

# Sediment model manuscript

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aggradation | sea level rise | tidal river management | polders | tidal amplification

Sea level rise threatens the densely populated and ecologically significant low-lying, coastal region of Bengal. Mitigating the effects of sea level rise (SLR) in this region will be especially difficult considering current widespread land management practices and the ongoing geopolitical tension between India and Bangladesh.

Coastal Bengal is situated within the delta formed by the confluence of the Ganges and Brahmaputra rivers and straddles the border between West Bengal, India to the east and Bangladesh to the west. The region is home to ~30 million people<sup>(1)</sup> and the ecologically critical Sundarbans mangrove forest. Since the 1960s, the region has seen a vast transformation through the reduction in natural mangrove habitat and the widespread construction of earthen embankments. These embankments surround large swaths of cleared land, known as polders, that accommodate the swelling population of the region.

While, preventing regular inundation by spring high tides, the creation of these embankments have had the unintended consequence of starving the interior of the polders of fresh sediment. Without this sediment, polder interiors have compacted resulting in significant elevation offset (1.0 m to 1.5 m) relative to the natural mangrove forest<sup>(2)</sup>. Polder elevations often sit precariously below local mean high water (MHW) levels leading to persistent waterlogging. Furthermore, many of these embankments are in disrepair and susceptible to breaching especially by storm surge as was the case with Cyclone Sidr (2007), Cyclone Aila (2009), and recently with Cyclone Amphan (2020).

Tidal river management (TRM) has been proposed as a possible augmentation of current land management practices to alleviate some of the issues caused by poldering. Under TRM, embankments are seasonally breached to allow tidal water inundation and sediment aggradation. Many low-lying areas may recover to an acceptable elevation within 5 to 10 years, though, some may take longer. There are a host of local socioeconomic, political, and governance considerations that may influence the success of TRM. Here, we neglect those considerations and focus on the general feasibility of TRM in regards to SLR and the sediment supply of the GB system. Future studies will focus on the social dynamics surrounding TRM.

Coastal Bengal is often seen as one of the most at-risk regions for SLR due to climate change. Infographics often depict large swaths of the Bengal coastline flooded under different SLR scenarios. However, this overly simplifies the

threats to the region and neglects the significant sediment contribution of the GB system in maintaining the natural elevation.

Estimates for increases in Relative Mean Sea Level (RMSL) in the GB delta range from 2.8 mm yr<sup>-1</sup> to 8.8 mm yr<sup>-1</sup>. However, RMSL neglects the widening of the tidal range in the polder region. On average, local high water levels in the polder region are increasing at a rate of 15.9 mm yr<sup>-1</sup><sup>(3)</sup>. While SLR is of paramount importance, tidal range amplification is the more imminent threat to the region. This is especially important considering the Bangladeshi government's recent reinvestment in poldering with a \$400 million loan from the World Bank for the Coastal Embankment Improvement Project - Phase I (CEIP-I).

As for the natural mangrove system, it is unclear how changing water levels will affect elevation. Some studies have shown that the region is incredibly resilient to increasing water levels due, in large part, to the abundant sediment supply of the GB system. This sediment is delivered to the platform periodically during spring high tide which helps maintain an equilibrium elevation approximately equivalent to mean higher high water (MHHW). But, this large volume of sediment delivered to coastal Bengal is not guaranteed.

Water has long been the focus of the geopolitical disputes between India and Bangladesh. However, the reduction in waterflow across the border portends a significant decrease in sediment flux. Estimates suggest sediment flux may be reduced by 39 % to 75 % for the Ganges and 9 % to 25 % for the Brahmaputra resulting in a change in aggradation from 3.6 mm yr<sup>-1</sup> to 2.5 mm yr<sup>-1</sup><sup>(4)</sup>.

The combination of increasing water levels and decreasing sediment supply may further intensify an already dire situation. Here, we use a zero-dimensional mass balance model of sediment aggradation to understand the impact that increasing water levels and decreasing sediment flux will have on the regions equilibrium elevation and consequently its resilience to climate change. We consider both the resilience of the

## Significance Statement

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Author contributions: C.M.T., J.G., and S.L.G. designed research; C.M.T. and J.G. performed research; C.M.T. analyzed data; C.M.T. wrote the paper; and C.M.T., J.G., and S.L.G. provided discussion and input on paper

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natural mangrove system and the ability of the polder system to recover to a more resilient elevation through TRM.

**Numerical model.** We modeled tidal platform elevation ( $\zeta$ ) using a zero-dimensional mass balance model using the basic formulation provided by Krone (5) and further refined by Allen (6), French (7), and Temmerman et al. (8, 9). The rate of tidal platform elevation change is described as

$$\frac{d\eta}{dt} = \frac{dS_M}{dt} + \frac{dS_O}{dt} + \frac{dP}{dt} + \frac{dM}{dt}, \quad [1]$$

where  $S_M$  is mineral sedimentation,  $S_O$  is organic matter sedimentation,  $P$  is compaction, and  $M$  is tectonic subsidence. Each term of equation 1 can be further expanded.

We approximate  $S_M$  as

$$S_M(t) = \int \frac{w_s C(t)}{\rho_b} dt, \quad [2]$$

where  $w_s$  is the characteristic settling velocity of a given grain size,  $C(t)$  is the depth-averaged and time-varying sediment concentration in the water column, and  $\rho_b$  is the dry bulk density of the sediment. We assume there is no resuspension of mineral sediment which is consistent with Krone's (5) initial formulation.

$w_s$  is calculated for a given grain size by using Stokes' law to determine the terminal velocity of a sphere falling through a fluid given by

$$w_s = \frac{2}{9} \frac{\rho_p - \rho_f}{\mu} g R^2 \quad [3]$$

where  $\rho_p$  is the mass density of the particle or grain,  $\rho_f$  is the mass density of the fluid,  $\mu$  is the dynamic viscosity of the fluid,  $g$  is the acceleration due to gravity, and  $R$  is the radius of the grain. This is approximation for  $w_s$  is consistent with previous similar studies (6, 8, 9). We assume basic properties of water for  $\rho_f$  ( $1000 \text{ kg m}^{-3}$ ) and  $\mu$  ( $1 \times 10^{-3} \text{ kg m}^{-1} \text{ s}^{-1}$ ) for simplicity. Salinity does vary seasonally which will change these values, but had little affect on the model output.

We capture the temporal variation of  $C(t)$  through the mass balance given as

$$\frac{d[h(t) - \zeta(t)]C(t)}{dt} = -w_s C(t) + C_{in} \frac{dh}{dt}, \quad [4]$$

where  $h$  is the height of the water column and  $C_{in}$  is the incoming suspended sediment concentration of the adjacent water column. We consider  $\zeta$  to be a function of time and update it at every timestep which differs from previous studies (5–10) which only update  $\zeta$  after every tidal cycle. The physical interpretation of equation 4 is that the first term is the mass flux above an area on the tidal platform, the second term is the mass flux extracted from the water column, and the third term is the mass flux from the adjacent water column. Further derivation of equation 4 results in

$$\frac{dC}{dt}[h(t) - \zeta(t)] = -w_s C(t) + [C_{in} - C(t)] \frac{dh}{dt} + C(t) \frac{d\zeta}{dt} \quad [5]$$

From equation 5, we can approximate the solution for concentration numerically.

**Model inputs.** We obtained model inputs from field measurements. We observed tidal height, grain size, suspended sediment concentration (SSC), and dry bulk density around Polder 32 over multiple field seasons from 2011 to 2016 (2, 11, 12).

For  $h$ , we extracted one year of contiguous tidal data from from a pressure sensor deployed within the tidal channel near Polder 32. We used the oce package in R (3.6.3) to create an idealized tidal curve from our data (?). The tidal curve was then shifted down so that mean higher high water would be 0.3 m above the Sundarban platform and 1.8 m above the polder surface ( $\zeta$ ). We replicated this tidal curve for each subsequent year for the length of the model run. Field observations confirm these benchmark elevation (2, 12, 13). In order to simulate sea level rise, the subsequent year tidal curves were increased at a linear rate of  $2 \text{ mm yr}^{-1}$  which is consistent with field observations.

For  $C_{in}$ , we use observed values of SSC from Hale et al. (11) that are characteristic of the tidal channels in the region. Similar to Temmerman et al. (8, 9), we scaled the observed tidal channel SSC by a factor as the flood waters are expected to have a lower SSC than the tidal channel due to lower flow velocities. For our preliminary study, we use a k-factor of 0.7. In future model iterations, we will better explore this relationship and determine an appropriate k-factor.

For  $\rho$ , we used values derived from conversations with Steven Goodbred and Carol Wilson.

## Materials and Methods

Please describe your materials and methods here. This can be more than one paragraph, and may contain subsections and equations as required.

**Subsection for Method.** Example text for subsection.

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