Appendices

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I - Troubleshooting

During troubleshooting, experience plays an important factor. In the event there is a problem that you cannot solve, seek help. Do not sacrifice production or quality; ask. This list is only a reference; use it judiciously.

Brittle Parts - The parts become brittle or break

Possible Causes	Actions
1. Resin is too cold	1.a. Increase backpressure.
	1.b. Increase melt temperature.
2. Material degradation in the barrel	2.a. Reduce melt temperature.
	2.b. Reduce backpressure.
	2.c. Reduce the injection rate.
	2.d. Purge, if necessary.
3. Material contamination	3.a. Verify material in the hopper.
	3.b. Purge, if necessary.
4. Material degradation during the	4. Decrease dryer time and/or
drying process	temperature.
5. Moisture in the material	5. Verify moisture content, dry
	properly.

Bubbles (voids) - Air trapped inside the part

Possible Causes	Actions
1. Moisture in the material	1. Check moisture content, dry properly.
2. Material is too hot	Decrease the melt temperature by adjusting to a suitable barrel temperature profile.
3. Inadequate venting	3. Ensure that the mold has adequate and clean vents.
4. Internal bubbles caused by shrinkage	4.a. Increase backpressure and/or hold pressure.4.b. Decrease the melt temperature.

Weld line - Lines on the part formed by two or more melt flows joining together

Possible Causes	Actions
1. Low mold temperature	1. Increase mold temperature.
2. Material is too cold	2. Increase melt temperature.
3. Low injection rate	3. Increase speed. Injection time
	should be significantly reduced.
4. Humid resin	4. Dry material properly.

Fading - Inadequate color

Possible Causes	Actions
1. Degraded material in the barrel	1. Purge the barrel.
2. High melt temperature	2. Decrease melt temperature by adjusting to a suitable barrel temperature profile.
3. Contaminated material	3. Check the material.
4. Inadequate vents	4. Clean existing vents or ventilate mold properly.

Burns - Marks on the part due to degradation

builds marks on the part due to degradation	
Possible Causes	Actions
1. High injection speed	1. Decrease injection speed.
2. High backpressure	2. Decrease backpressure.
3. Inadequate vents	3.a. Verify that there are vents.
	3.b. Clean vents.
4. Problems in mold design (material	4.a. Change the location of the gate.
suffers friction, causing degradation)	4.b. Ensure that the part has
	generous radii (no sharp
	corners).
5. Nozzle hole is too small or clogged	5. Replace or clean the nozzle.
6. High screw recovery	6. Decrease screw recovery speed.
7. High melt temperature	7. Decrease the melt temperature by
	adjusting to a suitable barrel
	temperature profile.

Buckling - Twisting or curving of the parts due to uneven shrinkage

Possible Causes	Actions
1. Hot parts upon ejection	1.a. Lower the mold temperature.
	1.b. Increase the cooling time.
2. Uneven part cooling	2. Adjust the temperatures of the
	mold faces.
3. Non-uniform wall thickness	3. Redesign the part.
4. Parts are overpacked	4. Decrease the hold pressure.

Cloudiness - Cloudy appearance in parts (more noticeable in clear

parts)

Possible Causes	Actions
1. Material contamination	1.a. Check material and change if
	necessary.
	1.b. Increase melt temperature.
2. Gases or moisture in the resin	2.a. Dry material properly.
	2.b. Ventilate mold properly.
3. Material is too cold	3. Increase the melt temperature.
4. Mold is too cold	4. Increase mold temperatures.
5. Mold release	5. Eliminate the use of mold release.

Flash - Excess plastic around the parting line

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Possible Causes	Actions
1. High hold pressure	1. Decrease hold pressure.
2. Mold is too hot	2. Lower mold temperatures.
3. Inadequate closing force	3. Increase tonnage.
4. High melt temperature	4. Lower the melt temperature.
5. Late transfer position to hold	5. Adjust to an appropriate transfer position and compensate by adjusting the same distance to the recovery position.
6. Material with moisture	6. Improve drying.

Flow lines - Marks in the direction of the melt flow

Possible Causes	Actions
1. Low mold temperature	1. Increase the mold temperature.
2. Material is too cold	2. Increase the melt temperature.
3. Inadequate runner/gate	3. Check the size of runner and gates,
	and request a redesign.
4. High injection speed	4. Decrease injection rate.
5. Humid resin	5. Dry material properly.

Worm-shaped jetting on the surface of the parts

worm shaped jetting on the surface of the parts	
Possible Causes	Actions
1. Gates too small	1. Verify and request a gate
	redesign.
2. Poorly localized gate	2. Request a redesign.
3. Injection speed too high	3. Slow down the injection rate.
4. Small nozzle hole	4. Replace nozzle.

Surface delamination – Layer separation on the surface of the pieces

Possible Causes	Actions
1. Contaminated material	1. Check the material and replace, if
	necessary.
2. Low melt temperature	2. Adjust to a suitable barrel
	temperature profile.
3. Melt mixture is not uniform	3. Increase backpressure.
4. Low mold temperature	4. Increase mold temperature.
5. Low injection rate	5. Increase speed. Injection time
	should be significantly reduced.

Incomplete Shot - Parts are not completely filled

Possible Causes	Actions
1. Low hold pressure	1. Increase hold pressure.
2. Short hold time	2. Increase hold time.
3. Unbalanced cavities	3. Balance the fill and redesign the mold, if
	necessary.
4. Low melt temperature	4. Increase the melt temperature by
	adjusting to an appropriate temperature
	profile.
5. Small runners/gates	5. Request a redesign of runners and/or
	gates.
6. Low mold temperature	6. Increase mold temperature.
7. Low recovery position	7. Verify that the transfer position is
	adequate, and then increase the recovery
	position.

Silver lines - Imperfections on the surface of the parts

Possible Causes	Actions
1. Moisture in the resin	1. Dry the material properly.
2. Obstruction in the nozzle	2. Clean the nozzle.
3. High injection speed	3. Slow down the injection rate.
4. High melt temperature	4. Lower the melt temperature with an appropriate barrel temperature profile.
5. Nozzle is too hot	5. Lower nozzle temperature.
6. Contaminated resin	6. Check the material; replace it if necessary.
7. Gates are too small	7. Increase gate size.

Sink - Depressions or sunken areas in sections of the parts

sink bepressions of sunken areas in sections of the parts		
Possible Causes	Actions	
1. Low injection rate	1. Increase speed. Injection time	
	should be significantly reduced.	
2. Inadequate design of the mold and/or	2. Redesign part (uniform wall	
part	thicknesses are required).	
3. Low melt temperature	3. Increase melt temperature with a	
	suitable temperature profile.	
4. Gas trapped in the mold	4. Vent the mold properly.	
5. Low hold pressure	5. Increase hold pressure.	
6. Excessive mold temperature causes	6. Lower the temperature of the	
shrinkage	mold.	
7. Low hold time	7. Increase hold time.	
8. Low mold temperature causing	8. Increase the temperature of the	
premature gate freezes	mold.	

The parts stick to the cavity

The parts stick to the cavity	
Possible Causes	Actions
1. Scratched cavity	1. Polish in the direction of
	demolding.
2. Static	2. Demagnetize the cavity.
3. High hold pressure	3. Decrease the hold pressure.
4. Short cooling time	4. Increase cooling time.
5. Shrinking in the wrong direction	5. Set the temperature of the core so
	it is higher than the cavity
	temperature.
6. Insufficient draft and/or detachment	6. Consider changes in part and/or
angle	mold design.

The parts stick to the core

Possible Causes	Actions
1. High hold pressure	1. Decrease the hold pressure.
2. High core temperature	2. Adjust the mold temperatures.
3. High melt temperature	3. Lower the melt temperature with a
	suitable temperature profile.
4. Insufficient draft and/or detachment	4. Consider changes in part and/or
angle	mold design.
5. Static	5. Demagnetize the cavity.

II - Universal Mold Data

Remember that these parameters are for the mold and the plastic. To be used they must be transferred or converted into injection machine parameters.

- 1. Mold name and number.
- 2. Name and type of material.
- 3. Filling time to get a fill of about 95%.
- 4. Weight of the parts at the time of transfer, with the hold turned off.
- 5. Plastic pressure at the time of transfer.
- 6. Total cycle time.
- 7. Hold time.
- 8. Hold pressure.
- 9. Total weight or total injection volume.
- 10. Cooling time.
- 11. Mold temperatures.
- 12. Flow and water to the mold.
- 13. Water temperatures entering the mold.
- 14. Water temperatures exiting the mold.
- 15. Water pressures entering the mold.
- 16. Water pressures exiting the mold.
- 17. Melt temperature entering the mold.
- 18. Time it takes to open the mold and eject the parts.
- 19. Time to completely close the mold.
- 20. Recovery volume.

III - General Procedures for $Universal\ Molding^{TM}$

I. Sizi	ng and Initial Data	
	Determine the clamping force →	
	Determine the required injection volume →	
3.	Select an approximated total cycle →	
4.	Determine the approximated resin consumption per hour -	
5.	Resin brand and type →	
6.	Colorant brand and type \rightarrow	
7.	Colorant % →	
8.	Regrind % →	
II. Au	xiliary Equipment	
1.	Water temperature control unit	
	Determine the water flow to the mold \rightarrow	
	Select an initial water temperature →	
2.	Dryer	
	Size the hopper dryer volume \rightarrow	
	Size the dry air flow \rightarrow	
	Drying temperature →	
3.	Colorant additive	
	% colorant required →	
	Determine the consumption of colorant/hour →	
4.	Regrind additive	
	% regrind required →	
	Determine the consumption of regrind/hour →	
	old and Machine Sizing	
1.	Horizontal distance →< between bars	
2.	Vertical distance →< between bars	
3.	. Closed distance → > minimum opening	
4.	. Open distance →< maximum opening	
5.	Ejector pattern \rightarrow =	
IV. In	jection Molding Machine Sizing	
1.	Injection unit	
	Determine % of Utilization, $U_{\%} \rightarrow$	
	Determine the transfer position \rightarrow	

	Determine the corresponding temperature profile \rightarrow
	Determine the backpressure. Ex: 750 psi plastic (machine =
	plastic/R _i)
2	Determine the approximated plasticizing position →
2.	Nozzle tip
	Length → Hole diameter →
	Hole diameter →
	Contact radius →
3.	Sprue bushing
	Hole diameter →
	Contact radius →
V. Init	tial process setup
	Start and set the auxiliary equipment parameters
	Dryer
	Water temperature controller
	Additive feeder
	Hot runner temperature control
2.	Injection unit
	Start and set the barrel temperature zones
	Set the backpressure
	Set the recovery speed
	Set the approximated recovery position
	Set the extended cooling time
3	Press setup
٥.	Set mold opening positions and speeds
	Set the mold protection
	Set the movements of the ejectors
	Set the movements of the cores, if applicable
T/I D	
	etermination of Machine Parameters
	the auxiliary equipment is ready and temperatures have been
reache	,
1.	Fill
	Determine the injection pressure limit →
	Determine the ideal injection time \rightarrow
	Readjust the injection volume to about 95%
	Note the final recovery position \rightarrow
	Perform the flow balance lab

2.	Hold
	Determine the hold pressure →
	Determine the hold time →
3.	Cooling
	Determine the water temperature of the mold →
	Fixed/Moving →/
	Determine the cooling time \rightarrow
4.	Recovery
	Adjust the recovery speed according to the new cooling time
	Note the recovery time →
5.	Recalculate the auxiliary equipment according to the new cycle
	time
VII (Convert to Universal Parameters
	ary Equipment
1.	Water temperature control (gpm/lpm) to mold → Water temperatures to mold Fixed/Movable →/
	Dryer
2.	<i>Hopper volume</i> →
	D
	Dry air flow \rightarrow Drying temperature \rightarrow
3	Additive feeder, % of colorant >
5.	Color consumption per hour \rightarrow
4	Regrind ratio, % →
,,	Regrind consumption per hour \rightarrow
Mold	Doto
	<u>Data</u> Horizontal distance →
	Vertical distance →
	Closed mold height →
	Open mold height →
	Ejector pattern \rightarrow
<i>7</i> .	Material → Color additive →
.	
	on Molding Machine – (m) machine / (u) Universal
	Clamping force →
	Total cycle time →
	Material consumption per hour →
4.	Press platens

	Horizontal distance between tie bars →
	Vertical distance between tie bars →
	Verify the ejectors pattern \rightarrow
	Maximum opening \rightarrow
	Minimum opening →
5.	• •
	Mold opening position →
	Mold opening and closing time →
6.	Injection
	% of barrel utilization →
	Injection pressure limit \rightarrow (m) (u)
	Ideal injection velocity \rightarrow (m)(u)
	Transfer position \rightarrow (m) (u)
	Recovery position \rightarrow (m) (u)
	Temperature profile \rightarrow //
7.	Hold
	Hold pressure \rightarrow (m) (u)
	Hold time →
8.	
	Water temperature of the mold Fixed/Movable →
	Cooling time →
9.	Recovery
	Recovery speed →
	Recovery time →
	Backpressure \rightarrow (m) (u)

IV – English terms in Spanish

- English terms in Spanish		
auger	tornillo sin fin	
backpressure	contrapresión	
barrel	barril	
barrier screw	tornillo con barrera	
blower	bomba	
boost to hold	de inyección a empaque	
cavity	cavidad	
check ring	anilla	
chiller	equipo de refrigeración	
cold slugs	pedazos fríos	
cores	noyos	
cushion	colchón	
dew point	temperatura de condensación/	
	temperatura de rocío	
discharge factor	densidad de plastificación	
drying hopper	tolva de secado	
eject-on-the-fly	expulsión mientras el molde	
	abre	
ejector pins	botadores	
ejector plates	platos de expulsión	
fill time	tiempo de inyección	
flash	rebaba	
gate	bebedero	
gate freeze	endurecimiento de bebederos	
hold	empaque	
hold pressure	presión de empaque	
hold time	tiempo de empaque	
hot runner	colada caliente	
hot drop/hot tip	punta caliente	
injection rate	flujo de llenado	
injection screw	tornillo de inyección	
injection speed	velocidad de llenado	
jetting	chorreo	
manifold	distribuidor	
melt flow	flujo del fundido	
melt flow number	índice de fluidez	
melt pressure	presión del fundido	
melt temperature	temperatura del fundido	

mold protect	protección del cierre del
	molde
molecular weight	peso molecular
nozzle	boquilla
nozzle tip	punta de la boquilla
pack and hold	empaque y sostén
packing pressure	presión de empaque
packing time	tiempo de empaque
parting line	partición del molde
pellet	gránulo
plastic residence time	tiempo de residencia
plasticizing/recovery	plastificación
robot	brazo mecánico
runners	coladas
shear rate	cambio cortante/
	velocidad cambiante
shear stress	esfuerzo cortante
shear thinning	licuar por fricción
shot size	volumen de llenado/volumen
	de la unidad de inyección
sprue	palo
sprue bushing	casquillo
stack mold	molde doble
stress	esfuerzo
suck-back	rechupe
tie bars	máquina con barras
tiebarless	máquina sin barras
transfer point	posición de transferencia
transfer pressure	presión de transferencia
valve gate	válvulas de bebederos
vents	ventosas

V - Spanish terms in English

anilla barril barrel bebedero gate bomba blower boquilla nozzle botadores ejector pins brazo mecánico robot cambio cortante/ velocidad cambiante casquillo sprue bushing cavidad cavity chorreo jetting colada caliente hot runner coladas runners colchón cushion contrapresión backpressure de inyección a empaque boost to hold densidad de plastificación discharge factor distribuidor manifold empaque y sostén pack and hold empaque y sostén pack and hold endurecimiento de bebederos equipo de refrigeración chiller esfuerzo stress expulsión mientras el molde abre flujo del llenado injection rate flujo del fundido melt flow gránulo pellet índice de fluidez melt flow number licuar por fricción shear thinning máquina con barras tiebars máquina sin barras tiebarless molde doble stack mold noyos cores palo parting line	- Spanish terms in English	
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de inyección a empaque boost to hold densidad de plastificación discharge factor distribuidor manifold empaque hold empaque hold empaque y sostén pack and hold endurecimiento de bebederos equipo de refrigeración chiller esfuerzo stress esfuerzo cortante shear stress expulsión mientras el molde abre flujo de llenado injection rate flujo del fundido melt flow gránulo pellet índice de fluidez melt flow number licuar por fricción shear thinning máquina con barras tiebarless molde doble noyos cores palo	colchón	cushion
densidad de plastificación distribuidor empaque empaque y sostén endurecimiento de bebederos equipo de refrigeración esfuerzo stress esfuerzo cortante expulsión mientras el molde abre flujo de llenado injection rate flujo del fundido gránulo gránulo pellet índice de fluidez melt flow number licuar por fricción shear thinning máquina con barras máquina sin barras tiebarless molde doble noyos palo discharge factor manifold hold expands del hold gate freeze equipo de refrigeración shear stress eject-on-the-fly eject-on-the-fly melt flow gránulo pellet findice de fluidez melt flow number licuar por fricción shear thinning máquina con barras tie bars máquina sin barras tiebarless molde doble stack mold noyos palo		backpressure
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molde doble stack mold noyos cores palo sprue	máquina con barras	tie bars
noyos cores palo sprue	máquina sin barras	tiebarless
palo sprue	molde doble	stack mold
•	noyos	cores
partición del molde parting line	palo	sprue
	partición del molde	parting line

1 67	11 1
pedazos fríos	cold slugs
peso molecular	molecular weight
plastificación	plasticizing/recovery
platos de expulsión	ejector plates
posición de transferencia	transfer point
presión de empaque	hold pressure
presión de empaque	packing pressure
presión de transferencia	transfer pressure
presión del fundido	melt pressure
protección del cierre del	mold protect
molde	_
punta caliente	hot drop/hot tip
punta de la boquilla	nozzle tip
rebaba	flash
rechupe	suck-back
temperatura de condensación/	dew point
temperatura de rocío	
temperatura del fundido	melt temperature
tiempo de empaque	hold time
tiempo de empaque	packing time
tiempo de inyección	fill time
tiempo de residencia	plastic residence time
tolva de secado	drying hopper
tornillo con barrera	barrier screw
tornillo de inyección	injection screw
tornillo sin fin	auger
válvulas de bebederos	valve gate
velocidad de llenado	injection speed
ventosas	vents
volumen de llenado/volumen	shot size
de la unidad de inyección	

VI - Operational Costs

(s.	3000+	\$230.00	\$0.064
an molder	2000- 2999	\$181.68	\$0.050
th Americ	1500- 1999	\$110.28 \$119.95	\$0.033
chine operating cost per hour, with operator and profit margin (North American molders)	1000- 1499	\$110.28	\$0.031
nd profit m	750-999	\$83.22	\$0.023
perator ar	500-749 750-999	\$68.14	\$0.019
our, with c	100-299 300-499	\$52.13	\$0.014
cost per h	100-299	\$41.92	\$0.012
operating	50-99	\$35.24	\$0.010
Machine	<50	\$33.31	\$0.009
2010	North America Tonnage Range	Average (US\$/hr)	Average (US\$/sec.)

Note: - this is a reference; consult your finance department for more exact values. - assume that a profit margin of 10 to 15% is included.

(Use only to estimate productivity gains, in US\$)

Note: The cost could be divided into three types, Basic, Optional, and Special.

Basic	Optional	Special
Depreciation	Robot	Class 8 Clean
		Room
Building	TCU	Inspection or QC
Interest	Packing equipment	Engineering
		assistance
Maintenance	Special injector;	Tooling support
	LIM, two colors,	
	high speed,	
Electricity	Crane	Material testing
Water	Quick mold change	Packaging and
		labeling equipment
Miscellaneous	Special screw	Special product
		handling
Labor	Additive Feeder	Mold storage
Marginal benefits		Mold maintenance
Inspection and QC		
Material		
Waste		
Secondary services		
Mold		
Overhead		
Earnings		

Bibliography

A. Brent Strong, 2000, "Plastics Materials and Processing", ISBN: 0-13-021626-7

Application Engineering, 1981, "Application Manual Water Group Products"

Douglas C. Montgomery, 2001, "Design and Analysis of Experiment", Arizona State University, ISBN 0-471-31649-0

Georg Menges and Paul Moren, 1993, "How to Make Injection Molds", Society of Plastics Engineers, ISBN 3-446-16305-0

Hansjurgen Saechtling, 1992, "Saechtling International Plastic Handbook", Society of Plastics Engineers, ISBN 3-46-14924-4

Jay Carender, 1997, "Injection Molding Reference Guide", Advance Process Engineering

John Bozzelli, Jan 1998, "Process Optimization and Setup-card Data Requirements", Cycleset

John Bozzelli, Jan. 1997, "How to Set First-Stage Pressure", Plastics World

Lawrence E. Nielsen and Robert F. Landel, 1994, "Mechanical Properties of Polymers and Composites", ISBN 0-8247-8964-4

Peter Kennedy, 1995 "Flow Analysis of Injection Molds", ISBN:1-56990-181-3

R. J. Young and P. A. Lovell, 1991, "Intruction to Polymers", ISBN: 0-412-30640-9

Shiro Matsuoka, 1992, "Relaxation Phenomena in Polymers", Society of Plastics Engineers

Thermoplastic Troubleshooting Guide, 2000, Ashland Distribution Company

Thomas Pyzdek and Roger W. Berger, 1992, "Quality Engineering Handbook", ISBN: 0-8247-8132-5

Tony Whealan and John Goff, 1994, "The Dynisco Injection Molders Hand Book", Dynisco Instruments

ULF W. Gedde, 1995, "Polymer Physics", ISBN 0-412-62640-3

Answers

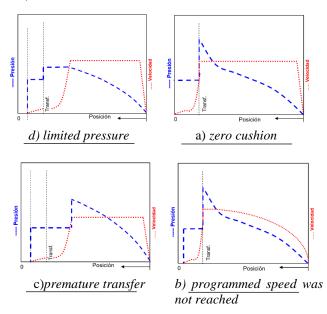
II. Injection Process Parameters

1) b. 2) b. 3) c. 4) b, c. 5) a. 6) b. 7) b, d. 8) a, d. 9) a. 10) b. 11) c, d.

12) b, c, d. **13**) a. **14**) b. **15**) b. **16**) b. **17**) a. **18**) b, c, d.

III. Process Graphs

1) b. 2) b. (3) c. 4) b. 5) c. 6) a. 7) c. 8) c. 9) b. 10)



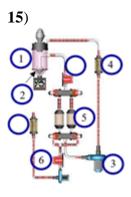
IV. Plastic Morphology

1) b. 2) c. (3) c. 4) a. 5) c. 6) c. 7) c.

V. Auxiliary Equipment

 $1) \ b. \ 2) \ c. \ 3) \ a, \ c, \ e. \ 4) \ b. \ 5) \ a. \ 6) \ b. \ 7) \ c. \ 8) \ b. \ 9) \ b. \ 10) \ a. \ 11) \ a.$

12) b. 13) b. 14) a.



Blending and Material Handling

1) b. 2) a.

Water Temperature Control to the Mold

1) b. 2) b. 3) c. 4) a. 5) b. 6) a. 7) a.

VI. Molding from the Desk

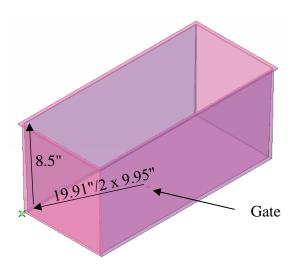
1) b. 2a) b. 2b) a. 2c) a. 3) d.

Injection Unit Sizing

1) b. 2) a. 3) a. 4) a. 5) a. 6) c. 7) a. 8) d.

9a) Area = 19.4in x 8.9in = 173in²

9b)



Farthest flow path = 8.5" + 9.95" = 18.45"Thinnest wall on the path = 0.08"Thin Wall - 18.45"/0.08" = 230

PF = 230 > 200; the force factor would be **2.5 ton/in²**

- 9c) Required clamping force = $173in^2 \times 2.5 \text{ ton/in}^2$ = 433 US tons of force (1 ton = 2000 lb)
- **9d**) Consumption = 1100/50s x 3600s/1h x 1 lb/454 gr = **174** lb/hr
- **9e**) Required volume = 1100gr/0.92gr/cc = **1196 cc**
- 9f) %U = (1196cc/2480cc)*100% = 48%
- 9g) $ton_{cooling} = 174 lb/hr / 50 lb/hr/ton = 3.5 ton_{cooling}$
- **9h**) gpm = $3.5 \text{ ton}_{\text{cooling}} \times 24 / 3^{\circ} \text{F} = 28 \text{gpm}$
- 9i) U% = 48% and is between 35% and 65%.

 The transfer would be between 12mm and 25mm.

 Transfer = 25mm 13mm (0.48-0.65)/0.3 = 17.6mm = 0.69in
- 9j) Recovery position = 1.27W/ δ D² + Transfer = 1.27*1100gr/[0.92gr/cc*(9cm)²] + 1.76cm = 20.51cm = 8.07in
- 9k) Start with 700 psi (47 bars) plastic pressure.
- **91**) 5% of fill = 0.05*8.07in = **0.4** in
- **9m**) From the Material Data sheet = 410° F
- **9n**) From a data sheet of a generic PS:

Injection	Nominal Value	Unit
Rear Temperature	424 to 480	°F
Middle Temperature	424 to 480	°F
Front Temperature	390 to 415	°F
Nozzle Temperature	415 to 469	°F
Mold Temperature	60 to 150	°F

Since the %U is almost 50%, use the average.

Feed zone = Compression zone = Metering zone = $452^{\circ}F$ Nozzle = $(415^{\circ}F + 469^{\circ}F)/2 = 442^{\circ}F$

90)

U%	Tr (# ciclos)
1%	140
2%	70
3%	47
4%	35
5%	28
6%	24
7%	20
8%	18
9%	16
10%	14
11%	13
12%	12
13%	11
14% - 15%	10
16% - 17%	9
18% - 19%	8
20% - 23%	7
24% - 27%	6
28% - 34%	5
35% - 46%	4
47% - 69%	3)
>70%	2

Residence time (cycles) = 3 cyclesResidence time(s) = $3 \text{ cycles } \times 50 \text{ s/cycles} = 150 \text{ seconds}$

9p) Consumption = 174 lb/hr

Drying hopper volume = $174 \text{ lb/hr x } 2 \text{ hours } / 35 \text{ lb/ft}^3$ = $9.94 \text{ ft}^3 = 281.5 \text{ liters}$

9q) Dry air flow = 174lb/hr x 0.75 cfm/(lb/hr) = **130.5** cfm

VII. Machine Rheology

1) b. 2) c. 3) c. 4) b. 5) c. 6) a. 7) a.

VIII. Determination of Injection Speed

1) a. 2) b. 3) b. 4) (a) a. 5) b. 6) a, c. 7) b. 8) b, c. 9) c. 10) d.

IX. Verifying Fill Balance

1) c. 2) b. 3) a. 4) a. 5) d. 6) b. 7) a. 8) b.

X. Determination of Hold Stage Parameters

1) a. 2) b. 3) b. 4) c. 5) a. 6) a, c. 7) b.

XI. Determination of Cooling Stage Parameters

1) b. 2) b. 3) d. 4) a. 5) a. 6) a. 7) d. 8) b.

9)

$$\frac{\overline{D}_{C} + \beta_{0}T_{M} + \beta_{1}t + \beta_{2}T_{F} + \beta_{3}T_{M}t + \beta_{4}T_{M}T_{F} + \beta_{5}tT_{F} + \beta_{6}T_{M}T_{F}t}{(1)(5)(2)(4)}$$

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Expert Opinions

"Universal Molding" is, in the Dominican Republic, an essential platform for the development of Dominican molders and the local industry has increasingly benefited by applying this knowledge to the improvement of its processes."

Miguel Calcaño, Plastics Consultant HDI Inc., Dominican Republic

"One of Wallyco's greatest pleasures was always the research and professional development of young Puerto Ricans. If I'm not mistaken, it was in 2000 that we provided resin and machine time to Dr. Ivan Baiges' students; among those I remember Roberto Pastor. Days of more questions than answers, which laid the foundation for corroborating or denying stories of molders and understanding the science behind the technique. Yes science, not magic, black box, or dark art. Once the technique was verified, thanks to the help of people such as Drs. Gregorio Velez and Ivan, it was reduced to its minimum essence, and a verified process of the best practices was developed. It is written at the level of the user, the person who must improve the process without formal education. There have been many changes from 2000 to this day, which will continue as *Universal MoldingTM* still has much to discover and teach. It is a great pride for me to have been involved in its beginnings, to have used its processes and to have trained as an instructor, and I wish Hector and *Universal MoldingTM* to continue to help the plastics industry and all those young Puerto Ricans who want to better themselves and their homeland with their performance."

J. Wally Cruz, Engineer and Plastics Engineer Specialist

"Universal Molding" is an excellent tool, not only for understanding the process of injection molding, but also for understanding the behavior of different types of plastics, in a simple way but always with a scientific basis. As an MU^{TM} student without any experience in the world of plastics, I was able to understand the groundwork and foundations of injection molding. Then, as an instructor, I could see how MU^{TM} helped so many people and industries optimize their molding processes with amazing results, not only in quality but also in economy."

Laureano J. Rodríguez, Sr. Account Manager West Contract Manufacturing "At the beginning of the 2000s, I was part of the revolution that was barely beginning in Costa Rica about how to scientifically establish a process during my time at Abbott Laboratories, which later became Hospira, and is known today as ICU Medical. It was there that the first MU^{TM} exercise was done outside Puerto Rico, entirely in Spanish and, for the first time in Costa Rica, it showed a better way to obtain objective evidence about from where the validated parameters came in the injection molding process, making MU^{TM} the pioneer of this revolution in CR. After that, the course was opened to other companies in the industry in Costa Rica, and it has been taught year after year to the present day. Subsequently, from 2008 to 2014 I had the privilege and pleasure as a member of HDI, Inc. to participate in seminars and conferences alongside Héctor Dilán as a presenter."

Harold Gamboa Calderón, Sr. Account Manager - Distribution PolyOne Corporation (Central America and Andean Region)

"I learned about $Universal\ Molding^{TM}$ when I was just starting my professional career. Thanks to Héctor and the $Universal\ Molding^{TM}$, my learning curve in the field of injection molding was exponential. This gave me the necessary tools to apply science during the development of different molding processes and was my foundation for the future of my career in plastics engineering.

During those first steps with $Universal\ Molding^{TM}$, together with Héctor, we managed to develop Rheology by Power, which moved away from rheology by viscosity, but at the same time obtained specific results in less time. Rheology by Power helps us greatly optimize the injection stage in a simple, short, and accurate way.

Now, after about 15 years working in the injection molding industry, I can say that $Universal\ Molding^{TM}$ is the basis and the most useful learning tool for anyone working in this area.

Héctor, thank you for the confidence and opportunity to work with you when I was just getting started in the industry."

Billy Torres, Technical Services Manager Microsystems UK