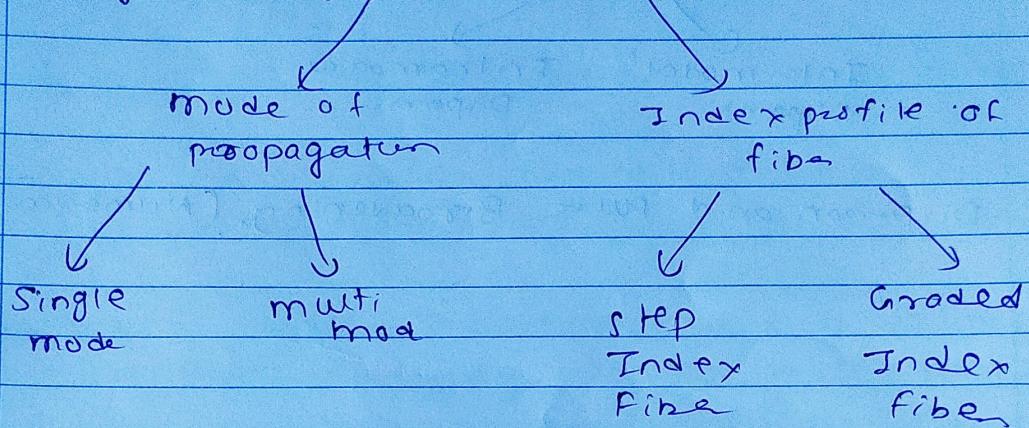
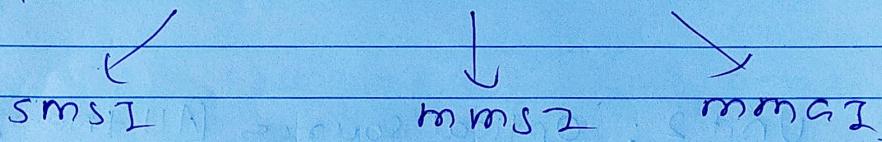


- * Basic Introduction
- * Shannon Renormal Capri.
- * Block Diagram of Optical Fibre
- * Advantages of Optical Fibres
- Concepts of Acceptance, Critical, NA
- Problems of Acceptance, Critical, NA.

* Light propagating in Fiber depends on



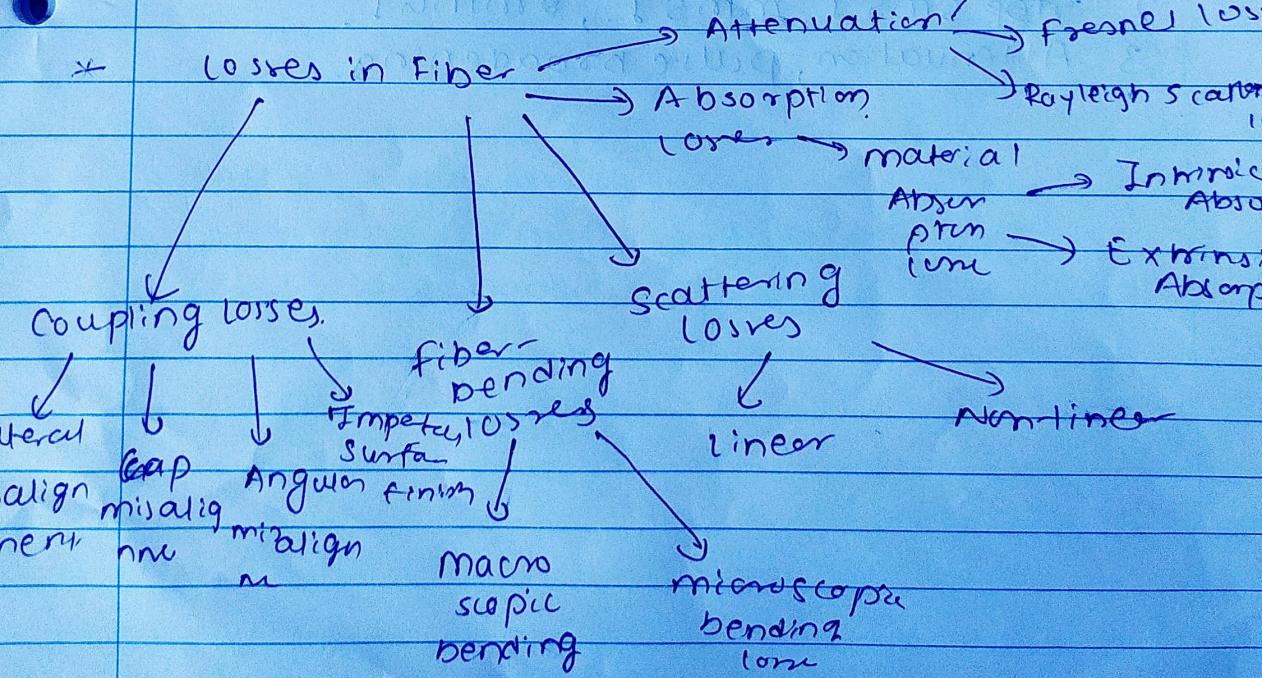
* Optical Fiber Classifications



* Comparison of SMST, MMST, MMG2

* Problems of MMST, MMG2, SMST, Intrinsic Losses

* Losses in Fiber





* Shannon's channel capacity:

- In comm' network, Imp Factor is channel capacity
- Channel capacity is the max. rate at which data can be sent across a channel from source to destination.
- Shannon-Hartley Theorem: gives the ~~inf~~ limit to information carrying capacity in bits per second. If channel has bandwidth (B) then the max info carrying capacity (C) of channel is given by:

$$C = B \cdot W \log_2 (1 + SNR) \text{ bits/sec.}$$

SNR is signal to noise ratio.

Effect of S/N on C: If $\frac{S}{N} \rightarrow \infty$ then $C \rightarrow \infty$

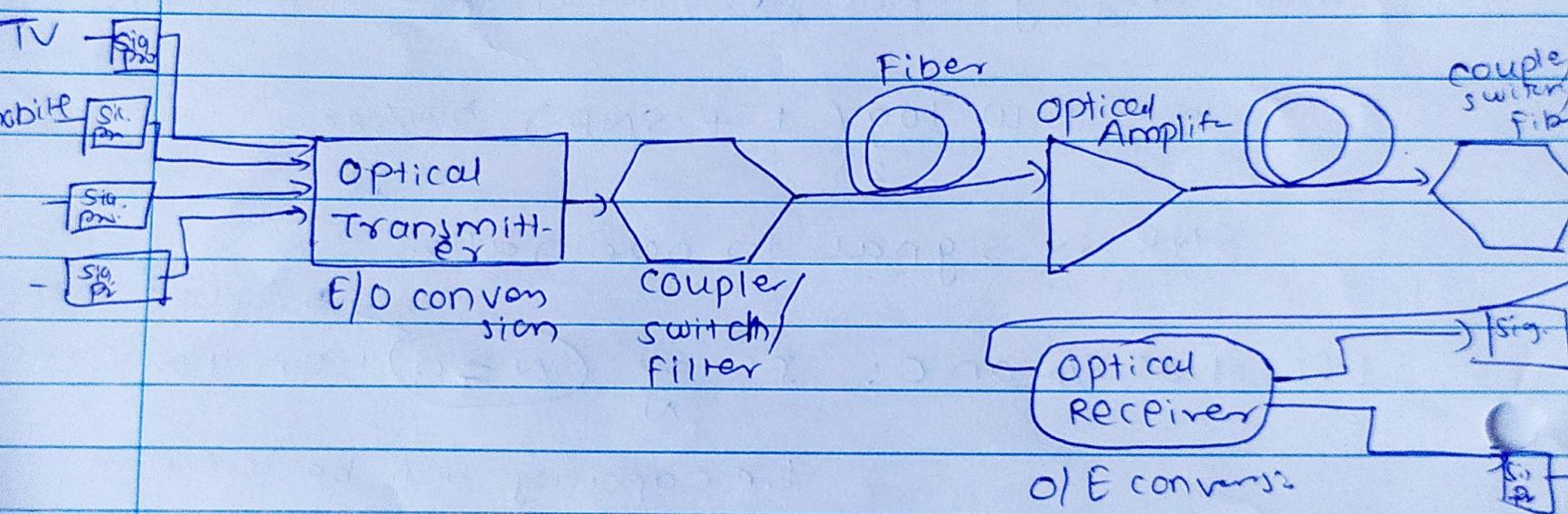
Effect of Bandwidth on C:

Increasing Bandwidth, decreases SNR since wider ^{the} bandwidth the more noise is introduced.

Units:

Peta	Tera	Giga	meg	kilo	Milli	micro	Nano	Pico	Fem
10^{15}	10^{12}	10^9	10^6	10^3	10^{-3}	10^{-6}	10^{-9}	10^{-12}	10^{-15}

* Block Diagram for Optical Fiber Communication Link:



E/O conversion \rightarrow E/O Transducer : LED / Laser Diodes

O/E conversion \rightarrow O/E Transducer : Photodiodes.

optical Amplifier \rightarrow Semiconductor / Doped Fiber / Raman

Coupler / switch / Filter : All-optical, depends on net w.

1. Source :

- source generates info into to send towards receiver
- output is a electrical signal.

Optical.

2. Transmitter:

- The info. fed to transmitter is electrical in nature.
But optic cable can only transmit optical signals.
- Therefore it is necessary to convert electrical to optical signal.
- This conversion done by electrical to optical transducers transducers like LED and LASER.

3. Filters:

- Filters are used to route the some of signal to the some of the networks.

4. Fiber :

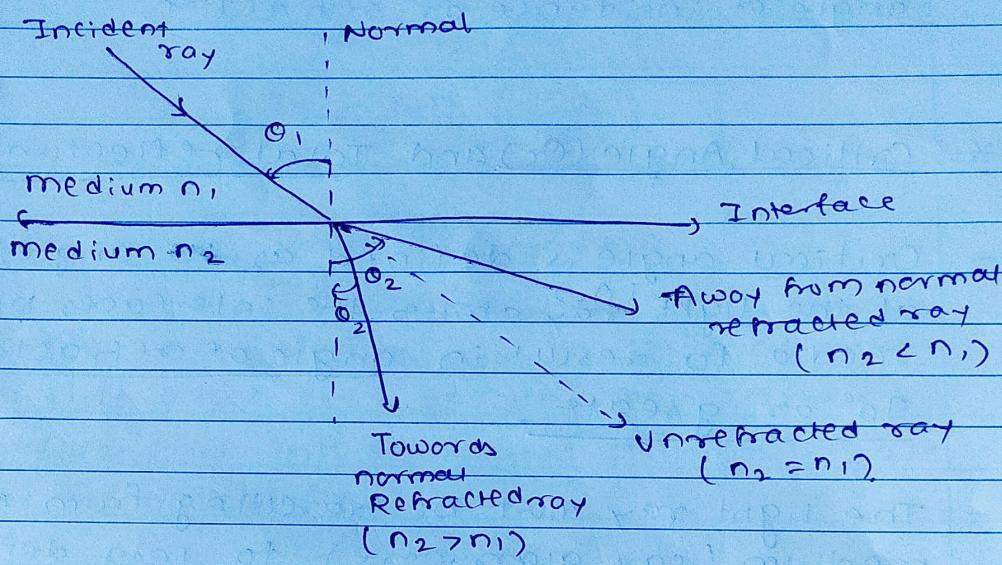
- The optical fiber cable is used to transmit the information from transmitter to receiver
- The cable generally consists of several cylindrical glass fibers.
- installed under sea or underground
- 0.2 dB/km attenuation.

5. Amplifier:

- To boost the power to transmit information to long distances , amplifiers are used.
- Semiconductor / Doped fiber / Raman Amplifiers are used to amplify the optical signal.

* Snell's law:

- Let ' n_1 ' and ' n_2 ' be the refractive indices of two mediums and let θ_1 and θ_2 be the angle of incidence and refraction resp.



- Snell's law explains the behavior of light rays striking the interface of two materials with different refractive indexes.

- The statement of Snell's law tells that the product refractive index by sine angle of incidence is constant for any ray of light striking the ~~surface~~ surface of two media.

$$n_1 \sin \theta_1 = n_2 \sin \theta_2$$

$$\frac{\sin \theta_1}{\sin \theta_2} = \frac{n_2}{n_1}$$

- As refractive index is equal to square root of constant, thus Snell's law can be.

$$\frac{\sin \theta_1}{\sin \theta_2} = \sqrt{\frac{E_{r2}}{E_{r1}}}$$

- This law is used in ray tracing to compute angle of incidence or refraction.

Critical Angle (θ_c) and Total reflection:

Critical angle is defined as the angle of incidence at the light ray strikes the interfaces between two media to result in angle of refraction θ_2 of 90° or greater.

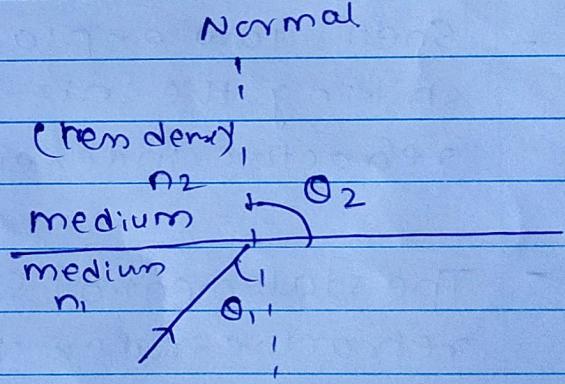
The light ray must be travelling from more dense medium (say glass core) to less dense medium (glass cladding).

Total reflection:

If the angle of incidence is greater than or equal to the critical angle, the angle of refraction will be

90° or greater. Hence the light ray cannot penetrate the less dense medium (cladding).

Therefore, total reflection takes place at interface of glass core and cladding with the angle of refraction equal to angle of incidence.





②

Snell's law :

$$n_1 \sin \theta_1 = n_2 \sin \theta_2$$

when $\theta_2 = 90^\circ$

$$n_1 \sin \theta_c = n_2 \sin 90^\circ$$

$$\therefore \sin \theta_c = \frac{n_2}{n_1}$$

$$\boxed{\theta_c = \sin^{-1} \left(\frac{n_2}{n_1} \right)}.$$

* Acceptance angle ($\theta_{\text{inc(max)}}$):

- Acceptance angle $\theta_{\text{inc(max)}}$ is the maximum angle at which the light ray can strike the air/glass core interface and still propagate down the optical fiber.
- It is the maximum value of external angle of incidence.
- The external angle of incidence θ_{in} must be less than the acceptance angle for successful travel down the optical fiber.
$$\theta_{\text{inc(max)}} = \sin^{-1} \left(\sqrt{n_1^2 - n_2^2} \right)$$
- Relationship b/w $\theta_{\text{inc(max)}}$ and θ_c :

Critical angle θ_c — minimum value of angle of incidence.

Acceptance angle $\theta_{\text{inc(max)}}$ — maximum value of angle of incidence.

If the light ray strike the glass core / cladding interface at an angle θ_{in} which is greater than the acceptance angle, then ray will be refracted into cladding.

Numerical Aperture (N.A.):

- It is defined as the sine of the acceptance angle $\theta_{in(max)}$, and it is unit less quantity. Its value ranges between -1 to +1.

$$N.A. = \sin \theta_{in(max)}$$

Expression for N.A.:

$$N.A. = \sqrt{n_1^2 - n_2^2}$$

$$N.A. = \frac{\sqrt{(n_1 - n_2)(n_1 + n_2)}}{2}$$

$$\Delta = \frac{n_1 - n_2}{n_1} \Rightarrow \Delta n_1 = n_1 - n_2$$

Let the diff. b/w n_1 and n_2 be very small.

$$\text{Then, } n_1 + n_2 = 2n_1$$

$$\therefore N.A. = \frac{\sqrt{(\Delta n_1)(2n_1)}}{2\Delta n_1^{1/2}}$$

$$\therefore N.A. = n_1(2\Delta)^{1/2}$$

6

Tells us that N.A. is dependent only on refractive index of core and cladding.

Expression for Δ :

$$\therefore \frac{\Delta}{n_1^2 - n_2^2} = n_1^2(2\Delta)^{1/2}$$

$$\therefore n_1^2 - n_2^2 = n_1^2(2\Delta)$$

$$\therefore \Delta = \frac{n_1^2 - n_2^2}{2n_1^2}$$

* Imp. of NA:

- (1) It is figure merit of N.A.
- (2) Used to measure the magnitude of accept. angle.
- (3) Describes the light collecting ability of ~~fib~~ optical fiber.
- (4) The amount of light can be accepted by optical fiber increases with increasing N.A.
- (5) N.A. does not depend on diameter of fiber core but in practice, the large core fibers tend to have larger value of N.A.

$$n_1 = 1.56, n_2 = 1.35, \theta_c = ? , \Delta = ? , \text{N.A.} = ? , \\ \text{Accept} = ?$$

$$\Rightarrow \theta_c = \sin^{-1} \left(\frac{1.35}{1.56} \right) = 59.93^\circ$$

$$\Delta = \frac{(1.56)^2 - (1.35)^2}{2 \times (1.56)^2} = 0.125 = 12.5\%$$

$$\text{N.A.} = \sin \cancel{\theta_c} \sqrt{1.56^2 - 1.35^2} = \cancel{59.93^\circ} = 0.78$$

$$\theta_{\text{in(max)}} = \sin^{-1}(\text{N.A.}) = \underline{\underline{51.26^\circ}}$$

* Types of modes in optical fiber:

- ① Cladding modes: modes corresponding to light rays passing through cladding layer.
- ② Bottom modes: modes travelling through the core layers of waveguide.
- ③ Refracted modes: modes generated because of refraction of light at core-cladding surface.
- ④ Leaky modes:
While passing through core layer some of the modes continuously loose their energies. These modes are leaky modes.

Condⁿ for optical mode:

- To remain a mode as guided mode, following condition should be satisfied:

$$n_2 k < \beta < n_1 k.$$

β = propagation factor

k = propagation constant $= 2\pi/\lambda$.

- Cut-off condⁿ is boundary bet^w guided and leaky mode. ($\beta = n_2 k$).
- Leaky modes starts when β becomes less than $n_2 k$.

mode	cond'n
Guided	$n_2 k < B < n_1 k$
cutoff	$B = n_2 k$
Leaky	$B < n_2 k$

* Light propagating in fiber depends on

mode of propagation

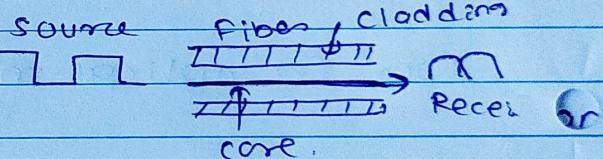
Index profile of fiber

1. Mode of propagation:

- path followed by light rays inside the fiber
- Two types: Single mode and multimode fibers

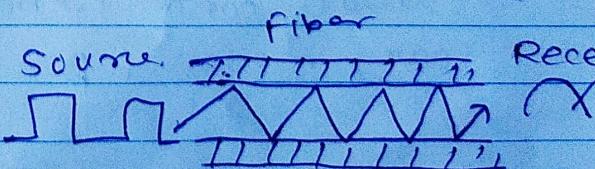
• Single Mode Fibers:

- The optical signal entering from one end of fiber has only one path to follow, that is along the centre of fiber.
- A highly focused light beam is produced, and it travels almost horizontally as shown in fig. The critical angle is close to 90° .
- Delays are negligible, reconstruction is easier



• Multimode Fibers:

- The optical signal entering from one end of fiber has more than one path to follow.



(5)

- multiple beam will follow diff. zigzag path as shown in Fig.
- no. of reflection depends on angle of incidence of beam.
- all beam do not reach simultaneously.

* IMP FORMULA:

The no. of modes supported by multimode fiber

$$M = \left(\frac{\pi d}{\lambda} \sqrt{n_1^2 - n_2^2} \right)^2$$

d = diameter (in meter)

λ = wavelength of light ray

M = no. of modes.

* Comparison of Single and Multi-mode fiber

	Single Mode	Multimode
1. No. of modes	only one	more than one
2. Shape of path	straight along axis of core	Zig Zag,
3. Distortion	less than multimode	more than single mode
4. Bandwidth	High	Low.
5. Data rate	Higher than multimode	lower than single mode
6. Application	wideband long haul transmission	For narrowband short distance transmission

2. Index profile of Fiber:

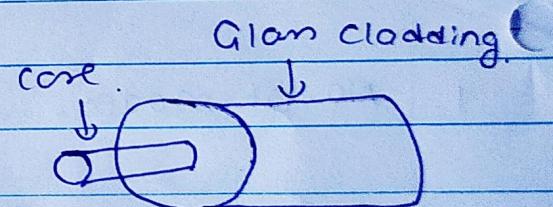
- Index profile is graphical representation of magnitude of refractive index on X-axis and radial distance from core axis on Y-axis.
- It tells us about the change in refractive index and nature of variation in refractive index with respect to radial distance.
- Types: Step Index and Graded Index.

a. Step Index Fibers:

- The optical fibers in which there is an abrupt change in refractive index at the core-cladding interface
- Types: Single mode step Index, Multimode step Index.

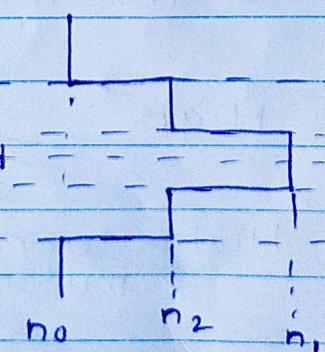
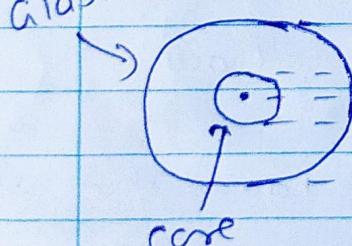
Single mode step Index:

- The construction of SMSI is shown.



Index profile:

Glass cladding.



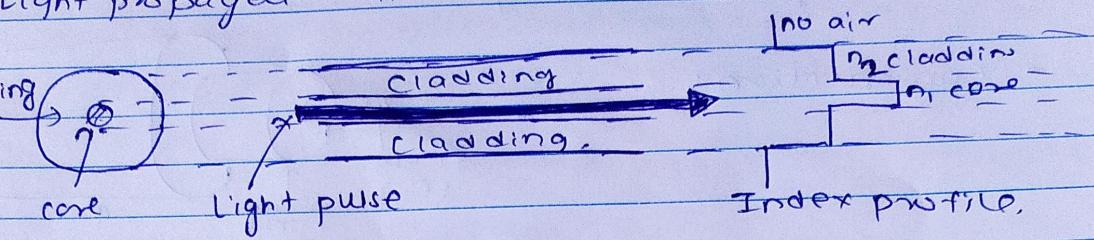
Refractive index of core - n_1 ,

Refractive index of cladding - n_2

$$\therefore n_1 > n_2$$

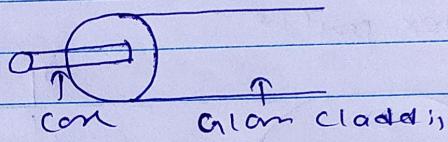
(6)

Light propagation in SMSI is shown below.



Multimode Step Index Fibers:

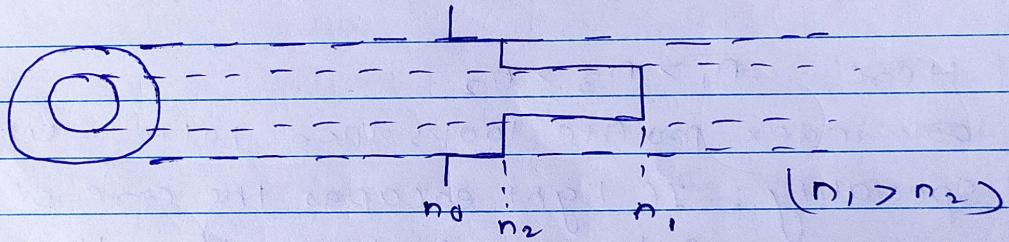
Construction:



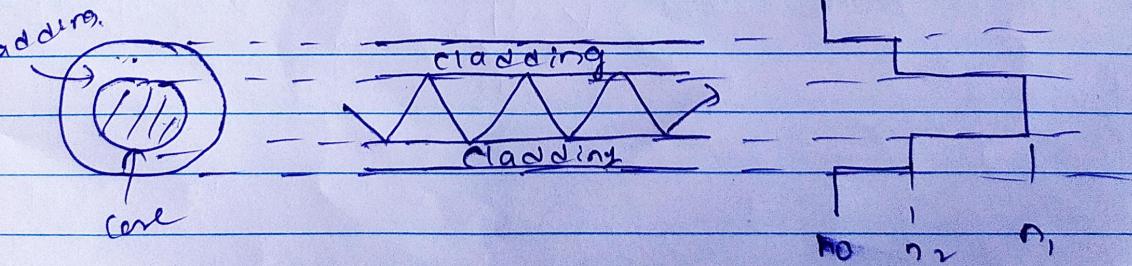
consists of glass core and cladding.

The diameter of core is much larger than compared to single mode step index fibre.

Index profile:

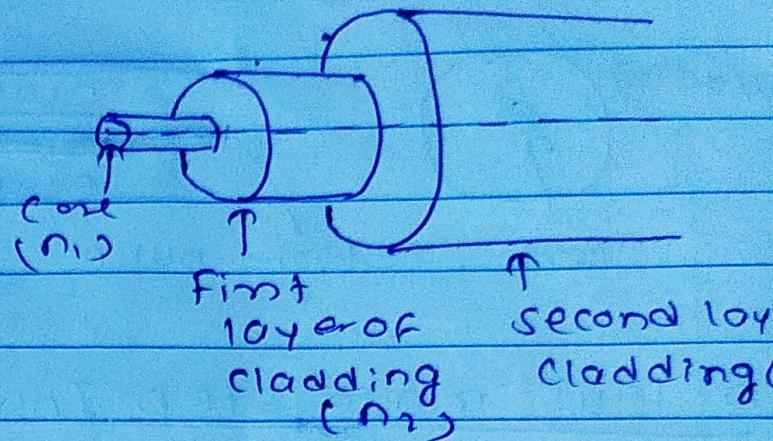


Propagation of light.

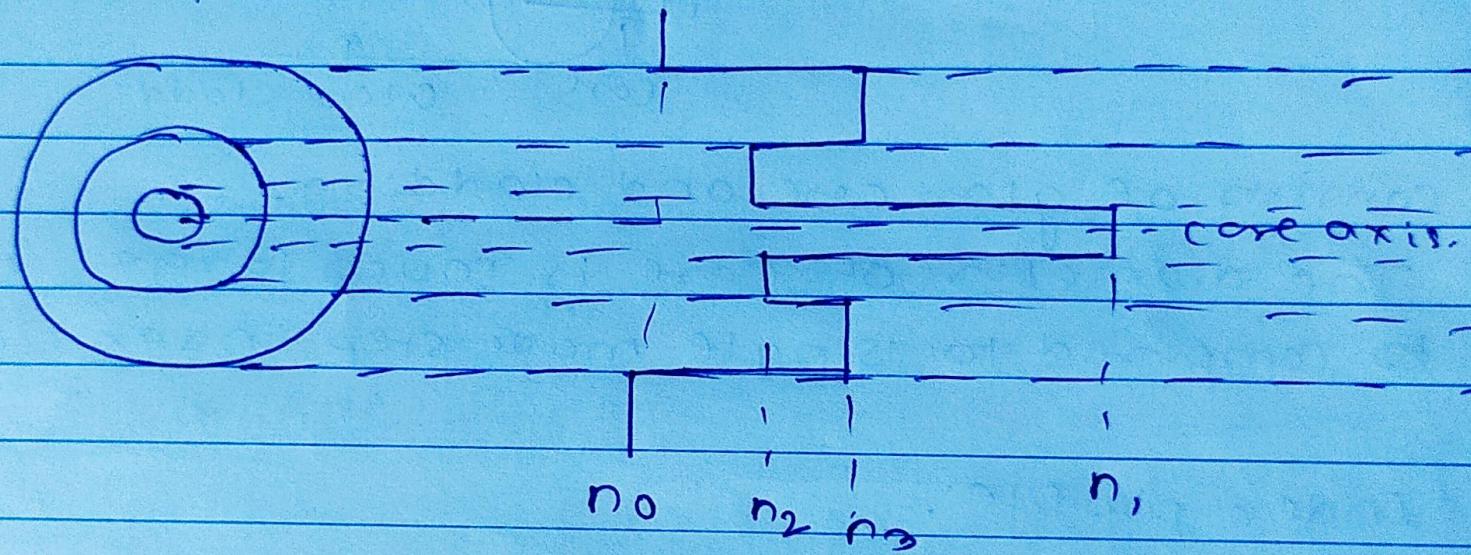


c. Index profile of W-profile fibre:

- Construction:



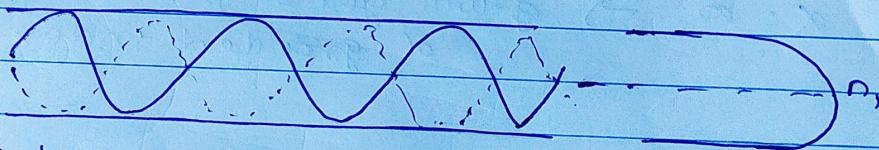
- Index profile



- Here, $n_1 > n_3 > n_2$.
- ~~look~~ index profile looks like letter-W.
- Speciality: If light escapes the core of fibre enters into first cladding. then it is completely absorbed in second cladding. This is because $(n_3 > n_2)$.

2. Graded Index Fibers:

- In this type, the refractive index of fiber core does not remain constant throughout its bulk. But it's non-uniform.
- The refractive index of core is max. at the center of core and decreases gradually towards the walls of core.
- To get this type of index profile, the material in fiber core is modified.
- Propagation of light:

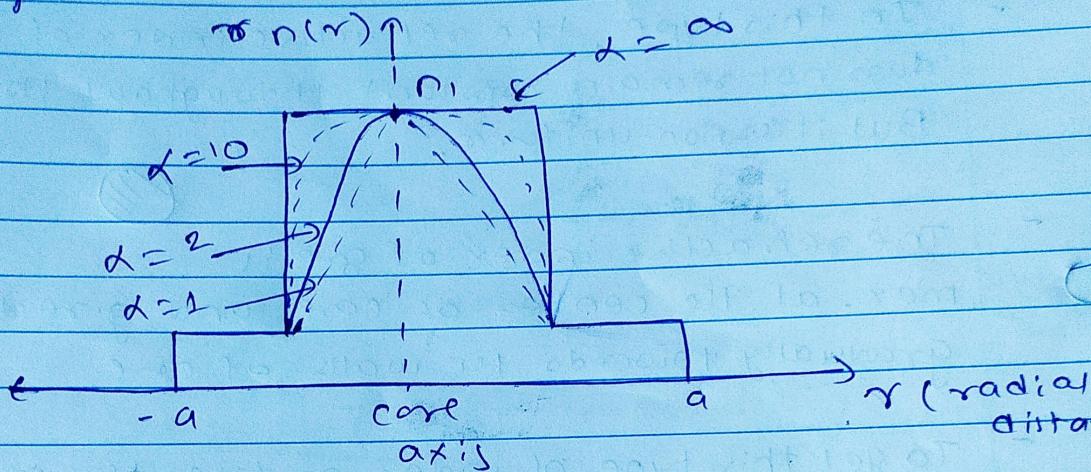


- Due to modification in index profile, the light gets refracted inside fiber core and does not travel in straight line.
- The rays are curved towards the center.
- The refractive index variation in core is,

$$n(r) = \begin{cases} n_1 \sqrt{1 - 2\Delta \left(\frac{r}{a}\right)^2} & \text{when } r \leq a \\ n_1 + 1 - 2\alpha, \approx n_2 & \text{when } r > a \end{cases}$$

Δ = Shape of index profile, a = Radius of core
 r = Radial distance from fiber axis.

Shape of refractive index profile changes with change in value of α .



$\alpha = 1 \rightarrow$ refractive index profile is triangular.

$\alpha = 2 \rightarrow$ It is parabolic

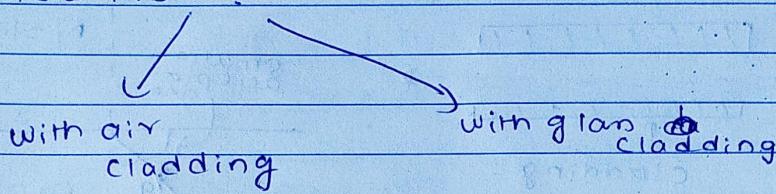
$\alpha = \infty \rightarrow$ will get step index profile instead of graded index profile.

Parameter	Step Index	Graded Index
1. Change in refractive index	refractive index changes abruptly.	refractive index changes gradually from centre to edge.
2. Path travelled by light rays	Straight line or zigzag path	curved paths.
3. Phenomenon resp for light pro.	Reflection	Refraction.
4. Size of acceptan. cone.	Smaller than graded index.	Longer than step index fiber.
5. Index profile.		

* Optical Fiber classification:

1. Single Mode Step index.
2. Multimode Step Index.
3. Multimode graded Index.

1. SSMI Fiber:

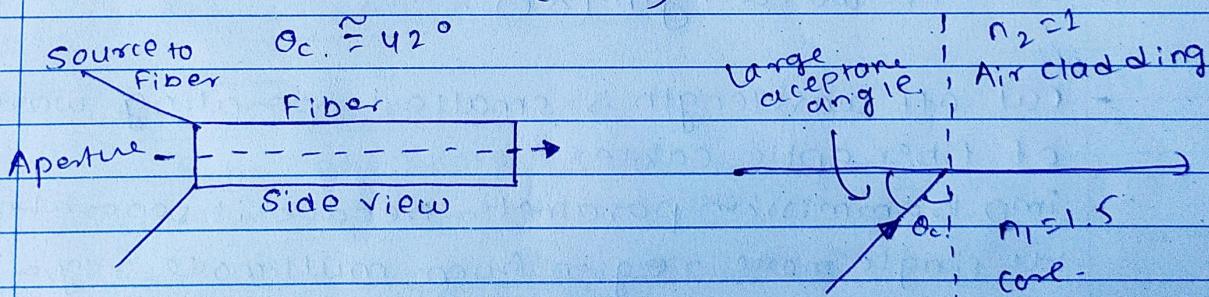


* SMSI fiber with air cladding:

- type of single mode step index fiber, there is no glass cladding used.
- outside cladding is air, with ($n_2 = 1$) and refractive index of glass core is ($n_1 = 1.5$).
- critical angle θ_c is defined as,

$$\theta_c = \sin^{-1} \left(\frac{n_2}{n_1} \right)$$

$$= \sin^{-1} \left(\frac{1}{1.5} \right)$$

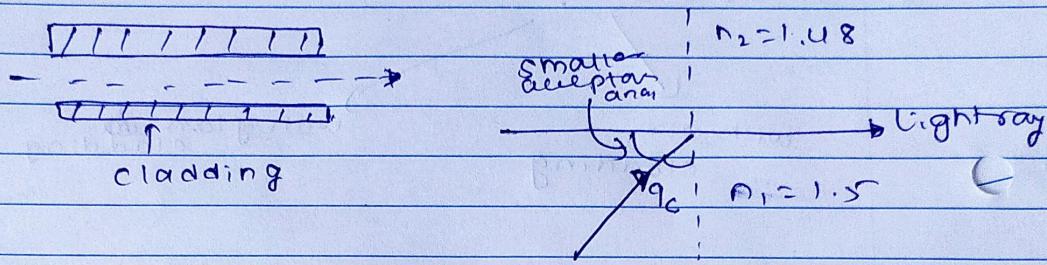


- The large acceptance angle makes easy for the light source to couple light into optical fiber.
- Very weak.

SMSI fiber with glass cladding:

Here, glass cladding is present.

The refractive index of core is $n_1 = 1.5$ and that of $n_2 = 1.48$. (glass cladding).



$$\theta_c = \sin^{-1} \left(\frac{n_2}{n_1} \right) = \sin^{-1} \left(\frac{1.48}{1.5} \right) = 80.63^\circ.$$

Critical angle (θ_c) is higher than that of single mode air cladding.

Difficult to couple light source.

propagation modes in single mode step Index Fiber :

CUT-OFF wavelength (λ_c):

Cut-off wavelength is smallest operating wavelength of fiber optic cable.

Imp transmission parameter because it separates the single mode region from multimode region.

V-number is given as,

$$V = \frac{2\pi a}{\lambda} \sqrt{n_1^2 - n_2^2}$$

$$V = \frac{2\pi}{\lambda} a (n_1 (2\Delta)^{1/2}) \quad - \textcircled{1}$$

$$\lambda = \frac{2\pi a (n_1 (2\Delta)^{1/2})}{V} \quad - \textcircled{2}$$

Cut-off wavelength :

$$\lambda_c = \frac{2\pi a (n_1 (2\Delta)^{1/2})}{V_c} \quad - \textcircled{3}$$

$V_c \leftarrow$ cut-off normalized freq.
 (. $V_c = 2.405$)

Dividing $\textcircled{3}$ and $\textcircled{2}$

$$\frac{\lambda_c}{V} = \frac{\lambda}{V_c}$$

$$\lambda_c = \frac{V\lambda}{V_c}$$

$$\boxed{\lambda_c = \frac{V\lambda}{2.405}} \quad (V_c = 2.405)$$

↓

Expression for cut-off wavelength of SMF I

2. Mode Field Diameter (MFD):

- Mode Field diameter is section of fiber where the most of the light energy travels.
- Value of MFD is larger than actual diameter of core. This happens because some of light rays travel through cladding.

Multimode Step Index (MMSI) Fiber:

Relation b/w No. of modes (M) and 'V' number

$$\sin \theta_{\text{in max}} = \sqrt{n_1^2 - n_2^2}$$

$\theta_{\text{in max}}$ is small,

$$\sin \theta_{\text{in max}} = \theta_{\text{in max}}$$

$$E = \pi \sin^2 \theta_{\text{in max}}$$

$$E = \pi \theta_{\text{in max}}$$

$$\theta_{\text{in max}} = \sqrt{n_1^2 - n_2^2}$$

$$E = \pi (n_1^2 - n_2^2)$$

$$A = \pi a^2$$

$$m = \frac{\pi a^2}{\lambda} (n_1^2 - n_2^2)$$

No. of modes per unit solid angle is

$$m = \frac{2\pi}{\lambda^2} E$$

$$m = \frac{2A}{\lambda^2} \pi (n_1^2 - n_2^2)$$

$$m = \frac{2\pi^2 a^2}{\lambda^2} (n_1^2 - n_2^2)$$

$$n_1^2 - n_2^2 = (NA)^2$$

$$m = \frac{2\pi^2 a^2 (NA)^2}{\lambda^2}$$

$$m = \frac{\pi^2 a^2}{\lambda^2}$$

$$v = \frac{\pi a (NA)}{\lambda}$$

Adv.

1. less expensive.
2. easy to manufacture.
3. easy to couple light

Disadv.

1. Received light pulse is distorted.
2. ~~less~~ less bandwith.
3. lower data rate.

Graded Δ Index:

Due to non-uniform density of core, the light ray with $\theta_i > \theta_c$ will progressively 'refracted' towards the centre of core and does not travel straight line.

$\sqrt{\alpha} \frac{1}{n} \Rightarrow$ velocity of light max at farthest min at travel close to center.

rays take same amount of time to reach an end, received light pulse is replica, small amount of distortion.

No. of guided modes is given by

$$m = \left(\frac{\alpha}{\alpha + 2} \right) (n, k, \alpha)^2 \Delta$$

$$k = \frac{2\pi}{\lambda}, v = \frac{2\pi}{\lambda} a n, \sqrt{2} \alpha$$

$$\therefore m = \left(\frac{\alpha}{\alpha + 2} \right) \frac{(2)}{2}$$

$$\text{at } \alpha \approx 1 \\ m = \frac{v^2}{4}$$



PICT, PUNE

Adv:-

- (1) less expensive.
- (2) easy to man.
- (3) easier to couple light than MMST, b: difficult than SMSI.

Disadv:-

- (1) Distortion more than SMSI, less than MMST.
- (2) MMCI fiber cable offer less bandwidth than ^{SMSI} SMSI.
- (3) support lower data rates than SMSI cable.

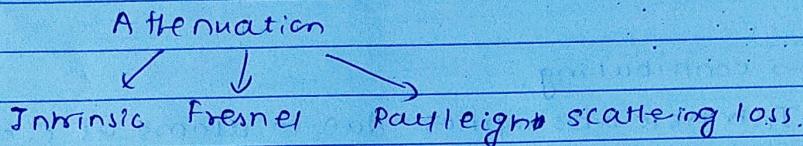
* Comparison:

	SMSI	MMST	MMCI
No. of paths	one	many	many
Distortion	less than both	more than SMSI, MMCI	less than MMST
Bandwidth	High	Low	lower than SMSI than MMCI
Data rate	High	low SMSI	low MMCI
cost	High	less	less
propagation delay	Difficult	Easy	Easy
bandwidth	Wideband	Narrow band	Narrowband

* Transmission Characteristics of Optical Fibers *

Attenuation.

- power loss taking place inside the fiber optic cable.
- amplitude gets reduced.



1. Intrinsic loss:

- scattering takes place at boundary of core and cladding layer.
- This scattering reduces power of signal.

2. Fresnel loss:

- due to change in refractive index at interface of core and cladding layer, Fresnel losses takes place.

3. Rayleigh scattering loss:

- causes due to submicroscopic variation in density of glass while manufacturing process.
- The impurities inside the glass act as reflecting and refracting faces.
- This power loss resulting due to scattering is called "Rayleigh Scattering loss".
- Improved manufacturing techniques can reduce loss.

- Expression for power loss:

$$A(\text{dB}) = 10 \log_{10} \left(\frac{P_{\text{in}}}{P_{\text{out}}} \right)$$

- attenuation in multimode fibers tends to be higher than single mode fibers.

- Att. coefficient in dB per km is given by,

$$A = \frac{10}{D} \log \left[\frac{P(0)}{P(D)} \right]$$

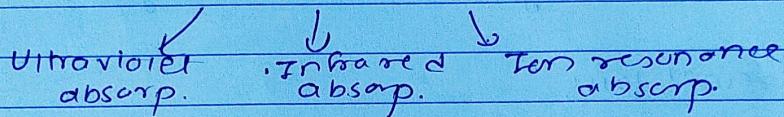
* Material absorption loss :

- Came :- defect in fabrication process of fiber optic cable.
- Transmitted light is dissipated as heat. This is called material absorption loss.

Factors contributing:

1. Intrinsic absorption due to atoms of fiber material
2. Extrinsic absorption due to impurity atoms.
3. Absorption due to atomic defects in glass material.

Intrinsic absorption



1. Ultraviolet absorp.:

- energy of light rays is given out to valence electrons of silica material used for manufac. of glass.
- The absorption of silica material increases in ultraviolet region. ∴ called as ultraviolet absorption.
- The absorption is of order of 0.1 dB/km .

2. Infrared absorp.:

- If wavelength of light rays in infrared region, then photons of light are absorbed by atoms in glass.
- The energy is converted to mechanical vibrations. Called as infrared absorption.

3. Ion resonance absorption:

- During manufacturing, the water molecules are trapped in the glass. These molecules produce OH^- ions in material.
- The absorption associated with water molecules is called Ion resonance absorption.

formulae

$$① \quad \Theta_c = \sin^{-1} \left(\frac{n_2}{n_1} \right)$$

$$② \quad N.A. = \sin \Theta_{\text{in(max)}} = \sqrt{n_1^2 - n_2^2} \\ = n_1 (2 \Delta)^{1/2}$$

$$③ \quad \Delta = \frac{n_1^2 - n_2^2}{2n_1^2}$$

$$④ \quad \Theta_{\text{in(max)}} = \sin^{-1} (N.A.) = \sin^{-1} (\sqrt{n_1^2 - n_2^2}) \\ = \sin^{-1} (n_1 (2 \Delta)^{1/2}).$$

⑤ Solid Acceptance angle,

$$\epsilon = \pi \sin^2 \Theta_{\text{in(max)}}.$$

$$\epsilon = \pi (N.A.)^2.$$

$$⑥ \quad V = \sqrt{k_0^2 n_1^2 - \beta^2} a, \quad \omega = \sqrt{(\beta^2 - k_0^2 n_1^2)} a$$

$$V = \sqrt{V^2 + \omega^2} = \frac{2\pi}{\lambda} a \sqrt{n_1^2 - n_2^2} \\ \begin{aligned} & \text{Normalized} \\ & \text{waveguide} \\ & \text{parameter} / V - \text{number} \\ & = \frac{2\pi}{\lambda} a (N.A.) = \frac{2\pi}{\lambda} a n_1 (2 \Delta)^{1/2} \end{aligned}$$

As V-number increases, the modes supported by fiber increases.

$$\text{Single mode Fiber: } N_c = 2.4048 \\ \therefore (0 < V < 2.4048)$$

(7) No. of modes in mmSI:

$$m = \left(\frac{\pi d}{\lambda} \right)^2 (n_1^2 - n_2^2)$$

$$m = \frac{v^2}{2}$$

(8) No. of modes in mmGI:

$$m = \left(\frac{d}{\Delta + 2} \right) (n_1 k a)^2 \Delta, \quad k = \frac{2\pi}{\lambda}$$

$$m = \frac{v^2}{4}$$

(9) Step index mode:

$$m = \frac{v^2}{2}$$

(10) Optical power that flows in cladding is,
(Total percent of power flowing through cladding)

$$\frac{P_{clad}}{P} = \frac{4}{3 \pi m}$$

P_{clad} = power in cladding

P = Total power

m = no. of modes

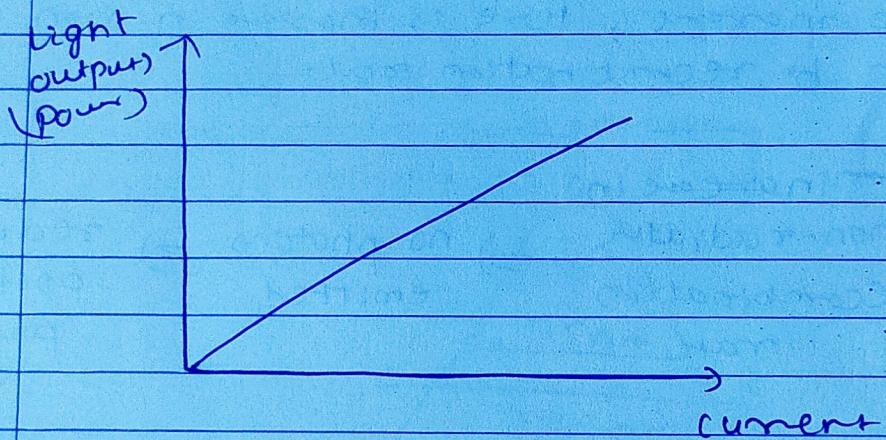
$$n_{ex} \approx \frac{1}{n(n+1)^2}$$

Power emitted from LED.

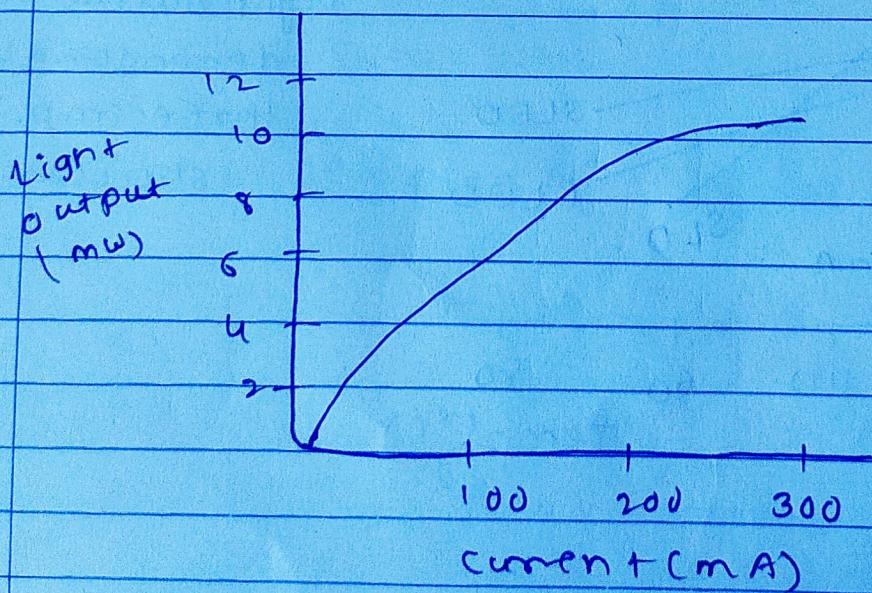
$$P = n_{ex} P_{int} = \frac{P_{int}}{n(n+1)^2}$$

* Power characteristic

Ideal:

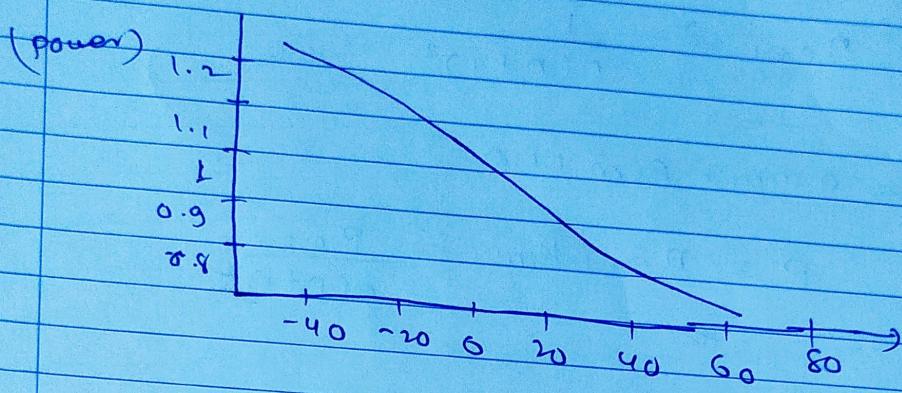


- The ideal output against current characteristics for



(AlGaAs surface emitting characteristics)

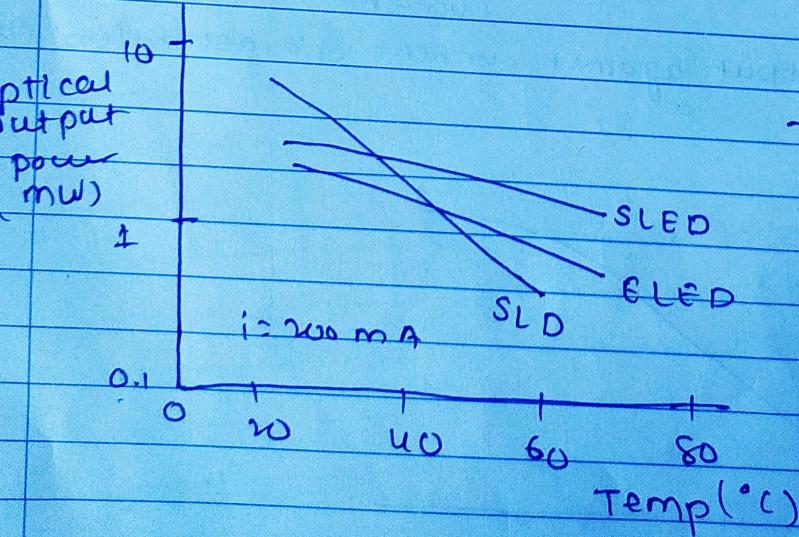
P vs Temp characteristics



- Power is inversely prop. to temp.
- decreases with increase in temp.
- As temp increase, there is increase in non-radiative to recombination rate.,,

Reduction in increase in
non-radiative
recombination
rate

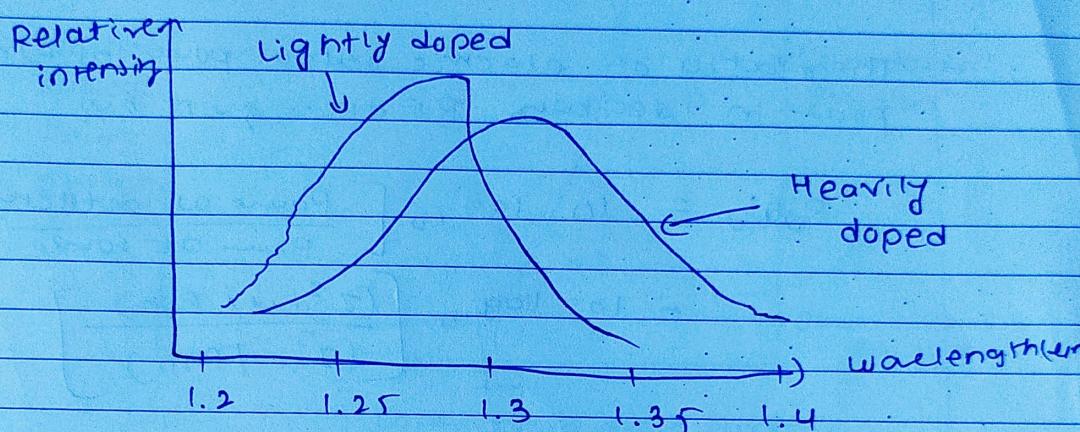
→ no photons emitted → reduce optical power



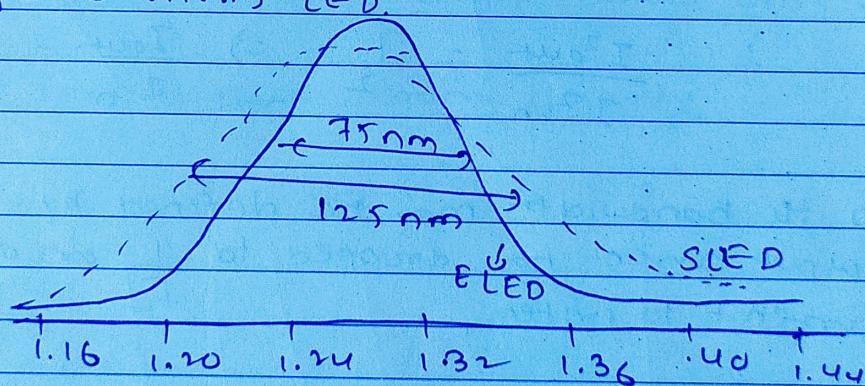
- Light output temp dependence is three imp. L structure.

* Spectral width:

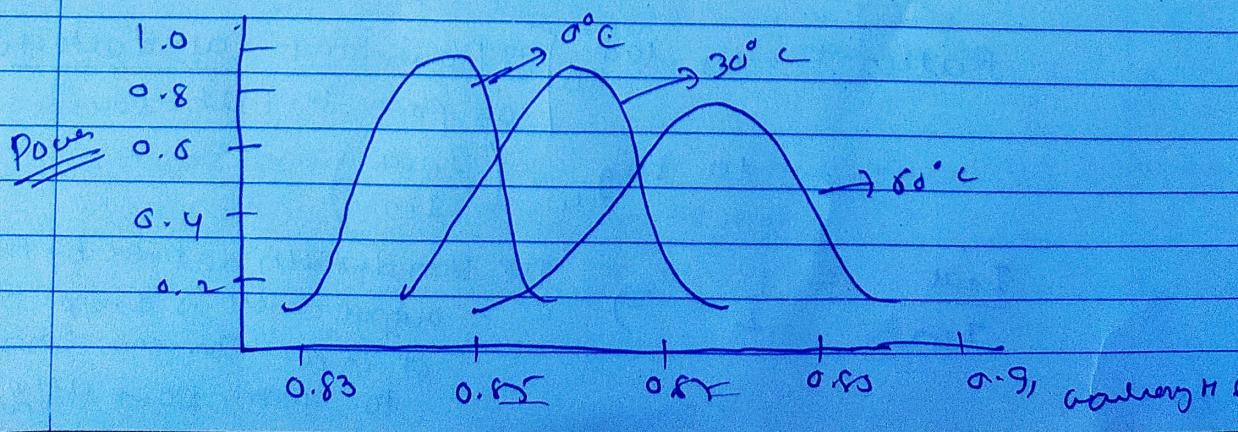
- output spectra for InGaAsP for both lightly doped and heavily doped.



- Spectral output characteristics for InGaAsP surface-edge-emitting LED.



- Effect of temp. on AlGaAs surface-emitting LED



* Modulation Bandwidth:

1. Electrical Bandwidth: Freq. at which the output power is reduced by 3 dB w.r.t. input electric power.
- The ratio of electric output power to electric input power in decibels RF dB is given by:

$$\text{Ratio} = 10 \log_{10} \left[\frac{\text{Power at detector}}{\text{Power at source}} \right]$$

$$= 10 \log_{10} \left[\frac{(I_{out}^2 / R_{in})}{(I_{in}^2 / R_{in})} \right]$$

Electrical dB point occurs when ratio of power is $\frac{1}{2}$.

$$\therefore \frac{I_{out}^2}{I_{in}^2} = \frac{1}{2} \Rightarrow \frac{I_{out}}{I_{in}} = \frac{1}{\sqrt{2}}$$

So the bandwidth may be defined by freq. when output current has dropped to $\frac{1}{\sqrt{2}}$ or 0.707 of input current to system.

- Optical Bandwidth: The freq. when detected power becomes half of its low freq. value.

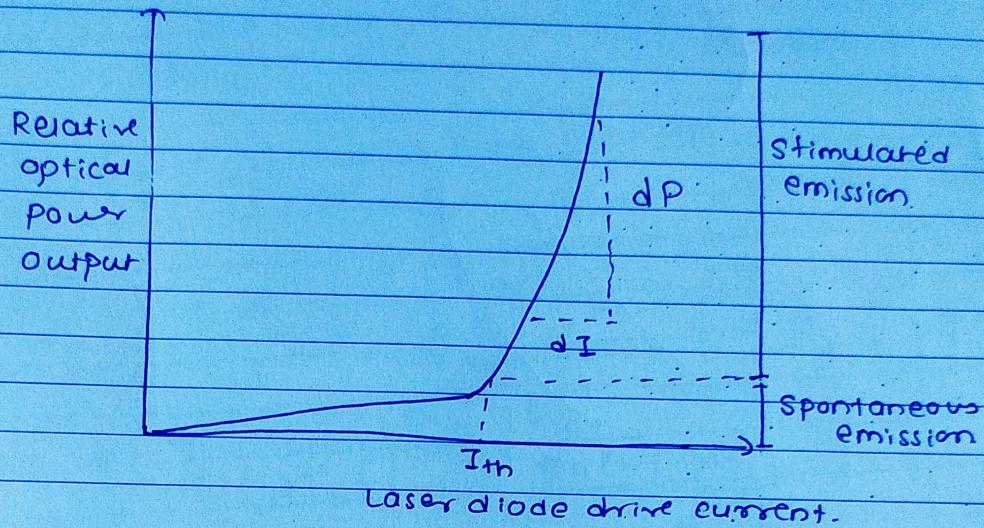
$$\text{Ratio} = 10 \log_{10} \left[\frac{\text{op. Power out (at detector)}}{\text{op. Power in (at source)}} \right]$$

$$= 10 \log_{10} \left(\frac{I_{out}}{I_{in}} \right)$$

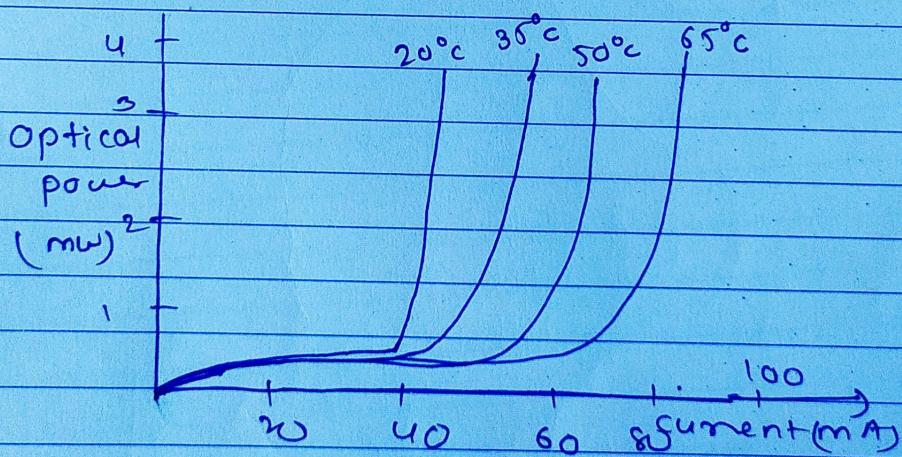
$$\frac{I_{out}}{I_{in}} = \frac{1}{2} \Rightarrow$$

The Bandwidth defined by freq. at which output current is dropped to $\frac{1}{2}$ of input current corresponds to electric power att. of $\frac{1}{2}$

- * LED along transmitter.
- * Power characteristics of LASER.



- As shown The fig. above shows relationship between optical output power and laser diode drive current.
- After I_{th} , the power increases linearly.



- Optical power of laser at const value of cur varies with change in temp.

Unit 2 - Formulas

* Efficiency of LED:

$$\eta_{int} = \frac{R_r}{R_r + R_{nr}}$$

$$\eta_{int} = \frac{I}{I_r - T}$$

$$\frac{1}{T} = \frac{1}{T_r} + \frac{1}{T_{nr}} \Rightarrow \text{Bulk lifetime.}$$

$$R_r = \tau_{int} \frac{I}{a}$$

$$P_{int} = \frac{\tau_{int} \times h \times c \times I}{q \times \lambda}$$

$$\eta_{ext} = \frac{I}{n(n+1)^2}$$

$$P = \frac{P_{int}}{\beta n(n+1)^2}$$