Today's lecture

- Linear phase filles
- Different fille design techniques
 - 1. Frequency sampling
 - 2. Least-square approximation
 - 3. Chebyshev approximation

Linear Phase Filles

h(n): length N FIR has linear phase $\theta(w) = k_1 + k_2 w$

$$H(\omega) = e^{-j\omega M} \sum_{n=0}^{N-1} h[n]e^{j\omega(M-n)}$$
 where $M = \frac{N-1}{2}$

Rewning this we can show that

Now assume that we have even symmetry, i.e., h(N-n-1)=h(2M-n) = h(n)

Then all the sine terms will drop away:

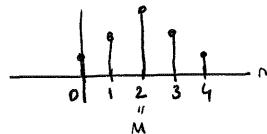
Amplimede response:

$$A(\omega) = \sum_{n=0}^{M-1} 2hE_n \cos(\omega (M-n)) + hEM$$
 if N is ODD

$$(n+M-n) = \sum_{n=1}^{M} 2h[M-n] cos(wn) + h[M]$$
 (Type I N ODD)

Example

$$N=5$$
, $h(h)=h(h-n)$, $M=\frac{N-1}{2}=2$



Other Types:

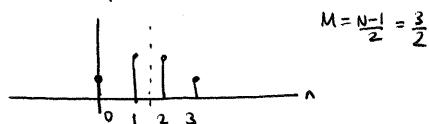
$$A(w) = \sum_{n=0}^{N/2-1} 2 h [n] \cos(w (M-n))$$

$$(n-1\frac{N}{2}-n) = \sum_{n=1}^{N/2} 2h\left[\frac{N}{2}-n\right]\cos\left(w\left(n-\frac{1}{2}\right)\right)$$

change of variobles $n \rightarrow N/2-n$

Type II N EVEN

Example



Recall that $\Theta(\omega) = K_1 + K_2 \omega$ and let $K_1 = \frac{\pi}{2}$

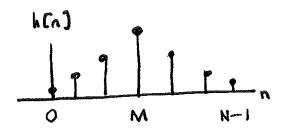
h(n) = -h(N-n-1) (odd symmetry)

$$A(w) = \sum_{n=0}^{M-1} 2h(n) \sin(w(m-n))$$
 Type III N ODD'

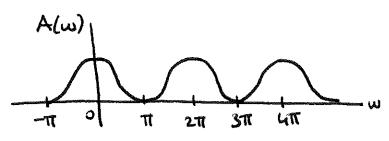
$$A(w) = \sum_{n=0}^{N/2-1} 2h(n) \sin(w(M-n))$$
 Type IV N EVEN!
$$= \sum_{n=1}^{N/2} 2h[\frac{N}{2}-n] \sin(w(n-\frac{1}{2}))$$
 2

4 possible types that give linear phase.

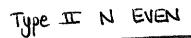
Type I N ODD

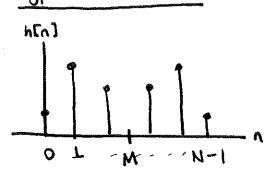


Has odd length Even gymnetric about M



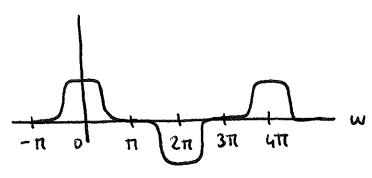
Even about w=0, TT
Periodic with 2TT
Law pass characteristics





Has even leight Even symmetric about $M = \frac{N-1}{2}$

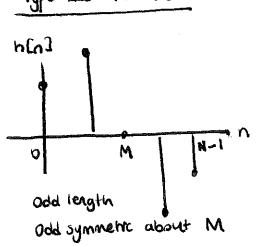




Even about w=0 Odd about w=TT Periodic with 4TT

Note: DTFT H(w) is always 2Tl periodic. A(w) is a continuous, real valued, smooth function based on both H(w) and LH(w): A(w) = I(H(w))

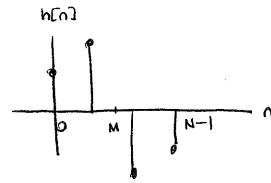
Type III N ODD

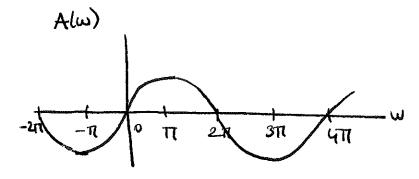


A(w)
-11 0 11 211 311 411

odd about w=0, TT Periodic with 2TT

Type IN N EVEN





Even leight odd symmetric about $M = \frac{N-1}{2}$

Odd about w=0

Even about w=TT

Periodic with 4TT

hotes

- · Types III, IV have A(0)=0 => bad for LPF
- . Types II, III have A(IT)=0 => bad for HPF
- o Type III is good for BPF.

Zero Locatrons for Linear Phase FIR Filters

$$H(z) = \sum_{n=0}^{N-1} h(n) z^{-n}$$

$$= 2^{-(N-1)} \left(h[0] 2^{N-1} + h[1] 2^{N-2} + \dots + h[N-1] \right)$$

1. If h[n] is real, then if $H(z)=0 \Rightarrow H(z^{+})=0$

Why?
$$H(z^*) = (z^*)^{-(N-1)} (hco)(z^*)^{N-1} + hco)(z^*)^{N-2} + \dots + hco-1)$$

$$(h(n) real) = (z^*)^{-(N-1)} (h^*(0)(z^*)^{N-1} + h^*(1)(z^*)^{N-2} + \dots + h^*(N-1))$$

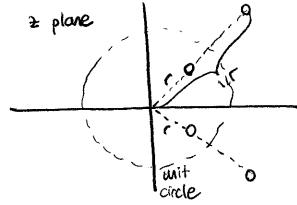
$$= (H(z))^* = 0$$

2. If
$$h(n) = \pm h(n-1-n)$$
 where $+$ for Types II-II , $-$ for Types III-III , then if $H(2)=0 \Rightarrow H(\frac{1}{2})=0$

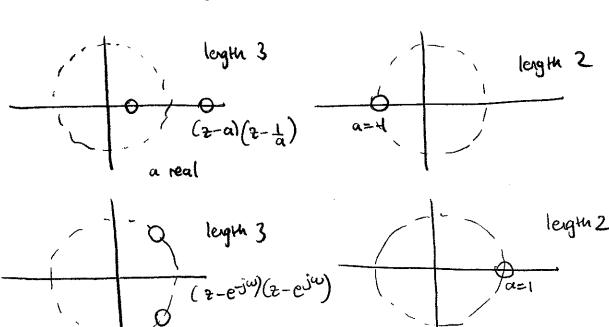
Why?
$$H(\frac{1}{2}) = z^{N-1} (n(0) z^{-(N-1)} + h(1) z^{-(N-2)} + \dots + h(N-1))$$

 $= \pm z^{N-1} (h(N-1) z^{-(N-1)} + h(N-2) z^{-(N-2)} + \dots + h(N-1))$
 $= \pm z^{N-1} [H(z) = 0]$

The zeros of linear phase, real FIR filters look like:

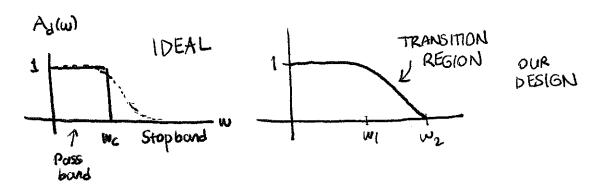


legth 5 filter,



* We could decompose or cascade these decompositions.

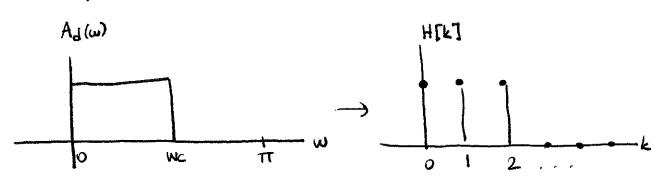
Different FIR Design Techniques



Different approximations

- Least-squares (LS): to minimize the average or squared error in frequency domain.
- Chebyshev approximation: to minimize the maximum error over cetain regions of frequency response.
- Butterworth: Taylor series approximation to desired response.

1. Frequency Sampling Design



Assume that we take N equally spaced samples in the frequency domain at

$$\frac{2TK}{N}$$
, $k=0,...,N-1$

The invese DFT

$$h(n) = \frac{1}{N} \sum_{k=0}^{N-1} H(k) e^{j2\pi k n}$$
, $n=0,...,N-1$

We have N equations and N unknowns => We can solve this.

Nlog N operations to implement DFT. (using FFT algorithm)

Now assume that head is real, linear phase.

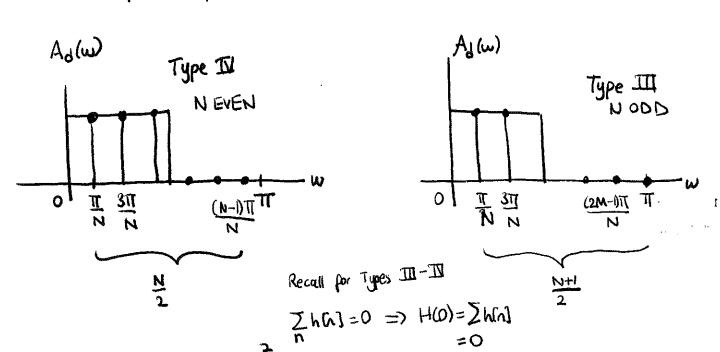
=) We can get a gain of 4. Why?*

$$h[n] = \frac{1}{N} \left[A[0] + \sum_{k=1}^{M} 2A[k] \cos \frac{2\pi(n-M)k}{N} \right]$$
 Type I

where $M = \frac{N-1}{2}$ and $A(0), \dots, A(M)$ are samples of amplitude response

* because $M \approx \frac{N}{2}$ and we only have the "cas" terms.

We have equivalent forms for other types (Types II, III, IV)



Note: We could also use non-uniform sampling. However, in that case we can no longer use IDFT.

- 2. Least-Squares (LS) error in frequency domain.
- a) L=N discrete frequency samples where L is the length of the filter $E = \sum_{k=0}^{L-1} |A(w_k) Ad(w_k)|^2 \quad \text{mean-squared error}$ k=0

 $W_k = \frac{2\pi r_k}{L}$, k=0,...,L-1, with amplitude samples $A_d(w_k)$.

From Purseual's theorem,

$$E = \sum_{n=-\frac{(L-1)}{2}}^{\frac{L-1}{2}} \left| h[n] - h_d[n] \right|^2$$

where halfol is a length-L FIR filter,

Using $M = \frac{N-1}{2}$ we newrite $E = \frac{1}{2}$

$$E = \sum_{n=-M}^{M} |n[n] - hd[n]|^2 + \sum_{n=-M+1}^{M} 2|hd[n]|^2$$
length N length L

period and except

To minimize E, take hind to agree with halfold on first N little taps, i.e., truncate halfold.

To adjust the 'residual enor', choose N appropriately.

Solving a LS problem

Recall that the amplitude response of a linear phase filter is

$$A(w) = \sum_{n=0}^{M-1} 2h[n]\cos(w(M-n)) + h[M]$$
 (Type I N ODD)

$$a = Fh$$
 where L>M+1, i.e., F is a tall matrix.

LX1

vector

matrix

invertible

T. T. T. H. transpose

$$h = (FTF)^{-1}FT\alpha$$
 is the solution that minimizes

 $(M+1)\times(M+1)$

matrix