

Analytical solutions for acoustic vortex beam radiation from planar and spherically focused circular pistons

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The University of Texas at Austin
Walker Department
of Mechanical Engineering
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Paraxial and ray approximations of acoustic vortex beams

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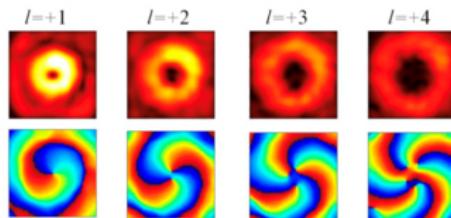
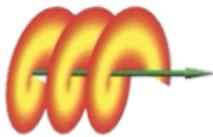
[Editor: Philip L. Marston] Pages: 2707–2723

J. Acoust. Soc. Am. **155** (4), April 2024 © 2024 Acoustical Society of America

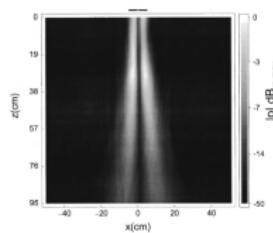
What is an acoustic vortex beam?

Characterized by...

- ▶ helical wavefronts
- ▶ orbital number ℓ = number of equiphase wavefronts in \perp plane
- ▶ zero acoustic pressure on axis



C. Shi et al. *P. Natl. Acad. Sci. U.S.A.* 114 (2017), pp. 7250–7253

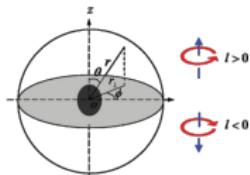


B. T. Hefner and P. L. Marston.
J. Acoust. Soc. Am. 106 (1999),
pp. 3313–3316

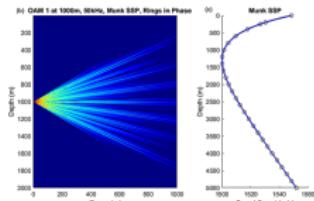
What is an acoustic vortex beam?

Used for...

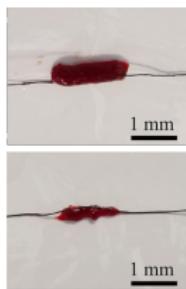
- ▶ particle manipulation
- ▶ underwater communications
- ▶ therapeutic biomedical ultrasound
- ▶ sound diffusion



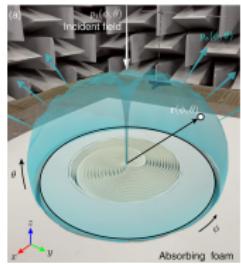
L. Zhang and
P. L. Marston.
Phys. Rev. E 84
(2011), pp. 1–5



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JASA Express Lett. 3
(2023), pp. 1–5



S. Guo et al.
Ultrasound Med. Biol.
48 (2022),
pp. 1907–1917



N. Jiménez,
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V. Romero-García.
Sci. Rep. 11 (2021),
pp. 1–13

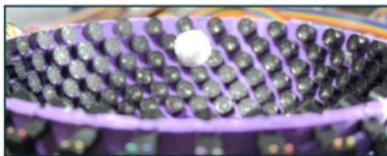
What is an acoustic vortex beam?

Generated by...

- ▶ phase plates
- ▶ transducer arrays
- ▶ metasurfaces



M. E. Terzi et al. *Moscow University Physics Bulletin* 72 (2017), pp. 61–67



A. Marzo, M. Caleap, and B. W. Drinkwater. *Phys. Rev. Lett.* 120 (2018), pp. 1–6



X. Jiang et al. *Phys. Rev. Lett.* 117 (2016), pp. 1–5

Previous analytical descriptions of vortex beams

- Bessel vortex beams are modes of the cylindrical wave equation:¹

$$p(r, \theta, z, t) = p_0 J_\ell(k_r r) e^{i(\ell\theta + k_z z - \omega t)}, \quad k = \frac{\omega}{c_0} = \sqrt{k_r^2 + k_z^2}. \quad (1)$$

- Gaussian vortex beams are generalizations of Gaussian beams:²

$$\begin{aligned} p(r, \theta, z, t) &= \sqrt{8\pi} \left(\frac{p_0 z}{kr^2} \right) \chi^{3/2} e^{-\chi} [I_{(\ell-1)/2}(\chi) - I_{(\ell+1)/2}(\chi)] \\ &\times e^{i[\ell\theta - (\ell+1)\pi/2 + kr^2/2z + k_z z - \omega t]}, \\ \chi(r, z) &= \frac{\frac{1}{8}(kar/z)^2}{1 - i(ka^2/2z)(1 - z/d)}. \end{aligned} \quad (2)$$

- Fields described by Eqs. (1) and (2) require infinite source conditions.
- Equation (1) implies infinite energy,³ because $\int_0^\infty |J_\ell(k_r r)|^2 r dr \rightarrow \infty$.
- **Objective: derive solutions for vortex fields radiated by circular pistons**

¹N. Jiménez et al. *Phys. Rev. E* 94 (2016), pp. 1–9.

²C. A. Gokani, M. R. Haberman, and M. F. Hamilton. *J. Acoust. Soc. Am.* 155 (2024), pp. 2707–2723.

³M. R. Lapointe. *Opt. Laser Technol.* 24 (1992), pp. 315–321.

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Paraxial equation and its integral solution

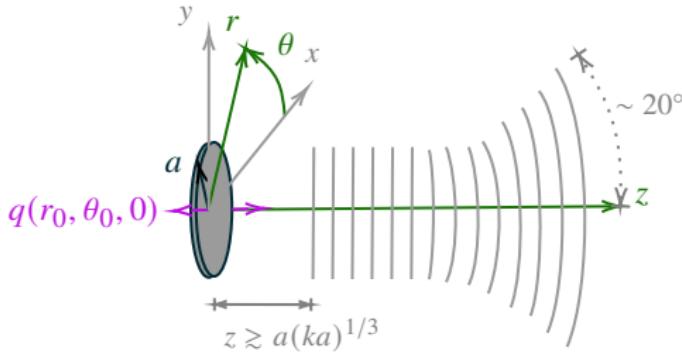
- For $p = qe^{i(kz - \omega t)}$ and $|\partial^2 q / \partial z^2| \ll 2k |\partial q / \partial z|$, $\nabla^2 p - c_0^{-2} \ddot{p} = 0$ reduces to

$$i2k \frac{\partial q}{\partial z} + \nabla_{\perp}^2 q = 0. \quad (3)$$

- ∇_{\perp}^2 is the Laplacian in the plane perpendicular to the z axis.
- Equation (3) is solved by the Fresnel diffraction integral:

$$q(r, \theta, z) = -\frac{ik}{2\pi z} \int_0^{2\pi} \int_0^{\infty} q(r_0, \theta_0, 0) e^{i(k/2z)[r^2 + r_0^2 - 2rr_0 \cos(\theta_0 - \theta)]} r_0 dr_0 d\theta_0,$$

where $q(r_0, \theta_0, 0)$ is the prescribed pressure field in the plane $z = 0$.



Vortex radiation from unfocused circular piston

- A circular **vortex** source condition is first considered:

$$q(r, \theta, 0) = p_0 \text{circ}(r/a) e^{i\ell\theta}, \quad (4)$$

where $\text{circ}(x) = 1$ for $0 \leq x \leq 1$ and 0 for $x > 1$.

- Insertion of Eq. (4) in the Fresnel diffraction integral leads to

$$q = -ikp_0 \frac{e^{i(ka^2/2z)r^2/a^2}}{z} e^{i\ell(\theta-\pi/2)} \int_0^a e^{i(ka^2/2z)r_0^2/a^2} J_\ell(krr_0/z) r_0 dr_0. \quad (5)$$

- Using Watson's relation,⁴ Eq. (5) reduces to

$$q = -\frac{ikp_0}{z} e^{i\ell(\theta-\pi/2)} \int_0^a J_\ell(krr_0/z) r_0 dr_0 \quad (6)$$

for $z \gg z_R$, where $z_R = ka^2/2$ is the Rayleigh distance.

⁴G. N. Watson. Cambridge, UK: Cambridge University Press, 1944, Sec. 2.2, Eq. (5).

Vortex radiation from unfocused circular piston

- Taking the integral in Eq. (6) leads to an analytical solution:

$$q_\ell(r, \theta, z) = -ip_0 \frac{z}{kr^2} e^{i\ell(\theta-\pi/2)} F_\ell(kar/z), \quad z \gg z_R, \quad (7)$$

where⁵

$$F_\ell(\xi) = \int_0^\xi J_\ell(t) t dt = \xi \frac{\Gamma(\ell/2 + 1)}{\Gamma(\ell/2)} \sum_{k=0}^{\infty} \frac{(\ell + 2k + 1)\Gamma(\ell/2 + k)}{\Gamma(\ell/2 + 2 + k)} J_{\ell+2k+1}(\xi). \quad (8)$$

- Equation (8) equals the following closed-form expressions for $1 \leq \ell \leq 4$:

$$F_0(\xi) = \xi J_1(\xi), \quad \ell = 0 \quad (9a)$$

$$F_1(\xi) = \frac{\pi}{2} \xi [\mathbf{H}_0(\xi) J_1(\xi) - \mathbf{H}_1(\xi) J_0(\xi)], \quad \ell = 1 \quad (9b)$$

$$F_2(\xi) = 2 - 2J_0(\xi) - \xi J_1(\xi), \quad \ell = 2 \quad (9c)$$

$$F_3(\xi) = \left[\frac{3\pi}{2} \xi \mathbf{H}_0(\xi) - 8 \right] J_1(\xi) + \left[4\xi - \frac{3\pi}{2} \xi \mathbf{H}_1(\xi) \right] J_0(\xi), \quad \ell = 3 \quad (9d)$$

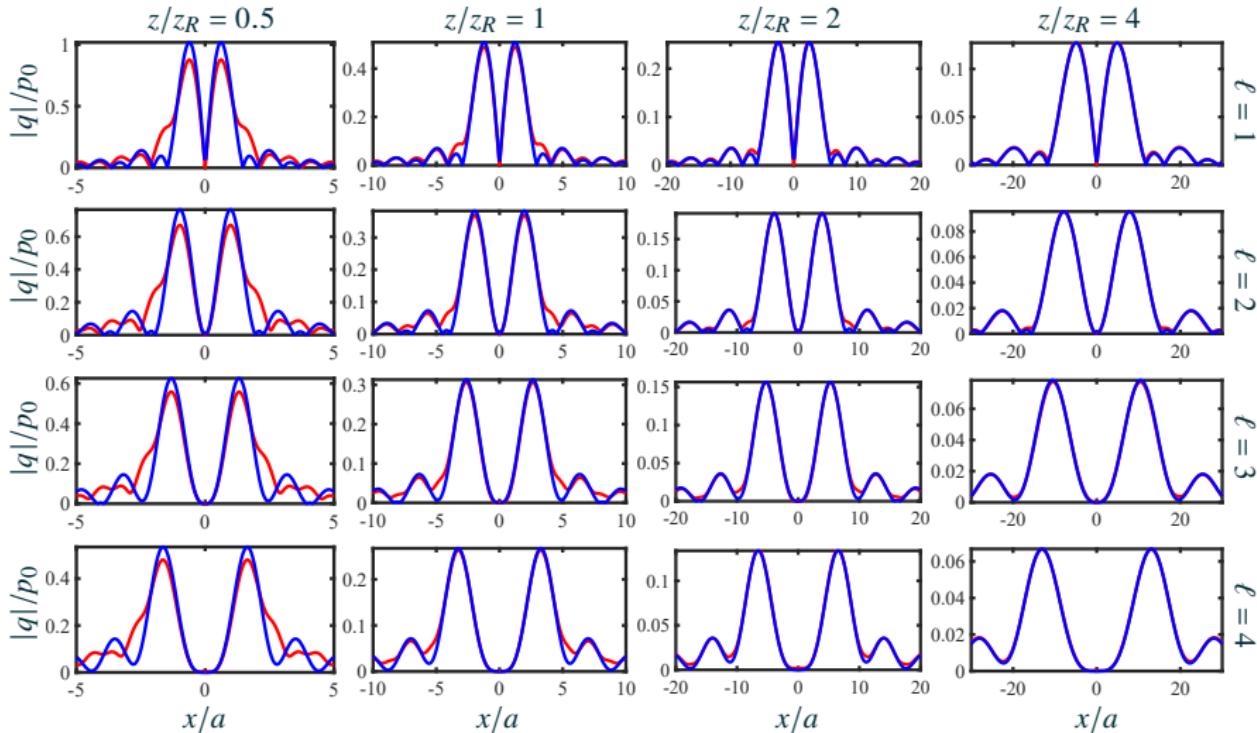
$$F_4(\xi) = 4 - 8J_1(\xi)/\xi - 4J_2(\xi) - \xi J_3(\xi). \quad \ell = 4 \quad (9e)$$

⁵M. Abramowitz and I. A. Stegun, editors. New York: Dover Publications, 1972, Item 11.1.1.

Verification of Eq. (7)

- The validity of Eq. (7) is assessed by comparison to

$$q(x, y, z) = \mathcal{F}_{xy}^{-1} \{ e^{ik_z z} \mathcal{F}_{xy} [q(x, y, 0)] \}, \quad k_z = k - (k_x^2 + k_y^2)/2k. \quad (10)$$



Vortex radiation from focused circular piston

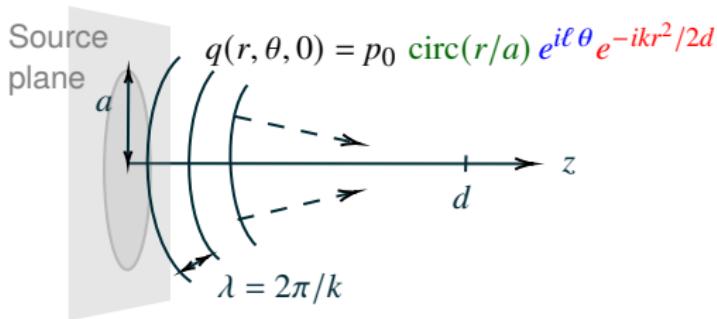
- To describe spherical focusing at a geometric focal length d , source condition (4) is multiplied by $\exp(-ikr^2/2d)$:

$$q(r, \theta, 0) = p_0 \text{ circ}(r/a) e^{i\ell\theta} e^{-ikr^2/2d}, \quad (11)$$

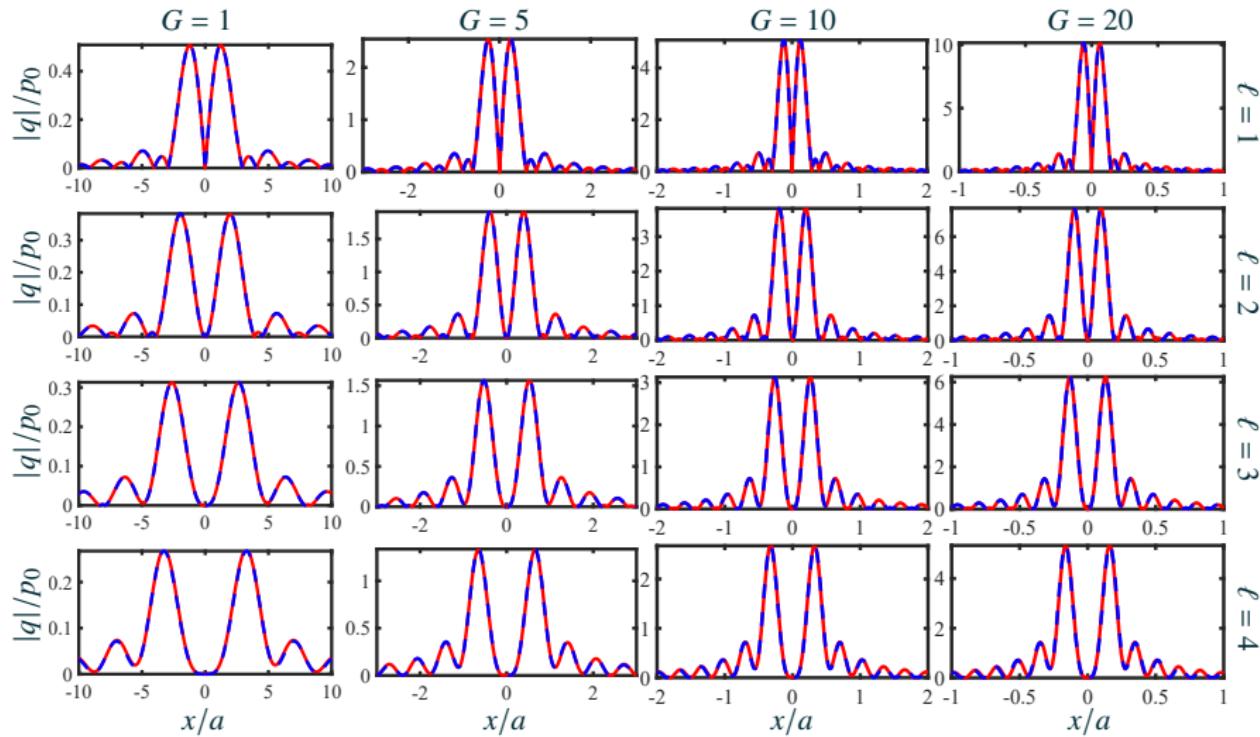
- An analytical solution of Eq. (3) is available at $z = d$:

$$q_\ell(r, \theta, d) = -ip_0 \frac{d}{kr^2} e^{ikr^2/2d} e^{i\ell(\theta-\pi/2)} F_\ell(kar/d), \quad (12)$$

where $F_\ell(\xi)$ is given by Eq. (8).



Verification of Eq. (12): analytical, Fourier



Outline

Introduction

Analytical solution of paraxial equation

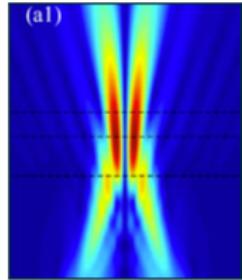
Vortex ring radius

Alternative approach to diffraction theory

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Vortex ring radius

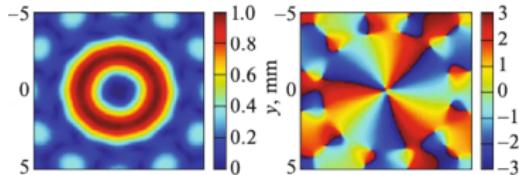
- ▶ The magnitudes of vortex beam fields are axisymmetric.
- ▶ In the far field of Eq. (7), the field is conical.
- ▶ In the geometric focal plane $z = d$ of Eq. (12), the field forms toroidal ring.
- ▶ Equations (7) and (12) can be used to find the radius of these features.



C. Zhou et al. *J. Appl. Phys.* 128 (2020), pp. 1–12



D. Baresch, J. -L. Thomas, and R. Marchiano. *Phys. Rev. Lett.* 116 (2016), pp. 1–6



M. E. Terzi et al. *Moscow University Physics Bulletin* 72 (2017), pp. 61–67

Vortex ring radius

- ▶ Maximizing Eqs. (7) and (12) in r amounts to solving

$$\frac{d|\xi^{-1}F_\ell(\xi)|}{d\xi} = 0,$$

where $\xi = kar/z$ (unfocused) and $\xi = kar/d$ (focused).

- ▶ Using Eq. (8) for F_ℓ and taking the derivative yields⁶

$$\sum_{k=0}^{\infty} \frac{(\ell+2k+1)\Gamma(\ell/2+k)}{\Gamma(\ell/2+2+k)} \left[\frac{J_{\ell+2k}(\xi) - J_{\ell+2k+2}(\xi)}{2\xi} - \frac{J_{\ell+2k+1}(\xi)}{\xi^2} \right] = 0. \quad (13)$$

- ▶ The roots ξ_ℓ of Eq. (13) are fit to a line: $\xi_\ell = 1.23\ell + 1.49$.
- ▶ Solving $\xi_\ell = kar_\ell/z$ and $\xi_\ell = kar_\ell/d$ for r_ℓ yields

$$r_\ell = \frac{\xi_\ell z}{ka}, \quad z \gg z_R, \quad (14a)$$

$$= \frac{\xi_\ell d}{ka}, \quad z = d. \quad (14b)$$

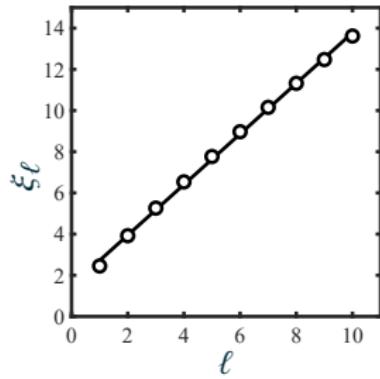
⁶I. S. Gradshteyn and I. M. Ryzhik. New York: Academic Press, 1980, Item 8.471-2.

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General Topics in Physical Acoustics: 5pPAA3

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Vortex ring radius



Comparison of roots ξ_ℓ (circles) with least-squares fit $\xi_\ell = 1.23\ell + 1.49$ (line)

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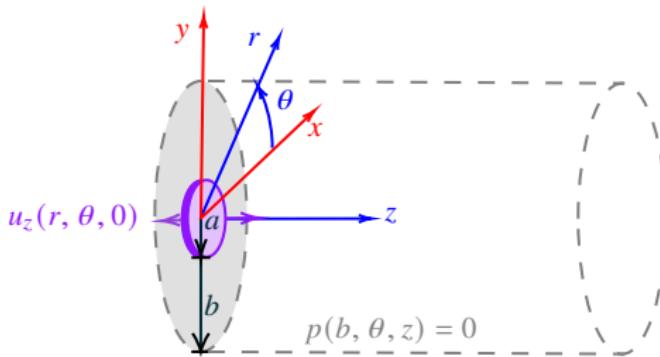
Alternative approach to diffraction theory

- The Rayleigh integral

$$p(\mathbf{r}) = -\frac{ik\rho_0 c_0}{2\pi} \int_{A_0} u_z(\mathbf{r}_0) \frac{e^{ik|\mathbf{r}-\mathbf{r}_0|}}{|\mathbf{r}-\mathbf{r}_0|} dA_0 \quad (15)$$

is the starting-point for the study of diffraction from circular pistons.

- Equation (15) is traditionally derived from the Helmholtz-Kirchhoff integral.⁷
- Consider a piston placed concentrically within a tube of radius b .



⁷A. D. Pierce. Cham, Switzerland: Springer, 2019, Eqs. (5.2.6) and (5.7.3).

Alternative approach to diffraction theory

- The solution of the Helmholtz equation for that scenario is

$$p(r, \theta, z) = \sum_{n=1}^{\infty} A_{\ell n} J_{\ell}(\alpha_{\ell n} r/b) e^{i(\ell \theta + \beta_{\ell n} z)}, \quad (16a)$$

$$A_{\ell n} = \frac{2k\rho_0 c_0 u_0}{\alpha_{\ell n}^2 \beta_{\ell n}} \frac{F_{\ell}(\alpha_{\ell n} a/b)}{J_{\ell+1}^2(\alpha_{\ell n})}, \quad \beta_{\ell n} = \sqrt{k^2 - k_r^2}, \quad k_r = \alpha_{\ell n}/b, \quad (16b)$$

where $\alpha_{\ell n}$ is the n^{th} root of J_{ℓ} .

- The ratio $\alpha_{\ell n}/b$ is vanishingly small except for large n , for which⁸

$$\alpha_{\ell n} \approx \pi(n - 1/4 + \ell/2), \quad n \gg 1. \quad (17)$$

- Defining $\zeta = \alpha_{\ell n} a/b \approx \frac{a}{b}\pi(n - 1/4 + \ell/2)$ for $n \gg 1$ sets $\Delta\zeta = \pi a/b$:

$$p = \rho_0 c_0 u_0 e^{i\ell\theta} \sum_{n=1}^{\infty} \frac{\Delta\zeta}{\zeta} \frac{F_{\ell}(\zeta) J_{\ell}(\zeta r/a)}{\sqrt{1 - (\zeta/ka)^2}} e^{ikz\sqrt{1 - (\zeta/ka)^2}}. \quad (18)$$

- As $b \rightarrow \infty$, Eq. (18) tends to

$$p = \rho_0 c_0 u_0 e^{i\ell\theta} \int_0^{\infty} \frac{F_{\ell}(\zeta) J_{\ell}(\zeta r/a)}{\zeta \sqrt{1 - (\zeta/ka)^2}} e^{ikz\sqrt{1 - (\zeta/ka)^2}} d\zeta. \quad (19)$$

⁸I. S. Gradshteyn and I. M. Ryzhik. New York: Academic Press, 1980, Eq. (8.547).

Alternative approach to diffraction theory

- ▶ Using Watson's relation⁹ and the 2D Fourier transforms

$$\mathcal{F}_{2D}\{f(r, \theta)\} = g(k_r, \psi) = \int_0^{2\pi} \int_0^{\infty} f(r, \theta) e^{-ik_r r \cos(\theta - \psi)} r dr d\theta, \quad (20a)$$

$$\mathcal{F}_{2D}^{-1}\{g(k_r, \psi)\} = f(r, \theta) = \int_0^{2\pi} \int_0^{\infty} g(k_r, \psi) e^{ik_r r \cos(\theta - \psi)} k_r dk_r d\psi, \quad (20b)$$

Eq. (19) recovers the angular spectrum method,

$$p(r, \theta, z) = \rho_0 c_0 k \mathcal{F}_{2D}^{-1}\{\mathcal{F}_{2D}\{u_z(r, \theta)\} e^{ik_z z} / k_z\}. \quad (21)$$

- ▶ Noting that $\mathcal{F}_{2D}\{e^{ikr}/r\} = i2\pi e^{ik_z|z|}/k_z$,¹⁰ where $r = \sqrt{x^2 + y^2 + z^2}$, Eq. (21) reduces to

$$p = -\frac{ik\rho_0 c_0}{2\pi} u(x, y) \ast \ast \frac{e^{ikr}}{r}. \quad (22)$$

- ▶ By the definition of the convolution operation, Eq. (22) recovers Eq. (15).

⁹G. N. Watson. Cambridge, UK: Cambridge University Press, 1944, Sec. 2.2, Eq. (5).

¹⁰L. T. Brekhovskikh, translated by R. T. Beyer. Academic Press, 1980, pp. 227–234.

Outline

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Thank you for listening!

Summary

- ▶ Solved paraxial equation for planar and focused circular vortex sources
- ▶ Calculated the ring radius for both solutions
- ▶ Derived alternative theory of diffraction from circular pistons

Further reading

- ▶ “Paraxial and ray approximations of acoustic vortex beams,”
J. Acoust. Soc. Am. **155**, 2707–2723 (2024).
- ▶ “Analytical solutions for acoustic vortex beam radiation from planar and spherically focused circular pistons,” JASA Express Lett. **4**, 124001 (2024).

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Notation I

Symbol	Description	Dimensions
a	source radius	m
c_0	speed of sound	m s^{-1}
d	focal length	m
G	focusing gain $ka^2/2d$	1
i	complex unit	1
\mathbf{k}	wavenumber	m^{-1}
ℓ	orbital number	1
ρ_0	ambient mass density	kg m^{-3}
p	acoustic pressure	$\text{kg m}^{-1} \text{s}^{-2}$
q	paraxial pressure	$\text{kg m}^{-1} \text{s}^{-2}$
\mathbf{R}	separation vector $\mathbf{R} = \mathbf{r} - \mathbf{r}'$	m
\mathbf{r}	position vector	m
\mathbf{v}	particle velocity	m s^{-1}
z_R	Rayleigh distance, $ka^2/2$	m
ω	angular frequency, $\omega = 2\pi f$	s^{-1}

Dimensionless form of Eq. (19)

- ▶ In terms of the dimensionless parameters

$$P \equiv p/\rho_0 c_0 u_0, \quad R \equiv r/a, \quad Z \equiv z/z_R, \quad K \equiv ka, \quad (23)$$

where z_R is the Rayleigh distance $ka^2/2$, and where

$$k_z/k = \sqrt{1 - (\zeta/K)^2}, \quad \zeta \equiv k_r a, \quad (24)$$

Eq. (19) becomes

$$P = e^{i\ell\theta} \int_0^\infty \frac{F_\ell(\zeta) J_\ell(\zeta R)}{\zeta \sqrt{1 - (\zeta/K)^2}} e^{iK^2 Z \sqrt{1 - (\zeta/K)^2}/2} d\zeta. \quad (25)$$

- ▶ Equation (25) is equivalent to and easier to evaluate than Eq. (21).

On-axis pressure of baffled circular piston

- Equation (25) can be evaluated analytically for $R = \ell = 0$:

$$P(Z) = \int_0^{\infty} \frac{J_1(\zeta)}{\sqrt{1 - (\zeta/K)^2}} e^{iK^2 Z \sqrt{1 - (\zeta/K)^2}/2} d\zeta. \quad (26)$$

- Equation (26) evaluates to¹¹

$$P(Z) = -iK I_{1/2}[-i\chi_-(Z)] K_{1/2}[-i\chi_+(Z)], \quad (27)$$

where I_ν and K_ν are the modified Bessel functions of order ν , and where

$$\chi_{\pm}(Z) = \frac{K}{2} \left[\sqrt{1 + (KZ/2)^2} \pm KZ/2 \right]. \quad (28)$$

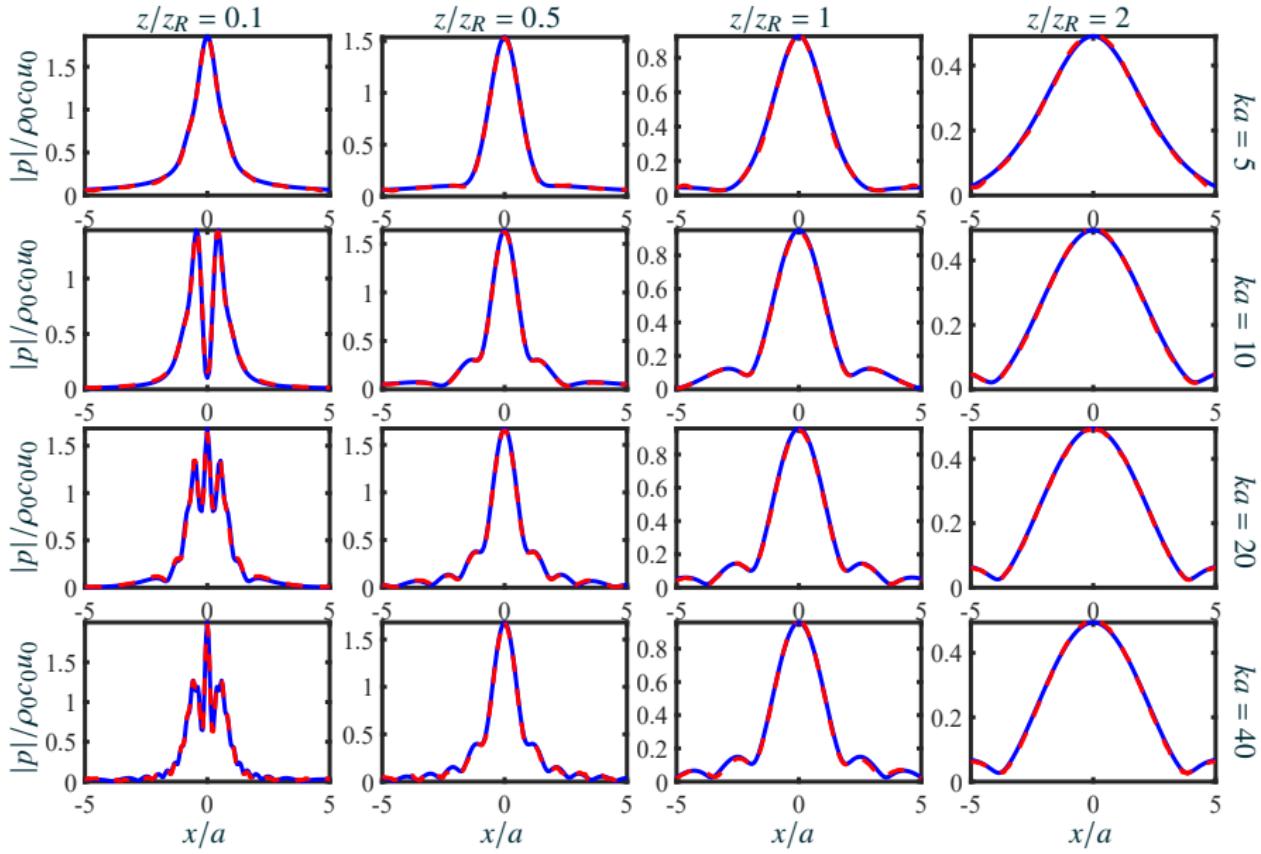
- Bessel function identities reduce Eq. (27) to

$$P(Z) = -2i \sin[\chi_-(Z)] e^{i\chi_+(Z)}, \quad (29)$$

recovering the on-axis pressure radiated by a planar circular piston.¹²

¹¹I. S. Gradshteyn and I. M. Ryzhik. New York: Academic Press, 1980, Item 6.637-1.

¹²A. D. Pierce. Cham, Switzerland: Springer, 2019, Eq. (5.7.3).

Equation (25) for $\ell = 0$: semi-analytical, Fourier

Equation (25) for $\ell = 1$: semi-analytical, Fourier