FORMULATION AND CALCULATION OF ISOPARAMETRIC MODELS

LECTURE 6

57 MINUTES

LECTURE 6 Formulation and calculation of isoparametric continuum elements

Truss, plane-stress, plane-strain, axisymmetric and three-dimensional elements

Variable-number-nodes elements, curved elements

Derivation of interpolations, displacement and strain interpolation matrices, the Jacobian transformation

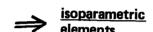
Various examples; shifting of internal nodes to achieve stress singularities for fracture mechanics analysis

TEXTBOOK: Sections: 5.1, 5.2, 5.3.1, 5.3.3, 5.5.1

Examples: 5.1, 5.2, 5.3, 5.4, 5.5, 5.6, 5.7, 5.8, 5.9, 5.10, 5.11, 5.12, 5.13, 5.14, 5.15, 5.16, 5.17

FORMULATION AND CALCULATION OF ISO-PARAMETRIC FINITE ELEMENTS

- interpolation matrices and element matrices
- We considered earlier (lecture 4) generalized coordinate finite element models
- We now want to discuss a more general approach to deriving the required



Isoparametric Elements
Basic Concept: (Continuum Elements)

Interpolate Geometry

$$x = \sum_{i=1}^{N} h_i x_i$$
; $y = \sum_{i=1}^{N} h_i y_i$; $z = \sum_{i=1}^{N} h_i z_i$

Interpolate Displacements

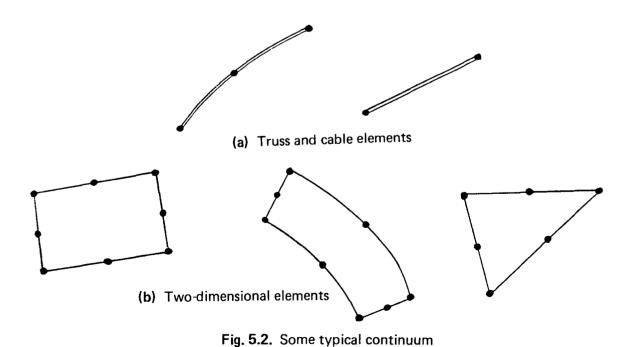
$$u = \sum_{i=1}^{N} h_i u_i$$
 $v = \sum_{i=1}^{N} h_i v_i$ $w = \sum_{i=1}^{N} h_i w_i$

N = number of nodes

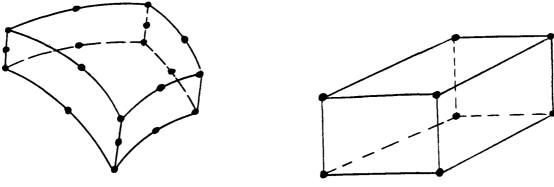
1/D Element Truss

2/D Elements Plane stress Plane strain Elements
Axisymmetric Analysis

3/D Elements Three-dimensional Thick Shell



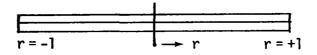
elements



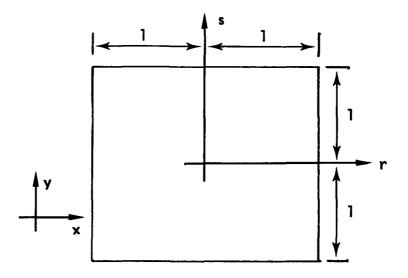
(c) Three-dimensional elements

Fig. 5.2. Some typical continuum elements

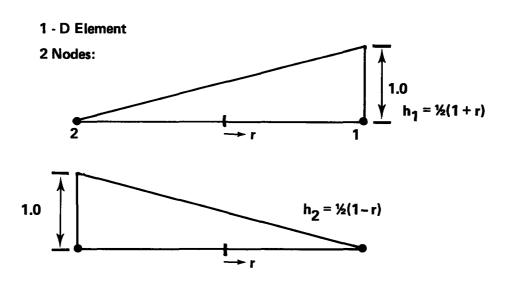
Consider special geometries first:



Truss, 2 units long

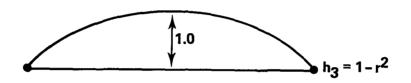


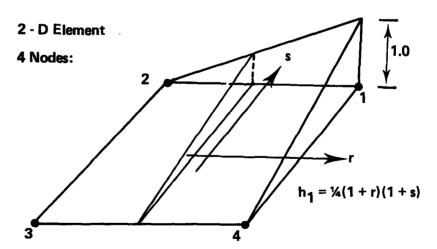
2/D element, 2x2 units
Similarly 3/D element 2x2x2 units (r-s-t axes)









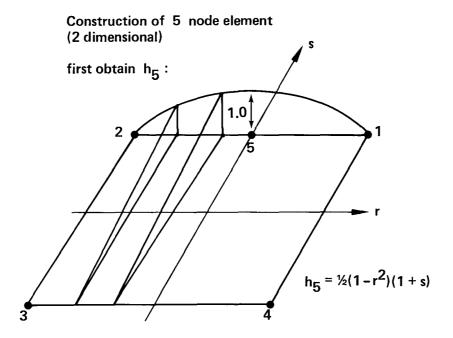


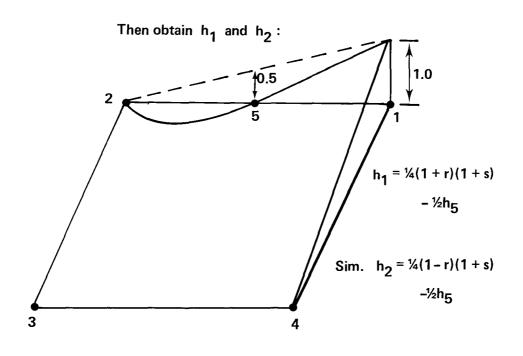
Similarly

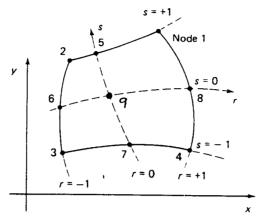
$$h_2 = \frac{1}{4}(1-r)(1+s)$$

$$h_3 = \frac{1}{1-r}(1-s)$$

$$h_4 = \frac{1}{4}(1+r)(1-s)$$







(a) Four to 9 variable-number-nodes two-dimensional element

Fig. 5.5. Interpolation functions of four to nine variable-number-nodes two-dimensional element.

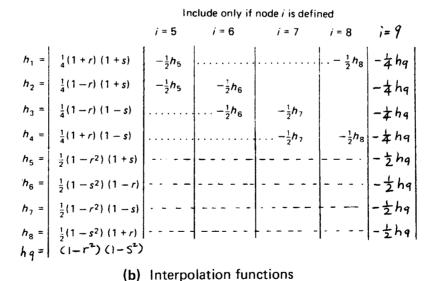


Fig. 5.5. Interpolation functions of four to nine variable-number-nodes two-dimensional element.

Having obtained the h_i we can construct the matrices \underline{H} and \underline{B} :

- The elements of <u>H</u> are the h (or zero)
- The elements of <u>B</u> are the derivatives of the h; (or zero),

Because for the 2x2x2 elements we can use

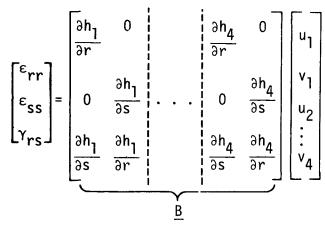
$$x = r$$

$$\mathbf{y} \equiv \mathbf{s}$$

$$z \equiv t$$

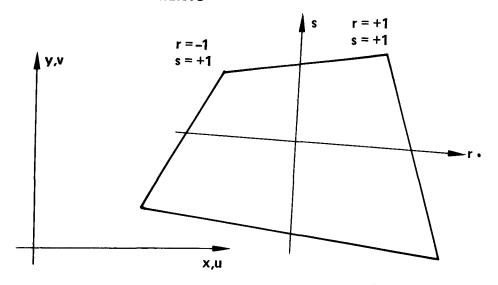
EXAMPLE 4 node 2 dim. element

$$\begin{bmatrix} u(r,s) \\ v(r,s) \end{bmatrix} = \begin{bmatrix} h_1 & 0 & h_2 & 0 & h_3 & 0 & h_4 & 0 \\ 0 & h_1 & 0 & h_2 & 0 & h_3 & 0 & h_4 \end{bmatrix} \begin{bmatrix} u_1 \\ v_1 \\ u_2 \\ \vdots \\ v_4 \end{bmatrix}$$



We note again $r \equiv x$ $s \equiv y$

GENERAL ELEMENTS



Displacement and geometry interpolation as before, but

$$\begin{bmatrix} \frac{\partial}{\partial r} \\ \frac{\partial}{\partial s} \end{bmatrix} = \begin{bmatrix} \frac{\partial x}{\partial r} & \frac{\partial y}{\partial r} \\ \frac{\partial x}{\partial s} & \frac{\partial y}{\partial s} \end{bmatrix} \begin{bmatrix} \frac{\partial}{\partial x} \\ \frac{\partial}{\partial y} \end{bmatrix}$$

Aside: cannot use $\frac{\partial}{\partial x} = \frac{\partial}{\partial r} \quad \frac{\partial r}{\partial x} + \dots$

$$\frac{\partial}{\partial r} = \underline{J} \quad \frac{\partial}{\partial x}$$
 (in general)

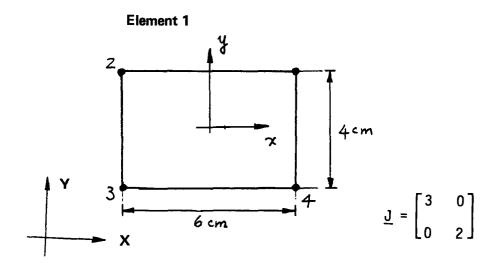
$$\frac{\partial}{\partial x} = \underline{J}^{-1} \frac{\partial}{\partial r}$$
 (5.25)

Using (5.25) we can find the matrix B of general elements

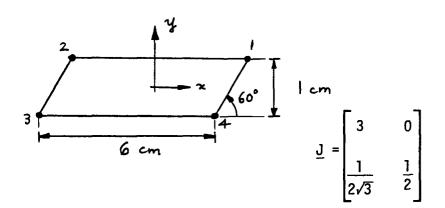
The H and B matrices are a function of r, s, t; for the integration thus use

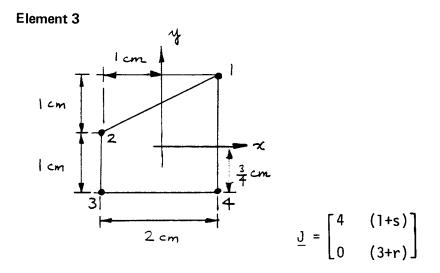
dv = det J dr ds dt

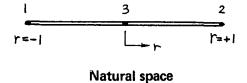
Fig. 5.9. Some two-dimensional elements

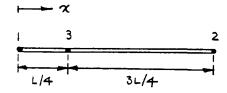












Actual physical space

Fig. 5.23. Quarter-point onedimensional element.

Here we have

$$x = \sum_{i=1}^{3} h_i x_i \Rightarrow x = \frac{L}{4} (1+r)^2$$

hence

$$\underline{J} = \left[\frac{L}{2} + \frac{r}{2} L \right]$$

and

$$\underline{B} = \frac{1}{\frac{L}{2} + \frac{r}{2}L} [h_{1,r} \quad h_{2,r} \quad h_{3,r}]$$

or

$$\underline{B} = \frac{1}{\frac{L}{2} + \frac{r}{2}L} [(-\frac{L}{2} + r) (\frac{L}{2} + r) - 2r]$$

Since

$$r = 2\sqrt{\frac{x}{L}} - 1$$

$$\underline{B} = \left[\begin{pmatrix} \frac{2}{L} - \frac{3}{2\sqrt{L}} & \frac{1}{\sqrt{x}} \end{pmatrix} \right] \begin{pmatrix} \frac{2}{L} - \frac{1}{2\sqrt{L}} & \frac{1}{\sqrt{x}} \end{pmatrix}$$

$$\left(\frac{2}{\sqrt{L}\sqrt{x}} - \frac{4}{L}\right)$$

We note

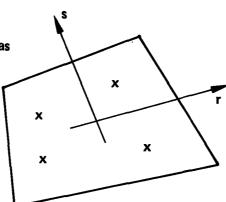
$$\frac{1}{\sqrt{X}}$$
 singularity at X = 0!

Numerical Integration

Gauss Integration
Newton-Cotes Formulas

$$\underline{K} = \sum_{i,j,k} \alpha_{ijk} \underline{F}_{ijk}$$

$$\underline{F} \approx \underline{B}^{\mathsf{T}} \, \underline{C} \, \underline{B} \, \det \underline{J}$$



MIT OpenCourseWare http://ocw.mit.edu

Resource: Finite Element Procedures for Solids and Structures Klaus-Jürgen Bathe

The following may not correspond to a particular course on MIT OpenCourseWare, but has been provided by the author as an individual learning resource.

For information about citing these materials or our Terms of Use, visit: http://ocw.mit.edu/terms.