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EE238 : Power Engineering II Solution to Assignment 1

1. Slip =
$$\frac{50-1.5}{50}$$
 = 0.03. Synchronous speed $N_s = \frac{120\times50}{8}$ = 750 r.p.m.
Rotor speed $N = (1-s)N_s = 750 \times (1-0.03) = 727.5$ r.p.m

2. Rotor frequency
$$f_r = \frac{90}{60} = 1.5$$
 Hz. Rotor speed $N = \frac{120 \times (50-1.5)}{6} = 970$ r.p.m. Output power $P = \omega_m \times T = \frac{2\pi \times 976}{60} \times 162 = 16455.7$ W. B.H.P = $\frac{16455.7}{746} = 22.1$ Mechanical power developed $P_m = (162+13.5) \times 2\pi \frac{970}{60} = 17826.9$ W Rotor Cu losses = $\frac{P_m s}{1-s} = 550$ W where $s = \frac{1.5}{50} = 0.03$ Input = $17826.98 + 550 + 750 = 19.2$ kW. Effeciency = 85.71 %.

3. Assume star connected stator.
$$V_{ph}=500/\sqrt{3}=289$$
 V. $X_m=289/36=8\Omega$. $R_c=V^2/P_c=166.71\Omega$

Input Imedance =
$$((0.062 + \frac{0.062}{0.02}) + j(0.21 + 0.21))||\frac{jX_mR_c}{jX_m+R_c} = 2.8\angle 27.66^\circ$$

Stator current $I_s = \frac{288.86}{2.8\angle 27.66^\circ} = 103.1\angle -27.66^\circ$

Power factor = $\cos(28^\circ) = 0.89 \text{ lag}$

Rotor current =
$$\frac{288.68}{(0.062+0.062/2)+j(0.21+0.21)} = 90.52 \angle -7.57^{\circ}$$

Rotor input per phase =
$$P_e = (90.52)^2 \frac{0.062}{0.02} = 25402.2 \text{ W}$$

Mech. power output per phase = $P_m = 25402.2 \times (1 - 0.02) = 24894 \text{ W}$

Output =
$$3 \times 24894 - 750 = 73932 \text{ W} = 99 \text{ h.p}$$

Input power =
$$\sqrt{3} \times 500 \times 103 \times 0.89 = 79465 \text{ W}$$

Efficiency =
$$\frac{73932}{79465}$$
 = 93%

4. Output= $50 \times 746 = 37300$ W. Input = 37300/0.9 = 41444 W. Total loss = 4144 W.

Let iron loss $=W_i$, Stator copper loss = Rotor copper loss $=W_c$

No load loss = Iron loss + Windage + Friction loss.

 $3 \times \text{Mech. losses} = W_i + \text{Mech loss. Therefore, Mech loss} = \frac{W_i}{2}$

 $Total\ loss = Stator\ Cu.\ loss + Rotor\ Cu.\ loss + Iron\ loss + Mech\ loss$

$$4144 = W_i + W_i + W_i + W_i/2$$

Therefore $W_i = 1184 \text{ W}$

Rotor input = Stator input - Stator Cu loss - Iron loss = 39076 W

% Slip =
$$\frac{\text{Rotor Cu loss}}{\text{Rotor Input}} = \frac{1184}{39076} \times 100 = 3.03\%$$

5. Synchronous speed = 1000 r.p.m. Slip = 0.05, $P_m = 30 \times 746 = 22350 \text{ W}$

Rotor Cu loss =
$$\frac{22380 \times 0.05}{1 - 0.05}$$
 = 1178 W

$$Input = \frac{22380}{1 - 0.05} + 2000 = 25.6kW$$

% Efficiency =
$$\frac{(30-2)\times746}{25600} \times 100 = 82\%$$

$$I_L = \frac{25600}{\sqrt{3} \times 550 \times 0.08} = 30.48 \text{ A}$$

Rotor frequency = $sf_s = 0.05 \times 50 \times 60 = 150$ cycles per min.

6. Rotor resistance referred to stator = $R'_r = 0.1 \times 1.75^2 = 0.306\Omega$

Rotor reactance referred to stator = $X'_r = 2.576\Omega$

Rotor current
$$I'_r = \frac{220/\sqrt{3}}{\sqrt{(\frac{0.306}{0.05})^2 + (2.576)^2}} = 18.72 \text{ A}$$

Total rotor input (airgap power) = $3I_r'^2 \frac{R_r'}{s} = 6574.3 \text{ W}$

Total torque = $T = \frac{P_2}{2\pi n_s}$ where $n_s = \frac{1500}{60}$ which gives T = 41.9 Nm

Rotor losses are not given, assume zero.

$$HP = \frac{6574 \times (1 - 0.05)}{746} = 8.37$$

Slip at max. torque = $\frac{R'_r}{X'_r} = 0.111$

Max torque =
$$\frac{3V_1^2}{4\pi n_s X_r'}$$
 = 56 Nm

Speed at max. torque = $N_s \times (1 - 0.111) = 1333$ rpm

7. $s = \frac{1000 - 975}{1000} = 0.025$. Rotor input = 40 - 1 = 39 kW.

Rotor Cu loss =
$$sP_2 = 0.025 \times 39 \times 10^3 = 975 \text{ W}$$

$$P_m = 39 \times (1 - 0.025) = 38.03 \text{ kW. Shaft HP} = \frac{38.03 - 2}{0.746} = 48.3$$

$$\%$$
 Efficiency = $\frac{36.025}{40} = 90\%$

8. $N_s = \frac{120 \times 50}{12} = 500 \text{ r.p.m.}$

Total resistance of the machine = $\frac{100 \times 10^3}{2 \times 250^2} = 0.53\Omega$

Rotor equivalent resistance = 0.27Ω

$$T = \frac{3I_r^{\prime 2}R_r^{\prime}}{2\pi N_s \times s}$$

Starting torque =
$$\frac{3I_r'^2R_r'}{2\pi N_s}$$
 = 955 Nm

9.
$$s_{max} = \frac{750 - 630}{750} = 0.16, s_{max} = \frac{R'_r}{X'_r}$$

$$X_r' = 0.4375\Omega$$
. s_{max} should be equal to 1 implies that $X_r' = R_r' + R_{ext}$

$$R_{ext} = 0.37\Omega$$

10. Core loss = 4.2 kW. No load p.f =
$$\frac{4200}{\sqrt{3} \times 460 \times 40}$$
 = 0.13

$$R_o = \frac{460/\sqrt{3}}{40 \times 0.13} = 51\Omega$$

$$X_m = R_o / \tan \theta = 6.7\Omega, R_{eq} = \frac{8 \times 10^3}{3 \times 140^2} = 0.136\Omega$$

$$Z_{eq} = \frac{100}{\sqrt{3} \times 140} = 0.412\Omega, X_{eq} = 0.389\Omega \text{ so } X'_r = 0.19\Omega$$

$$R_s = R'_r = 0.068\Omega$$
, $N_s = 900$ rpm, $s = \frac{900 - 873}{900} = 0.03$, $\frac{R'_r}{s} = 2.27\Omega$

$$Z_{eq} = [(2.27 + 0.068) + j0.389] ||\frac{j51 \times 6.7}{51 + j6.7} = 2.04 \angle 27^{\circ}$$

$$I_1 = \frac{460}{\sqrt{3} \times 2.04 \angle 27^{\circ}} = 130 \angle -27^{\circ} \text{ A}$$

Power input =
$$3 \times \frac{460}{\sqrt{3}} \times 130 \times \cos -27^{\circ} = 92.42 \text{ kW}$$

Stator Cu loss =
$$3 \times 130^2 \times 0.068 = 3458$$
 W, Air gap power = $92.42 - 3.458 - 4.2 = 3458$

84.76 kW

Rotor Cu loss =
$$84760 \times 0.03 = 2543 \text{ W}, P_m = 82217 \text{ W}$$

Power output =
$$82217 - 1000 = 81217 \text{ W}$$
.

$$\%$$
Efficiency = $\frac{81217}{92420}$ = 87.8%

11. Starting current taken from the supply with DOL =
$$\sqrt{3} \times \frac{500}{\sqrt{3}} = 248$$
 A Star-delta starting, phase voltage = $\frac{500}{\sqrt{3}}$, starting current = $\frac{289}{3.5} = 82.5$ A

12.
$$I'_r = \frac{230}{\sqrt{(\frac{1}{2})^2 + 1}}$$
, Total $P_m = \frac{3(1-s) \times 230^2 s^2}{s(1+s^2)}$

Total load torque =
$$33.68 \times \frac{N}{N_c}$$
 where $N = N_s(1-s)$

With mechanical loss neglected,
$$\frac{P_m}{2\pi N_s(1-s)/60}$$
 = Total load torque

Solving for s gives,
$$s = 0.063$$
 and $N = 3000(1 - s) = 2810$ rpm

13. kVA = 15, p.f =
$$0.6$$
, $\sin \phi = 0.8$

Real power =
$$9 \text{ kW}$$
, Reactive power = 12 kVAR

Improvement of power factor leaves
$$P$$
 unchanged. Q reduces to Q_1 .

Reduction in
$$Q = 12 - \frac{9 \times 0.6}{0.8} = 5.25$$
 kVAR

Per phase reduction in $Q = \frac{5.25}{3} = 1750$ VAR $\frac{V^2}{X_c} = 1750$ with V = 230V, value of C is 105μ F