

## Problem Set 1 Solution

AA274: Principles of Robotic Autonomy  
Stanford University  
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Chi Zhang  
SUNet ID: czhang94  
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### Problem 1: Optimal Control

- (i) Given the state vector  $\mathbf{x} = (x, y, \theta)$  and control vector  $\mathbf{u} = (V, \omega)$ , it is simple to find the co-state vector  $\mathbf{p} \in \mathbb{R}^3$ . The Hamiltonian is derived as

$$H(\mathbf{x}, \mathbf{u}, \mathbf{p}) = \lambda + V^2 + \omega^2 + p_1 V \cos(\theta) + p_2 V \sin(\theta) + p_3 \omega$$

The conditions for optimality are

$$\dot{\mathbf{x}}^* = \frac{\partial H}{\partial \mathbf{p}}(\mathbf{x}^*, \mathbf{u}^*, \mathbf{p}^*) = \begin{bmatrix} V^* \cos(\theta^*) \\ V^* \sin(\theta^*) \\ \omega^* \end{bmatrix}$$

$$\dot{\mathbf{p}}^* = -\frac{\partial H}{\partial \mathbf{x}}(\mathbf{x}^*, \mathbf{u}^*, \mathbf{p}^*) = \begin{bmatrix} 0 \\ 0 \\ V^* p_1^* \sin(\theta^*) - V^* p_2^* \cos(\theta^*) \end{bmatrix}$$

$$\mathbf{0} = -\frac{\partial H}{\partial \mathbf{u}}(\mathbf{x}^*, \mathbf{u}^*, \mathbf{p}^*) = \begin{bmatrix} 2V^* + p_1^* \cos(\theta^*) + p_2^* \sin(\theta^*) \\ 2\omega^* + p_3^* \end{bmatrix}$$

Considering control constraints, we also have

$$H(\mathbf{x}^*, \mathbf{u}^*, \mathbf{p}^*) \leq H(\mathbf{x}^*, \mathbf{u}, \mathbf{p}^*)$$

and boundary conditions (BCs) are

$$\mathbf{x}(0) = \begin{bmatrix} 0 \\ 0 \\ -\frac{\pi}{2} \end{bmatrix}, \quad \mathbf{x}(t_f) = \begin{bmatrix} 5 \\ 5 \\ -\frac{\pi}{2} \end{bmatrix}$$

From the above equations, we know

$$V^* = -\frac{p_1^* \cos(\theta^*) + p_2^* \sin(\theta^*)}{2}, \quad \omega^* = -\frac{p_3^*}{2}$$

Define a new state vector  $\mathbf{z} = (\mathbf{x}, \mathbf{p}, r)$  where  $r = t/t_f \in [0, 1]$ , then BVP becomes

$$\frac{d\mathbf{z}_i^*(\tau)}{d\tau} = \frac{d\dot{\mathbf{x}}^*(\tau)}{d\tau} = t_f \dot{\mathbf{x}}^* = r^*(\tau) \begin{bmatrix} V^*(\tau) \cos(\theta^*(\tau)) \\ V^*(\tau) \sin(\theta^*(\tau)) \\ \omega^*(\tau) \end{bmatrix} \quad (i = 1, 2, 3)$$

$$\frac{dz_i^*(\tau)}{d\tau} = \frac{d\dot{\mathbf{p}}^*(\tau)}{d\tau} = t_f \dot{\mathbf{p}}^* = r^*(\tau) \begin{bmatrix} 0 \\ 0 \\ V^*(\tau)p_1^*(\tau)\sin(\theta^*(\tau)) - V^*(\tau)p_2^*(\tau)\cos(\theta^*(\tau)) \end{bmatrix} \quad (i = 4, 5, 6)$$

$$\frac{dz_7^*(\tau)}{d\tau} = \frac{dr}{d\tau} = 0$$

and BCs become

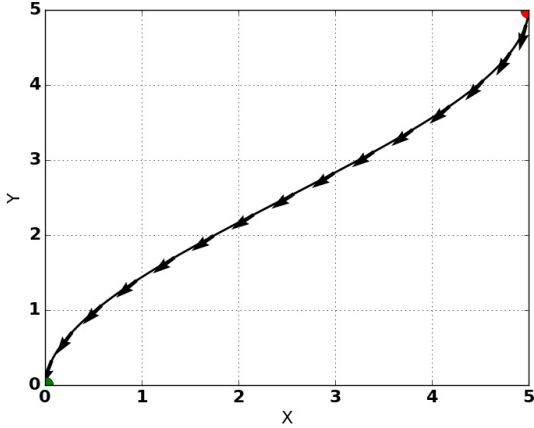
$$\mathbf{x}^*(0) = \begin{bmatrix} 0 \\ 0 \\ -\frac{\pi}{2} \end{bmatrix}, \quad \mathbf{x}^*(1) = \begin{bmatrix} 5 \\ 5 \\ -\frac{\pi}{2} \end{bmatrix}$$

since the final time  $t_f$  is free, *i.e.*  $\delta t_f$  is arbitrary, thus

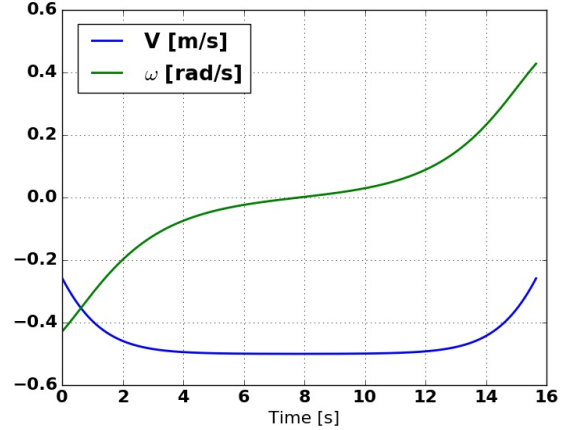
$$H(\mathbf{x}^*(1), \mathbf{u}^*(1), \mathbf{p}^*(1)) = 0$$

Here, we have seven ODEs for seven unknowns  $z_i (i = 1, 2, \dots, 7)$ , which is a 2P-BVP problem.

- (iii) In the cost function,  $\lambda$  can be considered as penalty for  $t_f$  in optimization. Therefore, the larger  $\lambda$ , the smaller  $t_f$ . Since the goal of optimization is to minimize  $J$ , using the largest feasible  $\lambda$  yields the smallest  $t_f$ . To put it more explicitly, the largest feasible  $\lambda$  will “make” the car move as quick as possible for the smallest  $t_f$ , pushing  $V$  to limit.
- (iv) With  $\lambda = 0.25$  and the initial guess  $\mathbf{p}_0 = [1.0, 1.0, -\frac{\pi}{2}, -1.0, -1.0, 5.0, 10.0]^T$ , it can be obtained the figures below:



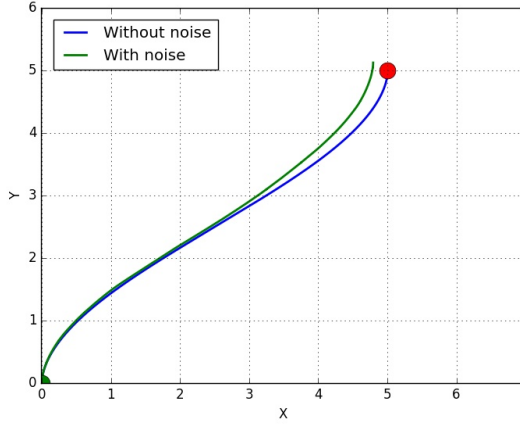
(a) optimal trajectory



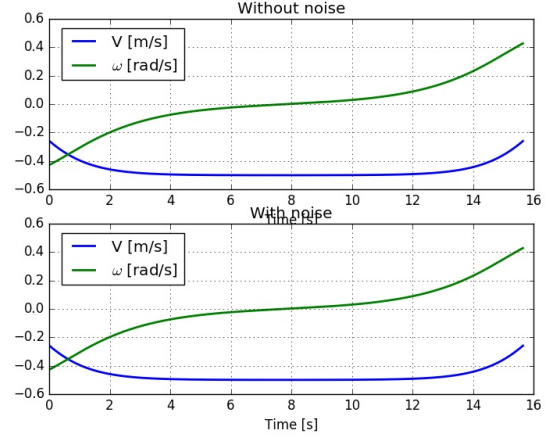
(b) optimal control history

It is trivial to verify the trajectory satisfies BCs and the control history satisfies given constraints, which are  $|V| \leq 0.5\text{m/s}$  and  $|\omega| \leq 1.0\text{rad/s}$ .

(v) The two plots are shown below:



(a) simulation trajectory



(b) simulation control history

## Problem 2: Differential Flatness

- (i) Given four basis functions  $\psi_i (i = 1, 2, 3, 4)$ , the initial and final conditions can be rearranged as

$$\begin{bmatrix} x(0) \\ y(0) \\ \dot{x}(0) \\ \dot{y}(0) \end{bmatrix} = \begin{bmatrix} 0 \\ 0 \\ 0 \\ -0.5 \end{bmatrix} \quad \begin{bmatrix} x(t_f) \\ y(t_f) \\ \dot{x}(t_f) \\ \dot{y}(t_f) \end{bmatrix} = \begin{bmatrix} 5 \\ 5 \\ 0 \\ -0.5 \end{bmatrix}$$

Then these conditions can be written in the form of matrix multiplication:

$$\begin{bmatrix} 1 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 1 & 0 & 0 & 0 & 0 & 0 & 0 \\ 1 & t_f & t_f^2 & t_f^3 & 0 & 0 & 0 & 0 \\ 0 & 1 & 2t_f & 3t_f^2 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 1 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 1 & 0 & 0 \\ 0 & 0 & 0 & 0 & 1 & t_f & t_f^2 & t_f^3 \\ 0 & 0 & 0 & 0 & 0 & 1 & 2t_f & 3t_f^2 \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \\ x_3 \\ x_4 \\ y_1 \\ y_2 \\ y_3 \\ y_4 \end{bmatrix} = \begin{bmatrix} 0 \\ 0 \\ 5 \\ 0 \\ 0 \\ -0.5 \\ 5 \\ -0.5 \end{bmatrix}$$

It can be observed that  $\omega$  will become undefined if  $J = 0$ . Also,  $\det(J) = V$ . If  $V(t_f) = 0$ , then  $J$  becomes non-invertible, leading to singularity issues.

- (ii) Solving the linear system above gives us  $x, y, \dot{x}, \dot{y}, \ddot{x}, \ddot{y}$ , and we already know that

$$\theta = \tan^{-1}\left(\frac{\dot{y}}{\dot{x}}\right)$$

$$V = \frac{\dot{x}}{\cos \theta} \quad \text{or} \quad V = \frac{\dot{y}}{\sin \theta} \quad \text{or} \quad V = \sqrt{\dot{x}^2 + \dot{y}^2}$$

Also, it can be obtained from kinetic constraints that

$$\ddot{x} = a \cos \theta - \omega(V \sin \theta) = a \cos \theta - \omega \dot{y} \quad (1)$$

$$\ddot{y} = a \sin \theta + \omega(V \cos \theta) = a \sin \theta + \omega \dot{x} \quad (2)$$

Do  $(2) \times V \cos \theta - (1) \times V \sin \theta$ , we have

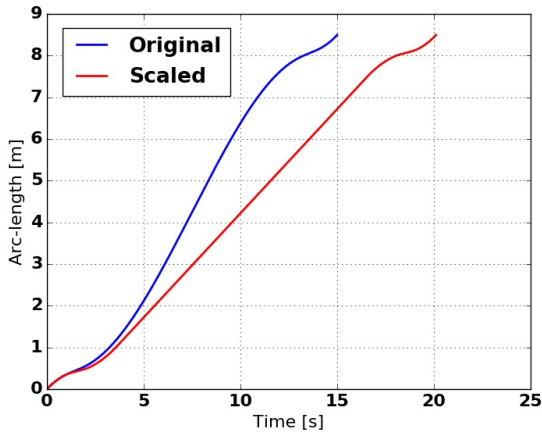
$$\ddot{y}(V \cos \theta) - \ddot{x}(V \sin \theta) = \omega[\dot{x}(V \cos \theta) + \dot{y}(V \sin \theta)]$$

$$\dot{x}\ddot{y} - \dot{y}\ddot{x} = \omega(\dot{x}^2 + \dot{y}^2) = \omega V^2$$

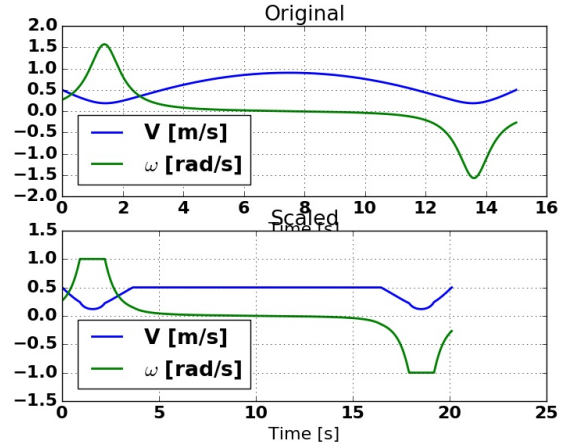
$$\omega = \frac{\dot{x}\ddot{y} - \dot{y}\ddot{x}}{V^2}$$

Following the expressions of  $\theta$ ,  $V$  and  $\omega$  derived above, it is trivial to implement.

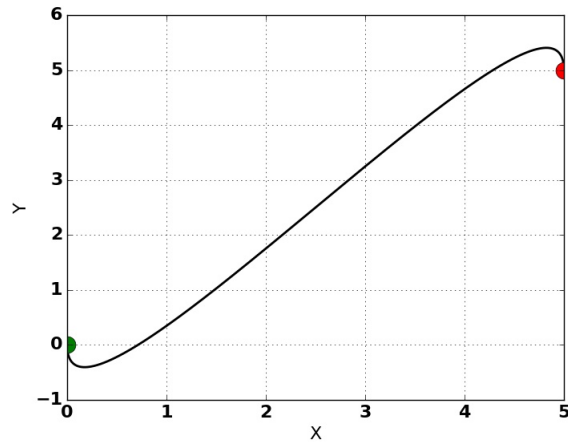
(v) The plots are shown below:



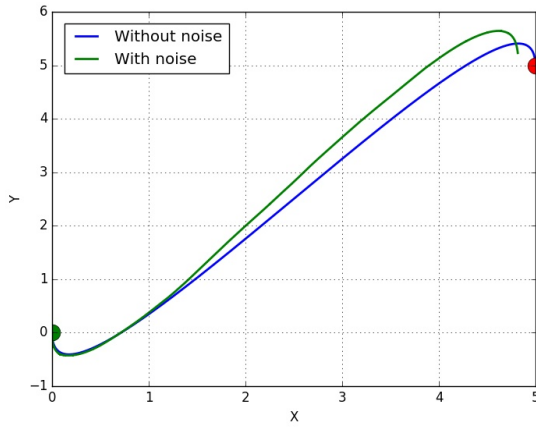
(a) arc-length history



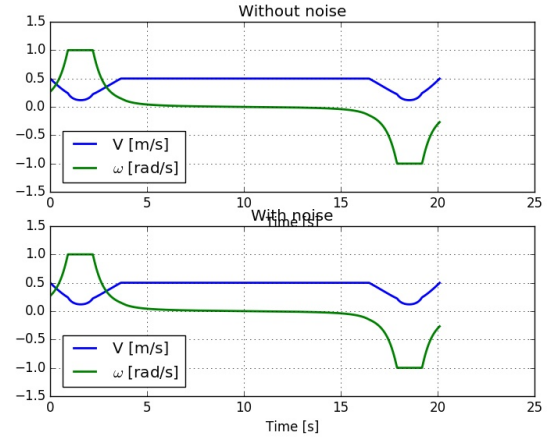
(b) control history



(c) solution trajectory



(d) simulation trajectory



(e) simulation control history

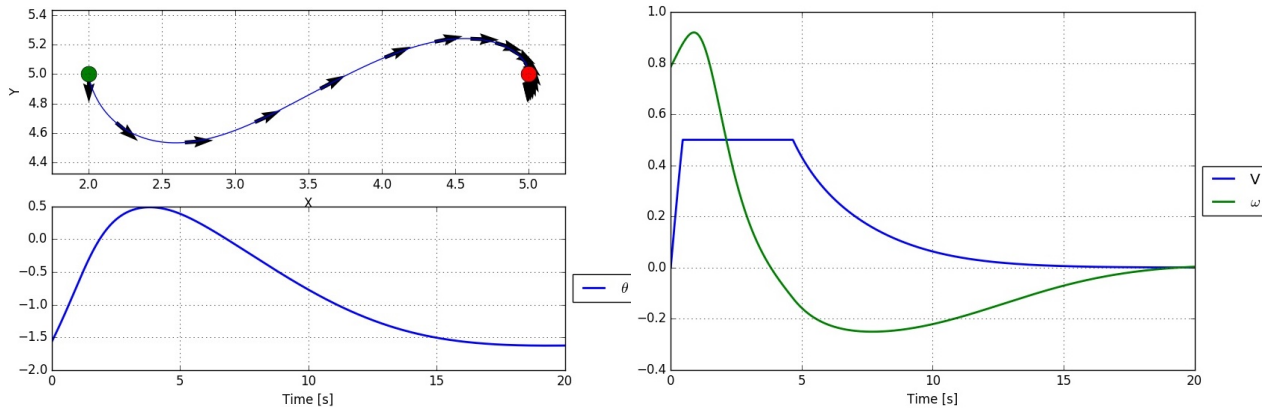
### Problem 3: Closed-loop Control I

- (i) See the code in `P3_pose_stabilization.py`.
- (ii) For the three conditions of parking, the initial positions and poses used are

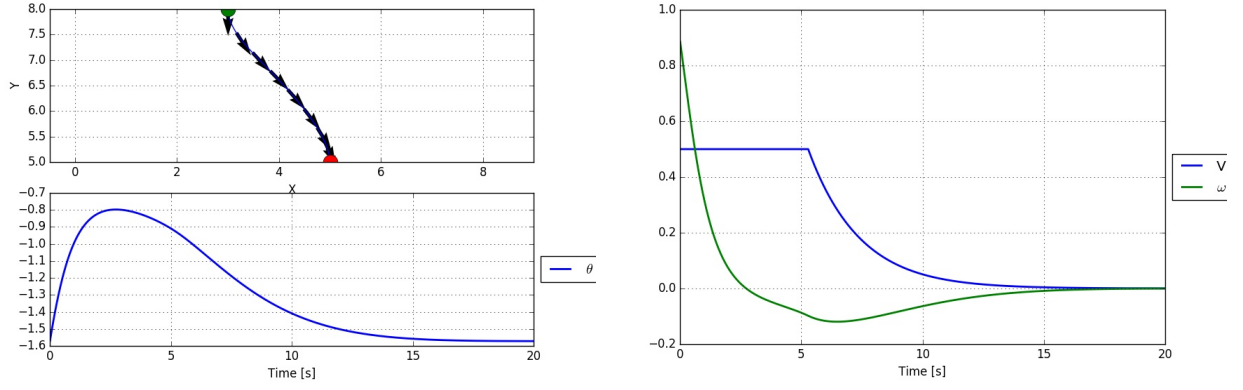
Parking Type	$x_0$	$y_0$	$\theta_0$
Forward	3.0	8.0	-1.57
Reverse	3.0	2.0	-1.57
Parallel	2.0	5.0	-1.57

and the final time  $t_f$  is set to 20.

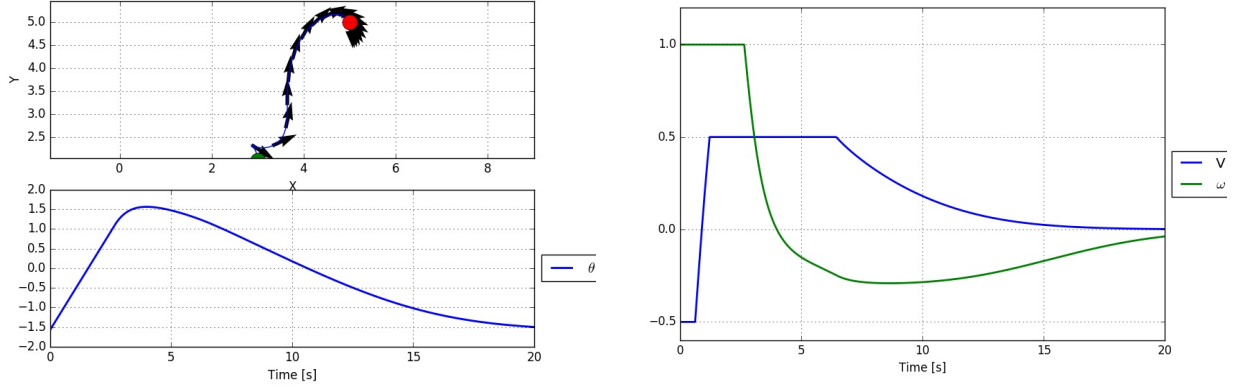
The generated plots are shown below:



(a) parallel parking



(b) forward parking



(c) reverse parking

## Problem 4: Closed-loop Control II

(i) Substitute  $\ddot{x}$ ,  $\ddot{y}$  with  $u_1$ ,  $u_2$  in Eq.(1) and Eq.(2), we have

$$u_1 = a \cos \theta - \omega(V \sin \theta) \quad (3)$$

$$u_2 = a \sin \theta + \omega(V \cos \theta) \quad (4)$$

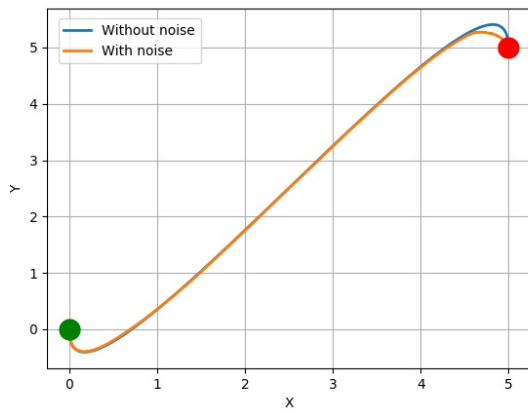
Do (3)  $\times \cos \theta$  + (4)  $\times \sin \theta$ , we have

$$a = \dot{V} = u_1 \cos \theta + u_2 \sin \theta$$

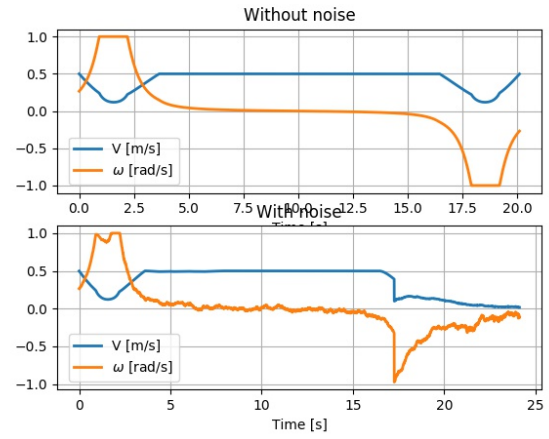
Do (4)  $\times \cos \theta$  - (3)  $\times \sin \theta$ , we have

$$\omega = \frac{u_2 \cos \theta - u_1 \sin \theta}{V}$$

(iv) The plots are shown below:



(a) simulation trajectory



(b) simulation control history

## Problem 5: Robot Operating System

- (i) The bag file was saved as `random_strings.bag`.
- (ii) The command is `rosbag play <filename>.bag`.
- (iii) The bag file was saved as `turtlebot.bag`.