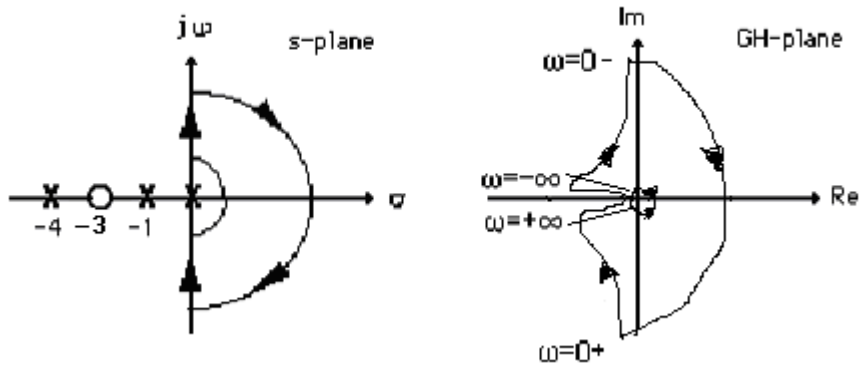


HW6

1. Chap 10 Prob. 1 (c)

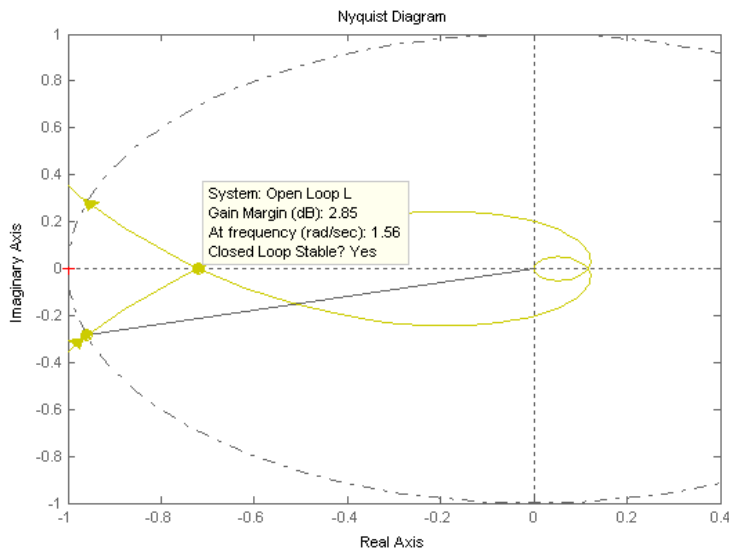
$$|G(j\omega)| = \frac{\sqrt{4+\omega^2}\sqrt{16+\omega^2}}{\omega\sqrt{1+\omega^2}\sqrt{9+\omega^2}}; \angle G(j\omega) = \tan^{-1}\frac{\omega}{2} + \tan^{-1}\frac{\omega}{4} - 90^\circ - \tan^{-1}\omega - \tan^{-1}\frac{\omega}{3}$$

2. Chap 10 Prob. 4 System 3



3. Chap 10 Prob. 8 System 2 and Prob. 9(b) for Prob. 8 System 2

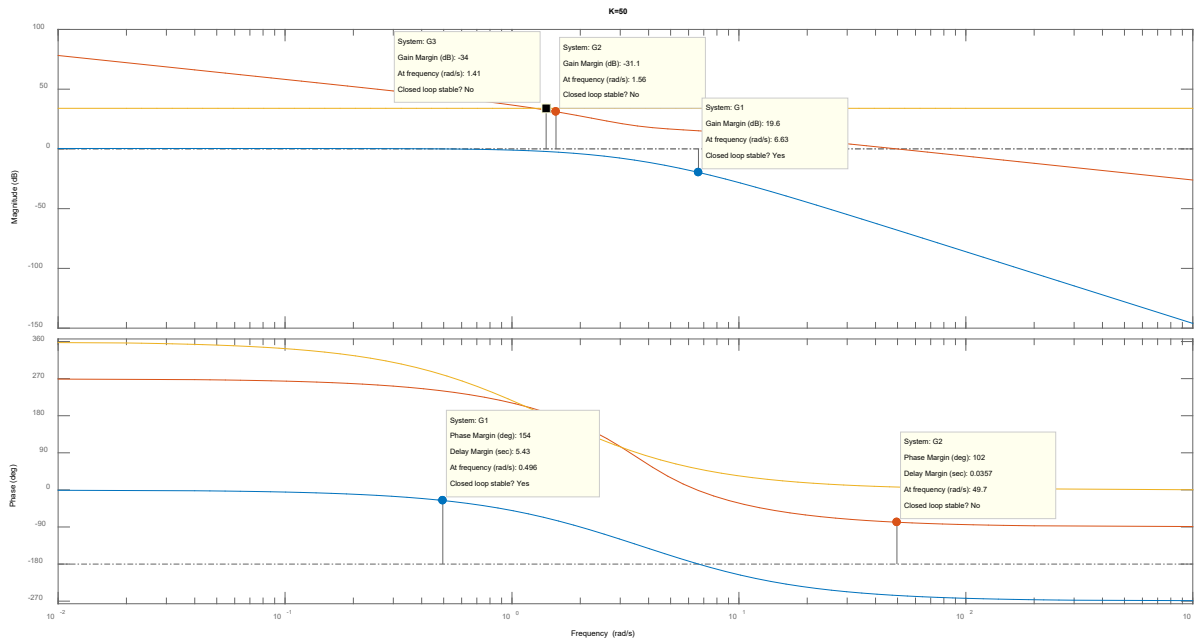
8. System 2: For $K = 1$,



The Nyquist diagram intersects the real axis at -0.720. Thus K can be increased to 1.39 before there are encirclements of -1.

There are no poles encircled by the contour. Thus $P = 0$. Hence, $Z = P - N$, $Z = 0 + 0$ if $K < 1.39$; $Z = 0 - (-2)$ if $K > 1.39$. Therefore stability if $0 < K < 1.39$.

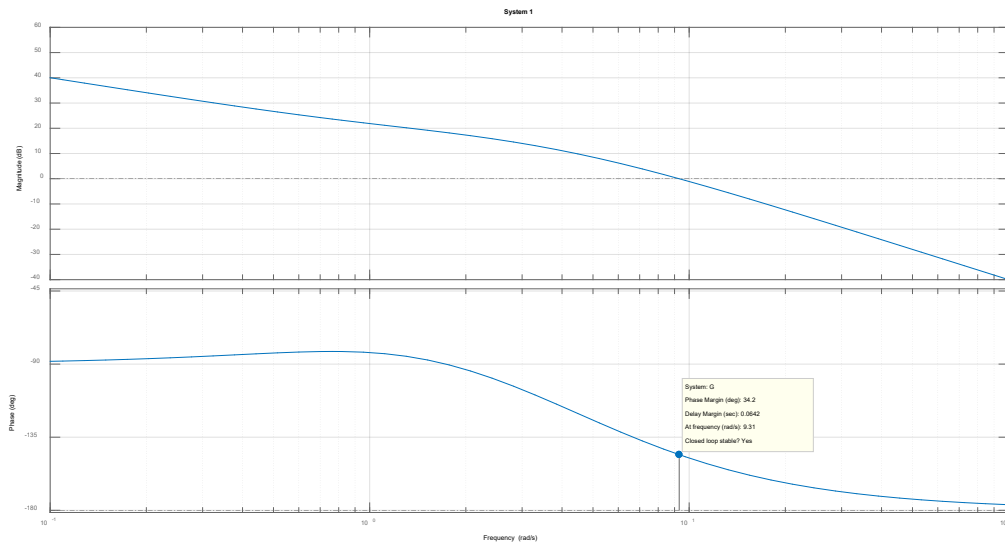
9b.



When $K = 50$ only the System 1 is closed loop stable, for the other two systems the gain margin and phase margin do not exist.

4. Chap 10 Prob. 19 System 1

The Bode plot is:



The phase margin is 34.2° . The open loop response is -7dB with -156° at approximately 14 rad/sec which is the Bandwidth of the closed loop system. Using Figure 10.48 $\zeta = 0.34$, so $\%OS = 100e^{-\frac{\zeta\pi}{\sqrt{1-\zeta^2}}} = 32.1\%$. Using Eq. (10.55) $T_s = 1.197\text{ sec}$ and Eq. (10.56) yields $T_p = 0.34\text{ sec}$.

5. Chap 10 Prob. 22

- From the Bode plots: Gain margin $\cong 20\text{ dB}$; phase margin $\cong 55^\circ$; 0 dB frequency $\cong 1\text{ rad/s}$; -180° frequency $\cong 4.5\text{ rad/s}$; bandwidth ($@-7\text{ dB}$ point) $\cong 2\text{ rad/s}$.
- From Eq. (10.73) $\zeta = 0.55$; from Eq. (4.38) $\%OS = 12.6$; from Eq. (10.55) $T_s = 4.41\text{ s}$; from Eq. (10.56) $T_p = 2.28\text{ s}$.