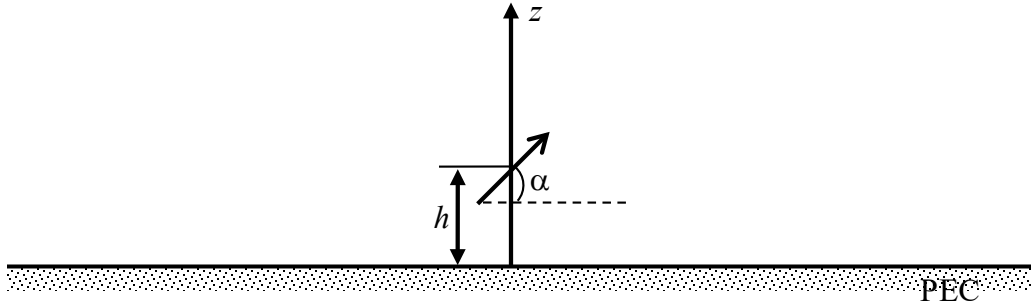


Applied Computational EM Homework Assignment #2

Problem 1

Consider the short current filament (dipole) $Id\ell$ radiating in free space in the presence of an infinite PEC surface as shown in Figure 1 below. The dipole is oriented at an angle α with respect to the x -axis.



- Derive the magnetic vector potential radiated by the short dipole.
- From the vector potential, derive the \mathbf{E} and \mathbf{H} fields radiated in the far-zone.

Solution

- The current element $Id\ell$ is resolved into two components:

$$Id\ell = Id\ell \cos \alpha \hat{\mathbf{x}} + Id\ell \sin \alpha \hat{\mathbf{z}} \quad (1)$$

According to image theory discussed in class, the image of the x -directed component of the current element $Id\ell$ is directed opposite to the x -directed component of the current element. The z -directed image, on the other hand, is directed in the same direction as the z -directed component of the current element. The overall magnetic vector potential due to the x and z current elements and their images are given by:

$$A_x = \frac{Id\ell \cos \alpha}{4\pi} \mu_0 \left(\frac{e^{-jk_0|\mathbf{r}-\mathbf{r}'_1|}}{|\mathbf{r}-\mathbf{r}'_1|} - \frac{e^{-jk_0|\mathbf{r}-\mathbf{r}'_2|}}{|\mathbf{r}-\mathbf{r}'_2|} \right) \quad (2)$$

$$A_z = \frac{Id\ell \sin \alpha}{4\pi} \mu_0 \left(\frac{e^{-jk_0|\mathbf{r}-\mathbf{r}'_1|}}{|\mathbf{r}-\mathbf{r}'_1|} + \frac{e^{-jk_0|\mathbf{r}-\mathbf{r}'_2|}}{|\mathbf{r}-\mathbf{r}'_2|} \right) \quad (3)$$

In (2) and (3), $\mathbf{r}'_1 = h\hat{\mathbf{z}}$, $\mathbf{r}'_2 = -h\hat{\mathbf{z}}$. In the far-field region we have

$$\begin{aligned} |\mathbf{r} - \mathbf{r}'_1| &= \left(r^2 - 2\mathbf{r} \cdot \mathbf{r}'_1 + r_1'^2 \right)^{1/2} = r \left(1 - \frac{2\mathbf{r} \cdot \mathbf{r}'_1}{r^2} + \frac{r_1'^2}{r^2} \right)^{1/2} \cong r - \hat{\mathbf{r}} \cdot \mathbf{r}'_1 = r - h \cos \theta \\ |\mathbf{r} - \mathbf{r}'_2| &\cong r + h \cos \theta \end{aligned} \quad (4)$$

Hence,

$$\begin{aligned} A_x &= \frac{Id \ell \cos \alpha}{4\pi} \mu_0 \frac{e^{-jk_0 r}}{r} \left(e^{jk_0 h \cos \theta} - e^{-jk_0 h \cos \theta} \right) \\ &= j \frac{Id \ell \cos \alpha}{2\pi} \mu_0 \frac{e^{-jk_0 r}}{r} \sin(k_0 h \cos \theta) \end{aligned} \quad (5)$$

$$\begin{aligned} A_z &= \frac{Id \ell \sin \alpha}{4\pi} \mu_0 \frac{e^{-jk_0 r}}{r} \left(e^{jk_0 h \cos \theta} + e^{-jk_0 h \cos \theta} \right) \\ &= \frac{Id \ell \sin \alpha}{2\pi} \mu_0 \frac{e^{-jk_0 r}}{r} \cos(k_0 h \cos \theta) \end{aligned} \quad (6)$$

In the far-field, we need the vector potential components A_θ and A_ϕ to compute the far-zone radiated field. These are given by

$$\begin{aligned} A_\theta &= A_x \cos \phi \cos \theta - A_z \sin \theta \\ &= -Id \ell \mu_0 \frac{e^{-jk_0 r}}{2\pi r} \left[\sin \alpha \sin \theta \cos(k_0 h \cos \theta) - j \cos \alpha \cos \phi \cos \theta \sin(k_0 h \cos \theta) \right] \end{aligned} \quad (7)$$

$$A_\phi = -A_x \sin \phi = -j Id \ell \cos \alpha \mu_0 \frac{e^{-jk_0 r}}{2\pi r} \sin \phi \sin(k_0 h \cos \theta) \quad (8)$$

b) In the far-field, the electric and magnetic fields are transverse to each other and to the \mathbf{r} direction. Hence,

$$\begin{aligned} E_\theta &= -j\omega A_\theta \\ E_\phi &= -j\omega A_\phi \end{aligned} \quad (9)$$

and

$$\mathbf{H} = \frac{1}{\eta_0} \hat{\mathbf{r}} \times \mathbf{E} = \frac{1}{\eta_0} \left(-E_\phi \hat{\boldsymbol{\theta}} + E_\theta \hat{\boldsymbol{\phi}} \right) \quad (10)$$

Problem 2

For the problem of TM^z scattering from a perfectly conducting infinite cylinder treated in class. Take $\theta_0 = 90^\circ$, $\phi_0 = 0$, $E_0 = 1$ V/m, frequency = 1, 5, 10, 20 GHz, radius $a = 0.25$ m.

- a) Calculate the electric surface current density induced on the surface of the cylinder. Note that the surface current density is given by

$$\mathbf{J}_s = (\hat{\mathbf{n}} \times \mathbf{H})_{\rho=a} = \hat{\mathbf{n}} \times (\mathbf{H}_i + \mathbf{H}_s)_{\rho=a}$$

where the unit surface normal is given by $\hat{\mathbf{n}} = \hat{\boldsymbol{\rho}}$.

- b) Calculate the physical optics approximation to the surface current density given by

$$\mathbf{J}_{PO} = 2(\hat{\mathbf{n}} \times \mathbf{H}_i)_{\rho=a}$$

- c) Compare the two results and comment on the differences.
d) Repeat steps (a) to (c) for the TE^z case.

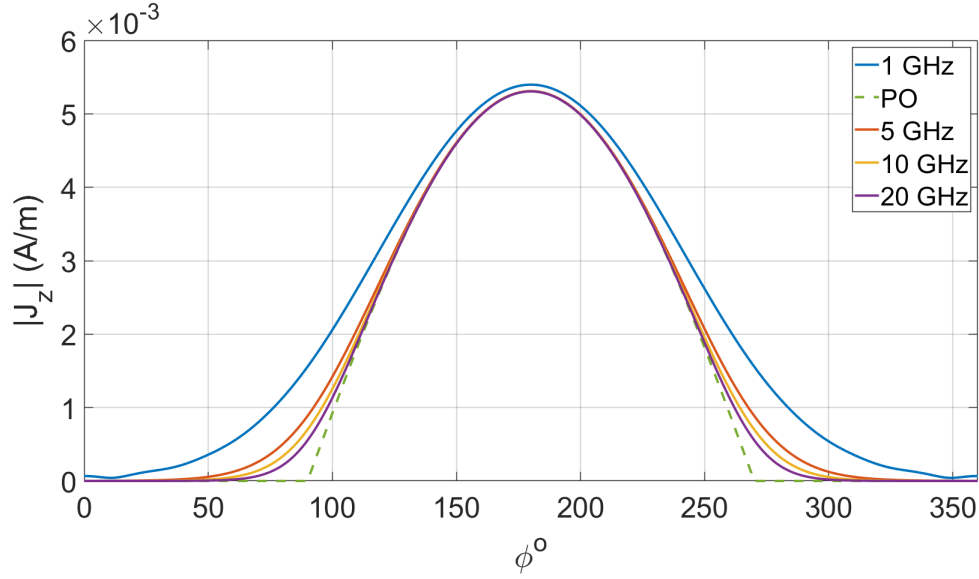
Solution

- a) The surface current was derived in class. The result is:

$$J_z = \frac{2E_0}{\pi k a \eta} \sum_{n=0}^{\infty} j^{-n} \epsilon_n \left[\frac{\cos(n\phi)}{H_n^{(2)}(ka)} \right]$$

- b) The physical optics current is given by

$$\begin{aligned} \mathbf{E}_i &= E_0 e^{-j\mathbf{k}_i \cdot \mathbf{r}} \hat{\mathbf{z}} \\ J_z^{PO} \hat{\mathbf{z}} &= 2(\hat{\boldsymbol{\rho}} \times \mathbf{H}_i)_{\rho=a} = -2 \left[\frac{E_0}{\eta} e^{-j\mathbf{k}_i \cdot \mathbf{r}} (\hat{\boldsymbol{\rho}} \times \hat{\mathbf{y}}) \right]_{\rho=a} = -2 \frac{E_0}{\eta} \cos \phi e^{-jka \cos \phi} \hat{\mathbf{z}} \end{aligned}$$



- c) The difference between the exact current and the physical optics current is due to diffraction effects not accounted for by the physical optics approximation.
- d) For the TE^z case, the electric current induced on the surface of the cylinder is given by

$$\mathbf{J} = \hat{\mathbf{n}} \times (\mathbf{H}^i + \mathbf{H}^s) \Big|_{\rho=a} = \hat{\mathbf{p}} \times (\mathbf{H}^i + \mathbf{H}^s) \Big|_{\rho=a} \quad (11)$$

At normal incidence, $\theta_i = \pi/2$, the incident magnetic field component expanded in term of cylindrical wave functions is given by (12). Note that when $\theta_i = \pi/2$, $H_\rho^i = H_\phi^i = 0$, and the only nonzero component of the incident magnetic field is given by

$$H_z^i = H_0 \sum_{n=-\infty}^{\infty} j^{-n} J_n(k\rho) e^{jn\phi} \quad (12)$$

As shown below, the only non-zero component of the magnetic field is given by

$$H_z^s = -H_0 \sum_{n=-\infty}^{\infty} j^{-n} \frac{J'_n(k_0 a)}{H_n^{(2)'}(k_0 a)} H_n^{(2)}(k_0 \rho) e^{jn\phi} \quad (13)$$

Substituting (12) and (13) into (11) and evaluating the resulting expression at $\rho = a$ yields

$$\begin{aligned}
J_\phi &= H_0 \sum_{n=-\infty}^{\infty} j^{-n} \frac{J'_n(ka) H_n^{(2)}(ka) - J_n(ka) H_n^{(2)'}(ka)}{H_n^{(2)'}(ka)} e^{jn\phi} \\
&= \frac{j2}{\pi ka} H_0 \sum_{n=-\infty}^{\infty} j^{-n} \frac{e^{jn\phi}}{H_n^{(2)'}(ka)}
\end{aligned} \tag{14}$$

The above result can be also written as follows

$$J_\phi = \frac{j2}{\pi ka} H_0 \left[\sum_{n=1}^{\infty} j^n \frac{e^{-jn\phi}}{H_{-n}^{(2)'}(ka)} + \sum_{n=0}^{\infty} j^{-n} \frac{e^{jn\phi}}{H_n^{(2)'}(ka)} \right] \tag{15}$$

From the recurrence relations of the Hankel function we have

$$\begin{aligned}
H_{-n}^{(2)'}(ka) &= -H_{-(n-1)}^{(2)}(ka) - \frac{n}{ka} H_{-n}^{(2)}(ka) \\
&= e^{-jn\pi} \left[H_{(n-1)}^{(2)}(ka) - \frac{n}{ka} H_n^{(2)}(ka) \right] \\
&= (-1)^n H_n^{(2)'}(ka)
\end{aligned} \tag{16}$$

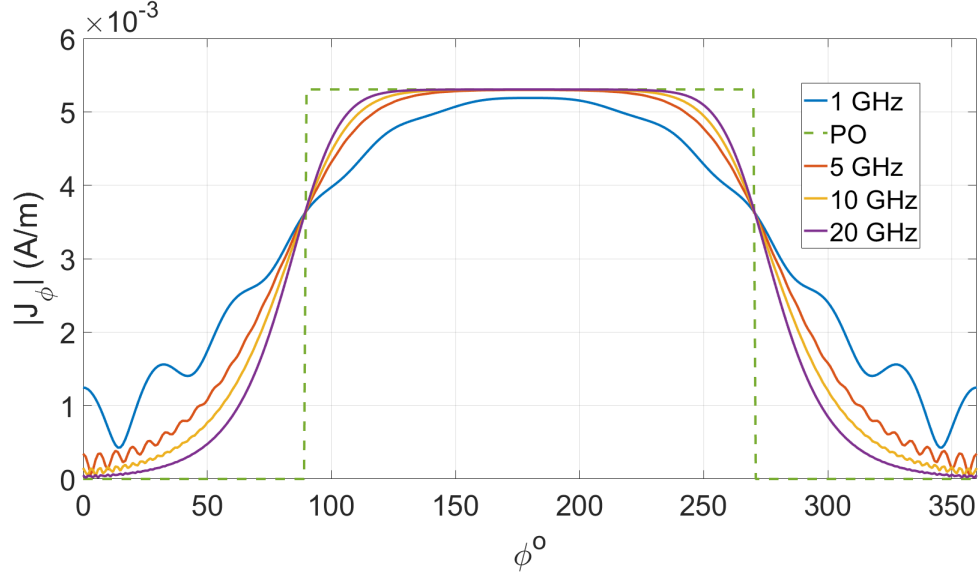
Substituting (16) into (15) we obtain

$$J_\phi = \frac{j2}{\pi ka} H_0 \sum_{n=0}^{\infty} \epsilon_n j^{-n} \frac{\cos(n\phi)}{H_n^{(2)'}(ka)} \tag{17}$$

The physical optics current in this case is given by

$$J_\phi^{PO} = \begin{cases} -2H_0 e^{-jka \cos \phi}, & \text{Lit region} \\ 0, & \text{Shadow region} \end{cases} \tag{18}$$

These currents are plotted below



Derivation of the TE^z Case Using Hertz Vectors

The procedure is analogous to the TM^z case, but we work with the incident magnetic field instead. In this case, the incident magnetic field is given by

$$\begin{aligned}\mathbf{H}_i &= -H_0 e^{-jk_i \cdot \mathbf{r}} \hat{\mathbf{\theta}}_0 \\ H_{zi} &= \mathbf{H}_i \cdot \hat{\mathbf{z}} = H_0 \sin \theta_0 e^{-jk_i \cdot \mathbf{r}}\end{aligned}\quad (19)$$

The magnetic Hertz potential (Π_{zi}^m) associated with the above incident magnetic field is derived in a manner analogous to the derivation of the (Π_{zi}^e) for the TM^z case. The result is

$$\Pi_{zi}^m = \frac{H_0}{k^2 \sin \theta_0} e^{-jkz \cos \theta_0} \sum_{n=-\infty}^{\infty} j^{-n} J_n(k\rho \sin \theta_0) e^{jn(\phi - \phi_0)} \quad (20)$$

The scattered Hertz potential is given by

$$\Pi_{zs}^m = \sum_{n=-\infty}^{\infty} j^{-n} A_{sn} e^{-jkz \cos \theta_0} H_n^{(2)}(k\rho \sin \theta_0) e^{jn(\phi - \phi_0)} \quad (21)$$

The boundary condition is that the tangential electric field E_ϕ must be zero at the surface of the cylinder. This field component is given by

$$E_\phi \Big|_{\rho=a} = j\omega\mu \frac{\partial \Pi_z^m}{\partial \rho} \Big|_{\rho=a} = 0 = \frac{\partial}{\partial \rho} (\Pi_{zi}^m + \Pi_{zs}^m) \Big|_{\rho=a} = 0 \quad (22)$$

In the above

$$\left. \frac{\partial \Pi_{zs}^m}{\partial \rho} \right|_{\rho=a} = k \sin \theta_0 \sum_{n=-\infty}^{\infty} j^{-n} A_{sn} e^{-jkz \cos \theta_0} H_n'^{(2)}(ka \sin \theta_0) e^{jn(\phi - \phi_0)} \quad (23)$$

$$\left. \frac{\partial \Pi_{zi}^m}{\partial \rho} \right|_{\rho=a} = \frac{H_0}{k} e^{-jkz \cos \theta_0} \sum_{n=-\infty}^{\infty} j^{-n} J_n'(ka \sin \theta_0) e^{jn(\phi - \phi_0)} \quad (24)$$

Substituting (23) and (24) into (22) and solving for A_{sn} we obtain

$$A_{sn} = -\frac{H_0}{k^2 \sin \theta_0} \frac{J_n'(ka \sin \theta_0)}{H_n'^{(2)}(ka \sin \theta_0)} \quad (25)$$

The scattered magnetic field is given in terms of the scattered Hertz vector by

$$\begin{aligned} H_\rho^s &= \frac{\partial^2 \Pi_{zs}^m}{\partial z \partial \rho} \\ &= jH_0 \cos \theta_0 \sum_{n=-\infty}^{\infty} j^{-n} \frac{J_n'(ka \sin \theta_0)}{H_n'^{(2)}(ka \sin \theta_0)} e^{-jkz \cos \theta_0} H_n^{(2)}(k\rho \sin \theta_0) e^{jn(\phi - \phi_0)} \end{aligned} \quad (26)$$

$$\begin{aligned} H_\phi^s &= \frac{1}{\rho} \frac{\partial^2 \Pi_{zs}^m}{\partial z \partial \phi} \\ &= -H_0 \frac{\cot \theta_0}{k\rho} \sum_{n=-\infty}^{\infty} nj^{-n} \frac{J_n'(ka \sin \theta_0)}{H_n'^{(2)}(ka \sin \theta_0)} e^{-jkz \cos \theta_0} H_n^{(2)}(k\rho \sin \theta_0) e^{jn(\phi - \phi_0)} \end{aligned} \quad (27)$$

$$\begin{aligned} H_z^s &= \left(k^2 + \frac{\partial^2}{\partial z^2} \right) \Pi_{zs}^m \\ &= -H_0 \sin \theta_0 \sum_{n=-\infty}^{\infty} j^{-n} \frac{J_n'(ka \sin \theta_0)}{H_n'^{(2)}(ka \sin \theta_0)} e^{-jkz \cos \theta_0} H_n^{(2)}(k\rho \sin \theta_0) e^{jn(\phi - \phi_0)} \end{aligned} \quad (28)$$