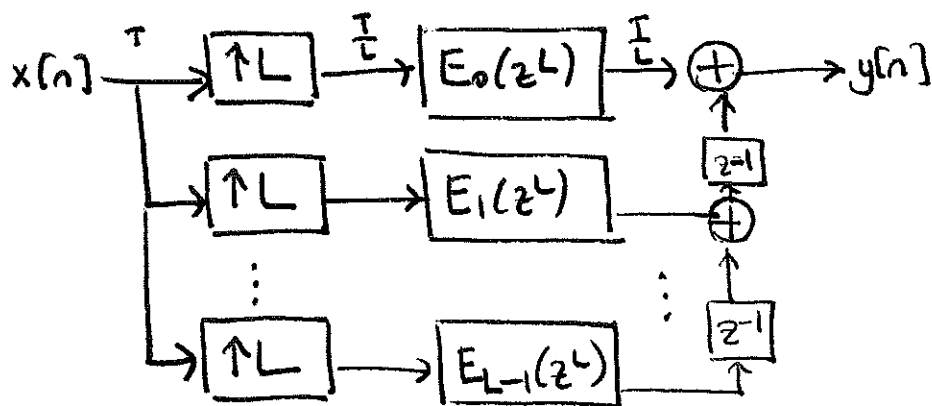
Computational savings by filtering at a low sampling rate.

If the original system was an N -tap filter, each of $e_i[n]$ is an N/M tap filter.

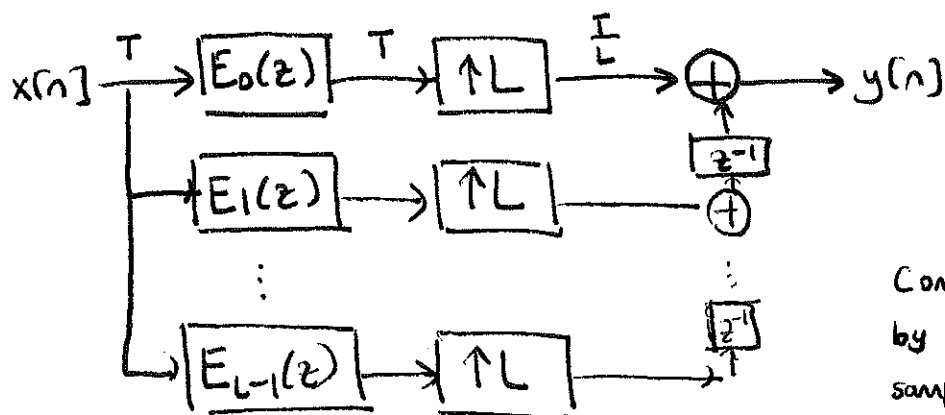
If the original realization was N multiplications per unit time
 polyphase " N/M " "



We generate data and $\frac{L-1}{L}$ fraction of values are 0.



Using the second identity, flip the upsampler and the filters.

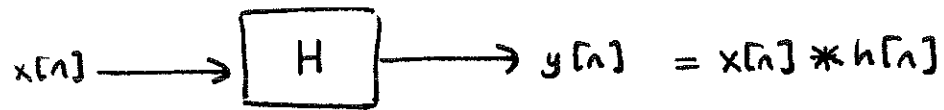


No zeros are explicitly filtered.

Computational savings
 by filtering at a low
 sampling rate.

Filter Design

LTI system



$$Y(\omega) = X(\omega) H(\omega)$$

Magnitude $|Y(\omega)| = |X(\omega)| |H(\omega)|$

Phase $\angle Y(\omega) = \angle X(\omega) + \angle H(\omega)$

$$Y(\omega) = |Y(\omega)| e^{j\angle Y(\omega)}$$

Low Pass Filters

LPF

- sampling rate changes
- aliasing
- reconstruction (interpolation)

Band Pass Filters

BPF

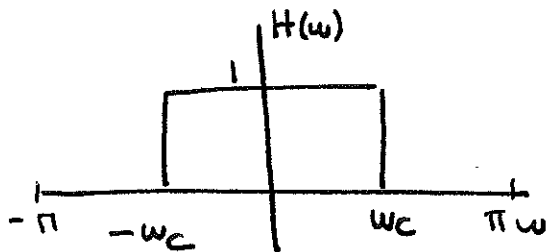
- wireless transmitters / receivers (to prevent interference)

High Pass Filters

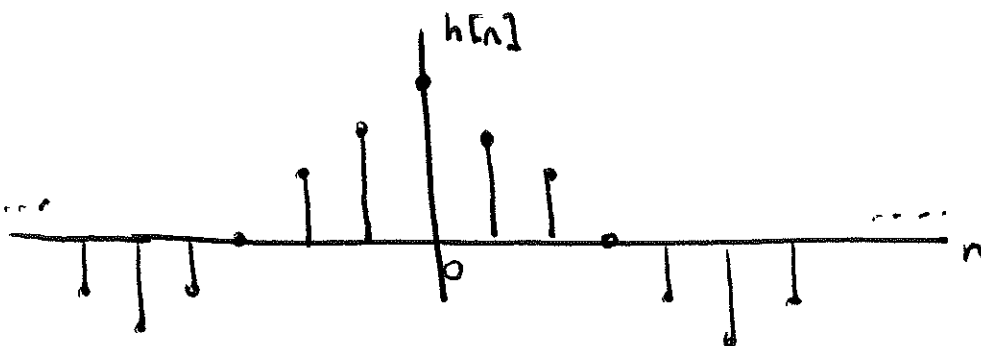
HPF

- cancelling low frequency noise
- audio amplifiers to boost volume.

Ideal low pass filter



$$H(\omega) = \begin{cases} 1, & \omega \leq |\omega_c| \\ 0 & \omega_c < \omega \leq \pi \end{cases}$$



$$h[n] = \frac{\sin \omega_c n}{\pi n}, \quad -\infty \leq n \leq \infty$$

CONS: infinite length impulse response (not practical)
non-causal ($h[n] \neq 0$ for $n < 0$)

Goal: Approximate $h[n]$:

- Finite impulse response (FIR)
- Causal

Ideal LPF has no phase shift (phases of input are not altered)

Ideal delay: $h_d[n] = \delta[n - n_d]$, $n_d > 0$

$$H_d(\omega) = e^{-j\omega n_d}, \quad -\pi \leq \omega \leq \pi$$

$$\Rightarrow |H_d(\omega)| = 1 \quad \text{and} \quad \angle H_d(\omega) = -\omega n_d, \quad -\pi \leq \omega \leq \pi$$

$\underbrace{\hspace{10em}}$
Phase is linear in ω

* We can tolerate linear distortion because each component of the input is moved in the same number of units.

As a result, we desire filters with linear phase:

$$H(\omega) = \begin{cases} e^{-j\omega n_d} & , \quad |\omega| < \omega_c \\ 0 & , \quad \omega_c \leq |\omega| \leq \pi \end{cases}$$

$$|H(\omega)| = \begin{cases} 1 & , \quad |\omega| < \omega_c \\ 0 & , \quad \omega_c \leq |\omega| \leq \pi \end{cases}, \quad \angle H(\omega) = -\omega n_d, \quad \omega \in [-\pi, \pi]$$

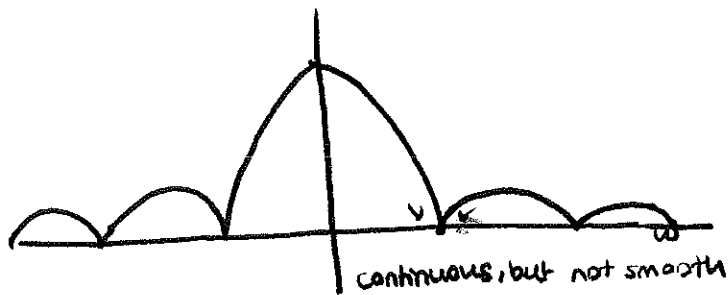
$$h[n] = \frac{\sin(\omega_c(n - n_d))}{\pi(n - n_d)}, \quad -\infty < n < \infty$$

This is a LPF

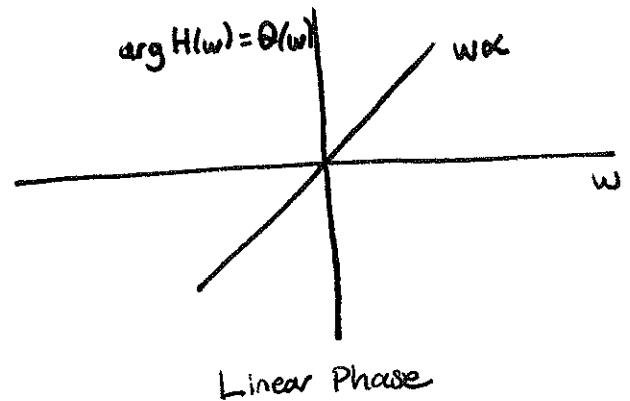
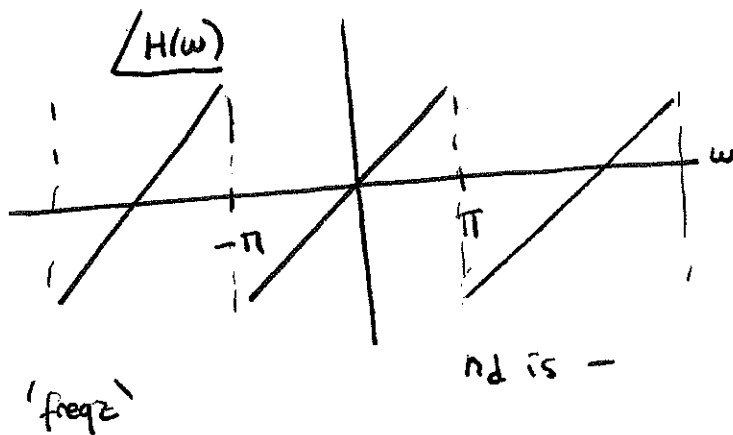
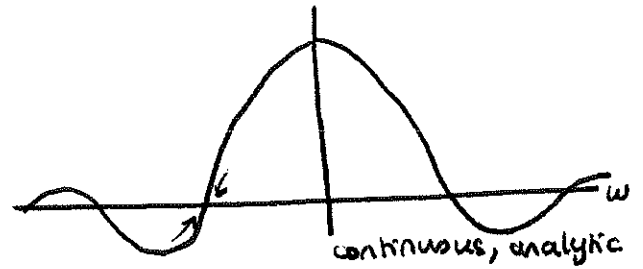
output is delayed by n_d units.

It is still not causal.

Arbitrary
 $|H(\omega)|$, magnitude response

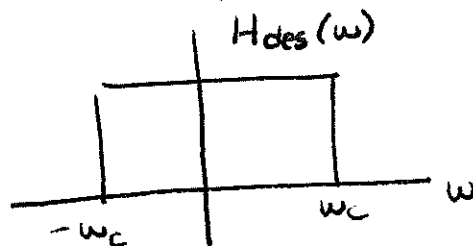


$A(\omega) = \pm |H(\omega)|$,
 Amplitude response



Filter Design Process

1. Start with desired frequency response



2. Choose a class of filters, e.g., length-N finite-impulse response (FIR) filter

3. Choose a measure of quality to approximate how close the design is to the desired performance

e.g., least-squares approximation

Chebyshev approximation

Taylor series approximation

4. Apply an algorithm to find the best realization of the filter.

We want real, causal and digital filters of the form

$$H(z) = \frac{b_0 + b_1 z^{-1} + b_2 z^{-2} + \dots + b_M z^{-M}}{1 + a_1 z^{-1} + a_2 z^{-2} + \dots + a_N z^{-N}} = \frac{Y(z)}{X(z)}$$

✓ If $a_1 = a_2 = \dots = a_N = 0 \Rightarrow$ FIR filter (output only depends on input)
otherwise \Rightarrow IIR filter (infinite impulse response) where output also depends on the previous outputs

We have the following approximation problem:

$$\min_{a, b} \|E(z)\| = \|H_{\text{des}}(z) - H(z)\|$$

\downarrow
error
 \downarrow
we design!

where $\|\cdot\|$ denotes the norm, e.g. absolute value $\|x\| = |x|$ or the Euclidean norm $\|x\|$ of vector $x = (x_1, \dots, x_n)$: $\|x\|_2 = \sqrt{x_1^2 + x_2^2 + \dots + x_n^2}$.

Linear Phase Filters

$h[n]$ is a length N filter (FIR) and assume that it has a linear phase: $\theta(\omega) = K_1 + K_2 \omega$.

$$H(\omega) = \sum_{n=0}^{N-1} h[n] e^{-j\omega n}$$

$$= e^{-j\omega M} \sum_{n=0}^{N-1} h[n] e^{-j\omega n} \cdot e^{j\omega M} \quad \text{where } M = \frac{N-1}{2}$$

$$= e^{-j\omega M} \sum_{n=0}^{N-1} h[n] e^{j\omega(M-n)}$$

Next we observe that

$$\text{If } n=0 \quad h[0]e^{j\omega M}$$

$$n=N-1 \quad h[N-1]e^{j\omega(M-N+1)} = h[N-1]e^{-j\omega M} \quad (\text{recall } M = \frac{N-1}{2})$$

$$n=1 \quad h[1]e^{j\omega(M-1)}$$

$$n=N-2 \quad h[N-2]e^{j\omega(M-N+2)} = h[N-2]e^{-j\omega(M-1)}$$

\vdots

We can rewrite $H(\omega)$ as

$$H(\omega) = e^{-j\omega M} \left((h[0] + h[N-1])\cos \omega M + j(h[0] - h[N-1])\sin \omega M \right. \\ + \\ (h[1] + h[N-2])\cos \omega(M-1) + j(h[1] - h[N-2])\sin \omega(M-1) \\ + \\ \left. \vdots \right)$$

If we have even symmetry, $h[n] = h[N-n-1] = h[2M-n]$, then all the sin terms will drop away:

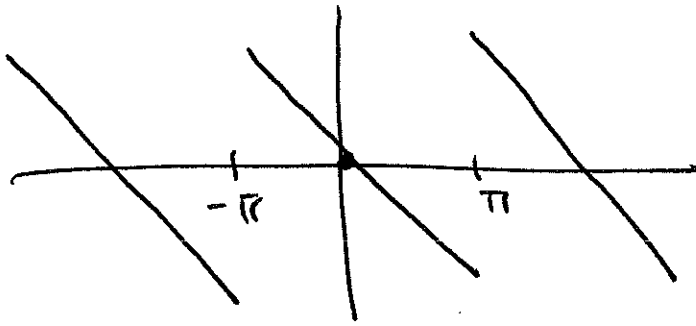
$$H(\omega) = e^{-j\omega M} \left((h[0] + h[N-1])\cos \omega M + (h[1] + h[N-2])\cos \omega(M-1) \right. \\ \left. + \dots \right)$$

Amplitude response:

$$A(\omega) = \sum_{n=0}^{M-1} 2h[n]\cos(\omega(M-n)) + h[M] \quad \text{if } N \text{ is odd}$$

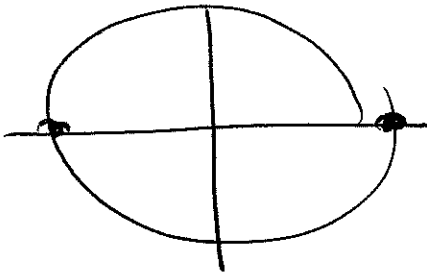
$$= \sum_{n=1}^M 2h[M-n]\cos(\omega n) + h[M] \quad \text{'Type I } N \text{ Odd'}$$

change of variables $n \rightarrow M-n$

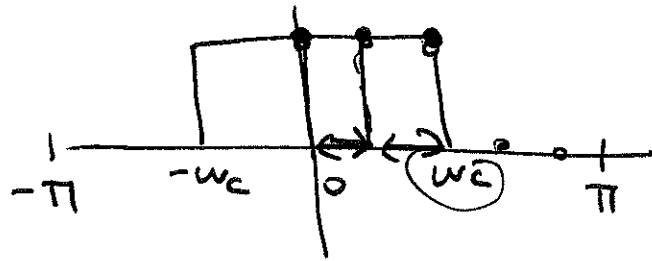


$$H(\omega) = |H(\omega)| e^{j \angle H(\omega)}$$

~~$H(\omega)$~~



$$H(\omega) = +1 e^{j \cdot 0} \rightarrow H(\omega) = -1 = 1 \cdot e^{j\pi}$$



N coefficient