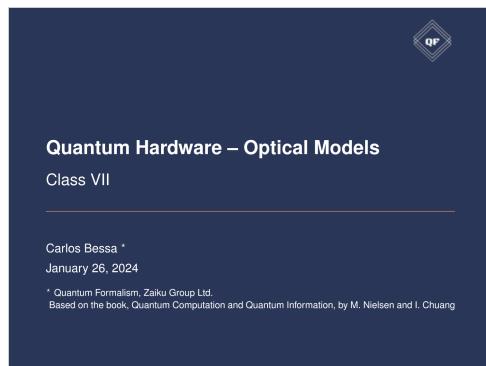


## Lecture12\_QHardware\_class7

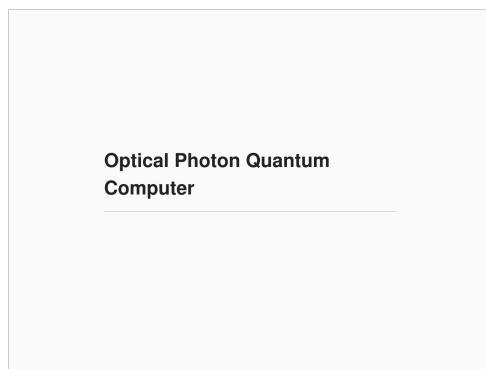
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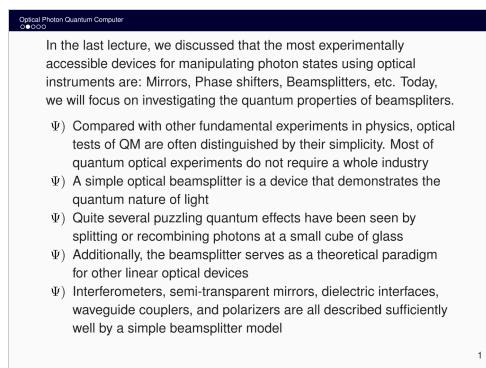
Lecture12...



The slide has a dark blue header with the QF logo. The title is "Quantum Hardware – Optical Models" and "Class VII". Below the title, it says "Carlos Bessa \* January 26, 2024". A note at the bottom states: "Quantum Formalism, Zaike Group Ltd. Based on the book, Quantum Computation and Quantum Information, by M. Nielsen and I. Chuang".



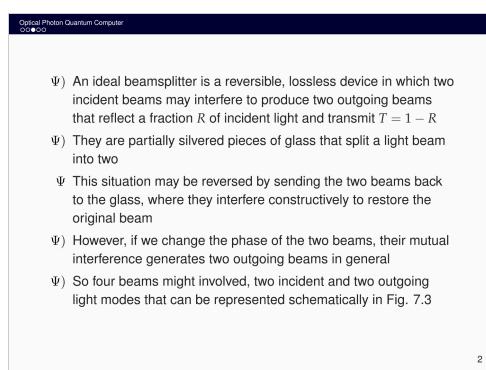
The slide has a light gray background with the title "Optical Photon Quantum Computer".



The slide has a dark blue header with the QPQC logo. The main text reads: "In the last lecture, we discussed that the most experimentally accessible devices for manipulating photon states using optical instruments are: Mirrors, Phase shifters, Beamsplitters, etc. Today, we will focus on investigating the quantum properties of beamsplitters." Below this is a list of bullet points:

- Ψ) Compared with other fundamental experiments in physics, optical tests of QM are often distinguished by their simplicity. Most of quantum optical experiments do not require a whole industry
- Ψ) A simple optical beamsplitter is a device that demonstrates the quantum nature of light
- Ψ) Quite several puzzling quantum effects have been seen by splitting or recombining photons at a small cube of glass
- Ψ) Additionally, the beamsplitter serves as a theoretical paradigm for other linear optical devices
- Ψ) Interferometers, semi-transparent mirrors, dielectric interfaces, waveguide couplers, and polarizers are all described sufficiently well by a simple beamsplitter model

1

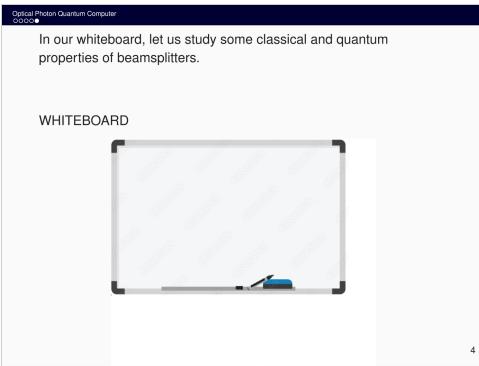
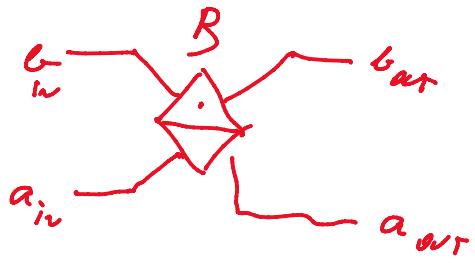
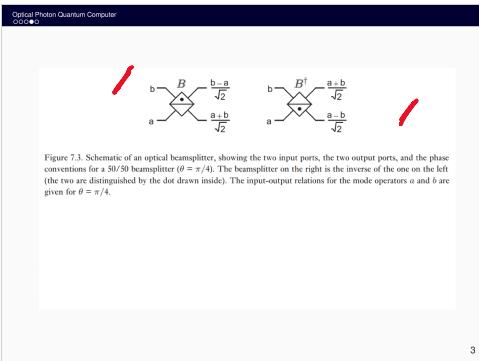


The slide has a dark blue header with the QPQC logo. The main text reads: "Ψ) An ideal beamsplitter is a reversible, lossless device in which two incident beams may interfere to produce two outgoing beams that reflect a fraction  $R$  of incident light and transmit  $T = 1 - R$ "

Below this is a list of bullet points:

- Ψ) They are partially silvered pieces of glass that split a light beam into two
- Ψ) This situation may be reversed by sending the two beams back to the glass, where they interfere constructively to restore the original beam
- Ψ) However, if we change the phase of the two beams, their mutual interference generates two outgoing beams in general
- Ψ) So four beams might involved, two incident and two outgoing light modes that can be represented schematically in Fig. 7.3

2



## BEAM SPLITTERS

- WHAT HAPPEN IF TWO COHERENT LIGHT BEAMS WITH COMPLEX AMPLITUDES  $a_{in}$  AND  $b_{in}$  INTERFERE?

- IN CLASSICAL OPTICS THE AMPLITUDES ARE SIMPLY SUPERIMPOSED ACCORDING TO THE LINEAR TRANSFORMATION

$$\begin{pmatrix} a_{out} \\ b_{out} \end{pmatrix} = B \begin{pmatrix} a_{in} \\ b_{in} \end{pmatrix}, \quad E \sim a e^{i k \cdot r - i \omega t}$$

$B$  is described by the matrix:  $B = \begin{pmatrix} B_{00} & B_{01} \\ B_{10} & B_{11} \end{pmatrix}$

$$B_{\text{clas}} = \begin{pmatrix} T & R \\ R & T \end{pmatrix} \sim \begin{pmatrix} \cos \theta & \sin \theta \\ -\sin \theta & \cos \theta \end{pmatrix}$$

THIS IS PHENOMENOLOGICALLY CONFIRMED!

- IN QUANTUM OPTICS THE COMPLEX AMPLITUDES  $a_{in}, b_{in}$

- IN QUANTUM OPTICS THE COMPLEX AMPLITUDES  $a_{in}, b_{in}$  CORRESPOND TO THE ANNihilation OPERATORS  $\hat{a}_{in}, \hat{b}_{in}$  OF THE INCIDENT FIELDS ( $\hat{E}_{in} \sim \hat{a}_{in}$ )
- THE OUTGOING BEAMS ARE CHARACTERIZED BY THE OPERATORS  $\hat{a}_{out}, \hat{b}_{out}$
- WE ASSUME THAT THE LINEAR VERSION GIVEN ABOVE IS ALSO VALID TO THE QUANTUM FIELDS

$$\begin{pmatrix} \hat{a}_{out} \\ \hat{b}_{out} \end{pmatrix} = B \begin{pmatrix} \hat{a}_{in} \\ \hat{b}_{in} \end{pmatrix}, \quad B = \begin{pmatrix} B_{00} & B_{01} \\ B_{10} & B_{11} \end{pmatrix}$$

- IN THIS MODEL WE CAN DESCRIBE MOST OF PASSIVE AND LOSSLESS DEVICES IN WHICH TWO BEAMS INTERFERE TO PRODUCE OUTGOING FIELDS

- LET'S DETERMINE SOME PROPERTIES OF THE BEAM SHITTEN

- CONSIDER THAT INCOMING LIGHT BEAMS AND OUTGOING BEAMS ARE BOTH INDEPENDENT BOSONIC MODES
  - WE ALREADY KNOW THE FOLLOWING RELATIONS:
- $$[a_{out}, a_{out}^+] = [a_{in}, a_{in}^+] = [b_{out}, b_{out}^+] = [b_{in}, b_{in}^+] = 1$$
- $$[a_{out}, b_{out}] = [a_{in}, b_{in}] = 0$$

$$\begin{aligned} \bullet [a_{out}, a_{out}^+] &= \left[ a_{in} B_{00} + b_{in} B_{01}, a_{in}^+ B_{00}^* + b_{in}^+ B_{01}^* \right] = 1 \\ &= [a_{in} B_{00}, a_{in}^+ B_{00}^*] + [a_{in} B_{00}, b_{in}^+ B_{01}^*] + [b_{in} B_{01}, a_{in}^+ B_{00}^*] + \\ &\quad + [b_{in} B_{01}, b_{in}^+ B_{01}^*] = 1 \\ &= |B_{00}|^2 [a_{in}, a_{in}^+] + B_{00} B_{01}^* [a_{in}, b_{in}] + B_{01} B_{00}^* [b_{in}, a_{in}^+] = 0 \end{aligned}$$

$$\begin{aligned}
 & \text{Left side} \\
 & = |B_{00}|^2 \left[ a_{in}, a_{in}^\dagger \right] + B_{00} B_{01}^* \left[ a_{in}, b_{in}^\dagger \right] + B_{01} B_{00}^* \left[ b_{in}, a_{in}^\dagger \right] \\
 & + |B_{01}|^2 \left[ b_{in}, b_{in}^\dagger \right] = 1 \\
 & \Rightarrow |B_{00}|^2 + |B_{01}|^2 = 1
 \end{aligned}$$

THE SAME FOR

$$\begin{aligned}
 & \left[ b_{out}, b_{out}^\dagger \right] = |B_{10}|^2 + |B_{11}|^2 = 1 \\
 & \left[ a_{out}, b_{out}^\dagger \right] = 0 \Rightarrow B_{00} B_{10}^* + B_{01} B_{11}^* = 0
 \end{aligned}$$

IN OTHER WORDS,  $B$  IS UNITARY

$$B^{-1} = B^* \quad (\text{HOMWORK})$$

- APART FROM THE UNITARITY, THE SCATTERING COEFFICIENTS ARE FREE PARAMETERS THAT DEPEND ON THE PARTICULAR EXPERIMENTAL SITUATION

- FOR OUR PURPOSE AND APPLICATIONS, WE ARE INTERESTED ON REAL NUMBERS MATRICES

- IN THIS CASE, WE COULD REPRESENT  $B$  IN TERMS OF THE TRANSMISSIVITY  $T$  AND THE REFLECTIVITY  $R$  AS

$$B = \begin{pmatrix} T & R \\ -R & T \end{pmatrix}, \quad B^* = B^{-1} = \begin{pmatrix} T & -R \\ R & T \end{pmatrix}$$

AND THE EQUATION  $T^2 + R^2 = 1$  (HOMWORK)

ACCOUNTS FOR ENERGY CONSERVATION OR LOSSLESS PORTS

- THE SIMPLEST CHOICE TO SATISFY THESE CONDITIONS IS  $T = \cos \theta$ ,  $R = \sin \theta$

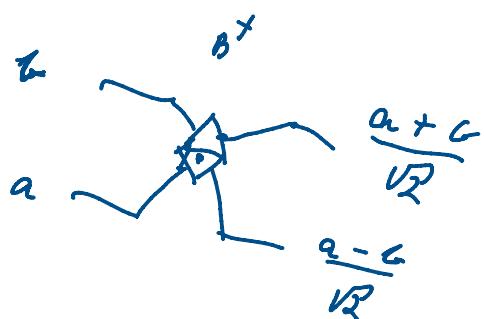
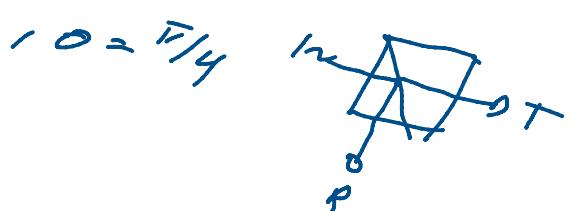
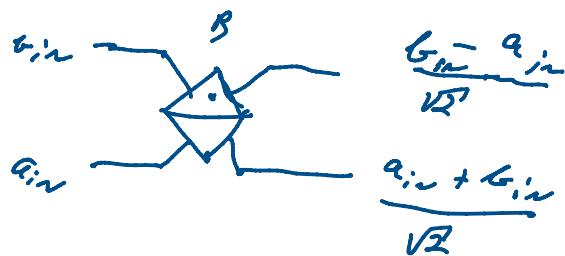
THEN,

$$\beta = \begin{pmatrix} \cos\theta & \sin\theta \\ -\sin\theta & \cos\theta \end{pmatrix}, \quad \beta^+ = \begin{pmatrix} \cos\theta & -\sin\theta \\ \sin\theta & \cos\theta \end{pmatrix}$$

$$\begin{pmatrix} a_{out} \\ b_{out} \end{pmatrix} = \begin{pmatrix} \cos\theta & \sin\theta \\ -\sin\theta & \cos\theta \end{pmatrix} \begin{pmatrix} a_{in} \\ b_{in} \end{pmatrix}$$

$$\left\{ \begin{array}{l} a_{out} = a_{in} \cos\theta + b_{in} \sin\theta \\ b_{out} = -a_{in} \sin\theta + b_{in} \cos\theta \end{array} \right. \quad (7.17)$$

$$\left\{ \begin{array}{l} a_{out} = -a_{in} \sin\theta + b_{in} \cos\theta \\ b_{out} = a_{in} \cos\theta + b_{in} \sin\theta \end{array} \right. \quad (7.18)$$



- WE COULD FIND THE SAME RESULT USING THE FOLLOWING HAMILTONIAN

$$H_{BS} = \theta (a\beta^+ - \beta^+ a)$$

AND THE BEAM SPLITTER PERFORMS THE UNITARY OPERATION

$$\beta = e^{i\theta} = e^{i\theta(a\beta^+ - \beta^+ a)}$$

- THE TRANSFORMATION EFFECTED BY  $\beta$  ON  $a$  AND  $b$  WHICH WILL BE LATEN USEFUL AT

$$\begin{cases} \beta a \beta^+ = a \cos \theta + b \sin \theta \\ \beta b \beta^+ = -a \sin \theta + b \cos \theta \end{cases} \quad (7.26)$$

TO VERIFY THESE RELATIONS WE USE THE BAUEN-GROBELL-HAUSDORF FORMULA

EXERCISE 4.49 :  $e^{\lambda G} + e^{-\lambda G} = \sum_{n=0}^{\infty} \frac{\lambda^n}{n!} c_n \quad (7.27)$

COMPLEMENTARY

$\lambda \rightarrow$  COMPLEX NUMBER

$A, G, c_n \rightarrow$  OPERATORS

$c_n$  IS DEFINED RECURSIVELY AS

$$\begin{aligned} & \cdot c_0 = A, \quad c_1 = [G, c_0], \quad c_2 = [G, c_1], \quad c_3 = [G, c_2] \dots \\ & c_n = [G, c_{n-1}] \end{aligned} \quad (I)$$

- SINCE WE ALREADY PROVED THAT  $[a, a^+] = \underline{1} = [\underline{b}, \underline{b}^+]$

EQUATION (VERSE-CHURNOV)

$$G = a b^+ - a^+ b$$

$$[G, a] = [a b^+ - a^+ b, a] = [a b^+, a] - [a^+ b, a] = a [b^+, a] + \overset{<0}{[a, a^+] b} + \overset{<-1}{-a^+ [G, a]} - \overset{<-1}{[a^+, a]} b$$

$$\cdot [G, a] = b \quad (II)$$

$$\cdot [G, b] = -a \quad (III)$$

$$c_{n, \text{EVEN}} = i^n a, \quad c_{n, \text{ODD}} = -i^{n+1} b$$

TO SEE THIS USE EQUATIONS (I), (II), (III)

$$\text{So } \underbrace{n(i^n b - a^+ b)}_{-\partial(a b^+ - a^+ b)} - \partial \underbrace{(a b^+ - a^+ b)}_{\partial G} = -\partial c$$

$$\text{So, } \beta a b^+ = e^{\theta \underbrace{(ab^+ - a^+ b)}_{G}} a e^{-\theta \underbrace{(a b^+ - a^+ b)}_{-G}} = e^{\theta G} a e^{-\theta G}$$

Using BCH-Fomula in the form of Eq. (7.27)

$$\beta a b^+ = e^{\theta G} a e^{-\theta G} = \sum_{n=0}^{\infty} \frac{\theta^n}{n!} c_n$$

$$\beta a b^+ = \sum_{n, \text{even}} \frac{(i\theta)^n}{n!} a - i \sum_{n, \text{odd}} \frac{(i\theta)^n}{n!} G = a \left( 1 - \frac{\theta^2}{2!} + \frac{\theta^4}{4!} + \dots \right) - i \left( i\theta - \frac{i\theta^3}{3!} + \frac{i\theta^5}{5!} + \dots \right)$$

$$\text{use: } \cos x = \sum_{n=0}^{\infty} (-1)^n \frac{x^{2n}}{(2n)!} = 1 - \frac{x^2}{2!} + \frac{x^4}{4!} + \dots - i \left( i\theta - \frac{i\theta^3}{3!} + \frac{i\theta^5}{5!} + \dots \right)$$

$$\sin x = \sum_{n=0}^{\infty} (-1)^n \frac{x^{2n+1}}{(2n+1)!} = x - \frac{x^3}{3!} + \frac{x^5}{5!} + \dots$$

$$\boxed{\beta a b^+ = a \cos \theta + b \sin \theta}$$

$$\bullet \beta b b^+ = b \cos \theta - a \sin \theta \quad (\text{HOMWORK})$$

In terms of quantum logic Gates,  $\beta$  performs a useful

operation

$$\begin{aligned} \beta |100\rangle &= e^{\theta(a^+b - a b^+)} |100\rangle = e^{\theta G} |100\rangle \\ &= \left[ 1 + \theta G + \frac{(\theta G)^2}{2!} + \frac{(\theta G)^3}{3!} + \dots \right] |100\rangle \end{aligned}$$

$$\begin{aligned} \bullet G |100\rangle &\approx (g_g^+ g_g - g_b^+ g_b) |100\rangle = (a^+ b - a b^+) |10\rangle_a \otimes |10\rangle_b \\ &= |11\rangle_a \otimes 0 - 0 \otimes |11\rangle_b = 0 \end{aligned}$$

$$\beta |100\rangle = (1 + 0 + 0 \dots) |100\rangle = |100\rangle$$

- THIS MEANS THAT WHEN NO PHOTONS IN EITHER INPUT MODE EXIST NO PHOTONS WILL EXIST IN EITHER OUTPUT

- THIS MEANS THAT WHEN NO PHOTONS ARE IN THE MODE EXIST, NO PHOTONS WILL EXIST IN EITHER OUTPUT MODE

- LET'S SEE WHAT HAPPENS IF ONE SINGLE PHOTON EXISTS, FOR INSTANCE, IN MODE A

$$|1_L\rangle = a^\dagger |0_L\rangle$$

$$\beta |0_L\rangle = \beta |0\rangle_a \otimes |1\rangle_a = \beta |0\rangle_a \otimes a^\dagger |0\rangle_a$$

$$\beta |0_L\rangle = \beta a^\dagger |00\rangle, \text{ but, } \beta^T \beta = \hat{I}$$

$$\beta |0_L\rangle = \beta a^\dagger \underbrace{\beta^\dagger \beta |00\rangle}_{|00\rangle} = \beta a^\dagger \beta^\dagger |00\rangle$$

$$\text{AND FROM EQ. (7.33)} \Rightarrow \beta^2 \beta^\dagger = a^\dagger \cos\theta + b^\dagger \sin\theta$$

AND WE COULD PROVE THAT  $\beta a^\dagger \beta^\dagger = a^\dagger \cos\theta + b^\dagger \sin\theta$   
(HOMWORK)

$$\beta |0_L\rangle = \beta a^\dagger \beta^\dagger |00\rangle = (a^\dagger \cos\theta + b^\dagger \sin\theta) |00\rangle$$

$$= a^\dagger |00\rangle \cos\theta + b^\dagger |00\rangle \sin\theta$$

$$\boxed{\beta |0_L\rangle = |0_L\rangle \cos\theta + |1_L\rangle \sin\theta}$$

$$\boxed{-\beta |1_L\rangle = |1_L\rangle \cos\theta - |0_L\rangle \sin\theta} \quad (\text{HOMWORK})$$

- THUS ON THE  $|0_L\rangle$  AND  $|1_L\rangle$  MANIFOLD STATES

$$|1_O\rangle = |1_L\rangle, |0_O\rangle = |0_L\rangle$$

$$\rightarrow \beta |0_O\rangle = \beta |0_L\rangle = \cos\theta |0_L\rangle + \sin\theta |1_L\rangle$$

$$\rightarrow \beta |1_O\rangle = \beta |1_L\rangle = \cos\theta |1_L\rangle - \sin\theta |0_L\rangle$$

- MATRIX REPRESENTATION FOR  $\beta$

$$\beta = \begin{pmatrix} \cos\theta & -\sin\theta \\ \sin\theta & \cos\theta \end{pmatrix} \quad (7.35)$$

- NOTE THAT, WE COULD WRITE (7.35) WITH

$$\beta = e^{-i\theta Y}, \quad Y = \begin{pmatrix} 0 & -i \\ i & 0 \end{pmatrix}$$

USING FORMULA (2.58)  $\Rightarrow e^{i\theta(\vec{v} \cdot \vec{\sigma})} = \cos\theta I + i \sin\theta \vec{v} \cdot \vec{\sigma}$

$$e^{-i\alpha Y} = \begin{pmatrix} \cos\theta & -\sin\theta \\ \sin\theta & \cos\theta \end{pmatrix}, \quad \cancel{\text{cros}}$$

- PHASE SHIFTS AND BEAM SPLITTERS TOGETHER ALLOW  
MAINTAINING SINGLE QUBIT OPERATIONS TO BE PERFORMED TO OPTIMAL  
QUBIT

$$\rho \rightarrow R_z(\alpha) = e^{-i\alpha Z/2} \rightarrow \text{PERFORMS A } R_z-\text{ROTATION}$$

$$\beta \rightarrow R_y(\alpha) = e^{-i\alpha Y/2} \rightarrow \text{" " " } R_y-\text{ROTATION}$$