I rusured of labor c) catisfied Normal Mode Expansion of 6 Let V be enclosed by locally reacting surfaces. Then the eigenfus satisfying V2 4n(F) + leu 4n(F) = 0 where N=(liw,N) in 3D, are orthogonal: 111 tn(2)tn/2)dV = VNn&nn1 (5) Green's for satisfies (72+165) B(5/15) =- 8(5-15) Tet

G(F|Fo) = ZANYN(F)

-1... Z (-k2+k2) Autu(F) =-8(F-F2) (4) Take III (4) Yn/(F) dV and use (2): (- lei+ lez) AuV Nn = - 4, (Po) $Au = \frac{4u(\vec{r}_0)}{VNu(k\vec{u}-k^2)}$ $G(\vec{r}|\vec{r}_0) = \sqrt{2} \frac{4u(\vec{r}_0)4u(\vec{r}_0)}{Nu(k\vec{u}-k^2)} = G(\vec{r}_0|\vec{r}_0)$ (5) MFI (9.5.14) V for next. ter snuple some with vol. vel. Q

PW(F(Fe) = -ikpolo QG(F(Fe))

=ikpolo V Z 4u(F)4u(Fo)

=ikpolo V Z 11/162-1621

maybe as howeverted (M1), p. 500) Example Rectangulær Rossus (LXWXH)
For regid walls Lemn (x1912) = WS ETTX COS WITY COS MT12 Remn = Weun = T /(2)2+(W)2+(H)2 News = Zezwzn , zn=1, 1=0 = z, 1>0 (l, w, u) = (0,0,1), (0,1,0), etc. Damping is important when $\omega \simeq \omega_n$. Consider sniple harmorin oscillativ: $X + \frac{1}{7}X + W_0^2X = 0$ Tet X=Aest: 57+本5+W3=0 (7) Eigenvolues: = - = = = = = [- (ZWoT)2 = - = + i = 1 (2001)2-1, underdamped ~- == i wo, lightly damped [12004)2>>1]

So for light damping X=Ae-t/zre±1wot 1X12 = Ae-t/r

7 = exponential decay time for system evergy

For ferred response set $S=-i\omega$ on LHS of (9): $S^{2}+\frac{1}{T}S+\omega\delta^{2}=-\omega^{2}-\frac{i\omega}{T}+\omega\delta^{2}$ $=-(\omega^{2}-\omega\delta^{2}+i\omega/T)$ Thus write $R^{2}-R^{2}=\frac{1}{C^{2}}(\omega^{2}-\omega^{2})$

whose $T_N = decay time fry meder$

Thus for hard walls (121>) to(0) with light damping [(2wn71)2>>1]

~ POCO VNu Yn(F) fulFo), W=Wu

Note that quality factor of neodo 1 is On=Wn Ty- (Maybe use OF to distinguish from well)