

## Solutions for: Introduction to IIR Filters Tutorial

1. How is a recursive digital filter different from a non-recursive digital filter? Explain in a few sentences and draw two example system diagrams, one of a recursive filter and one of non-recursive filter.

**Solution** A recursive filter uses past output values ( $y[n - i]$ ) for the calculation of the current output  $y[n]$ :

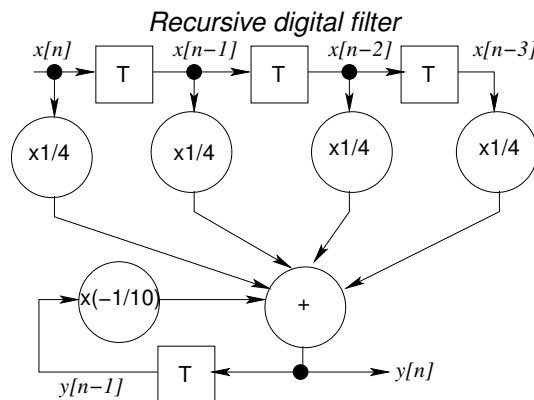
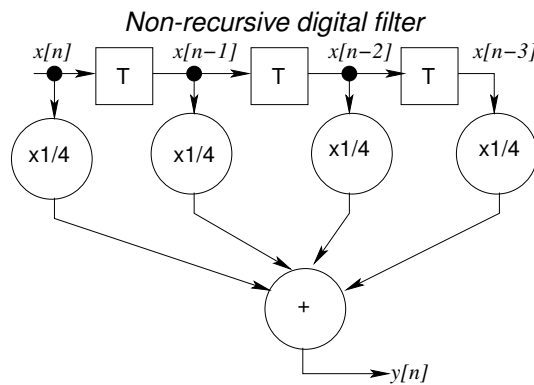
- *Recursive Filter Example*

$$y[n] = 0.5y[n - 1] + 0.5x[n].$$

A non-recursive filter only uses input values  $x[n - i]$  where  $i \geq 0$ :

- *Non-recursive Filter Example*

$$y[n] = 0.5x[n - 1] + 0.5x[n].$$



2. Design a bandpass filter using the pole-zero placement method with:

- centre frequency  $\Omega_0 = \pi/2$
- bandwidth  $\Omega_{bw} = \pi/8$
- complete attenuation at  $\Omega_{r1} = 0$  and  $\Omega_{r2} = \pi$

**Solution** Bandpass filter has 2 poles at  $\pm\Omega_0 = \pm\pi/2$  radians. Therefore

$$H(z) = K \frac{\text{zeros}}{(z - r \exp(j\pi/2))(z - r \exp(-j\pi/2))}$$

The radii of the poles are given by:

$$r \cong 1 - \frac{\Omega_{bw}}{2} = 1 - \frac{\pi/8}{2} = 0.80365;$$

and the zeros are at  $\Omega_{r1} = 0$  and  $\Omega_{r2} = \pi$ , so that

$$H(z) = K \frac{(z - \exp(j\Omega_{r1}))(z - \exp(j\Omega_{r2}))}{(z - 0.80365 \exp(j\pi/2))(z - 0.80365 \exp(-j\pi/2))}.$$

As

- $\exp(\Omega_{r1}) = \exp(j0) = \cos(0) + j \sin(0) = 1 - j0 = 1$
- $\exp(\Omega_{r2}) = \exp(j\pi) = \cos(\pi) + j \sin(\pi) = -1 + j0 = -1,$

then the transfer function becomes:

$$H(z) = K \frac{(z-1)(z+1)}{(z-0.80365 \exp(j\pi/2))(z-0.80365 \exp(-j\pi/2))}.$$

Using Euler's identity,

- $\exp(j\pi/2) = \cos(\pi/2) + j \sin(\pi/2) = +j$
- and  $\exp(j\pi/2) = \cos(\pi/2) - j \sin(\pi/2) = -j,$

so that

$$H(z) = K \frac{(z-1)(z+1)}{(z-0.80365j)(z+0.80365j)}.$$

3. Calculate the difference equation for the above system.

**Solution** Recall that  $H(z) = \frac{Y(z)}{X(z)}$ ,

$$H(z) = \frac{Y(z)}{X(z)} = K \frac{(z-1)(z+1)}{(z-0.80365j)(z+0.80365j)} = K \frac{z^2 - 1}{z^2 + 0.64585}.$$

Then

$$Y(z)(z^2 + 0.64585) = X(z)K(z^2 - 1).$$

Remembering that each  $z^{-1}$  is a unit **delay**, so that **each  $z$  is a unit advance**, then the difference equation is:

$$y[n+2] + 0.64585y[n] = K(x[n+2] - x[n])$$

which can be made causal by making  $n = n - 2$  so that

$$y[n] + 0.64585y[n-2] = K(x[n] - x[n-2]).$$

$K$  is not known, but can be used to make the peak pass band gain to be **unity**.

4. Calculate and sketch the frequency response for the above filter from the  $z$ -plane representation.

**Solution** Using the generalized difference equation form:

$$H(\Omega) = \frac{\sum_{k=0}^M b[k] \exp(-jk\Omega)}{1 + \sum_{k=1}^N a[k] \exp(-jk\Omega)}.$$

So that (using Euler's identity):

$$H(\Omega) = \frac{K(1 - \cos(2\Omega) + j \sin(2\Omega))}{1 + 0.64585(\cos(2\Omega) - j \sin(2\Omega))}$$

which has magnitude frequency response:

$$\text{Mag}(H(\Omega))^2 = \frac{K((1 - \cos(2\Omega))^2 + \sin^2(2\Omega))}{(1 + 0.64585 \cos(2\Omega))^2 + \sin^2(2\Omega)}.$$

5. For the above system, with sampling frequency  $500Hz$ :

(a) What is the bandpass centre frequency?

**Solution** Converting from digital to analogue, we know that  $2\pi$  digital frequency corresponds to the analogue sampling frequency ( $f_s = 500Hz$ ). Therefore we can use  $f = \frac{\text{digital frequency}}{2\pi} \times f_s$ .  
Therefore centre frequency:

$$f_0 = \frac{\pi/2}{2\pi} f_s = 125Hz.$$

(b) The bandwidth?

**Solution** Bandwidth:

$$f_{bw} = \frac{\pi/8}{2\pi} f_s = 31.25 Hz.$$

6. Design a digital bandstop filter using pole-zero placement method with following parameters:

- Centre frequency  $\Omega_0 = \pi/10$  radians (complete attenuation)
- Bandstop width,  $\Omega_w = 2\Omega_{cf} = \pi/20$  radians

**Solution**

- Complete attenuation at  $\Omega_0 = \pi/10$ , therefore x2 zeros (complex-conjugate pair) at  $\pm\Omega_0 = \pm\pi/10$ :

$$H(z) = K \frac{(z - \exp(j\pi/10))(z - \exp(-j\pi/10))}{\text{poles}}$$

- Centre frequency at  $\Omega_0 = \pi/10$  radians, therefore x2 poles (complex-conjugate pair) at  $\pm\Omega_0 = \pm\pi/10$ ,

$$H(z) = K \frac{(z - \exp(j\pi/10))(z - \exp(-j\pi/10))}{(z - r \exp(j\pi/10))(z - r \exp(-j\pi/10))}$$

- The poles are **scaled** with radius  $r$  to control **the width of the band stop**,

$$r \cong 1 - \frac{\Omega_w}{2} = 1 - \frac{\pi/20}{2} = 0.92146$$

- resulting in:

$$H(z) = K \frac{(z - \exp(j\pi/10))(z - \exp(-j\pi/10))}{(z - 0.92146 \exp(j\pi/10))(z - 0.92146 \exp(-j\pi/10))}$$

- Transfer function is then (using Euler's identity like before):

$$H(z) = K \frac{z^2 - 1.9021z + 1}{z^2 - 1.7527z + 0.84909}$$

- As before, each  $z$  is a **unit advance**, so

$$y[n+2] - 1.7527y[n+1] + 0.84909y[n] = K(x[n+2] - 1.9021x[n+1] + x[n])$$

letting  $n = n - 2$ , making it causal:

$$y[n] - 1.7527y[n-1] + 0.84909y[n-2] = K(x[n] - 1.9021x[n-1] + x[n-2]).$$

7. Convert the following single pole low pass analog filter into a digital filter ( $z$ -plane form transfer function) with digital cut-off frequency  $\Omega_{cf} = 0.3\pi$  using the bilinear transformation method:

$$H(s) = \frac{\omega_{cf}}{s + \omega_{cf}}.$$

**Solution**

(a) Calculate **analogue cut-off frequency**  $\omega_{cf}$  from **digital cut-off frequency**  $\Omega_{cf} = 0.2\pi$ :

$$\omega_{cf} = 2f_s \tan(\Omega_{cf}/2) = 2f_s \tan(0.1\pi) = 2f_s A$$

(b) Therefore **analogue transfer function**:

$$H(s) = \frac{2f_s A}{s + 2f_s A}$$

(c) Apply **bilinear transformation**:  $s = 2f_s \frac{1-z^{-1}}{1+z^{-1}}$ :

$$H(z) = \frac{2f_s A}{2f_s \frac{1-z^{-1}}{1+z^{-1}} + 2f_s A} = \left( \frac{2f_s}{2f_s} \right) \frac{A(1+z^{-1})}{(1-z^{-1}) + A(1+z^{-1})}$$

(d) The  $z$ -transform transfer function of the filter is then:

$$H(z) = \frac{Y(z)}{X(z)} = \frac{A + Az^{-1}}{1 + A + (A - 1)z^{-1}} \quad (1)$$

where  $A = \tan(0.1\pi)$ .

8. Is the digital filter for the above stable?

**Solution** Rearranging to determine **the poles** for **stability analysis** gives:

$$H(z) = \frac{A}{1 + A} \frac{z + 1}{z + \frac{A-1}{1+A}}.$$

- So there is 1 pole at  $z + \frac{A-1}{1+A} = 0$  or  $z = -\frac{A-1}{1+A}$ .
- Remember  $A = \tan(0.1\pi)$ , so the pole is:  $z = -0.50953$ ,
- *the magnitude is less than 1, so the filter is stable.*

9. Calculate the time domain difference equation from the  $z$ -plane representation of the transfer function.

**Solution** Multiplying both sides by both denominators of equation (1) results in

$$Y(z) \{1 + A + (A - 1)z^{-1}\} = X(z) \{A + Az^{-1}\}$$

Remembering that each  $z^{-1}$  is a unit **delay**, so that

$$(1 + A)y[n] + (A - 1)y[n - 1] = Ax[n] + Ax[n - 1]$$

Dividing through by  $(1 + A)$  and rearranging gives

$$y[n] = \frac{A}{1 + A} (x[n] + x[n - 1]) - \frac{A - 1}{1 + A} y[n - 1],$$

where  $A = \tan(0.1\pi)$ .

*This is now a difference equation we can use to filter a signal.*

10. Calculate and sketch the magnitude frequency response for the above filter, using the bilinear transformation method.

**Solution** The analogue transfer function from step 2 in earlier slide was:

$$H(s) = \frac{2f_s A}{s + 2f_s A}$$

The  $s$ -plane variable  $s$  can be replaced by the Fourier complex frequency variable  $j\omega$ ,

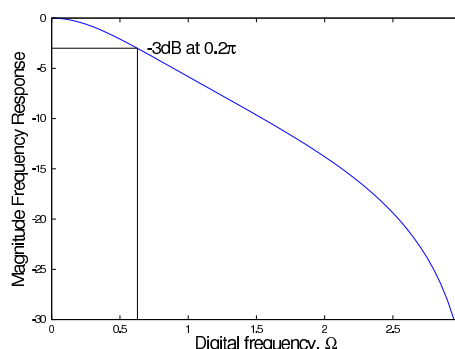
$$H(\omega) = H(s) \Big|_{s=j\omega} = \frac{2f_s A}{j\omega + 2f_s A}.$$

The Fourier frequency can then be converted to the digital frequency  $\Omega$  using  $\omega = 2f_s \tan\left(\frac{\Omega}{2}\right)$  (the bilinear transformation of the frequencies):

$$H(\Omega) = H(\omega) \Big|_{\omega=2f_s \tan(\frac{\Omega}{2})} = \frac{2f_s A}{j2f_s \tan(\frac{\Omega}{2}) + 2f_s A} = \frac{A}{j \tan(\frac{\Omega}{2}) + A}$$

again where  $A = \tan(0.1\pi)$ . So the magnitude frequency response calculated directly from the Bilinear transformation is:

$$|H(\Omega)| = \sqrt{\frac{A^2}{(\tan(\frac{\Omega}{2}))^2 + A^2}} = \sqrt{\frac{(\tan(0.1\pi))^2}{(\tan(\frac{\Omega}{2}))^2 + (\tan(0.1\pi))^2}}$$



The designed cut-off frequency  $\Omega_{cf} = 0.2\pi$  is confirmed by this plot which can be found manually by calculating the decibel value of  $20 \log_{10} |H(\Omega)|$  at  $\Omega = 0.2\pi$ .

11. List the advantages and disadvantages of recursive filters in comparison to non-recursive filters.

**Solution**

| Characteristic                         | IIR         | FIR      |
|--|-------------|----------|
| Multiplications                        | least       | most     |
| Coefficient quantification sensitivity | can be high | very low |
| Overflow errors                        | can be high | very low |
| Stability                              | by design   | always   |
| Linear phase                           | no          | always   |
| Simulate analog filter                 | yes         | no       |
| Coefficient memory                     | least       | most     |
| Design complexity                      | moderate    | simple   |

*adapted from "Understanding digital signal processing" by R. G. Lyons*